

GC-008

**Contents for Stormwater Management Facilities As-built Files**

Each file is to contain:

- ① As-built plan
- ② Completed construction certification
- ③ Construction Plan
- ④ Design Calculations
- ⑤ Watershed Map
- ⑥ Maintenance Agreement
7. Correspondence with owners
- ⑧ Inspection Records
9. Enforcement Actions

COPY

COUNTY OF JAMES CITY, VIRGINIA

DECLARATION OF COVENANTS

INSPECTION/MAINTENANCE OF DRAINAGE SYSTEM

THIS DECLARATION, made this 9<sup>th</sup> day of August, 20 07,  
between JAMES RIVER BAPTIST CHURCH, and  
all successors in interest, ("COVENANTOR(S),") owner(s) of the following property:

Street Address: 4931 Centerville Rd. Williamsburg, Va. 23188  
Legal Description: James River Baptist Church  
Project Name: James River Baptist Church/Multi-Ministry Building  
Document No. \_\_\_\_\_, Deed Book 28, 81, & 84, Page No. 230, 217, & 551;  
Instrument No. \_\_\_\_\_, and the County of James City, Virginia ("COUNTY.")

WITNESSETH:

We, the COVENANTOR(S), with full authority to execute deeds, mortgages, other covenants, and all rights, titles and interests in the property described above, do hereby covenant with the COUNTY as follows:

1. The COVENANTOR(S) shall provide maintenance for the drainage system including any runoff control facilities, conveyance systems and associated easements, hereinafter referred to as the "SYSTEM," located on and serving the above-described property to ensure that the SYSTEM is and remains in proper working condition in accordance with approved design standards, and with the law and applicable executive regulations. The SYSTEM shall not include any elements located within any Virginia Department of Transportation rights-of-way.

2. If necessary, the COVENANTOR(S) shall levy regular or special assessments against all present or subsequent owners of property served by the SYSTEM to ensure that the SYSTEM is properly maintained.

3. The COVENANTOR(S) shall provide and maintain perpetual access from public right-of-ways to the SYSTEM for the COUNTY, its agent and its contractor.

4. The COVENANTOR(S) shall grant the COUNTY, its agent and its contractor a right of entry to the SYSTEM for the purpose of inspecting, monitoring, operating, installing, constructing, reconstructing, maintaining or repairing the SYSTEM.

5. If, after reasonable notice by the COUNTY, the COVENANTOR(S) shall fail to maintain the SYSTEM in accordance with the approved design standards and with the law and applicable executive regulations, the COUNTY may perform all necessary repair or maintenance work, and the COUNTY may assess the COVENANTOR(S) and/or all property served by the SYSTEM for the cost of the work and any applicable penalties.

6. The COVENANTOR(S) shall indemnify and save the COUNTY harmless from any and all claims for damages to persons or property arising from the installation, construction, maintenance, repair, operation or use of the SYSTEM.

*Instrument # 070024680*

*Recorded on Sept. 4, 2007*

7. The COVENANTOR(s) shall promptly notify the COUNTY when the COVENANTOR(S) legally transfers any of the COVENANTOR(S)' responsibilities for the SYSTEM. The COVENANTOR(S)' shall supply the COUNTY with a copy of any document of transfer, executed by both parties.

8. The covenants contained herein shall run with the land and shall bind the COVENANTOR(S) and the COVENANTOR(S)' heirs, executors, administrators, successors and assignees, and shall bind all present and subsequent owners of property served by the SYSTEM.

9. This COVENANT shall be recorded in the County Land Records.

IN WITNESS WHEREOF, the COVENANTOR(S) have executed this DECLARATION OF COVENANTS as of the date first above written.

COVENANTOR(S)

D. Steven Mallory, Trustee

Print Name/Title Douglas S. Mallory, Trustee

ATTEST:

Queen C. Schatzger

COVENANTOR(S)

Richard W. Aadahl Trustee

Print Name/Title Richard W. Aadahl, Trustee

ATTEST:

Queen C. Schatzger

COVENANTOR(S)

James H. Richardson Trustee

Print Name/Title James H. Richardson, Trustee

ATTEST:

Queen C. Schatzger

COMMONWEALTH OF VIRGINIA

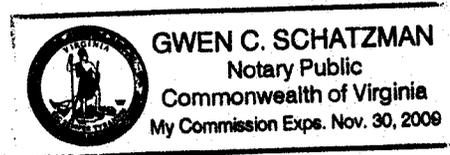
~~CITY/COUNTY OF~~ JAMES CITY

I hereby certify that on this 16<sup>th</sup> day of AUGUST, 2007, before the subscribed, a Notary Public of the State of Virginia, personally appeared D.S. MAUORY, R.W. Aadahl, J.H. RICHARDSON and did acknowledge the foregoing instrument to be their Act.

IN WITNESS WHEREOF, I have hereunto set my hand and official seal this 16<sup>th</sup> day of AUGUST, 2007.

Gwen C. Schatzman 361448  
Notary Public

My Commission expires: 11/30/09



Approved as to form:

A. A. [Signature]  
County Attorney

This Declaration of Covenants prepared by:

L Bruce Abbott  
(Print Name)

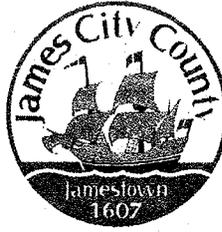
Project Engineer AES  
(Title)

5248 Olde Towne Rd.  
(Address)

Williamsburg, Va. 23188  
(City) (State) (Zip)

(757) 253-0040  
(Phone Number)

drainage1.pre



James City County, Virginia  
Environmental Division

Stormwater Management / BMP Facilities  
Record Drawing and Construction Certification Forms

(Note: In accordance with the requirements of the Chesapeake Bay Preservation Ordinance, Chapter 23, Section 23-10(4), BMP's shall be designed and constructed in accordance with the manual entitled James City County Guidelines for Design and Construction of Stormwater Management BMP's. Erosion and sediment control policy and approved plans generally require that at the completion of the project and prior to release of surety, an "as-built" plan prepared by a registered Professional Engineer or Certified Land Surveyor must be provided for the drainage system for the project, including any Best Management Practice (BMP) facilities. In addition, for BMP facilities involving the construction of an impounding structure or dam embankment, certification is required by a Professional Engineer who has inspected the structure during its construction. Currently there are over 20 water quality type BMP's accepted by the County.)

**Section 1 – Site Information:**

Project Name: Multi-Ministry Building - James River Baptist Church  
Structure/BMP Name: \_\_\_\_\_  
Project Location: 4931 Centerville Road  
BMP Location: Southwest Corner of Property  
County Plan No.: SP - 044 - 06

Project Type:  Residential  Business Tax Map/Parcel No.: 3040100001  
 Commercial  Office BMP ID Code (if known): 66008  
 Institutional  Industrial Zoning District: A1  
 Public  Roadway Land Use: Church  
 Other Site Area (sf or acres): 5.81

Brief Description of Stormwater Management/BMP Facility: Wet Pond

Nearest Visible Landmark to SWM/BMP Facility: James River Baptist Church Building

Nearest Vertical Ground Control (if known):  JCC Geodetic Ground Control  USGS  Temporary  Arbitrary  Other  
Station Number or Name: 313  
Datum or Reference Elevation: 97.45  
Control Description: A 3 1/4" Disk in concrete located in grass median at Manchester Road.  
Control Location from Subject Facility: 0.65 mi. south of site

**Section 2 – Stormwater Management / BMP Facility Construction Information:**

PreConstruction Meeting Held for Construction of SWM/BMP Facility:  Yes  No  Unknown  
Approx. Construction Start Date for SWM/BMP Facility: 9/07  
Facility Monitored by County Representative during Construction:  Yes  No  Unknown  
Name of Site Work Contractor Who Constructed Facility: Reeds Enterprises, LLC  
Name of Professional Firm Who Routinely Monitored Construction: ECS Mid-Atlantic, LLC  
Date of Completion for SWM/BMP Facility: 5/08  
Date of Record Drawing/Construction Certification Submittal: 5/08

***(Note: Record Drawing and Construction Certifications are required within thirty (30) days of the completion of Stormwater Management and/or BMP facility construction. Record Drawings and Construction Certifications must be reviewed and approved by the James City County Environmental Division prior to final inspection, acceptance and bond or surety release.)***

**Section 3 – Owner / Designer / Contractor Information:**

Owner/Developer: *(Note: Site Owner or Applicant responsible for development of the project.)*

Name: James River Baptist Church  
Mailing Address: 4931 Centerville Road  
Williamsburg, Va. 23188  
Business Phone: (757) 258-0303 Fax: \_\_\_\_\_  
Contact Person: Bruce Abbott Title: \_\_\_\_\_

Design Professional: *(Note: Professional Engineer or Certified Land Surveyor responsible for the design and preparation of plans and specifications for the Stormwater Management / BMP facility.)*

Firm Name: AES Consulting Engineers  
Mailing Address: 5248 Olde Towne Road  
Williamsburg, Va. 23188  
Business Phone: (757) 253-0040  
Fax: (757) 220-8994  
Responsible Plan Preparer: Mark Richardson P.E.  
Title: Senior Project Manager  
Plan Name: Multi-Ministry Building James River Baptist Church  
Firm's Project No. 9552  
Plan Date: 4/14/06  
Sheet No.'s Applicable to SWM/BMP Facility: 1 / 5 / 7 /

BMP Contractor: *(Note: Site Work Contractor directly responsible for construction of the Stormwater Management / BMP facility.)*

Name: Reeds Enterprises, LLC  
Mailing Address: 145 Saw mill road  
williamsburg, Va. 23188  
Business Phone: (757) 259-9011  
Fax: (757) 282-2468  
Contact Person: Wayne Reed  
Site Foreman/Supervisor: Scott Lindsay  
Specialty Subcontractors & Purpose (for BMP Construction Only):  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

**Section 4 – Professional Certifications:**

Certifying Professionals: *(Note: A Registered Professional Engineer or Certified Land Surveyor is responsible for preparation of a Record Drawing, sometimes referred to as an As-Built plan, for the drainage system for the project including any Stormwater Management/BMP Facilities. A Registered Professional Engineer is responsible for the inspection, monitoring and certification of Stormwater Management / BMP facilities during its construction.)*

**Record Drawing and Construction Certifications for Stormwater Management / BMP Facilities**

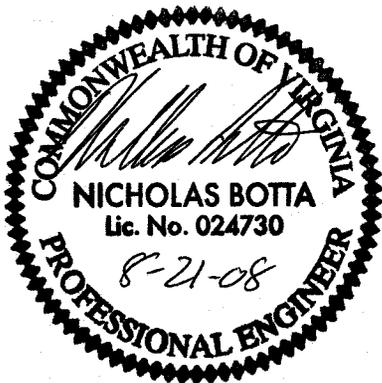
**Record Drawing Certification**

Firm Name: AES CONSULTING ENGINEERS  
Mailing Address: 5248 OLDE TOWNE ROAD  
SUITE 1, WILLIAMSBURG, VA 23188  
Business Phone: 757-253-0040  
Fax: 757-220-8994

Name: NICHOLAS BOTTA, P.E.  
Title: PROJECT ENGINEER

Signature: *Nicholas Botta*  
Date: 8-21-08

I hereby certify to the best of my knowledge and belief that this record drawing represents the actual condition of the Stormwater Management / BMP facility. The facility appears to conform with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.



(Seal)

Virginia Registered Professional Engineer  
Or Certified Land Surveyor

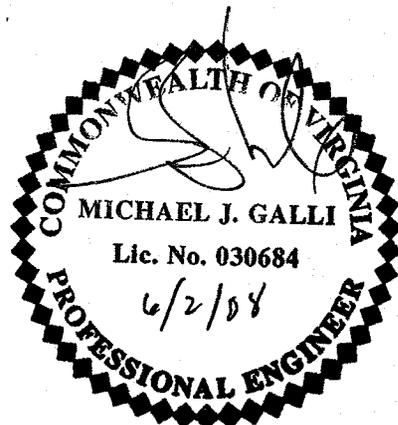
**Construction Certification**

Firm Name: ECS Mid-Atlantic, LLC  
Mailing Address: 108 Ingram Road, Unit 1  
Williamsburg, Va. 23188  
Business Phone: (757) 229-6677  
Fax: (757) 229-9978

Name: Michael J. Galli  
Title: Vice President

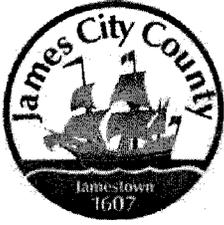
Signature: *Michael J. Galli*  
Date: 6/2/08

I hereby certify to the best of my knowledge and belief that this Stormwater Management / BMP facility was monitored and constructed in accordance with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.



(Seal)

Virginia Registered  
Professional Engineer



**James City County Environmental Division  
Stormwater Management/BMP Record Drawing &  
Construction Certification Review  
Tracking Form**

Project Name: James River Baptist Church  
County Plan No.: SP-044-06  
Stormwater Management Facility: GC008  
BMP Phase #:  I  II  III  
 Information Package Received. Date/By: 8-26-08  
 Completeness Check:  
 Record Drawing Date/By: 8-26-08 (resubmitted) AES  
 Construction Certification Date/By: 8-26-08 ECS  
 RD/CC Standard Forms (Required for all BMPs after Feb 1<sup>st</sup> 2001 Only)  
 Insp/Maint Agreement # / Date: 8/9/07  
 BMP Maintenance Plan Location: Sheet 7 - approved Plan  
 Other: \_\_\_\_\_  
 Standard E&SC Note on Approved Plan Requiring RD/CC or County comment in plan review  
 Yes  No Location: Sheet 7 - approved plan  
 Assign County BMP ID Code #: Code: GC008  
 Preliminary Input/Log into Division's "As-Built Tracking Log"  
 Add Location to GIS Map. Obtain basic site information (GPIN, Owner, Address, etc.)  
 Preliminary Log into Access Database (BMP ID #, Plan No., GPIN, Project Name, etc.)  
 Active Project File Review (correspondence, H&H, design computations, etc.)  
 Initial As-Built File setup (File label, folder, copy plan/details/design information, etc.)  
 Inspector Check of RD/CC (forward to Inspector using transmittal for cursory review).  
 Pre-Inspection Drawing Review of Approved Plan (quick look prior to Field Inspection).  
 Final Inspection (FI) Performed Date: 12/3/08  
 Record Drawing (RD) Review Date: 9/08  
 Construction Certification (CC) Review Date: 9/08  
 Actions:  
 No comments.  
 Comments. Letter Forwarded. Date: \_\_\_\_\_  
 Record Drawing (RD)  
 Construction Certification (CC)  
 Construction-Related (CR)  
 Site Issues (SI)  
 Other: \_\_\_\_\_  
 Second Submission: 6/08 & 8/08  
 Reinspection (if necessary): all reinspections completed as of 12/3/08  
 Acceptable for SWM Purposes (RD/CC/CR/Other). Ok to proceed with bond release.  
 Complete "Surety Request Form".  
 Check/Clean active file of any remaining material and finish "As-Built" file.  
 Add to County BMP Inventory/Inspection schedule (Phase I, II or III).  
 Copy Final Inspection Report into County BMP Inspection Program file.  
 Obtain Digital Photographs of BMP and save into County BMP Inventory.  
 Request mylar/reproducible from As-Built plan preparer.  
 Complete "As-built Tracking Log".  
 Last check of BMP Access Database (County BMP Inventory).  
 Add BMP to JCC Hydrology & Hydraulic database (optional).  
 Add BMP to Municipal BMP list (if a County-owned facility).  
 Add BMP to PRIDE BMP ratings database.

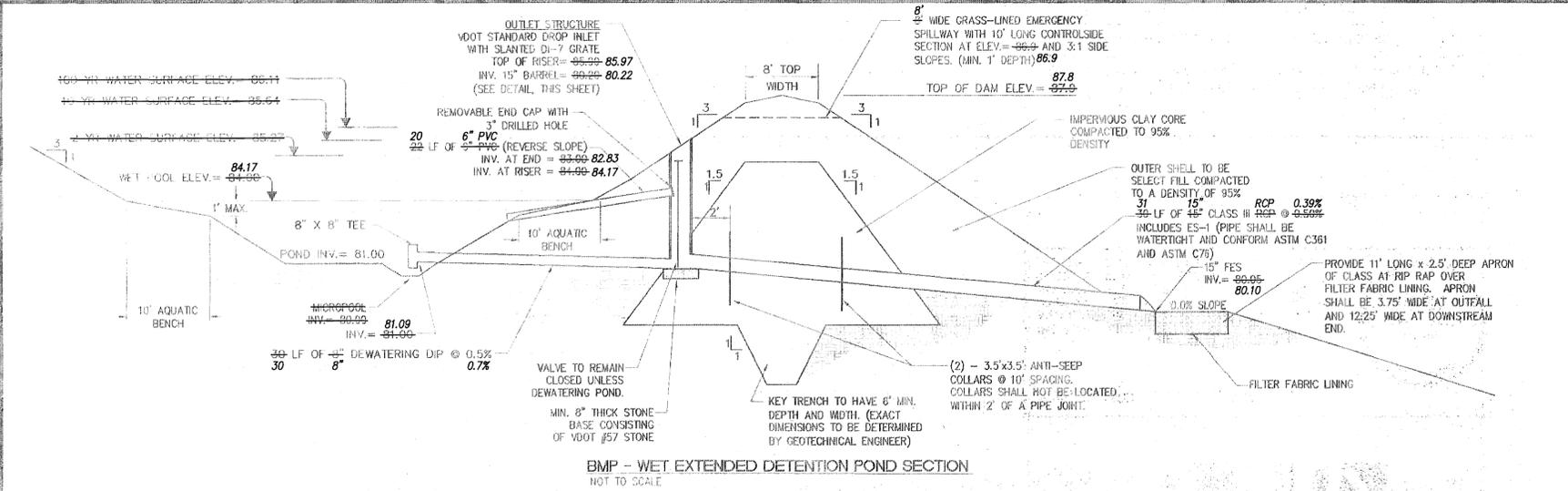
**Final Sign-Off**

Inspector: [Signature]  
Chief Engineer: [Signature]

Date: 12/4/08  
Date: 12/4/08

\*\*\* See separate checklist, if needed.





BMP - WET EXTENDED DETENTION POND SECTION  
NOT TO SCALE

**STORMWATER MANAGEMENT/ BMP FACILITY MAINTENANCE PLAN**

PROPER MAINTENANCE OF THIS FACILITY IS ENCOURAGED TO PREVENT THE INTRODUCTION OF DEBRIS AND SEDIMENT IN TO THE FACILITY, SPILLWAY AND DOWNSTREAM WATERWAYS. FOLLOWING INSTALLATION OF THE FACILITY AND ESTABLISHMENT OF VEGETATION IN DISTURBED AREAS, INSPECTIONS FOR SEDIMENT BUILDUPS WILL BE PERFORMED AT LEAST QUARTERLY. IT IS ANTICIPATED THAT UNDER NORMAL CONDITIONS, SEDIMENT REMOVAL FROM THE FACILITY WILL BE REQUIRED EVERY 10 YEARS. IF OTHER CONSTRUCTION OR RELATED ACTIVITIES ARE PERFORMED ON UP-SLOPE AREAS, ADEQUATE PROTECTION SHOULD BE PROVIDED AND INSPECTIONS PERFORMED AT LEAST ONCE WEEKLY.

A DESIGNATED REPRESENTATIVE OF THE OWNER WILL INSPECT THE SWM STRUCTURE AFTER EACH SIGNIFICANT RAINFALL EVENT OR THE FOLLOWING WORKING DAY IF A WEEKEND OR HOLIDAY OCCURS. A SIGNIFICANT RAINFALL FOR THIS STRUCTURE IS DEFINED AS ONE (1) INCH OR MORE OF GAUGED RAINFALL WITHIN A 24 HOUR PERIOD. ONCE PER YEAR, A REPRESENTATIVE OF THE COUNTY MAY JOINTLY INSPECT THE STRUCTURE. APPROPRIATE ACTION PERFORMED AT THE COST OF THE OWNER, WILL BE TAKEN TO ENSURE APPROPRIATE MAINTENANCE.

**INSPECTION AND MAINTENANCE OF THE FACILITY WILL CONSIST OF THE FOLLOWING ADDITIONAL MEASURES:**

1. THE INSPECTION FOR SEDIMENT BUILDUP WILL BE PERFORMED BY VISUAL INSPECTION AND A PHYSICAL DETERMINATION OF SEDIMENT DEPTH WITHIN THE STORAGE AREA. IF THE SEDIMENT REACHES THE DEPTH OF 1.5 FT. ABOVE THE BOTTOM OF SEDIMENT FOREBAY (i.e. CLEANOUT ELEVATION 82.5), REMOVAL IS REQUIRED USING A RUBBER-WHEELED BACKHOE. AT THE SAME TIME, OR AT LEAST ONCE PER YEAR, CLEAN THE RISER BOTTOM AND OUTLET PIPE OF ACCUMULATED SEDIMENTS. DISPOSE OF SEDIMENTS REMOVED FROM THE FACILITY AT AN ACCEPTABLE DISPOSAL AREA.
2. PERFORM MAINTENANCE MOWING OF POND GRASSES AT LEAST TWICE EACH YEAR. GRASSES SUCH AS TALL FESCUE SHOULD BE MOWED IN EARLY SUMMER AFTER EMERGENCE OF THE HEADS ON COOL SEASON GRASSES AND IN LATE FALL TO PREVENT SEEDS OF ANNUAL WEEDS FROM MATURING. MOWING OF LEGUMES CAN BE LESS FREQUENT.
3. PERFORM SOIL SAMPLING ON STABILIZED POND SOIL AREAS ONCE EVERY FOUR (4) YEARS. SOIL SAMPLING AND TESTING SHOULD BE PERFORMED BY A QUALIFIED INDEPENDENT TESTING LABORATORY. APPLY ADDITIONAL LIME AND FERTILIZER IN ACCORDANCE WITH TEST RECOMMENDATIONS.
4. IN STABILIZED POND AREAS, IF VEGETATION COVERS LESS THAN 40% OF SOIL SURFACE, LIME, FERTILIZE AND SEED IN ACCORDANCE WITH RECOMMENDATIONS FOR NEW SEEDING AS LISTED IN THE DAM CONSTRUCTION NOTES. IF VEGETATION COVERS MORE THAN 40% BUT LESS THAN 70% OF SOIL SURFACES, LIME, FERTILIZE AND OVERSEED IN ACCORDANCE WITH THE CURRENT SEEDING RECOMMENDATIONS OR REQUIREMENTS OF THE VESCH.
5. PERFORM QUARTERLY INSPECTIONS OF THE RISER SECTION AND CREST OF SPILLWAY FOR THE OBSERVANCE OF COLLECTED DEBRIS. IMMEDIATELY REMOVE ANY DEBRIS TO MAINTAIN THE INTEGRITY OF THE STRUCTURE AND PROVIDE AN ATTRACTIVE APPEARANCE.
6. PERFORM YEARLY STRUCTURAL INSPECTIONS OF THE FACILITY FOR DAMAGE. STRUCTURAL INSPECTION SHALL BE PERFORMED ON THE CONCRETE RISER, TRASH RACK, ORIFICE/ WEIR(S), OUTLET BARREL AND POND EMBANKMENT. IF DAMAGE IS EVIDENT, FURTHER INVESTIGATION BY A PROFESSIONAL ENGINEER MAY BE REQUIRED TO ASSESS THE INTEGRITY OF THE STRUCTURE.
7. PERFORM QUARTERLY INSPECTIONS OF THE GRADED SIDE SLOPES OF THE DETENTION FACILITY FOR SIGNS OF ANIMAL/ RODENT BORROWS OR SLOPE EROSION. IMMEDIATELY PERFORM NECESSARY REPAIRS, RESEEDING OR RESEEDING AS APPROPRIATE.
8. PERFORM YEARLY OBSERVATIONS OF PERIMETER AREAS SURROUNDING THE FACILITY TO ENSURE CHANGES IN LAND USE, TOPOGRAPHY OR ACCESS HAVE NOT OCCURRED AND DO NOT AFFECT THE OPERATION, MAINTENANCE, ACCESS OR SAFETY FEATURES AS PROVIDED. APPROPRIATE ACTION IS REQUIRED TO ENSURE ADEQUACY AND TO PROVIDE A CLEAR, SAFE PASSAGE FOR MAINTENANCE VEHICLES TO THE EMBANKMENT AND PRINCIPLE FLOW CONTROL STRUCTURES.
9. INSPECT AND EXERCISE POND DRAIN VALVE ON AN ANNUAL BASIS.
10. RECORD KEEPING: THE OWNER OR DESIGNATED REPRESENTATIVE SHALL KEEP REASONABLE, ACCURATE WRITTEN RECORDS OR INSPECTIONS PERFORMED FOR THE STRUCTURE. RECORDS SHALL DOCUMENT THE REPAIRS PERFORMED. COPIES SHALL BE PROVIDED TO THE COUNTY UPON REQUEST.
11. THE FACILITY SHALL NOT BE MODIFIED IN ANY WAY WITHOUT PRIOR CONSENT/ APPROVAL OF JAMES CITY COUNTY.
12. DEAD OR DYING PLANT MATERIAL SHALL BE REPLACED AFTER THE FIRST GROWING SEASON. THE POND SLOPE SHOULD BE MAINTAINED IN A NATURAL STATE WITH THE EXCEPTION THAT CHOKING VINES AND NON-NATIVE INVASIVE SPECIES SHOULD BE REMOVED BY HAND METHODS ONLY AT THE ONSET OF THE SECOND GROWING SEASON.

**GENERAL NOTES FOR CONSTRUCTION OF STORMWATER BASINS**

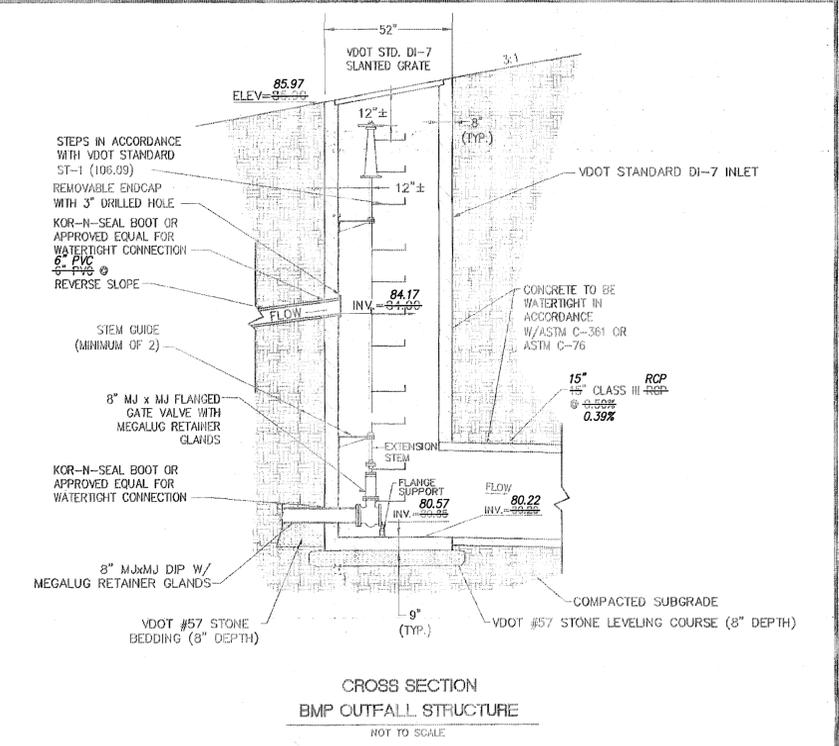
1. THE CONTRACTOR SHALL PROVIDE ALL WORK AND MATERIALS NEEDED TO CONSTRUCT THE STORMWATER BASIN, STORMWATER MANAGEMENT PRACTICES, BEST MANAGEMENT PRACTICES, SEDIMENT BASINS AND TRAPS. THE WORK SHALL INCLUDE ALL LABOR, MATERIALS, EQUIPMENT AND MATERIALS NEEDED FOR THE COMPLETION OF GRADING AND EARTHWORK ASSOCIATED WITH THE CONSTRUCTION.
2. THE CONTRACTOR SHALL CONSULT AND PROVIDE FOR THE SERVICES OF A GEOTECHNICAL ENGINEER. THE GEOTECHNICAL ENGINEER SHALL PROVIDE TEST RESULTS ON PLACED DAM MATERIALS, IDENTIFYING SOIL CLASSIFICATION, PERMEABILITY, PLASTICITY INDEX, AND COMPACTION. ALL TESTS SHALL BE IN CONFORMANCE WITH ASTM STANDARDS. THE COST OF THE SERVICES OF THE GEOTECHNICAL ENGINEER SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR. SATISFACTORY GEOTECHNICAL RESULTS ARE NEEDED PRIOR TO FINAL APPROVAL.
3. ALL INSPECTIONS REQUIRED FOR THE WORK SHALL BE PERFORMED BY A GEOTECHNICAL ENGINEER AT THE EXPENSE OF THE GENERAL CONTRACTOR.
4. ON-SITE EXCAVATED MATERIAL, IF DETERMINED SUITABLE FOR USE IN DAM CONSTRUCTION BY A GEOTECHNICAL ENGINEER, MAY BE USED FOR DAM CONSTRUCTION. SHOULD ADDITIONAL MATERIAL BE REQUIRED, THE CONTRACTOR SHALL IDENTIFY THE NEED FOR MATERIAL TO THE OWNER, AS ADDITIONAL BORROW MATERIAL MAY BE AVAILABLE ON THE PROPERTY. ALL EXCAVATED MATERIAL DETERMINED BY THE GEOTECHNICAL ENGINEER TO BE UNSUITABLE SHALL BE DISPOSED OF PROPERLY AT THE CONTRACTOR'S EXPENSE. ALL EXCAVATED MATERIAL NOT REQUIRED FOR BACKFILLING SHALL EITHER BE DEPOSITED ON SITE AND SPREAD BY THE CONTRACTOR, OR SHALL BE DEPOSITED IN AN AREA ON THE PROPERTY AS DIRECTED BY THE OWNER. THE CONTRACTOR SHALL PROVIDE PROPER STABILIZATION AND EROSION AND SEDIMENT CONTROL MEASURES NEEDED TO CONTROL AS PER THE VESCH THIRD EDITION.
5. UNDERCUT FOR THE FOUNDATION OF THE DAM EMBANKMENT SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATION. THE FOUNDATION SHALL BE BACKFILLED WITH SOILS CLASSIFIED AS SM, SC, OR CL UNDER THE UNIFIED SOIL CLASSIFICATION SYSTEM. SOILS SHALL HAVE A MINIMUM OF 15% BY WEIGHT FINES, HAVING A PLASTICITY INDEX OF 30% AND A PERMEABILITY OF 0.0004 IN./SEC. OR LESS. FILL SHALL BE COMPACTED IN 8-INCH LOOSE THICKNESS LIFTS, OR AS DIRECTED BY THE GEOTECHNICAL ENGINEER, TO A DRY DENSITY OF 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY (ASTM D-698). EXCAVATION FOR THE DAM KEY SHALL BE IN ACCORDANCE TO THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS. HEIGHT, DEPTH, AND WIDTH OF THE KEY SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS. THE KEY SHALL BE FORMED USING SOILS CLASSIFIED AS CL OR CH, WITH A PERMEABILITY OF 0.0004 IN./SEC. OR LESS.
6. THE DAM CORE SHALL BE AS CONSTRUCTED WITH NON-EXPANSIVE CL OR CH CLAYEY MATERIAL WITH PERMEABILITY OF 0.0004 IN./SEC. OR LESS. THE FILL OF THE CORE SHALL BE MADE IN 8-INCH LOOSE THICKNESS LIFTS, OR AS DIRECTED BY THE GEOTECHNICAL ENGINEER, MOISTURE CONDITIONED TO WITHIN -1%/+3% OF THE OPTIMUM MOISTURE CONTENT, AND COMPACTED TO A MINIMUM 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY (ASTM D-698). SIZE, SHAPE, WIDTH, DEPTH, AND HEIGHT OF THE DAM CORE SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS. TO COVER THE DAM CORE, A SILTY FINE SAND OR CLAYEY SOIL (SM, SC, OR CL) SHALL BE PLACED.
7. IN ORDER TO MAINTAIN A WET POOL, THE BOTTOM SURFACE OF THE BMP, ALONG WITH THE SIDE SLOPES TO A HEIGHT AT LEAST 4 FEET ABOVE THE BOTTOM, SHALL CONSIST OF A LAYER OF LOW PERMEABILITY SOIL, SUCH AS CL OR CH, AT LEAST 2 FEET THICK. IF A WET POOL IS UNABLE TO BE ESTABLISHED AND MAINTAINED, THE CONTRACTOR SHALL EXCAVATE THE BOTTOM MATERIAL AND REINSTALL A LOW PERMEABILITY SOIL AT THE DIRECTION OF THE DESIGN ENGINEER AND GEOTECHNICAL ENGINEER.
8. THE STORMWATER MANAGEMENT/BMP FACILITIES SHOWN ON THESE PLANS REQUIRE THE SUBMISSION, REVIEW AND APPROVAL OF RECORD DRAWING(S) AND CONSTRUCTION CERTIFICATION PRIOR TO RELEASE OF THE POSTED BOND/SURETY. THE GEOTECHNICAL ENGINEER IS TO ENSURE THAT HIS/HER INSPECTION OF THE SWM/BMP CONSTRUCTION ACTIVITY IS PERFORMED DURING AND FOLLOWING CONSTRUCTION OF THE SWM/BMP IN ACCORDANCE WITH THE JAMES CITY COUNTY ENVIRONMENTAL DIVISION STORMWATER MANAGEMENT/BMP FACILITIES DESIGN GUIDELINES HANDBOOK, DATED AUGUST 30, 2000.

**DAM CONSTRUCTION NOTES**

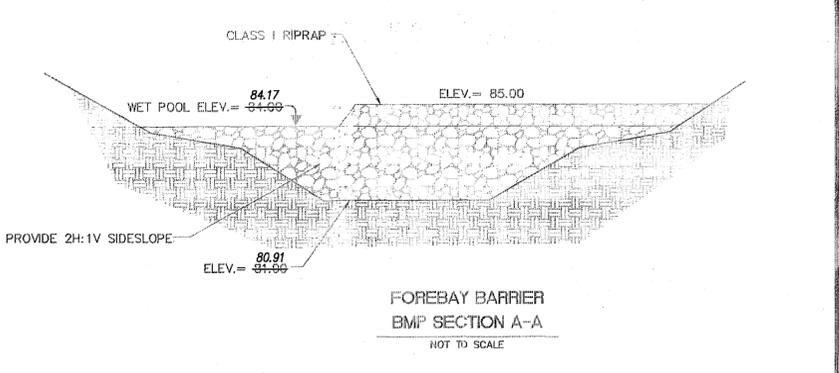
1. THE CONTRACTOR SHALL REFER TO THE "REPORT OF SUBSURFACE AND GEOTECHNICAL ENGINEERING ANALYSIS" PREPARED BY EES MID-ATLANTIC, LLC, DATED JULY 28, 2008 FOR SPECIFICATIONS ON THE CONSTRUCTION OF THE BMP FACILITY, INCLUDING THE EMBANKMENT.
2. THE GEOTECHNICAL SUBSURFACE EXPLORATION REPORT AT THE PROPOSED DAM SITE HAS BEEN PERFORMED TO ENSURE SUITABILITY OF THE SUBGRADE. THE GEOTECHNICAL INVESTIGATION HAS DETERMINED THE SUITABILITY OF THE FILL MATERIAL. THESE RECOMMENDATIONS ARE HEREBY MADE A PART OF THE DAM'S CONSTRUCTION SPECIFICATIONS. A REPRESENTATIVE OF THE GEOTECHNICAL CONSULTANT SHALL BE ON SITE DURING CONSTRUCTION TO ENSURE PROPER MATERIALS AND DAM CONSTRUCTION METHODS ARE UTILIZED. FOLLOWING DAM CONSTRUCTION, THE GEOTECHNICAL CONSULTANT SHALL PROVIDE WRITTEN DOCUMENTATION, SIGNED BY A PROFESSIONAL ENGINEER, THAT THE DAM WAS BUILT IN ACCORDANCE WITH THEIR RECOMMENDATIONS, PLANS, AND SPECIFICATIONS. THE GEOTECHNICAL CONSULTANT SHALL COORDINATE WITH THE DESIGN ENGINEER TO COMPLETE THE JOE ENVIRONMENTAL DIVISION STORMWATER MANAGEMENT/BMP FACILITIES CONSTRUCTION AND AS-BUILT CERTIFICATION FORM. THE CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATING THE DAM CONSTRUCTION SCHEDULE WITH THE GEOTECHNICAL CONSULTANT IN ORDER TO ENSURE ON-SITE MONITORING.
3. SITE PREPARATION: THE CONTRACTOR SHALL STRIP ALL AREAS OF THE PERMANENT COVER IN CONSTRUCTION AREA TO REMOVE ALL UNSUITABLE MATERIALS. THE UNSUITABLE MATERIALS TO BE REMOVED BY STRIPPING SHALL INCLUDE ALL TOPSOIL, DEBRIS AND VEGETATIVE MATTER, INCLUDING STUMPS AND ROOTS, AND ALL OTHER MATERIALS WHICH MAY BE UNSUITABLE FOR USE IN THE PERMANENT CONSTRUCTION.
4. EMBANKMENT: THE EXPOSED SUB GRADE SOILS SHALL BE CAREFULLY INSPECTED BY THE GEOTECHNICAL ENGINEER. ANY UNSUITABLE MATERIALS THIS EXPOSED SHALL BE REMOVED AND REPLACED WITH A WELL COMPACTED, STABLE MATERIAL. DENSITY TESTING, AT THE DISCRETION OF THE OWNER/GEOTECHNICAL ENGINEER, SHALL BE PERFORMED AT THIS TIME. THE EMBANKMENT SHALL BE KEPT INTO THE UNDISTURBED (EXISTING) SOIL STRATUM. EMBANKMENT SHOULD BE KEPT AT LEAST 4 FEET INTO THE SPANION OR AS SPECIFIED BY THE GEOTECHNICAL ENGINEER (WITHIN 6 FT. MIN). THE EMBANKMENT FOUNDATION AND ABUTMENTS SHALL BEAR ON FIRM AND STABLE EXISTING SUB-GRADE WHICH HAS BEEN PREPARED SO AS TO REMOVE ALL ORGANIC, LOOSE, AND GENERALLY UNSUITABLE MATERIAL. ALL MATERIALS TO BE USED FOR BACKFILL OR COMPACTED FILL SHALL BE INSPECTED AND, IF NECESSARY, TESTED BY THE GEOTECHNICAL ENGINEER IN ACCORDANCE WITH ASTM D698 PRIOR TO PLACEMENT TO DETERMINE IF THEY ARE SUITABLE FOR THE INTENDED USE. THE FILL MATERIAL SHALL BE TAKEN FROM APPROVED BORROW AREAS. IT SHALL BE CLEAN MINERAL SOIL, FREE OF ROOTS, WOOD VEGETATION, OVERSIZED STONES, ROCKS, OR OTHER OBSCURABLE MATERIALS. MATERIALS TO BE USED FOR THE CONSTRUCTION OF THE SHELL SHALL BE SELECTED BASED ON FREE OF STUMPS, ROOTS, ROCKS, TRASH, ETC. AND SHALL BE MORE PERVIOUS THAN THE IMPERVIOUS CLAY CORE. AREAS ON WHICH FILL IS TO BE PLACED SHALL BE SCOURED A MINIMUM OF 4 INCHES PRIOR TO PLACEMENT OF FILL. THE FILL MATERIAL'S MOISTURE CONTENT SHALL BE AT 2% OF OPTIMUM MOISTURE CONTENT AS DETERMINED BY ASTM D2216. FILL MATERIAL SHALL BE PLACED IN HORIZONTAL LIFTS NOT EXCEEDING 8 INCHES IN THICKNESS AND IN CONTINUOUS LAYERS OVER THE ENTIRE LENGTH OF THE FILL. FILL MATERIAL SHALL BE COMPACTED TO A MINIMUM 95% OF THE MAXIMUM DRY DENSITY OBTAINED IN ACCORDANCE WITH ASTM SPECIFICATION D-698, STANDARD PROCTOR METHOD. FINISHED GRADES SHALL BE MERGED NATURALLY INTO THE EXISTING GRADES AND NOT EXCEED A SLOPE GREATER THAN 3:1.
5. CUTOFF DRENCH/KEY TRENCH: THE DRENCH SHALL BE EXCAVATED ALONG THE CENTERLINE OF THE DAM. THE MINIMUM DEPTH SHALL BE AS SHOWN ON THE PLANS AND SHALL EXTEND UP BOTH ABUTMENTS. THE BOTTOM WIDTH SHALL BE WIDE ENOUGH TO PERMIT OPERATION OF COMPACTING EQUIPMENT. THE SIDE SLOPES SHALL BE NO STEEPER THAN 1:1.
6. PRINCIPAL SPILLWAY: THE BOTTOM OF THE SPILLWAY RISER FOUNDATION BASE EXCAVATION SHALL BE OBSERVED BY THE GEOTECHNICAL ENGINEER TO ENSURE THAT ALL UNSUITABLE AND LOOSE MATERIALS ARE REMOVED AND THAT ACCEPTABLE BEARING CONDITIONS EXIST IN THE FOUNDATION'S BASE. ALL JOINTS IN THE PRINCIPAL SPILLWAY STRUCTURE SHALL BE WATER TIGHT CONSTRUCTION. PERVIOUS MATERIALS SUCH AS SAND, GRAVEL OR CRUSHED STONE SHALL NOT BE USED AS BACKFILL AROUND THE BARREL OR ANTI-SEEP COLLARS. FILL MATERIAL SHALL BE PLACED AROUND THE PIPE IN 4 INCH LAYERS AND COMPACTED BY HAND TO THE SAME DENSITY AS THE EMBANKMENT. A MINIMUM OF TWO FEET OF FILL SHALL BE HAND-COMPACTED OVER THE BARREL BEFORE CROSSING IT WITH CONSTRUCTION EQUIPMENT.
7. VEGETATIVE STABILIZATION: FINAL VEGETATIVE COVER (STABILIZATION) SHALL CONSIST OF TOP SOILING, LIMING, FERTILIZING, SEEDING, AND MULCHING TO ASSURE A FIRM STAND OF GRASS AS SOON AS PRACTICAL. SEDIMENT BASINS AND OTHER TEMPORARY EROSION CONTROL MEASURES ARE TO BE REMOVED ONLY WHEN STABILIZATION IS COMPLETE. FINAL VEGETATIVE COVER SHALL BE PROVIDED IN ACCORDANCE WITH THE FOLLOWING:  
TOPSOIL: AT LEAST 4" THICKNESS OBTAINED FROM STOCKPILES ON SITE, FREE OF LARGE DEBRIS.  
LIME: 4,000#/ACRE (008/1,000 S.F.)  
SEED: KEYWAY 31 2L PERMANENT 250#/ACRE (04/1,000 S.F.)  
FERTILIZER: 10/10/10 MIX, 1,000#/ACRE FALL (238/1,000 S.F.)  
MULCH: STRAW OR HAY (LOCALLY OBTAINED) 4,000#/ACRE (008/1,000 S.F.)

**CONSTRUCTION SEQUENCE**

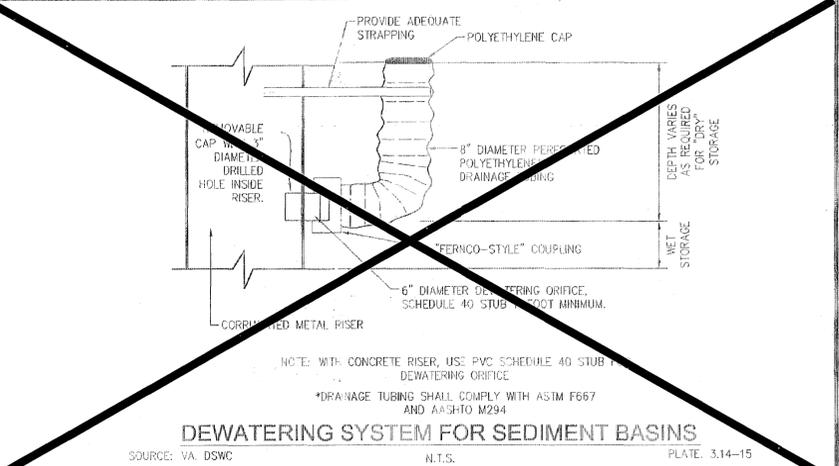
1. PRIOR TO OBTAINING LAND DISTURBING PERMIT, THE CONTRACTOR SHALL OBTAIN A VSMF PERMIT (VIRGINIA STORMWATER MANAGEMENT PROGRAM) FROM DCR (VIRGINIA DEPARTMENT OF CONSERVATION AND RECREATION).
2. THE CONTRACTOR SHALL SCHEDULE A PRE-CONSTRUCTION MEETING WITH THE JAMES CITY COUNTY ENVIRONMENTAL DIVISION PRIOR TO BEGINNING ANY WORK AT THE SITE.
3. CONTACT "MISS UTILITY" FOR PUBLIC SERVICES AND HAVE A PRIVATE UTILITY LOCATOR FOR PRIVATE SERVICES.
4. INSTALL CONSTRUCTION ENTRANCE, SAFETY FENCE, SILT FENCE, AND TREE PROTECTION.
5. INSTALL SEDIMENT BASIN (SEE DAM CONSTRUCTION NOTES) AND DIVERSION DIKE WITH RIPRAP-LINED CHANNEL.
6. INSTALL GRASS LINED CHANNEL TO RIPRAP-LINED CHANNEL IN SEDIMENT BASIN.
7. CLEAR AND GRUB REMAINDER OF SITE, AND DEMOLISH AND REMOVE ALL DEMOLITION ITEMS.
8. INSTALL UTILITIES AND STORM SEWER.
9. GRADE PARKING LOT AND INSTALL FILL DIVERSION PER VESCH SPEC. 3.10 AND RIGHT-OF-WAY DIVERSION PER VESCH SPEC. 3.11. ADJUST DIVERSIONS DURING FILL OPERATION.
10. PREPARE BUILDING PAD AND ADJUST DIVERSIONS AS NECESSARY.
11. CONSTRUCT BUILDING.
12. CONSTRUCT PROPOSED SIDEWALKS, CURB, AND CURB & GUTTER.
13. CONSTRUCT PARKING LOT AND STRIPING.
14. PREPARE FINAL GRADING AND PLANT LANDSCAPING.
15. LAY PERMANENT SEEDING AND MULCH.
16. PROVIDE FINAL CLEANOUT OF SEDIMENT BASIN AND CONVERT TO BMP AFTER FINAL SITE STABILIZATION.
17. REMOVE ALL EROSION AND SEDIMENT CONTROL MEASURES WITHIN THIRTY DAYS OF FINAL SITE STABILIZATION, BUT ONLY AFTER APPROVAL IS OBTAINED FROM THE ASSIGNED JAMES CITY COUNTY ENVIRONMENTAL INSPECTOR.



CROSS SECTION  
BMP OUTFALL STRUCTURE  
NOT TO SCALE



FOREBAY BARRIER  
BMP SECTION A-A  
NOT TO SCALE



DEWATERING SYSTEM FOR SEDIMENT BASINS  
SOURCE: VA DSWC N.T.S. PLATE 3.14-15

NO.	DATE	REVISION / COMMENT / NOTE
1	8/25/06	REVISED FOR COUNTY COMMENTS
2	12/8/06	REVISED FOR COUNTY COMMENTS
3	2/12/07	REVISED FOR USA COMMENTS
4		
5		

5248 Old Towne Road, Suite 1  
Williamsburg, Virginia 23188  
(757) 253-0040  
Fax (757) 220-8894

**CONSULTING ENGINEERS**  
WILLIAMSBURG • RICHMOND • GLOUCESTER

STORMWATER MANAGEMENT/BMP PLAN

MULTI-MINISTRY BUILDING  
JAMES RIVER BAPTIST CHURCH

JAMES CITY COUNTY  
POW-HATAN DISTRICT  
VIRGINIA

Designed HB	Drawn LBA
Scale N.T.S.	Date 4/14/06
Project No. 9532	
Drawing No. 7 AS-BUILT	

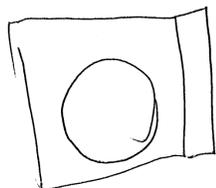
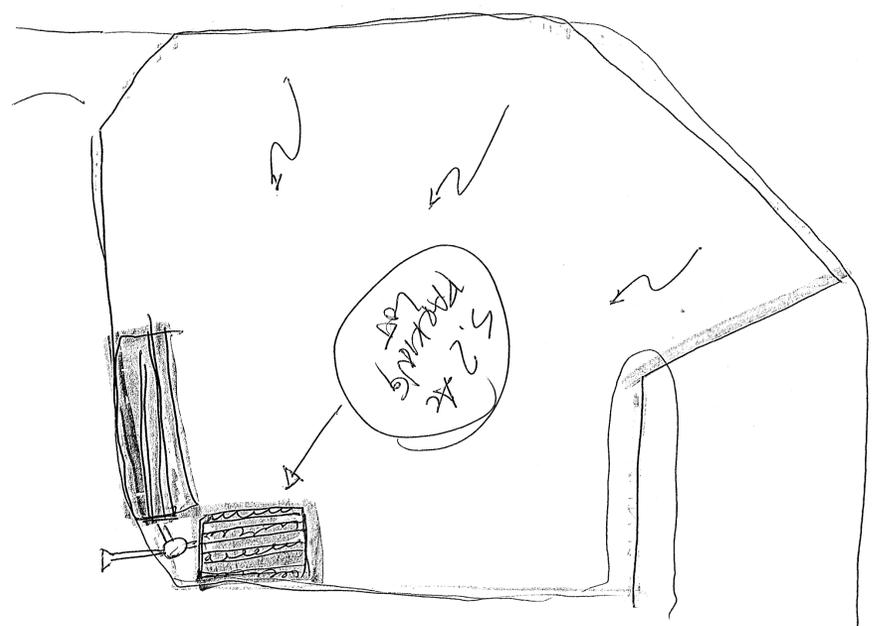


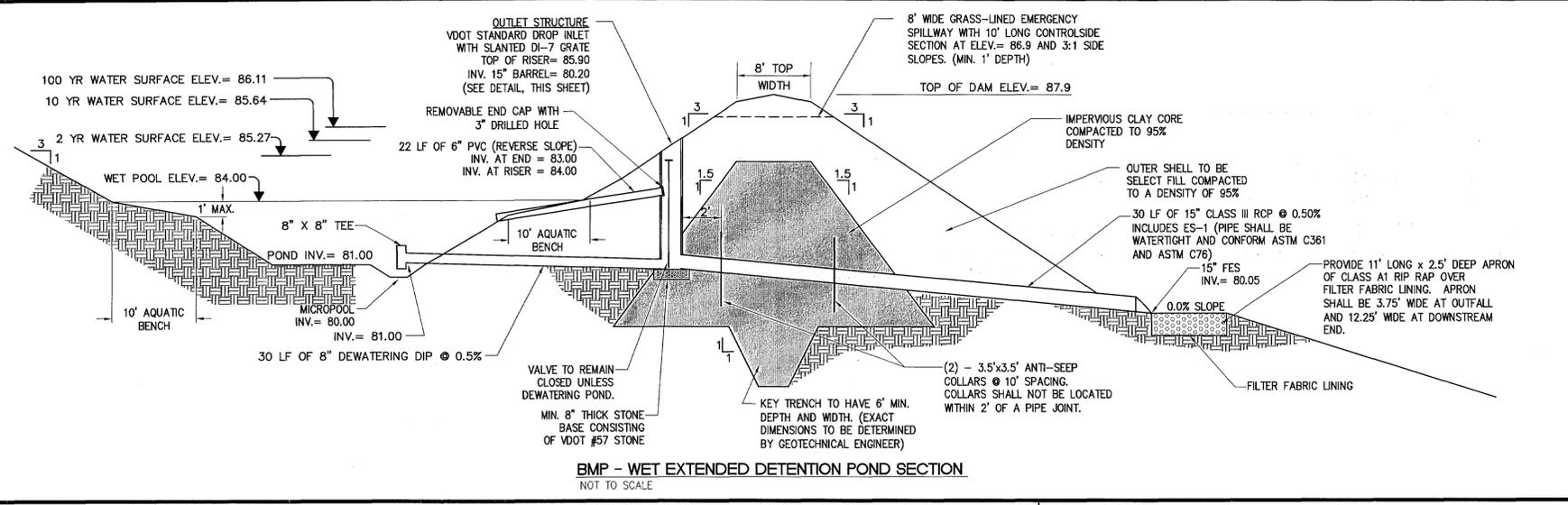




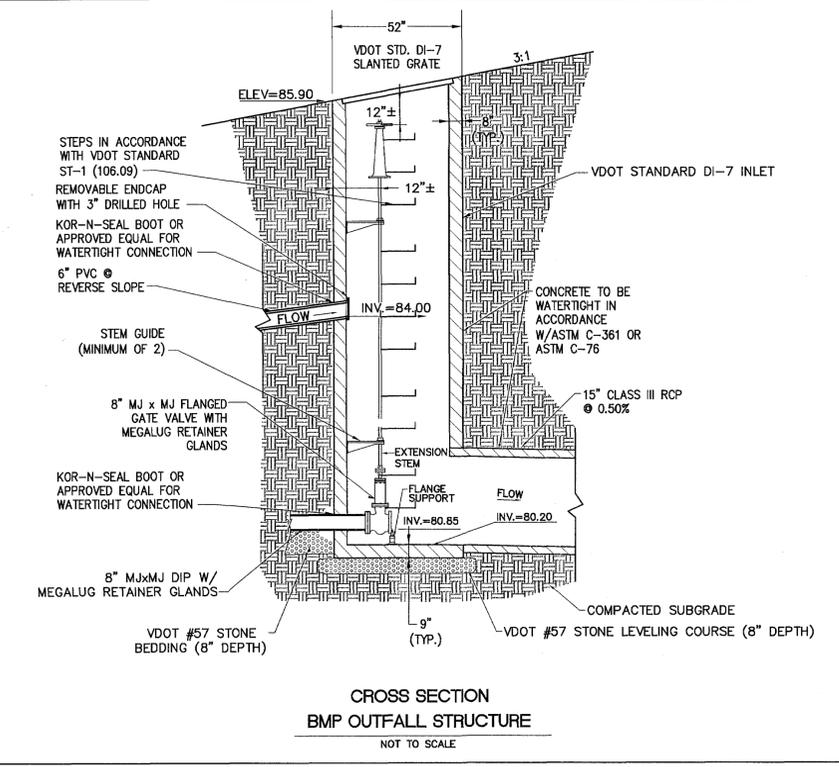








**BMP - WET EXTENDED DETENTION POND SECTION**  
NOT TO SCALE



**CROSS SECTION BMP OUTFALL STRUCTURE**  
NOT TO SCALE

**STORMWATER MANAGEMENT/ BMP FACILITY MAINTENANCE PLAN**

PROPER MAINTENANCE OF THIS FACILITY IS ENCOURAGED TO PREVENT THE INTRODUCTION OF DEBRIS AND SEDIMENT INTO THE FACILITY, SPILLWAY AND DOWNSTREAM WATERWAYS. FOLLOWING INSTALLATION OF THE FACILITY AND ESTABLISHMENT OF VEGETATION IN DISTURBED AREAS, INSPECTIONS FOR SEDIMENT BUILDUPS WILL BE PERFORMED AT LEAST QUARTERLY. IT IS ANTICIPATED THAT UNDER NORMAL CONDITIONS, SEDIMENT REMOVAL FROM THE FACILITY WILL BE REQUIRED ONCE EVERY 10 YEARS. IF OTHER CONSTRUCTION OR RELATED ACTIVITIES ARE PERFORMED ON UPSLOPE AREAS, ADEQUATE PROTECTION SHOULD BE PROVIDED AND INSPECTIONS PERFORMED AT LEAST ONCE WEEKLY.

A DESIGNATED REPRESENTATIVE OF THE OWNER WILL INSPECT THE SWM STRUCTURE AFTER EACH SIGNIFICANT RAINFALL EVENT OR THE FOLLOWING WORKING DAY IF A WEEKEND OR HOLIDAY OCCURS. A SIGNIFICANT RAINFALL FOR THIS STRUCTURE IS DEFINED AS ONE (1) INCH OR MORE OF GAUGED RAINFALL WITHIN A 24 HOUR PERIOD. ONCE PER YEAR, A REPRESENTATIVE OF THE COUNTY MAY JOINTLY INSPECT THE STRUCTURE. APPROPRIATE ACTION, PERFORMED AT THE COST OF THE OWNER, WILL BE TAKEN TO ENSURE APPROPRIATE MAINTENANCE.

**INSPECTION AND MAINTENANCE OF THE FACILITY WILL CONSIST OF THE FOLLOWING ADDITIONAL MEASURES:**

1. THE INSPECTION FOR SEDIMENT BUILDUP WILL BE PERFORMED BY VISUAL INSPECTION AND A PHYSICAL DETERMINATION OF SEDIMENT DEPTH WITHIN THE STORAGE AREA. IF THE SEDIMENT REACHES THE DEPTH OF 1.5 FT. ABOVE THE BOTTOM OF SEDIMENT FOREBAY (i.e. CLEANOUT ELEVATION 82.5), REMOVAL IS REQUIRED USING A RUBBER-WHEELED BACKHOE. AT THE SAME TIME, OR AT LEAST ONCE PER YEAR, CLEAN THE RISER BOTTOM AND OUTLET PIPE OF ACCUMULATED SEDIMENTS. DISPOSE OF SEDIMENTS REMOVED FROM THE FACILITY AT AN ACCEPTABLE DISPOSAL AREA.
2. PERFORM MAINTENANCE MOWING OF POND GRASSES AT LEAST TWICE EACH YEAR. GRASSES SUCH AS TALL FESCUE SHOULD BE MOWED IN EARLY SUMMER AFTER EMERGENCE OF THE HEADS ON COOL SEASON GRASSES AND IN LATE FALL TO PREVENT SEEDS OF ANNUAL WEEDS FROM MATURING. MOWING OF LEGUMES CAN BE LESS FREQUENT.
3. PERFORM SOIL SAMPLING ON STABILIZED POND SOIL AREAS ONCE EVERY FOUR (4) YEARS. SOIL SAMPLING AND TESTING SHOULD BE PERFORMED BY A QUALIFIED INDEPENDENT TESTING LABORATORY. APPLY ADDITIONAL LIME AND FERTILIZER IN ACCORDANCE WITH TEST RECOMMENDATIONS.
4. IN STABILIZED POND AREAS, IF VEGETATION COVERS LESS THAN 40% OF SOIL SURFACE, LIME, FERTILIZE AND SEED IN ACCORDANCE WITH RECOMMENDATIONS FOR NEW SEEDING AS LISTED IN THE DAM CONSTRUCTION NOTES. IF VEGETATION COVERS MORE THAN 40% BUT LESS THAN 70% OF SOIL SURFACES, LIME, FERTILIZE AND OVERSEED IN ACCORDANCE WITH THE CURRENT SEEDING RECOMMENDATIONS OR REQUIREMENTS OF THE VESCH.
5. PERFORM QUARTERLY INSPECTIONS OF THE RISER SECTION AND CREST OF SPILLWAY FOR THE OBSERVANCE OF COLLECTED DEBRIS. IMMEDIATELY REMOVE ANY DEBRIS TO MAINTAIN THE INTEGRITY OF THE STRUCTURE AND PROVIDE AN ATTRACTIVE APPEARANCE.
6. PERFORM YEARLY STRUCTURAL INSPECTIONS OF THE FACILITY FOR DAMAGE. STRUCTURAL INSPECTION SHALL BE PERFORMED ON THE CONCRETE RISER, TRASH RACK, ORIFICE/ WEIR(S), OUTLET BARREL AND POND EMBANKMENT. IF DAMAGE IS EVIDENT, FURTHER INVESTIGATION BY A PROFESSIONAL ENGINEER MAY BE REQUIRED TO ASSESS THE INTEGRITY OF THE STRUCTURE.
7. PERFORM QUARTERLY INSPECTIONS OF THE GRADED SIDE SLOPES OF THE DETENTION FACILITY FOR SIGNS OF ANIMAL/ RODENT BORROWS OR SLOPE EROSION. IMMEDIATELY PERFORM NECESSARY REPAIRS, REFILLING OR RESEEDING AS APPROPRIATE.
8. PERFORM YEARLY OBSERVATIONS OF PERIMETER AREAS SURROUNDING THE FACILITY TO ENSURE CHANGES IN LAND USE, TOPOGRAPHY OR ACCESS HAVE NOT OCCURRED AND DO NOT AFFECT THE OPERATION, MAINTENANCE, ACCESS OR SAFETY FEATURES AS PROVIDED. APPROPRIATE ACTION IS REQUIRED TO ENSURE ADEQUACY AND TO PROVIDE A CLEAR, SAFE PASSAGE FOR MAINTENANCE VEHICLES TO THE EMBANKMENT AND PRINCIPLE FLOW CONTROL STRUCTURES.
9. INSPECT AND EXERCISE POND DRAIN VALVE ON AN ANNUAL BASIS.
10. RECORD KEEPING. THE OWNER OR DESIGNATED REPRESENTATIVE SHALL KEEP REASONABLE, ACCURATE WRITTEN RECORDS OR INSPECTIONS PERFORMED FOR THE STRUCTURE. RECORDS SHALL DOCUMENT THE REPAIRS PERFORMED. COPIES SHALL BE PROVIDED TO THE COUNTY UPON REQUEST.
11. THE FACILITY SHALL NOT BE MODIFIED IN ANY WAY WITHOUT PRIOR CONSENT/ APPROVAL OF JAMES CITY COUNTY.
12. DEAD OR DYING PLANT MATERIAL SHALL BE REPLACED AFTER THE FIRST GROWING SEASON. THE POND SLOPE SHOULD BE MAINTAINED IN A NATURAL STATE WITH THE EXCEPTION THAT CHOKING VINES AND NON-NATIVE INVASIVE SPECIES SHOULD BE REMOVED BY HAND METHODS ONLY AT THE ONSET OF THE SECOND GROWING SEASON.

**GENERAL NOTES FOR CONSTRUCTION OF STORMWATER BASINS**

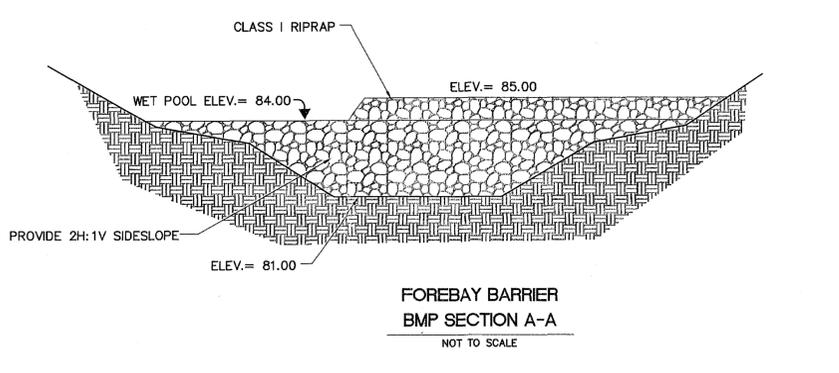
1. THE CONTRACTOR SHALL PROVIDE ALL WORK AND MATERIALS NEEDED TO CONSTRUCT THE STORMWATER BASIN, STORMWATER MANAGEMENT PONDS, BEST MANAGEMENT PRACTICES, SEDIMENT BASINS AND SEDIMENT TRAPS. THE WORK SHALL INCLUDE ALL LABOR, MATERIALS, EQUIPMENT AND MATERIALS NEEDED FOR THE COMPLETION OF GRADING AND EARTHWORK ASSOCIATED WITH THE CONSTRUCTION.
2. THE CONTRACTOR SHALL CONSULT AND PROVIDE FOR THE SERVICES OF A GEOTECHNICAL ENGINEER. THE GEOTECHNICAL ENGINEER SHALL PROVIDE TEST RESULTS ON PLACED DAM MATERIALS, IDENTIFYING SOIL CLASSIFICATION, PERMEABILITY, PLASTICITY INDEX, AND COMPACTION. ALL TESTS SHALL BE IN CONFORMANCE WITH ASTM STANDARDS. THE COST OF THE SERVICES OF THE GEOTECHNICAL ENGINEER SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR. SATISFACTORY GEOTECHNICAL RESULTS ARE NEEDED PRIOR TO FINAL APPROVAL.
3. ALL INSPECTIONS REQUIRED FOR THE WORK SHALL BE PERFORMED BY A GEOTECHNICAL ENGINEER AT THE EXPENSE OF THE GENERAL CONTRACTOR.
4. ON-SITE EXCAVATED MATERIAL, IF DETERMINED SUITABLE FOR USE IN DAM CONSTRUCTION BY A GEOTECHNICAL ENGINEER, MAY BE USED FOR DAM CONSTRUCTION. SHOULD ADDITIONAL MATERIAL BE REQUIRED, THE CONTRACTOR SHALL IDENTIFY THE NEED FOR MATERIAL TO THE OWNER, AS ADDITIONAL BORROW MATERIAL MAY BE AVAILABLE ON THE PROPERTY. ALL EXCAVATED MATERIAL DETERMINED BY THE GEOTECHNICAL ENGINEER TO BE UNSUITABLE SHALL BE DISPOSED OF PROPERLY AT THE CONTRACTOR'S EXPENSE. ALL EXCAVATED MATERIAL NOT REQUIRED FOR BACKFILLING SHALL EITHER BE DEPOSITED ON SITE AND SPREAD BY THE CONTRACTOR, OR SHALL BE DEPOSITED IN AN AREA ON THE PROPERTY AS DIRECTED BY THE OWNER. THE CONTRACTOR SHALL PROVIDE PROPER STABILIZATION, AND EROSION AND SEDIMENT CONTROL MEASURES NEEDED TO CONTROL AS PER THE VESCH THIRD EDITION.
5. UNDERCUT FOR THE FOUNDATION OF THE DAM EMBANKMENT SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATION. THE FOUNDATION SHALL BE BACKFILLED WITH SOILS CLASSIFIED AS SM, SC, OR CL UNDER THE UNIFIED SOIL CLASSIFICATION SYSTEM. SOILS SHALL HAVE A MINIMUM OF 15% BY WEIGHT FINES, HAVING A PLASTICITY INDEX OF 30% AND A PERMEABILITY OF 0.0004 IN./SEC. OR LESS. FILL SHALL BE COMPACTED IN 8-INCH LOOSE THICKNESS LIFTS, OR AS DIRECTED BY THE GEOTECHNICAL ENGINEER, TO A DRY DENSITY OF 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY (ASTM D-698). EXCAVATION FOR THE DAM KEY SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS. HEIGHT, DEPTH, AND WIDTH OF THE KEY SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS. THE KEY SHALL BE FORMED USING SOILS CLASSIFIED AS CL OR CH, WITH A PERMEABILITY OF 0.0004 IN./SEC. OR LESS.
6. THE DAM CORE SHALL BE AS CONSTRUCTED WITH NON-EXPANSIVE CL OR CH CLAYEY MATERIAL WITH PERMEABILITY OF 0.0004 IN./SEC. OR LESS. THE FILL OF THE CORE SHALL BE MADE IN 8-INCH LOOSE THICKNESS LIFTS, OR AS DIRECTED BY THE GEOTECHNICAL ENGINEER, MOISTURE CONDITIONED TO WITHIN -1%/+3% OF THE OPTIMUM MOISTURE CONTENT, AND COMPACTED TO A MINIMUM 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY (ASTM D-698). SIZE, SHAPE, WIDTH, DEPTH, AND HEIGHT OF THE DAM CORE SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS. TO COVER THE DAM CORE, A SILTY FINE SAND OR CLAYEY SOIL (SM, SC, OR CL) SHALL BE PLACED.
7. IN ORDER TO MAINTAIN A WET POOL, THE BOTTOM SURFACE OF THE BMP, ALONG WITH THE SIDE SLOPES TO A HEIGHT AT LEAST 4 FEET ABOVE THE BOTTOM, SHALL CONSIST OF A LAYER OF LOW PERMEABILITY SOIL, SUCH AS CL OR CH, AT LEAST 2 FEET THICK. IF A WET POOL IS UNABLE TO BE ESTABLISHED AND MAINTAINED, THE CONTRACTOR SHALL EXCAVATE THE BOTTOM MATERIAL AND REINSTALL A LOW PERMEABILITY SOIL AT THE DIRECTION OF THE DESIGN ENGINEER AND GEOTECHNICAL ENGINEER.
8. THE STORMWATER MANAGEMENT/BMP FACILITIES SHOWN ON THESE PLANS REQUIRE THE SUBMISSION, REVIEW AND APPROVAL OF RECORD DRAWING(S) AND CONSTRUCTION CERTIFICATION PRIOR TO RELEASE OF THE POSTED BOND/SURETY. THE GEOTECHNICAL ENGINEER IS TO ENSURE THAT HIS/HER INSPECTION OF THE SWM/BMP CONSTRUCTION ACTIVITY IS PERFORMED DURING AND FOLLOWING CONSTRUCTION OF THE SWM/BMP IN ACCORDANCE WITH THE JAMES CITY COUNTY ENVIRONMENTAL DIVISION STORMWATER MANAGEMENT/BMP FACILITIES DESIGN GUIDELINES HANDBOOK, DATED AUGUST 30, 2000.

**DAM CONSTRUCTION NOTES**

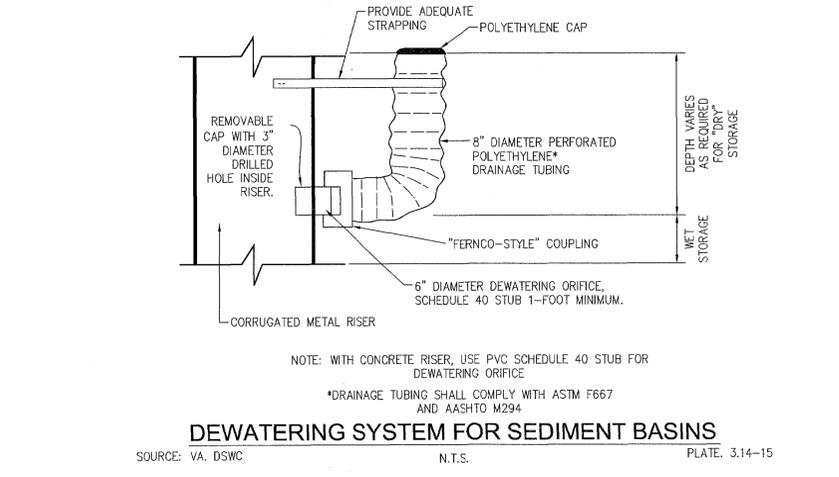
1. THE CONTRACTOR SHALL REFER TO THE "REPORT OF SUBSURFACE AND GEOTECHNICAL ENGINEERING ANALYSIS" PREPARED BY ECS MID-ATLANTIC, LLC, DATED JULY 28, 2006 FOR SPECIFICATIONS ON THE CONSTRUCTION OF THE BMP FACILITY, INCLUDING THE EMBANKMENT.
2. THE GEOTECHNICAL SUBSURFACE EXPLORATION REPORT AT THE PROPOSED DAM SITE HAS BEEN PERFORMED TO ENSURE SUITABILITY OF THE SUBGRADE. THE GEOTECHNICAL INVESTIGATION HAS DETERMINED THE SUITABILITY OF THE FILL MATERIAL. THESE RECOMMENDATIONS ARE HEREBY MADE A PART OF THE DAM'S CONSTRUCTION SPECIFICATIONS. A REPRESENTATIVE OF THE GEOTECHNICAL CONSULTANT SHALL BE ON SITE DURING CONSTRUCTION TO ENSURE PROPER MATERIALS AND DAM CONSTRUCTION METHODS ARE UTILIZED. FOLLOWING DAM CONSTRUCTION, THE GEOTECHNICAL CONSULTANT SHALL PROVIDE WRITTEN DOCUMENTATION, SIGNED BY A PROFESSIONAL ENGINEER, THAT THE DAM WAS BUILT IN ACCORDANCE WITH THEIR RECOMMENDATIONS, PLANS, AND SPECIFICATIONS. THE GEOTECHNICAL CONSULTANT SHALL COORDINATE WITH THE DESIGN ENGINEER IN ORDER TO COMPLETE THE JCC ENVIRONMENTAL DIVISION STORMWATER MANAGEMENT/BMP FACILITIES CONSTRUCTION AND AS-BUILT CERTIFICATION FORM. THE CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATING THE DAM CONSTRUCTION SCHEDULE WITH THE GEOTECHNICAL CONSULTANT IN ORDER TO ENSURE ON-SITE MONITORING.
3. SITE PREPARATION: THE CONTRACTOR SHALL STRIP ALL AREAS OF THE PERMANENT COVER IN CONSTRUCTION AREA TO REMOVE ALL UNSUITABLE MATERIALS. THE UNSUITABLE MATERIALS TO BE REMOVED BY STRIPPING SHALL INCLUDE ALL TOPSOIL, DEBRIS AND VEGETATIVE MATTER, INCLUDING STUMPS AND ROOTS, AND ALL OTHER MATERIALS WHICH MAY BE UNSUITABLE FOR USE IN THE PERMANENT CONSTRUCTION.
4. EMBANKMENT: THE EXPOSED SUB GRADE SOILS SHALL BE CAREFULLY INSPECTED BY THE GEOTECHNICAL ENGINEER. ANY UNSUITABLE MATERIALS THUS EXPOSED SHALL BE REMOVED AND REPLACED WITH A WELL COMPACTED, SUITABLE MATERIAL. DENSITY TESTING, AT THE DISCRETION OF THE OWNER/GEOTECHNICAL ENGINEER, SHALL BE PERFORMED AT THIS TIME. THE EMBANKMENT SHALL BE KEPT INTO THE UNDISTURBED (EXISTING) SOIL STRATUM. EMBANKMENT SHOULD BE KEPT AT LEAST 4 FEET INTO THE STRATUM OR AS SPECIFIED BY THE GEOTECHNICAL ENGINEER (WHICHEVER IS GREATER). THE EMBANKMENT FOUNDATION AND ADJUTMENTS SHALL BEAR ON FIRM AND STABLE EXISTING SUB-GRADE WHICH HAS BEEN PREPARED SO AS TO REMOVE ALL ORGANIC, LOOSE, AND GENERALLY UNSUITABLE MATERIAL. ALL MATERIALS TO BE USED FOR BACKFILL OR COMPACTED FILL SHALL BE INSPECTED AND, IF NECESSARY, TESTED BY THE GEOTECHNICAL ENGINEER IN ACCORDANCE WITH ASTM D2487 PRIOR TO PLACEMENT, TO DETERMINE IF THEY ARE SUITABLE FOR THE INTENDED USE. THE FILL MATERIAL SHALL BE TAKEN FROM APPROVED BORROW AREAS. IT SHALL BE CLEAN MINERAL SOIL, FREE OF ROOTS, WOOD VEGETATION, OVERSIZED STONES, ROCKS, OR OTHER OBJECTIONABLE MATERIALS. MATERIALS TO BE USED IN THE CONSTRUCTION OF THE SHELL SHALL BE SELECT BACKFILL FREE OF STUMPS, ROOTS, ROCKS, TRASH, ETC. AND SHALL BE MORE PERVIOUS THAN THE IMPERVIOUS CLAY CORE. AREAS ON WHICH FILL IS TO BE PLACED SHALL BE SCARIFIED A MINIMUM OF 4 INCHES PRIOR TO PLACEMENT OF FILL. THE FILL MATERIAL'S MOISTURE CONTENT SHALL BE 4-1/2% OF OPTIMUM MOISTURE CONTENT AS DETERMINED BY ASTM D2216. FILL MATERIAL SHALL BE PLACED IN HORIZONTAL LIFTS NOT EXCEEDING 8 INCHES IN LOOSE THICKNESS AND IN CONTINUOUS LAYERS OVER THE ENTIRE LENGTH OF THE FILL. FILL MATERIAL SHALL BE COMPACTED TO A MINIMUM 95% OF THE MAXIMUM DRY DENSITY OBTAINED IN ACCORDANCE WITH ASTM SPECIFICATION D-1586, STANDARD PROCTOR METHOD. FINISHED GRADES SHALL BE MERGED NATURALLY INTO THE EXISTING GRADES AND NOT EXCEED A SLOPE GREATER THAN 3:1.
5. CUTOFF TRENCH/KEY TRENCH: THE TRENCH SHALL BE EXCAVATED ALONG THE CENTERLINE OF THE DAM. THE MINIMUM DEPTH SHALL BE AS SHOWN ON THE PLANS AND SHALL EXTEND UP BOTH ABUTMENTS. THE BOTTOM WIDTH SHALL BE WIDE ENOUGH TO PERMIT OPERATION OF COMPACTING EQUIPMENT. THE SIDE SLOPES SHALL BE NO STEEPER THAN 1:1.
6. PRINCIPAL SPILLWAY: THE BOTTOM OF THE SPILLWAY RISER FOUNDATION BASE EXCAVATION SHALL BE OBSERVED BY THE GEOTECHNICAL ENGINEER TO ENSURE THAT ALL UNSUITABLE AND LOOSE MATERIALS ARE REMOVED AND THAT ACCEPTABLE BEARING CONDITIONS EXIST IN THE FOUNDATION'S BASE. ALL JOINTS IN THE PRINCIPAL SPILLWAY STRUCTURE SHALL BE WATERTIGHT CONSTRUCTION. PERVIOUS MATERIALS SUCH AS SAND, GRAVEL OR CRUSHED STONE SHALL NOT BE USED AS BACKFILL AROUND THE BARREL OR ANTI-SEEP COLLARS. FILL MATERIAL SHALL BE PLACED AROUND THE PIPE IN 4 INCH LAYERS AND COMPACTED BY HAND TO THE SAME DENSITY AS THE EMBANKMENT TO A MINIMUM OF TWO FEET OF FILL SHALL BE HAND-COMPACTED OVER THE BARREL BEFORE CROSSING IT WITH CONSTRUCTION EQUIPMENT.
7. VEGETATIVE STABILIZATION: FINAL VEGETATIVE COVER (STABILIZATION) SHALL CONSIST OF TOP SOILING, LIMING, FERTILIZING, SEEDING, AND MULCHING TO ASSURE A FIRM STAND OF GRASS AS SOON AS PRACTICAL. SEDIMENT BASINS AND OTHER TEMPORARY EROSION CONTROL MEASURES ARE TO BE REMOVED ONLY WHEN STABILIZATION IS COMPLETE. FINAL VEGETATIVE COVER SHALL BE PROVIDED IN ACCORDANCE WITH THE FOLLOWING:  
TOPSOIL: AT LEAST 4" THICKNESS OBTAINED FROM STOCKPILES ON SITE, FREE OF LARGE DEBRIS.  
LIME: 4,000#/ACRE (90#/1,000 S.F.)  
SEED: KENTUCKY 31 TALL FESCUE 250#/ACRE (6#/1,000 S.F.)  
FERTILIZER: 10/10/10 MIX, 1,000#/ACRE FALL (25#/1,000 S.F.)  
MULCH: STRAW OR HAY (LOCALLY OBTAINED) 4,000#/ACRE (90#/1,000 S.F.)

**CONSTRUCTION SEQUENCE**

1. PRIOR TO OBTAINING LAND DISTURBING PERMIT, THE CONTRACTOR SHALL OBTAIN A VSPM PERMIT (VIRGINIA STORMWATER MANAGEMENT PROGRAM) FROM DCR (VIRGINIA DEPARTMENT OF CONSERVATION AND RECREATION).
2. THE CONTRACTOR SHALL SCHEDULE A PRE-CONSTRUCTION MEETING WITH THE JAMES CITY COUNTY ENVIRONMENTAL DIVISION PRIOR TO BEGINNING ANY WORK AT THE SITE.
3. CONTACT "MISS UTILITY" FOR PUBLIC SERVICES AND HAVE A PRIVATE UTILITY LOCATOR FOR PRIVATE SERVICES.
4. INSTALL CONSTRUCTION ENTRANCE, SAFETY FENCE, SILT FENCE, AND TREE PROTECTION.
5. INSTALL SEDIMENT BASIN (SEE DAM CONSTRUCTION NOTES) AND DIVERSION DIKE WITH RIPRAP-LINED CHANNEL.
6. INSTALL GRASS LINED CHANNEL TO RIPRAP-LINED CHANNEL IN SEDIMENT BASIN.
7. CLEAR AND GRUB REMAINDER OF SITE, AND DEMOLISH AND REMOVE ALL DEMOLITION ITEMS.
8. INSTALL UTILITIES AND STORM SEWER.
9. GRADE PARKING LOT AND INSTALL FILL DIVERSION PER VESCH SPEC. 3.10 AND RIGHT-OF-WAY DIVERSION PER VESCH SPEC. 3.11. ADJUST DIVERSIONS DURING FILL OPERATION.
10. PREPARE BUILDING PAD AND ADJUST DIVERSIONS AS NECESSARY.
11. CONSTRUCT BUILDING.
12. CONSTRUCT PROPOSED SIDEWALKS, CURB, AND CURB & GUTTER.
13. CONSTRUCT PARKING LOT AND STRIPING.
14. PREPARE FINAL GRADING AND PLANT LANDSCAPING.
15. PLANT PERMANENT SEEDING AND MULCH.
16. PROVIDE FINAL CLEANOUT OF SEDIMENT BASIN AND CONVERT TO BMP AFTER FINAL SITE STABILIZATION.
17. REMOVE ALL EROSION AND SEDIMENT CONTROL MEASURES WITHIN THIRTY DAYS OF FINAL SITE STABILIZATION, BUT ONLY AFTER APPROVAL IS OBTAINED FROM THE ASSIGNED JAMES CITY COUNTY ENVIRONMENTAL INSPECTOR.



**FOREBAY BARRIER BMP SECTION A-A**  
NOT TO SCALE



**DEWATERING SYSTEM FOR SEDIMENT BASINS**  
SOURCE: VA. DSWC N.T.S. PLATE: 3.14-15

NO.	DATE	REVISION / COMMENT / NOTE	BY
3	2/22/07	REVISED PER JCSA COMMENTS	LBA
2	12/19/06	REVISED PER COUNTY COMMENTS	BEIS
1	12/25/06	REVISED PER COUNTY COMMENTS	BEIS



5248 Old Towne Road, Suite 1  
Williamsburg, Virginia 23188  
(757) 253-0040  
Fax (757) 220-8994



CONSULTING ENGINEERS  
WILLIAMSBURG • RICHMOND • GLOUCESTER

DESIGNED		DRAWN	
SCALE	DATE	PROJECT NO.	DRAWING NO.
N.T.S.	4/14/06	9552	7

STORMWATER MANAGEMENT/BMP PLAN  
MULTI-MINISTRY BUILDING  
JAMES RIVER BAPTIST CHURCH  
POWhatan DISTRICT  
JAMES CITY COUNTY  
VIRGINIA

---

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***DRAINAGE CALCULATIONS***  
***FOR***  
***JAMES RIVER BAPTIST CHURCH***

*Prepared By:*

AES Consulting Engineers  
5248 Olde Towne Road, Suite 1  
Williamsburg, Virginia 23188

April 13, 2006  
Revised August 23, 2006

AES Project No. 9552



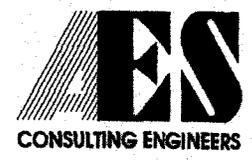


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- I INTRODUCTION
- II EXISTING SITE CONDITIONS
- III PROPOSED SITE CONDITIONS
- IV SUMMARY

**APPENDICES**

- SEDIMENT BASIN
- STORM SEWER
- STORMWATER MANAGEMENT
- DRAINAGE AREA MAPS



## I INTRODUCTION

The proposed project represents the expansion of the James River Baptist Church. The site is located on the southwest corner of the intersection of Centerville Road and Jolly Pond Road. The site is bounded to the west and southwest by Tax Map Parcel (30-4)(1-7) which is currently wooded, and to the south by Tax Map Parcel (30-4)(1-6) which is the site of an existing office building. The project consists of the construction of a 9,683 SF building and the expansion of the parking lot.

## II EXISTING SITE CONDITIONS

The James River Baptist Church site consists of an existing 10,108 SF building, associated parking, and two cemeteries generally located on the east side of the 5.01 acre property. Approximately 3.5 acres of the property is currently undeveloped and is a combination of woods and open area. Slopes on the property range from 1 - 17%. The property drains offsite in all directions because of a high point in the middle of the property.

## III PROPOSED SITE CONDITIONS

Stormwater runoff from 2.84 acres of the site will be collected in two separate storm drainage systems - (1) a system of inlets and storm pipe and (2) a grass channel - and conveyed to a proposed extended detention-wet pond located in the southwest corner of the property. The wet storage volume of the BMP is designed to meet the volume created from 1 inch of rainfall over both the existing and proposed impervious coverage (1.26 acres) of the 2.84 acre drainage area. The dry storage volume of the BMP is designed to attenuate the 2 and 10 year storms, in addition to the channel protection requirements as outlined in the *James City County Guidelines for Design and Construction of Stormwater Management BMP's*.

The Modified Rational Method was used since the drainage area to the BMP is only  $\pm 3$  acres. The Critical Storm Duration was calculated using the method outlined in Chapter 5 of the Virginia Stormwater Management Handbook. The 1 year - 24 hour SCS storm was routed through the BMP to ensure the entire volume passes through the 3" orifice only.

The BMP will initially be used as a temporary sediment basin during construction. The sediment basin will be built to the dimensions of the permanent BMP including outfall structure, bench, emergency spillway, outlet protection, etc. The outfall structure will be equipped with a dewatering device, and later converted to the permanent low flow orifice. The 2-year and 25-year storms were routed through the temporary sediment trap using the Modified Rational Method.

The following is a detailed breakdown of the methodology for the stormwater management calculations:

Pre-Development

A 3.03 acre area of the site drains offsite across the southern boundary line of the property and is divided into two subareas:

- Area “Pre-1” = 0.74 acres (Area that drains southward to an existing channel near the southeast corner of the property)
- Area “Pre-2” = 2.29 acres (Area that primarily drains southward without a well defined channel)

Post-Development

Post-development runoff from most of this 3.03 acre area, as well as a small area that currently drains to the northern part of the site, is directed to the proposed BMP.

- Pond = 2.84 acres (Area draining to the BMP)
- Area “Post A” = 0.08 acres (Portion of Area “Pre-1” that does not flow to BMP)
- Area “Post B” = 0.30 acres (Portion of Area “Pre-2” that does not flow to BMP)
- 0.19 acres (Portion of 2.84 acre area that drained to the north before development)

The Critical Storm Duration

- The 3.03 acre area was used to determine the pre-development peak flow across the southern property line
- The 2.84 acre area was used to create inflow hydrographs to the BMP.
- Runoff from areas “Post A” and “Post B” are added to the discharge of the BMP to determine the total post-development flows across the southern property line to determine the overall effect of this development plan. These values are then compared to the pre-development runoff from the 3.03 acre area.

	Discharge from BMP	Area “Post A” Post-Dev Runoff	Area “Post B” Post-Dev Runoff	Total Post-Dev Flow across Southern Property Line	Pre-Dev Runoff from 3.03 Acre Area
2-year Storm	0.25 CFS	0.14 CFS	0.52 CFS	0.91 CFS	5.37 CFS
10-year Storm	0.29 CFS	0.18 CFS	0.67 CFS	1.14 CFS	6.98 CFS

A Storm Duration Factor of 1.97 was calculated for the Modified Rational Method Inflow Hydrographs of the BMP. This factor was calculated using a time of concentration of 10 minutes and used to develop the post-development inflow hydrographs.

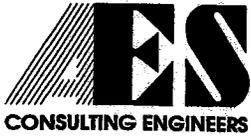
The proposed BMP will discharge at the property line where Design Point #1 is located for Area Pre-1. This is the only natural channel that exists at the property line along the southern boundary of the site. The sum of the attenuated flow from the BMP and the runoff from Area "Post A" are less than the pre-development flows from Area Pre-1. The results, using the 2-year 24-hour storm are as follows:

	Discharge from BMP	Area "Post A" Post-Dev Runoff 0.08 Acre Area	Total Post-Dev Flow at Design Point #1	Area "Pre-1" Pre-Dev Runoff 0.74 Acre Area
2-year Storm	0.54 CFS	0.12 CFS	0.66 CFS	0.94 CFS

### III SUMMARY

1. The temporary sediment basin, constructed to the same dimensions as the final BMP and using the BMP outlet structure will function properly for the 2-year and 25-year storms.
2. The BMP passes the 1-year 24-hour storm through the 3" orifice without using the principle spillway.
3. The Modified Rational 2-year, 10-year, and 100-year storms flow through the BMP without using the emergency spillway.
4. The post-development peak flow across the southern property line from the 3.03 acre area is less than the pre-development flow.
5. The post-development 2-year 24-hour discharge at Design Point #1 (the sum of the discharge from the BMP and the discharge from a small area that does not flow through the BMP) is less than the pre-development flow.

# SEDIMENT BASIN



Williamsburg (757) 253-0040  
 Gloucester (804) 693-4450  
 Richmond (804) 330-8040

Project: James River Baptist Church  
 Project No.: 9552  
 Subject: Sediment Basin Design  
 Date: August 23, 2006  
 Calculated By: N. Botta

1992

3.14

**TEMPORARY SEDIMENT BASIN DESIGN DATA SHEET**  
 (with or without an emergency spillway)

Total area draining to basin 2.84 acres.

Basin Volume Design

**Wet Storage:**

1. Minimum required volume = 67 cu. yds. x Total Drainage Area (acres).

$$67 \text{ cu. yds.} \times \underline{2.84} \text{ acres} = \underline{190.28} \text{ cu. yds.}$$

2. Available basin volume = 226 cu. yds. at elevation 84. (From storage - elevation curve)

3. Excavate 226 cu. yds. to obtain required volume\*.

\* Elevation corresponding to required volume = invert of the dewatering orifice.

4. Available volume before cleanout required.

$$33 \text{ cu. yds.} \times \underline{2.84} \text{ acres} = \underline{93.72} \text{ cu. yds.}$$

5. Elevation corresponding to cleanout level = 82.75.

(From Storage - Elevation Curve)

6. Distance from invert of the dewatering orifice to cleanout level = 1.25 ft. (Min. = 1.0 ft.)

**Dry Storage:**

7. Minimum required volume = 67 cu. yds. x Total Drainage Area (acres).

$$67 \text{ cu. yds.} \times \underline{2.84} \text{ acres} = \underline{190.28} \text{ cu. yds.}$$

8. Total available basin volume at crest of riser\* = 588 cu. yds. at elevation 85.9. (From Storage - Elevation Curve)
- \*Minimum = 134 cu. yds./acre of total drainage area.
9. Diameter of dewatering orifice = 3 in.
10. Diameter of flexible tubing = 6 in. (diameter of dewatering orifice plus 2 inches).

### Preliminary Design Elevations

11. Crest of Riser = 85.9  
 Top of Dam = 87.9  
 Design High Water = 86.9  
 Upstream Toe of Dam = 81

### Basin Shape

12.  $\frac{\text{Length of Flow}}{\text{Effective Width}} = \frac{L}{We} = \underline{1}$
- If  $> 2$ , baffles are not required \_\_\_\_\_
- If  $< 2$ , baffles are required ✓

### Runoff

13.  $Q_2 = \underline{5.73}$  cfs (From Chapter 5)
14.  $Q_{25} = \underline{8.68}$  cfs (From Chapter 5)

### Principal Spillway Design

15. With emergency spillway, required spillway capacity  $Q_p = Q_2 = \underline{5.73}$  cfs. (riser and barrel)
- Without emergency spillway, required spillway capacity  $Q_p = Q_{25} \underline{8.68}$  cfs. (riser and barrel)

16. With emergency spillway:

Assumed available head (h) = 1 ft. (Using  $Q_2$ )

$h = \text{Crest of Emergency Spillway Elevation} - \text{Crest of Riser Elevation}$

Without emergency spillway:

Assumed available head (h) = n/a ft. (Using  $Q_{25}$ )

$h = \text{Design High Water Elevation} - \text{Crest of Riser Elevation}$

17. Riser diameter ( $D_r$ ) = 36 in. Actual head (h) = 1 ft.

(From Plate 3.14-8.)

Note: Avoid orifice flow conditions.

18. Barrel length (l) = 30 ft.

Head (H) on barrel through embankment = 6.23 ft.

(From Plate 3.14-7.)

19. Barrel diameter = 15 in.

(From Table 3.14-B [concrete pipe] or Table 3.14-A [corrugated pipe]).

20. Trash rack and anti-vortex device

Diameter = 36 inches.

Height = n/a inches.

(From Table 3.14-D.)

### Emergency Spillway Design

21. Required spillway capacity  $Q_e = Q_{25} - Q_p =$  2.95 cfs.

22. Bottom width (b) = 8 ft.; the slope of the exit channel (s) = 0.1 ft./foot; and the minimum length of the exit channel (x) = 75 ft.

(From Table 3.14-C)

Anti-Seep Collar Design

23. Depth of water at principal spillway crest (Y) = 4.9 ft.  
 Slope of upstream face of embankment (Z) = 3 :1.  
 Slope of principal spillway barrel ( $S_b$ ) = 0.5 %  
 Length of barrel in saturated zone ( $L_s$ ) = 30 ft.
24. Number of collars required = 2 dimensions = 3.5' x 3.5'

(From Plate 3.14-12).

Final Design Elevations

25. Top of Dam = 87.9  
 Design High Water = 85.86  
 Emergency Spillway Crest = 86.9  
 Principal Spillway Crest = 85.9  
 Dewatering Orifice Invert = 84.0  
 Cleanout Elevation = 82.75  
 Elevation of Upstream Toe of Dam  
 or Excavated Bottom of "Wet Storage  
 Area" (if excavation was performed) = 81

# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 8:0 PM

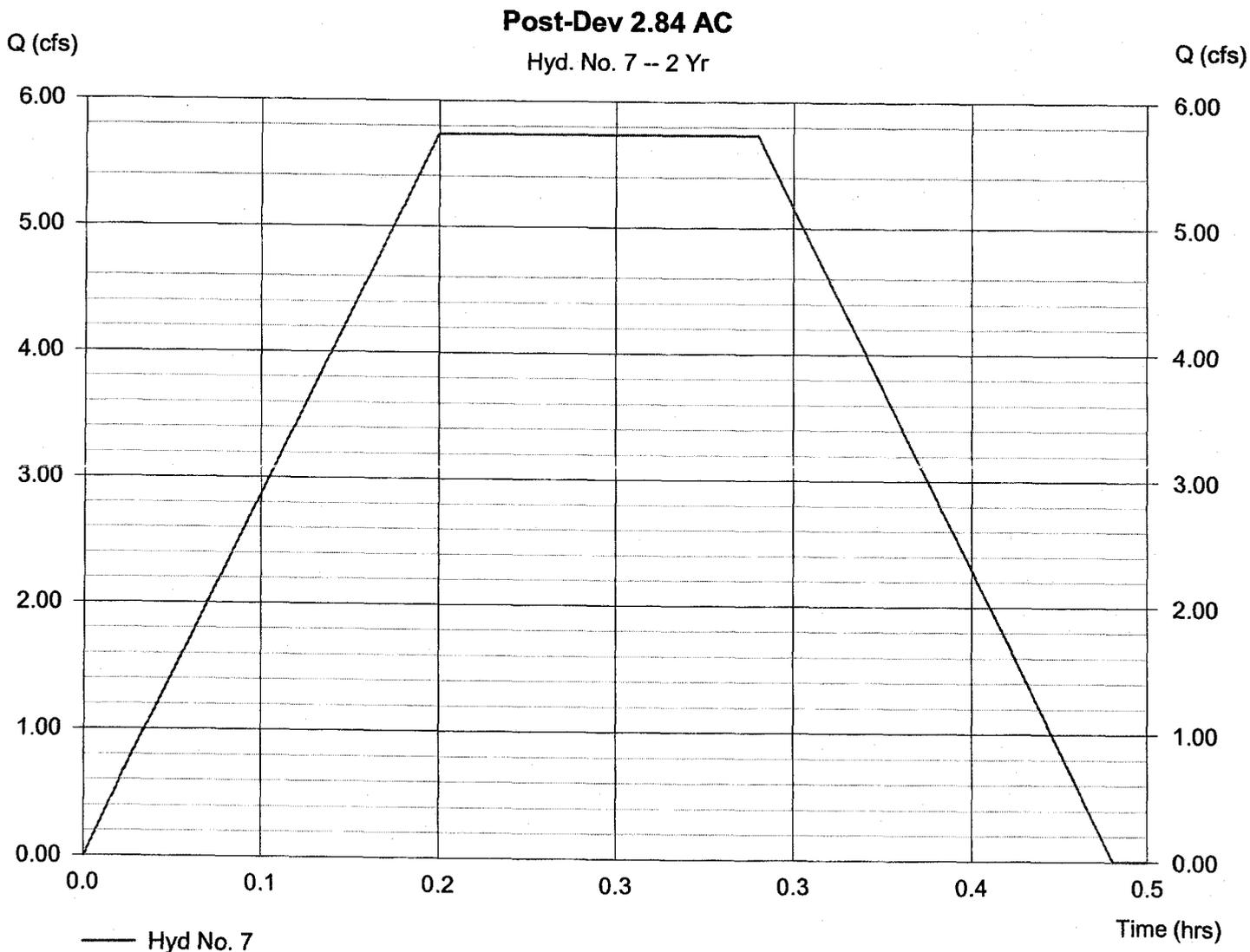
## Hyd. No. 7

Post-Dev 2.84 AC

Hydrograph type = Mod. Rational  
Storm frequency = 2 yrs  
Drainage area = 2.8 ac  
Intensity = 3.422 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 5.73 cfs  
Time interval = 1 min  
Runoff coeff. = 0.59  
Tc by User = 10 min  
Storm duration = 1.97 x Tc

Hydrograph Volume = 6,777 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 8:0 PM

## Hyd. No. 8

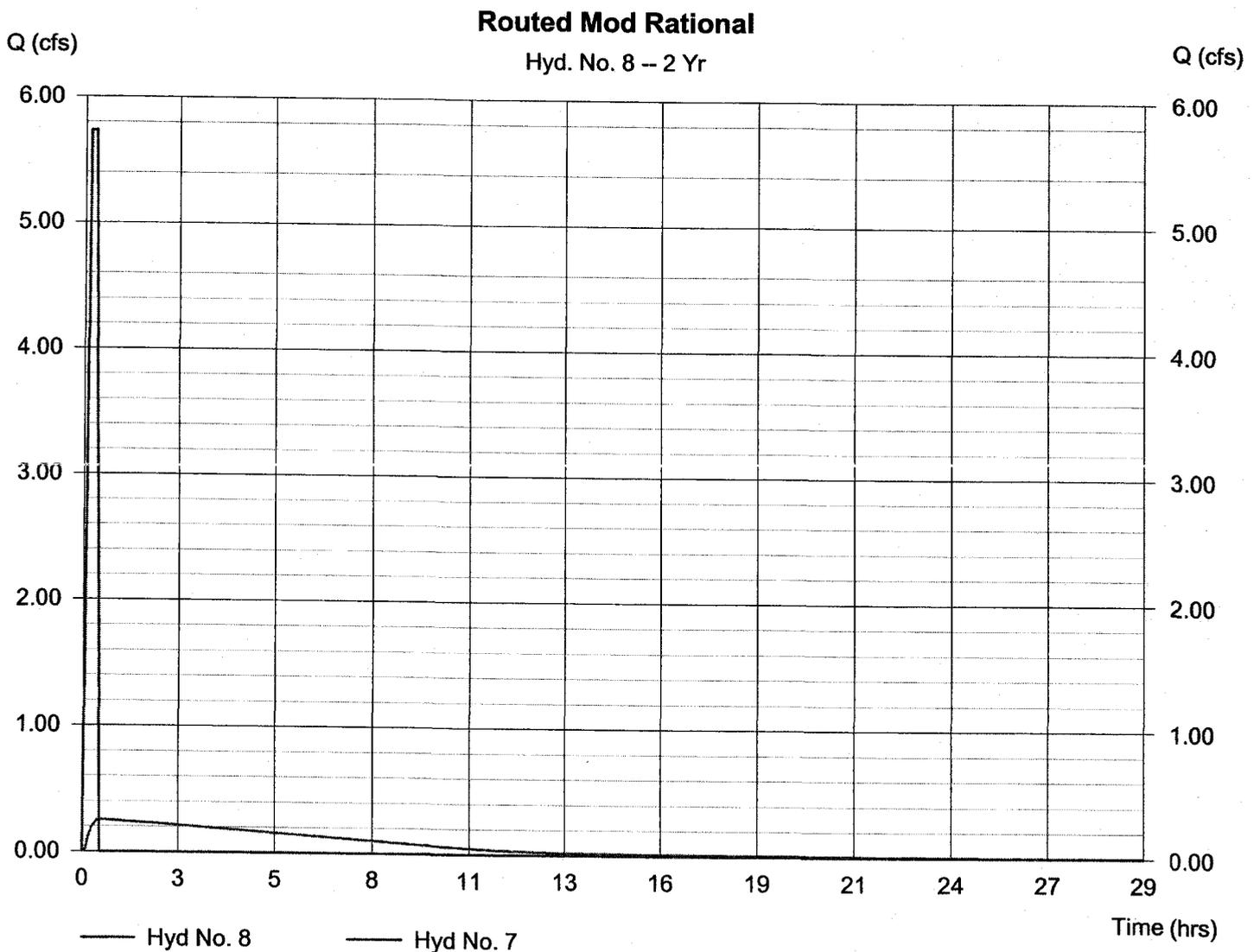
Routed Mod Rational

Hydrograph type = Reservoir  
Storm frequency = 2 yrs  
Inflow hyd. No. = 7  
Reservoir name = JRBC Pond

Peak discharge = 0.25 cfs  
Time interval = 1 min  
Max. Elevation = 85.27 ft  
Max. Storage = 12,384 cuft

Storage Indication method used. Wet pond routing start elevation = 84.00 ft.

Hydrograph Volume = 6,512 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 8:0 PM

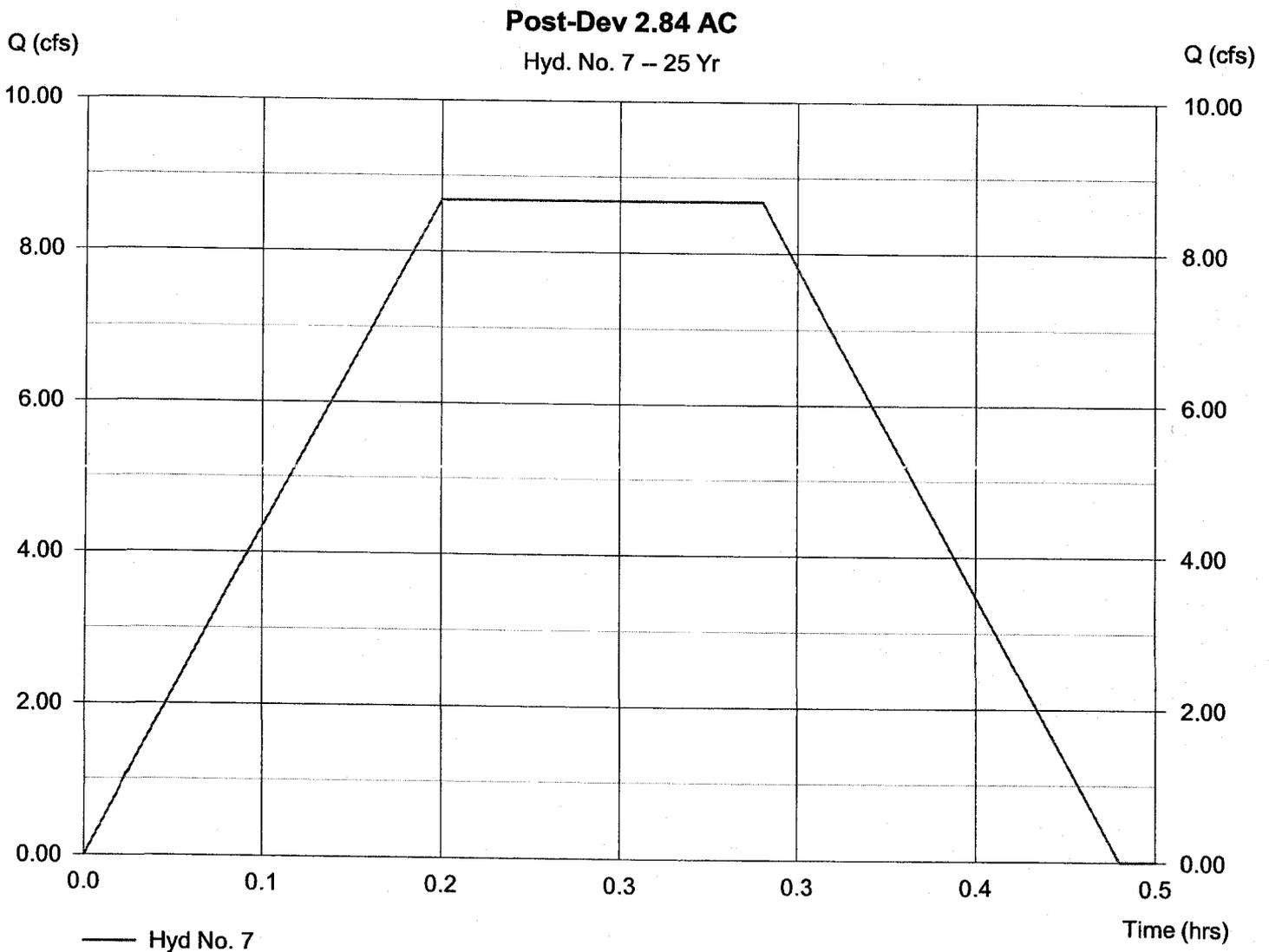
## Hyd. No. 7

Post-Dev 2.84 AC

Hydrograph type = Mod. Rational  
Storm frequency = 25 yrs  
Drainage area = 2.8 ac  
Intensity = 5.181 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 8.68 cfs  
Time interval = 1 min  
Runoff coeff. = 0.59  
Tc by User = 10 min  
Storm duration = 1.97 x Tc

Hydrograph Volume = 10,262 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 8:0 PM

## Hyd. No. 8

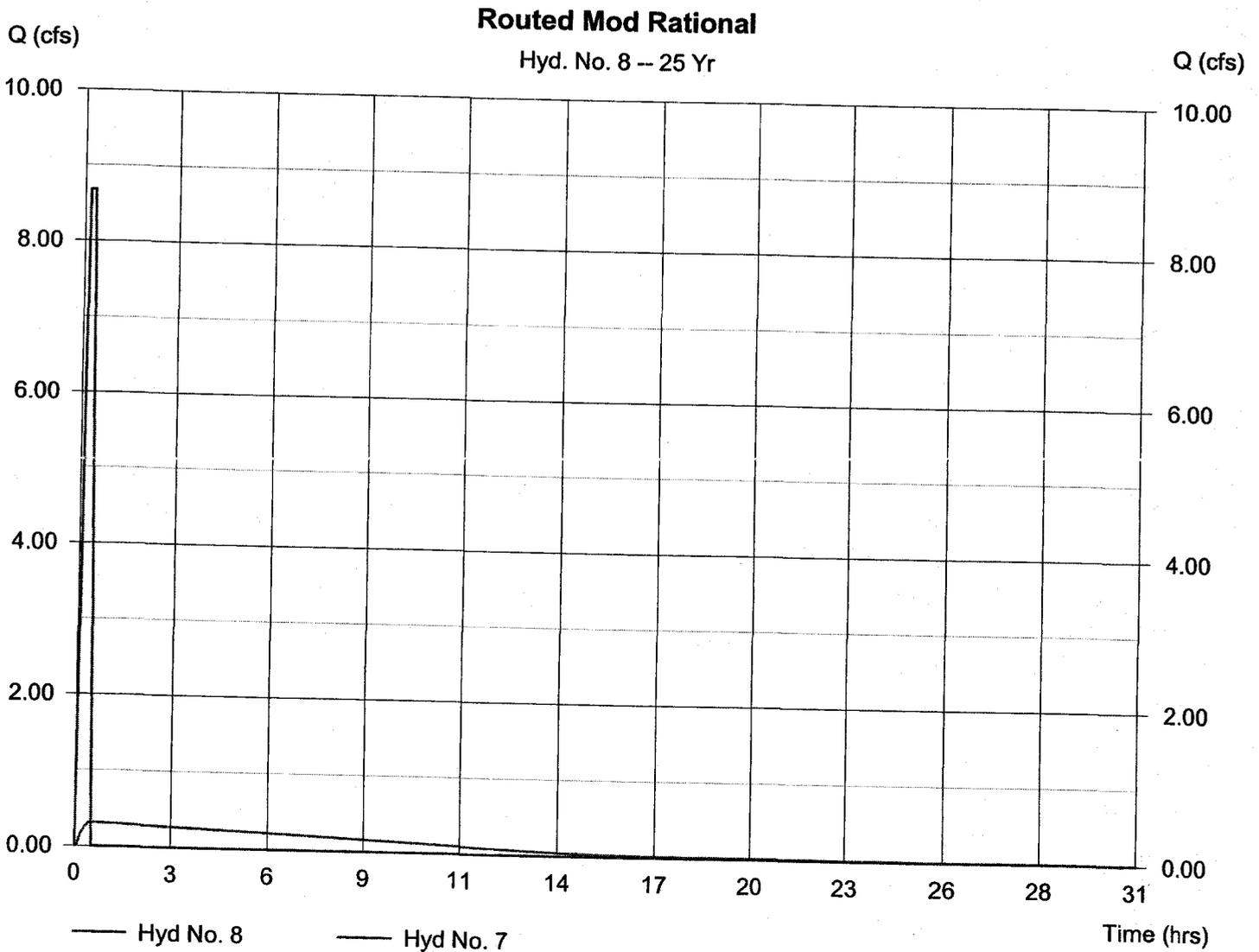
Routed Mod Rational

Hydrograph type = Reservoir  
Storm frequency = 25 yrs  
Inflow hyd. No. = 7  
Reservoir name = JRBC Pond

Peak discharge = 0.31 cfs  
Time interval = 1 min  
Max. Elevation = 85.86 ft  
Max. Storage = 15,675 cuft

Storage Indication method used. Wet pond routing start elevation = 84.00 ft.

Hydrograph Volume = 9,873 cuft



# Pond Report

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:44 PM

## Pond No. 1 - JRBC Pond

### Pond Data

Pond storage is based on known contour areas. Average end area method used.

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	81.00	1,044	0	0
1.00	82.00	1,464	1,254	1,254
2.00	83.00	1,940	1,702	2,956
3.00	84.00	4,362	3,151	6,107
4.00	85.00	5,181	4,772	10,879
4.90	85.90	5,910	4,991	15,869
5.00	86.00	6,023	597	16,466
5.90	86.90	6,910	5,820	22,286
6.00	87.00	6,996	695	22,981

### Culvert / Orifice Structures

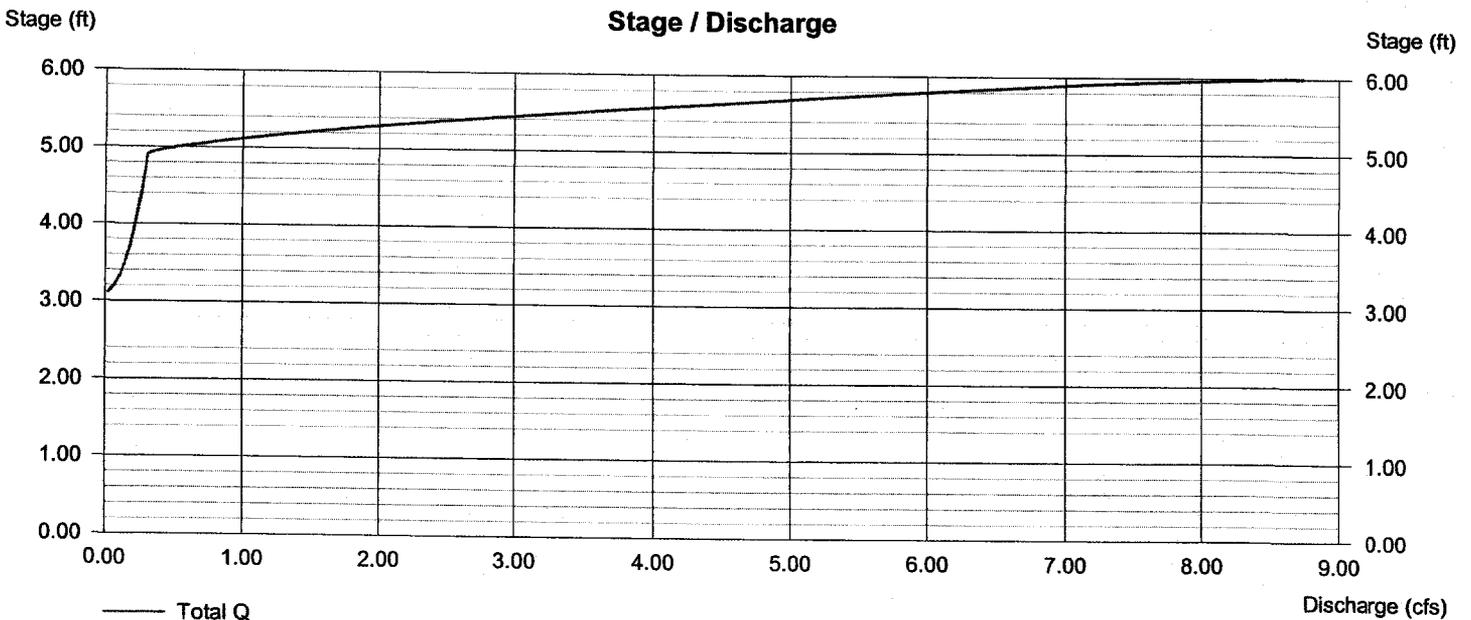
	[A]	[B]	[C]	[D]
Rise (in)	= 15.00	3.00	0.00	0.00
Span (in)	= 15.00	3.00	0.00	0.00
No. Barrels	= 1	1	0	0
Invert El. (ft)	= 80.20	84.00	0.00	0.00
Length (ft)	= 30.00	0.00	0.00	0.00
Slope (%)	= 0.50	0.00	0.00	0.00
N-Value	= .013	.013	.000	.000
Orif. Coeff.	= 0.60	0.60	0.00	0.00
Multi-Stage	= n/a	Yes	No	No

### Weir Structures

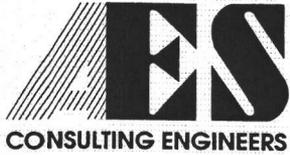
	[A]	[B]	[C]	[D]
Crest Len (ft)	= 2.00	8.00	0.00	0.00
Crest El. (ft)	= 85.90	86.90	0.00	0.00
Weir Coeff.	= 3.33	2.60	3.33	0.00
Weir Type	= Riser	Broad	---	---
Multi-Stage	= Yes	Yes	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.



**STORM SEWER**



Williamsburg (757) 253-0040  
 Gloucester (804) 693-4450  
 Richmond (804) 330-8040

Project: **James River Baptist Church**  
 Project No.: **9552**  
 Subject: **Runoff Coefficients & Curve Numbers**  
 Date: **August 23, 2006**  
 Calculated By: **N. Botta**

**Subject Area:** Drainage System #1 - Inlets and Pipes to Pond

Area Description	Area	C	Impervious 0.90	Open 0.30				Area
Inlet #1-3	0.27	0.72	0.19	0.08				0.27
Inlet #1-4	0.77	0.67	0.47	0.30				0.77
Inlet #1-5	0.24	0.83	0.21	0.03				0.24
Inlet #1-6	0.05	0.66	0.03	0.02				0.05
Inlet #1-7	0.11	0.68	0.07	0.04				0.11
<b>TOTAL</b>	<b>1.44</b>	<b>0.70</b>	<b>0.97</b>	<b>0.47</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>1.44</b>
					<b>1.44</b>			

**Subject Area:** Grass-lined Channel to Pond

Area Description	Area	C	Impervious 0.90	Open 0.30				Area
Pt. #A	0.64	0.56	0.28	0.36				0.64
Pt. #B	0.80	0.51	0.28	0.52				0.80

**Subject Area:** Pre-Development Drainage Areas

Area Description	Area	C	Impervious 0.90	Open 0.30				Area
Pre 1	0.74	0.30	0.00	0.74				0.74
Pre 2	2.29	0.41	0.42	1.87				2.29
<b>TOTAL</b>	<b>3.03</b>	<b>0.38</b>	<b>0.42</b>	<b>2.61</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>3.03</b>
					<b>3.03</b>			

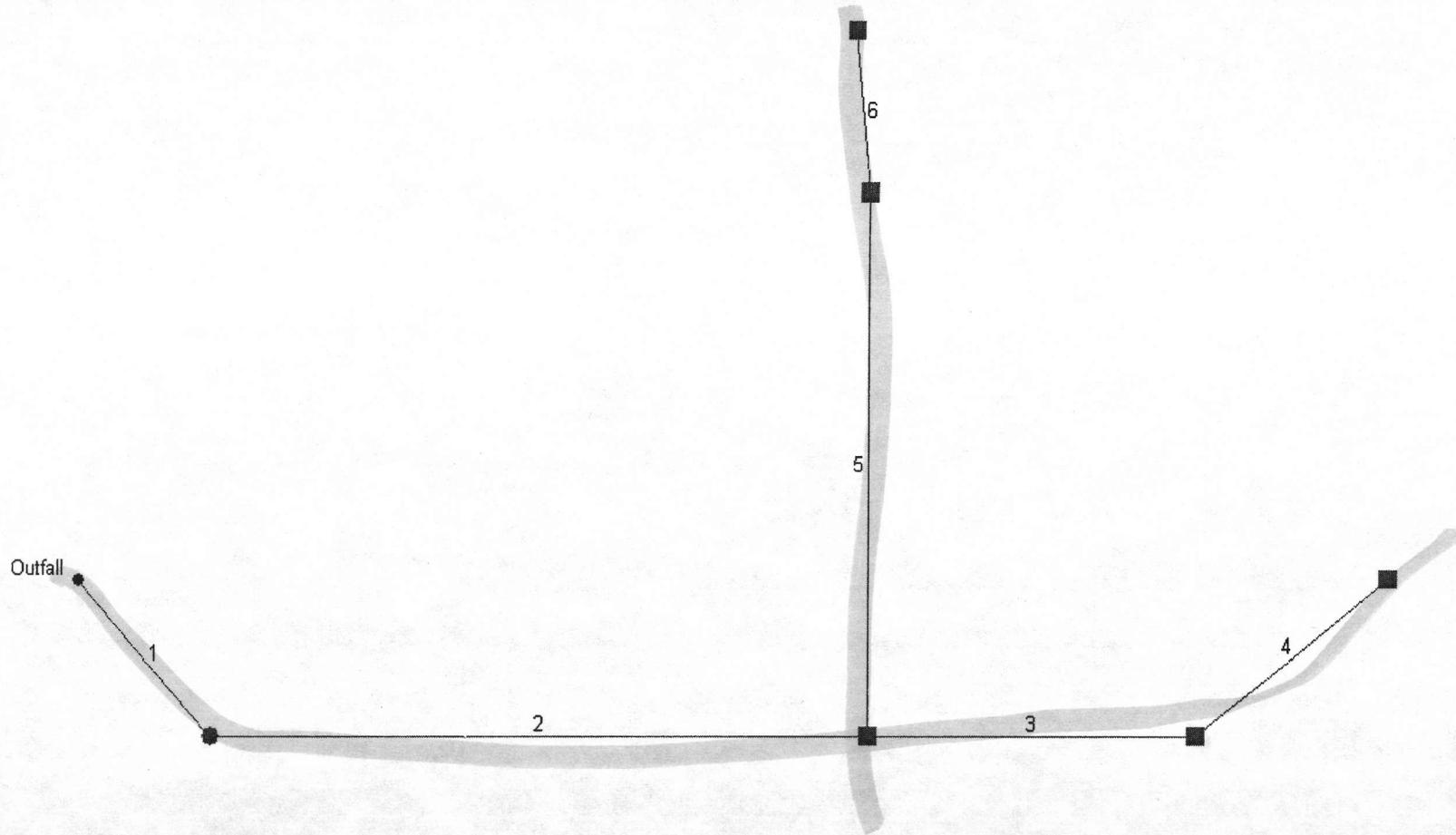
**Subject Area:** Post-Development Drainage Areas

Area Description	Area	C	Impervious 0.90	Open 0.30				Area
To Pond	2.84	0.59	1.36	1.48				2.84
Post A	0.08	0.30		0.08				0.08
Post B	0.30	0.30		0.30				0.30

**Subject Area:** Post-Development Drainage Area To Pond for SCS Storms

Area Description	Area	CN	Impervious 98	Open 70				Area
To Pond	2.84	83	1.36	1.48				2.84
Pre 1	0.74	70		0.74				0.74
Post A	0.08	70		0.08				0.08

# Hydraflow Plan View



Project File: 9552 JRBC Storm.stm

No. Lines: 6

08-17-2006

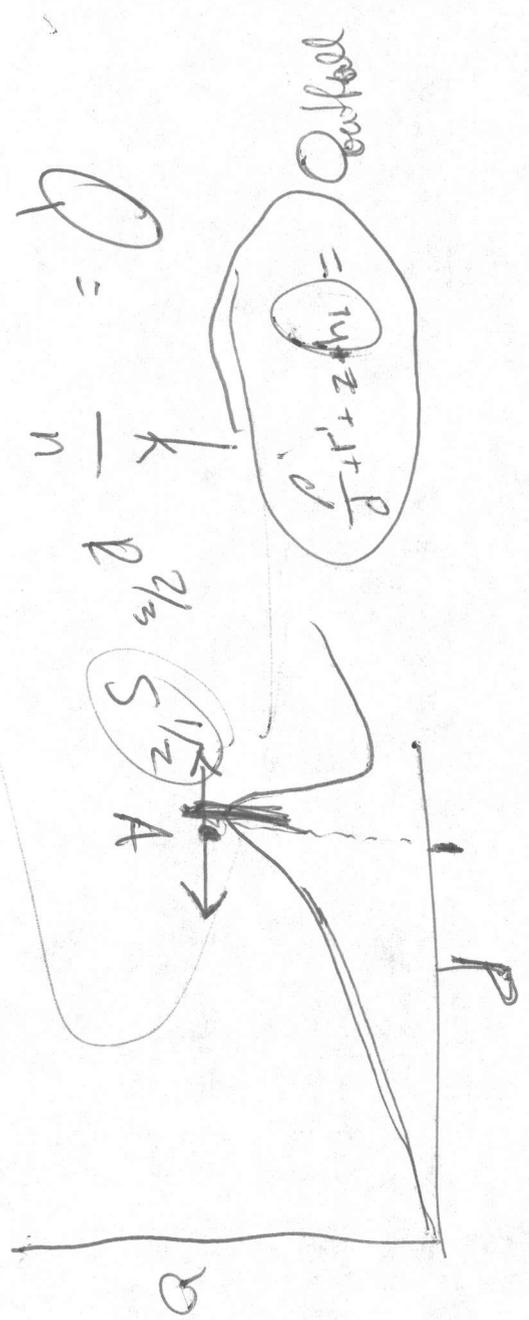
# Storm Sewer Inventory Report

Line No.	Alignment				Flow Data				Physical Data								Line ID
	Dnstr line No.	Line length (ft)	Defl angle (deg)	Junc type	Known Q (cfs)	Drng area (ac)	Runoff coeff (C)	Inlet time (min)	Invert El Dn (ft)	Line slope (%)	Invert El Up (ft)	Line size (in)	Line type	N value (n)	J-loss coeff (K)	Inlet/Rim El (ft)	
1	End	70.0	47.0	MH	0.00	0.00	0.00	0.0	81.00	1.14	81.80	18	Cir	0.013	0.77	87.50	1-2 - 1-1
2	1	238.0	-47.0	Curb	0.00	0.27	0.72	5.0	81.80	1.13	84.50	15	Cir	0.013	1.50	91.30	1-3 - 1-2
3	2	119.0	0.0	Curb	0.00	0.77	0.67	10.0	84.50	0.60	85.21	15	Cir	0.013	0.98	88.40	1-4 - 1-3
4	3	86.0	-37.0	Curb	0.00	0.24	0.83	5.0	85.21	0.60	85.73	15	Cir	0.013	1.00	89.55	1-5 - 1-4
5	2	180.0	-90.0	DrGr	0.00	0.05	0.66	5.0	84.50	3.89	91.50	12	Cir	0.013	0.50	95.80	1-6 - 1-3
6	5	54.0	-6.0	DrGr	0.00	0.11	0.68	5.0	91.50	0.93	92.00	12	Cir	0.013	1.00	95.80	1-7 - 1-6

Project File: 9552 JRBC Storm.stm

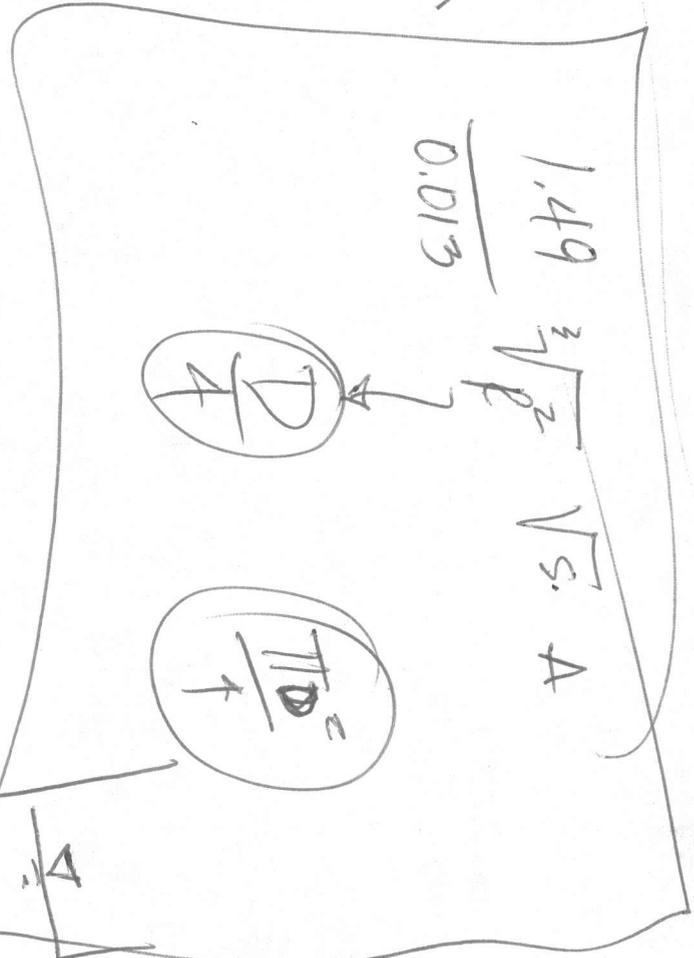
Number of lines: 6

Date: 08-17-2006



$S_1$

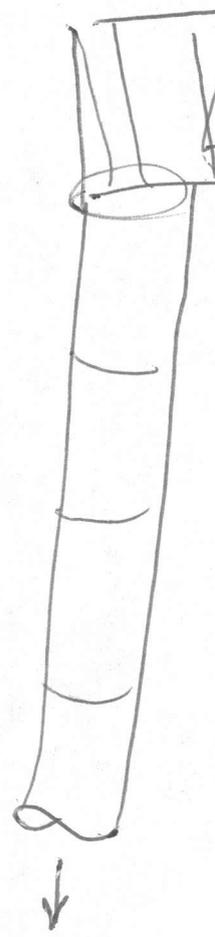
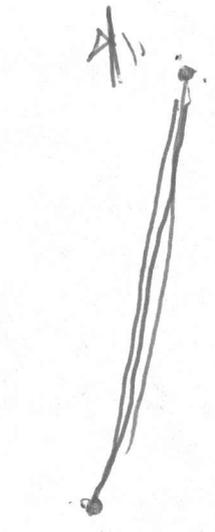
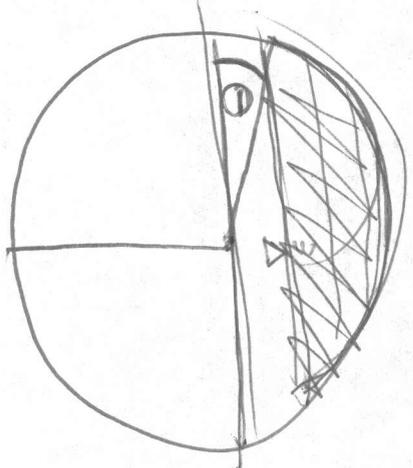
$Q$



$D$

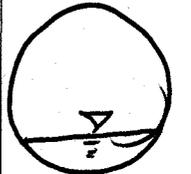
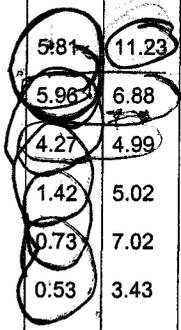
$\frac{\pi D^2}{4}$

$\frac{V}{L}$



# Storm Sewer Tabulation

Station		Len (ft)	Drng Area		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr (ac)	Total (ac)		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	
1	End	70.0	0.00	1.44	0.00	0.00	1.02	0.0	11.4	5.7	5.81	11.23	3.29	18	1.14	81.80	81.00	84.61	84.40	87.50	81.00	1-2 - 1-1
2	1	238.0	0.27	1.44	0.72	0.19	1.02	5.0	10.6	5.9	5.96	6.88	4.86	15	1.13	84.50	81.80	86.77	84.74	91.30	87.50	1-3 - 1-2
3	2	119.0	0.77	1.01	0.67	0.52	0.72	10.0	10.0	6.0	4.27	4.99	3.48	15	0.60	85.21	84.50	88.02	87.50	88.40	91.30	1-4 - 1-3
4	3	86.0	0.24	0.24	0.83	0.20	0.20	5.0	5.0	7.1	1.42	5.02	1.16	15	0.60	85.73	85.21	88.42	88.38	89.55	88.40	1-5 - 1-4
5	2	180.0	0.05	0.16	0.66	0.03	0.11	5.0	6.3	6.8	0.73	7.02	1.89	12	3.89	91.50	84.50	91.86	87.68	95.80	91.30	1-6 - 1-3
6	5	54.0	0.11	0.11	0.68	0.07	0.07	5.0	5.0	7.1	0.53	3.43	2.00	12	0.93	92.00	91.50	92.31	91.98	95.80	95.80	1-7 - 1-6

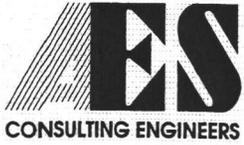


Project File: 9552 JRBC Storm.stm

Number of lines: 6

Run Date: 08-17-2006

NOTES: Intensity = 143.72 / (Inlet time + 19.20) ^ 0.94; Return period = 10 Yrs.



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Project  
 Project No.  
 Subject  
 Date  
 Calculated By

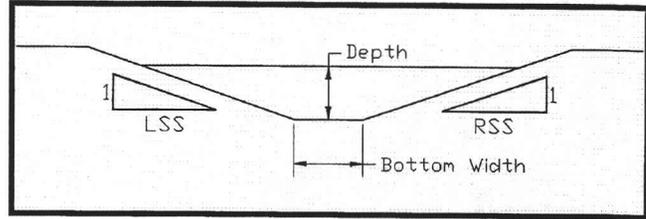
James River Baptist Church
9552
Channel Design
August 23, 2006
N. Botta

**Design Point: A**

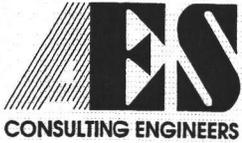
Drainage Area = 0.64 Acres (Area draining to Design Point)  
 C = 0.56 (Runoff Coefficient)  
 I = 7.13 in/hr (Design Rainfall Intensity) 10 year storm - Tc = 5 min.  
 Q = C I A (Peak Flow)  
 = 0.56 x 7.13 x 0.64  
 = 2.56 CFS

**Channel Characteristics**

Rt. Sideslope = 4.00 :1  
 Lt. Sideslope = 4.00 :1  
 Base Width = 0.00 Ft.  
 Max. Depth = 2.50 Ft.  
 Channel Slope = 1.00 %  
 Mannings (n) = 0.020 (Grass Lined)



Depth of Flow = 0.48 Ft.  
 Area = 0.90 SF  
 Hydraulic Radius = 0.23 Ft.  
 Velocity (V) = 2.79 Ft./sec. (From Manning's Equation)  
 Flow (Q) = 2.52 CFS (From Continuity Equation Q=AV)  
 Wetted Perimeter = 3.92 Ft.



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Channel Design
August 23, 2006
N. Botta

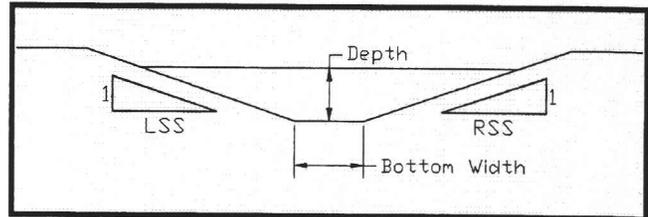
**Design Point: B**

Drainage Area = 0.80 Acres (Area draining to Design Point)  
 C = 0.51 (Runoff Coefficient)  
 I = 7.13 in/hr (Design Rainfall Intensity) 10 year storm - Tc = 5 min.

$Q = C I A$  (Peak Flow)  
 = 0.8 x 7.13 x 0.8  
 = 2.91 CFS

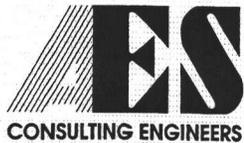
**Channel Characteristics**

Rt. Sideslope = 4.00 :1  
 Lt. Sideslope = 4.00 :1  
 Base Width = 0.00 Ft.  
 Max. Depth = 2.00 Ft.



Channel Slope = 4.00 %  
 Mannings (n) = 0.020 (Grass Lined w/ EC-3 Matting)

Depth of Flow = 0.39 Ft.  
 Area = 0.60 SF  
 Hydraulic Radius = 0.19 Ft.  
 Velocity (V) = 4.86 Ft./sec. (From Manning's Equation)  
 Flow (Q) = 2.90 CFS (From Continuity Equation  $Q=AV$ )  
 Wetted Perimeter = 3.18 Ft.



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Project  
 Project No.  
 Subject  
 Date  
 Calculated By

<b>James River Baptist Church</b>
<b>9552</b>
<b>Channel Design</b>
<b>August 23, 2006</b>
<b>N. Botta</b>

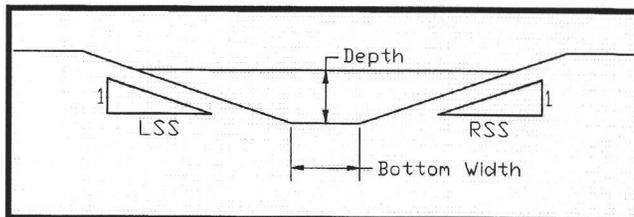
**Design Point: C**

Drainage Area = 0.80 Acres (Area draining to Design Point)  
 C = 0.51 (Runoff Coefficient)  
 I = 7.13 in/hr (Design Rainfall Intensity) 10 year storm - Tc = 5 min.

$Q = C I A$  (Peak Flow)  
 = 0.8 x 7.13 x 0.8  
 = 2.91 CFS

**Channel Characteristics**

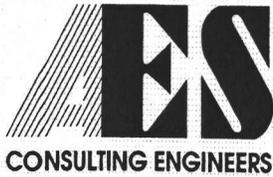
Rt. Sideslope = 3.00 :1  
 Lt. Sideslope = 3.00 :1  
 Base Width = 0.00 Ft.  
 Max. Depth = 2.00 Ft.



Channel Slope = 33.30 %  
 Mannings (n) = 0.045 (Riprap Lining)

Depth of Flow = 0.39 Ft.  
 Area = 0.47 SF  
 Hydraulic Radius = 0.19 Ft.  
 Velocity (V) = 6.23 Ft./sec. (From Manning's Equation)  
 Flow (Q) = 2.90 CFS (From Continuity Equation  $Q=AV$ )  
 Wetted Perimeter = 2.49 Ft.

# STORMWATER MANAGEMENT



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Project  
Project No.  
Subject  
Date  
Calculated By

James River Baptist Church
9552
Water Quality Volume
August 23, 2006
N. Botta

BMP Type = Wet Extended Detention Pond

$$\begin{aligned} \text{Water Quality Volume} &= 0.5 \text{ in.} \times 1.26 \text{ acres of impervious coverage} \\ &= (0.5 / 12) \times (43,560 \times 1.26) \\ &= \boxed{2287 \text{ CF}} \end{aligned}$$

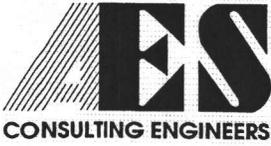
$$\begin{aligned} \text{Total Storage Volume Required} &= 4 \times \text{Water Quality Volume} \\ &= 4 \times 2287 \\ &= 9147.6 \text{ CF} \end{aligned}$$

$$\begin{aligned} \text{Min. Wet Storage Volume Required} &= 2 \times \text{Water Quality Volume} \\ &= 2 \times 2287 \\ &= 4574 \text{ CF} \end{aligned}$$

Wet Storage Volume Provided = 6107 CF Elevation = 84.00 (Permanent Pool Elevation)

$$\begin{aligned} \text{Min. Dry Storage Volume Required} &= 2 \times \text{Water Quality Volume} \\ &= 2 \times 2287 \\ &= 4574 \text{ CF} \end{aligned}$$

Dry Storage Volume Provided = 9762 CF Elevation = 85.90 (Top of Riser)



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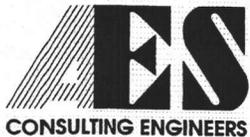
Project  
 Project No.  
 Subject  
 Date  
 Calculated By

James River Baptist Church
9552
Sediment Forebay Design
August 23, 2006
N. Botta

Required Forebay Volume = 0.1 in. x 1.26 acres of impervious coverage  
 = (0.1 / 12) x (43,560 x 1.26) = 457 CF

Forebay Volume Provided = 1263 CF Elevation = 84.00

Stage (FT)	Elevation (FT)	Area (SF)	Incremental Volume (CF)	Total Volume (CF)
0	81	62		0
1	82	194	128	128
2	83	381	288	416
3	84	1314	848	1263



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Project:	James River Baptist Church
Project No.:	9552
Subject:	Critical Storm Duration Modified Rational Method
Date:	August 23, 2006
Calculated By:	N. Botta

Equation 5-5 - Virginia Stormwater Management Handbook

$$T_d = \sqrt{\frac{2 C A a (b - t_c/4)}{q_o}} - b$$

- C = 0.59 Post-Development Runoff Coefficient
- A = 2.84 Drainage Area (Acres)
- t<sub>c</sub> = 10 Post Development Time of Concentration (Minutes)
- a = 185.06 From Table 5-5 for James City County (10 year storm)
- b = 20.81

Equation 5-2 - Virginia Stormwater Management Handbook

$$I_{post} = \frac{a}{b + T_d} \quad \text{Rainfall Intensity where } T_d = t_c$$

I<sub>post</sub> = 6.01 in/hr

q<sub>o</sub> = (C<sub>pre-dev</sub>) (I) (A) Allowable Peak Outflow (10 year storm)

- C = 0.38 Pre-Development Runoff Coefficient
- A<sub>pre</sub> = 3.03 Pre-Development Drainage Area (Acres)
- t<sub>c</sub> = 10 Pre-Development Time of Concentration (Minutes)
- I<sub>pre</sub> = 6.01 in/hr

q<sub>o</sub> = 6.92 CFS Pre-Development Peak Flow (10 year storm)

Using Equation 5-5

T <sub>d</sub> = 19.71 Minutes
--------------------------------

Storm Duration Factor = T<sub>d</sub>/t<sub>c</sub> = 1.97 x t<sub>c</sub>

# TR55 Tc Worksheet

Hydraflow Hydrographs by Intelisolve

**Hyd. No. 2**

Pre-Dev 0.74 Ac

<u>Description</u>	<u>A</u>	<u>B</u>	<u>C</u>	<u>Totals</u>
<b>Sheet Flow</b>				
Manning's n-value	= 0.150	0.400	0.011	
Flow length (ft)	= 40.0	20.0	0.0	
Two-year 24-hr precip. (in)	= 3.50	3.50	0.00	
Land slope (%)	= 2.00	3.00	0.00	
<b>Travel Time (min)</b>	<b>= 4.50</b>	<b>+</b>	<b>4.82</b>	<b>+</b>
			<b>0.00</b>	<b>= 9.32</b>
<b>Shallow Concentrated Flow</b>				
Flow length (ft)	= 220.00	0.00	0.00	
Watercourse slope (%)	= 8.00	0.00	0.00	
Surface description	= Unpaved	Paved	Paved	
Average velocity (ft/s)	= 4.56	0.00	0.00	
<b>Travel Time (min)</b>	<b>= 0.80</b>	<b>+</b>	<b>0.00</b>	<b>+</b>
			<b>0.00</b>	<b>= 0.80</b>
<b>Channel Flow</b>				
X sectional flow area (sqft)	= 0.00	0.00	0.00	
Wetted perimeter (ft)	= 0.00	0.00	0.00	
Channel slope (%)	= 0.00	0.00	0.00	
Manning's n-value	= 0.015	0.015	0.015	
Velocity (ft/s)	= 0.00	0.00	0.00	
Flow length (ft)	= 0.0	0.0	0.0	
<b>Travel Time (min)</b>	<b>= 0.00</b>	<b>+</b>	<b>0.00</b>	<b>+</b>
			<b>0.00</b>	<b>= 0.00</b>
<b>Total Travel Time, Tc</b>	.....			<b>10.00 min</b>

# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:44 PM

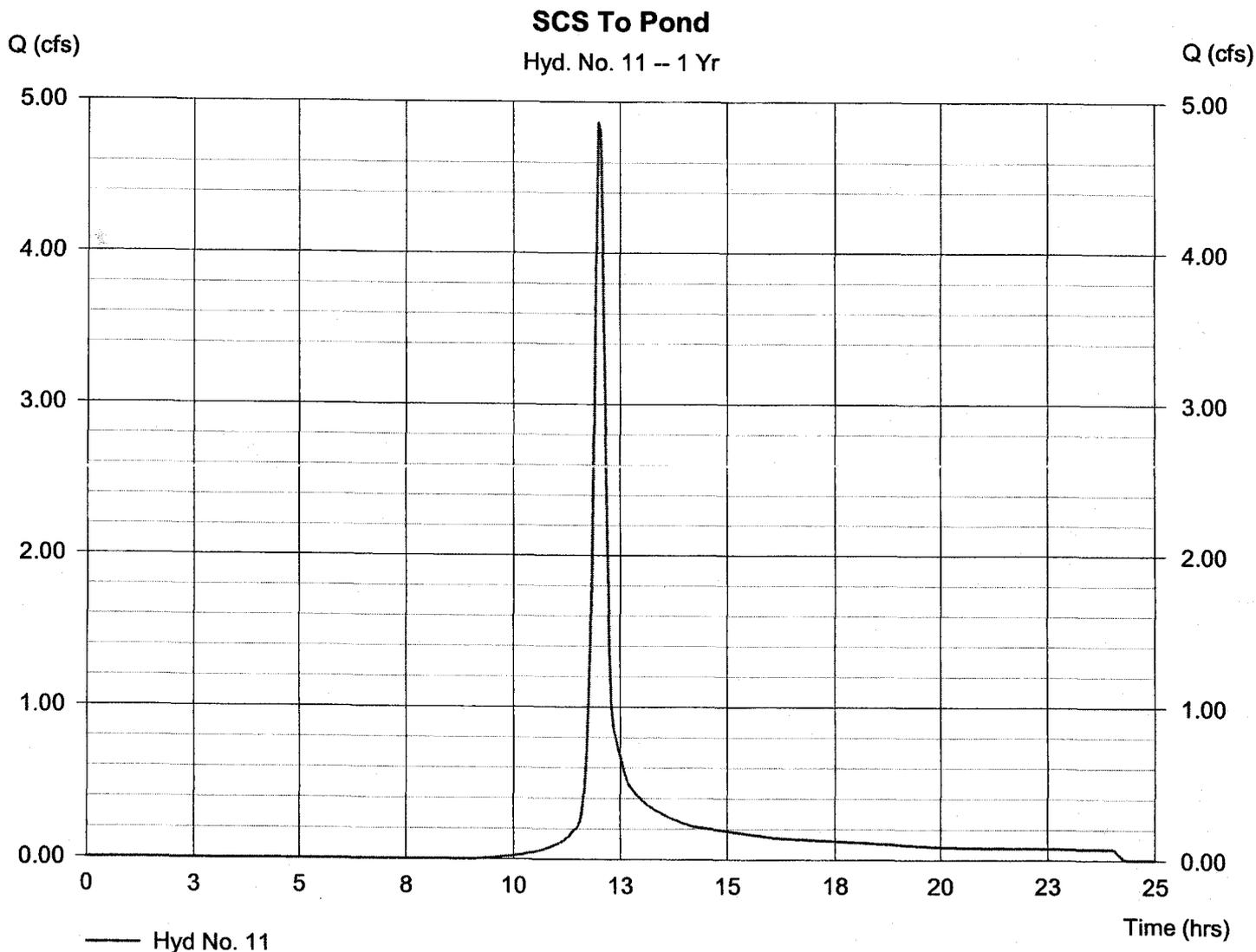
## Hyd. No. 11

### SCS To Pond

Hydrograph type = SCS Runoff  
Storm frequency = 1 yrs  
Drainage area = 2.84 ac  
Basin Slope = 0.0 %  
Tc method = USER  
Total precip. = 2.80 in  
Storm duration = 24 hrs

Peak discharge = 4.86 cfs  
Time interval = 3 min  
Curve number = 83  
Hydraulic length = 0 ft  
Time of conc. (Tc) = 10 min  
Distribution = Type II  
Shape factor = 484

Hydrograph Volume = 13,271 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intellisolve

Tuesday, Aug 22 2006, 7:44 PM

## Hyd. No. 12

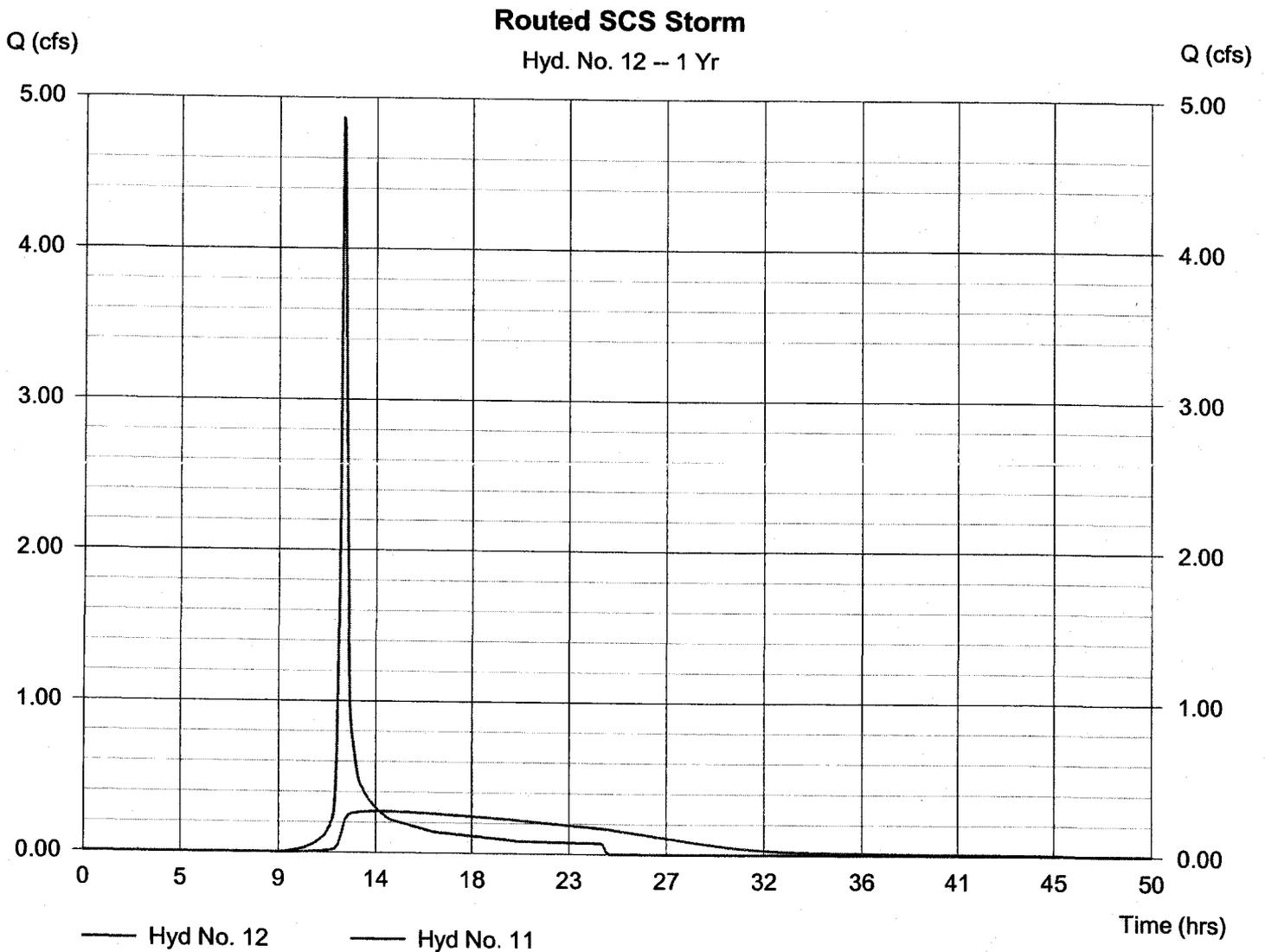
Routed SCS Storm

Hydrograph type = Reservoir  
Storm frequency = 1 yrs  
Inflow hyd. No. = 11  
Reservoir name = JRBC Pond

Peak discharge = 0.27 cfs  
Time interval = 3 min  
Max. Elevation = 85.43 ft  
Max. Storage = 13,281 cuft

Storage Indication method used. Wet pond routing start elevation = 84.00 ft.

Hydrograph Volume = 13,248 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:44 PM

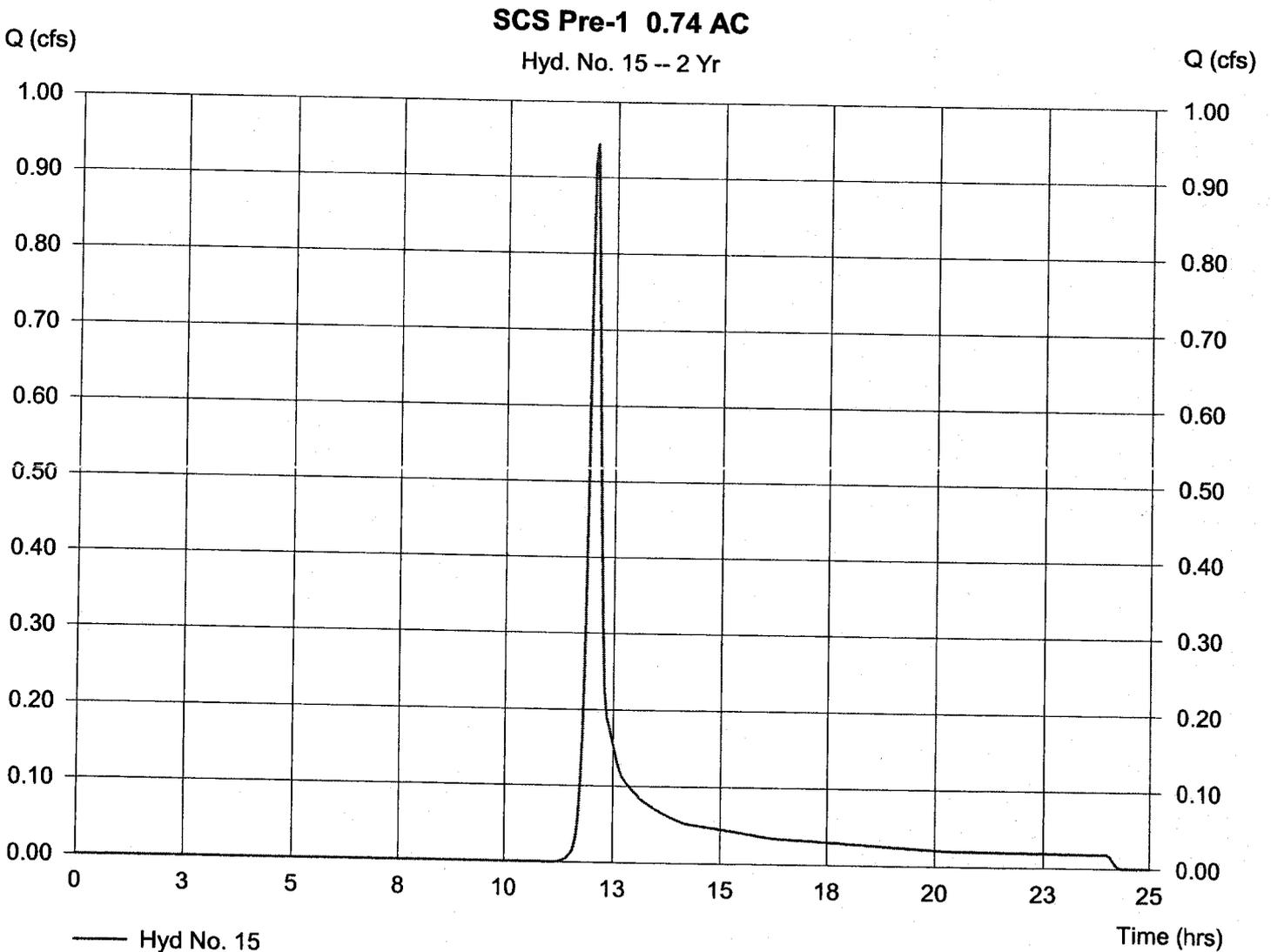
## Hyd. No. 15

SCS Pre-1 0.74 AC

Hydrograph type = SCS Runoff  
Storm frequency = 2 yrs  
Drainage area = 0.74 ac  
Basin Slope = 0.0 %  
Tc method = USER  
Total precip. = 3.50 in  
Storm duration = 24 hrs

Peak discharge = 0.94 cfs  
Time interval = 3 min  
Curve number = 70  
Hydraulic length = 0 ft  
Time of conc. (Tc) = 10 min  
Distribution = Type II  
Shape factor = 484

Hydrograph Volume = 2,708 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:44 PM

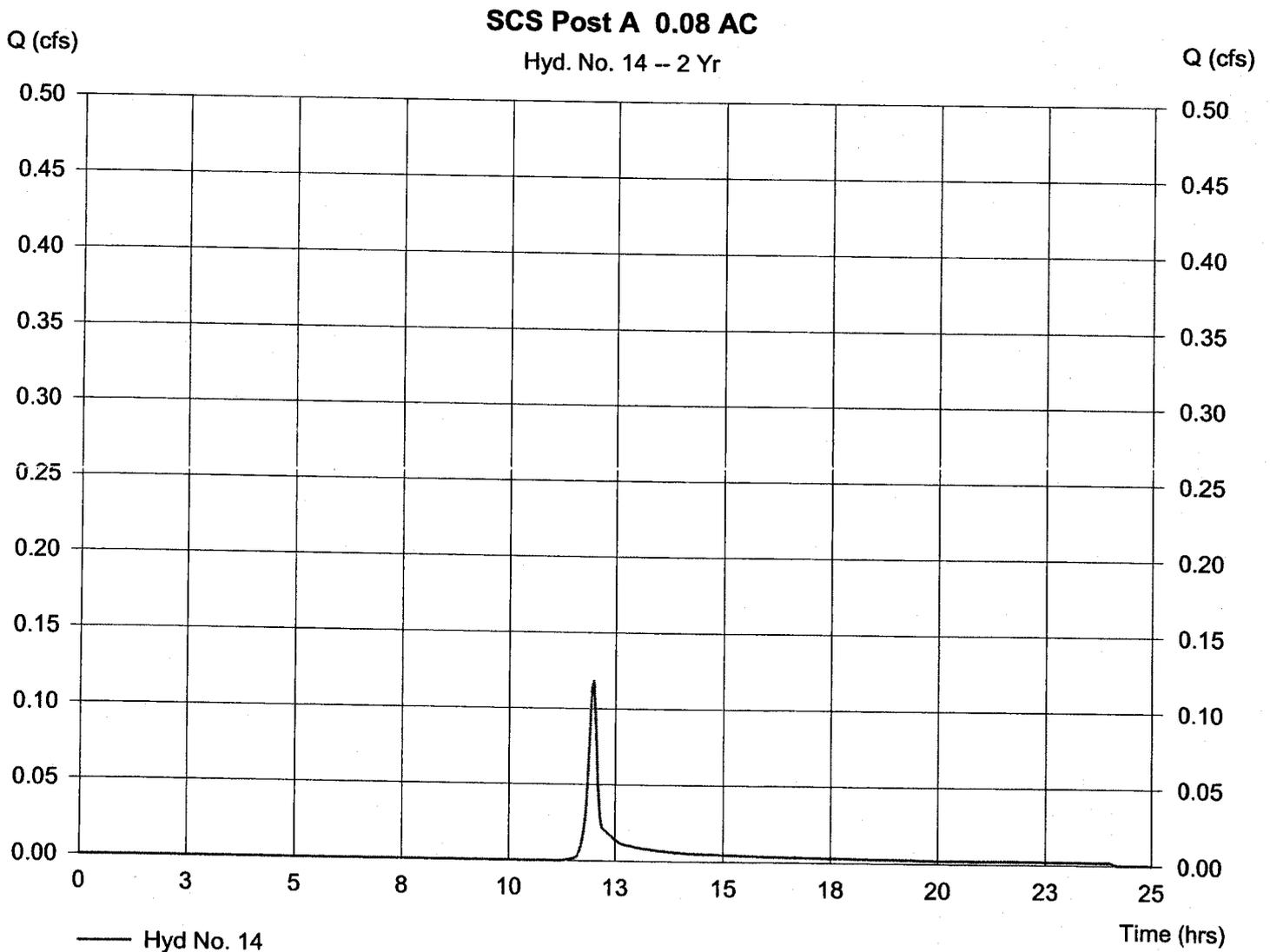
## Hyd. No. 14

SCS Post A 0.08 AC

Hydrograph type = SCS Runoff  
Storm frequency = 2 yrs  
Drainage area = 0.08 ac  
Basin Slope = 0.0 %  
Tc method = USER  
Total precip. = 3.50 in  
Storm duration = 24 hrs

Peak discharge = 0.12 cfs  
Time interval = 3 min  
Curve number = 70  
Hydraulic length = 0 ft  
Time of conc. (Tc) = 5 min  
Distribution = Type II  
Shape factor = 484

Hydrograph Volume = 274 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:44 PM

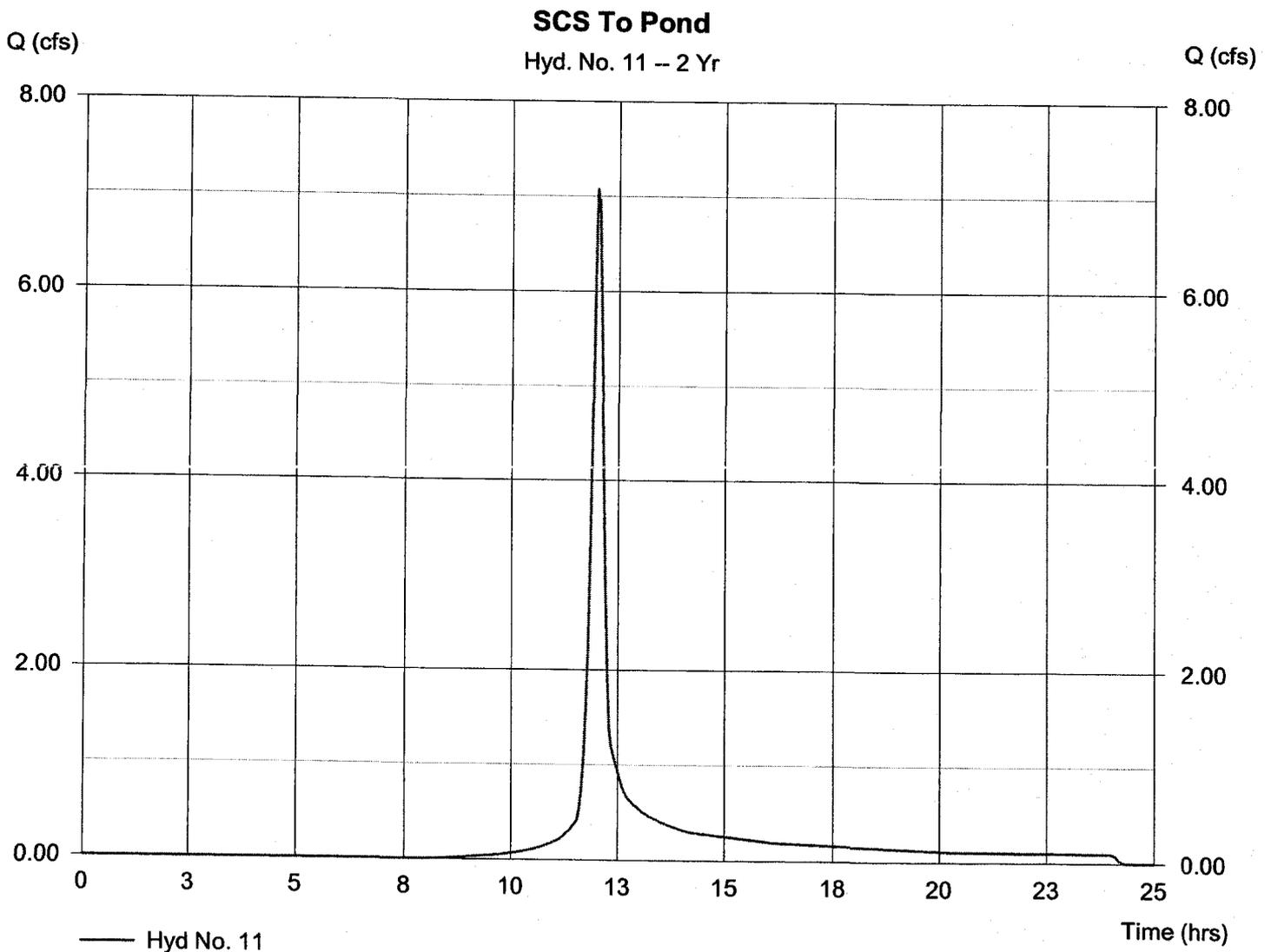
## Hyd. No. 11

### SCS To Pond

Hydrograph type = SCS Runoff  
Storm frequency = 2 yrs  
Drainage area = 2.84 ac  
Basin Slope = 0.0 %  
Tc method = USER  
Total precip. = 3.50 in  
Storm duration = 24 hrs

Peak discharge = 7.07 cfs  
Time interval = 3 min  
Curve number = 83  
Hydraulic length = 0 ft  
Time of conc. (Tc) = 10 min  
Distribution = Type II  
Shape factor = 484

Hydrograph Volume = 19,160 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intellisolve

Tuesday, Aug 22 2006, 7:44 PM

## Hyd. No. 12

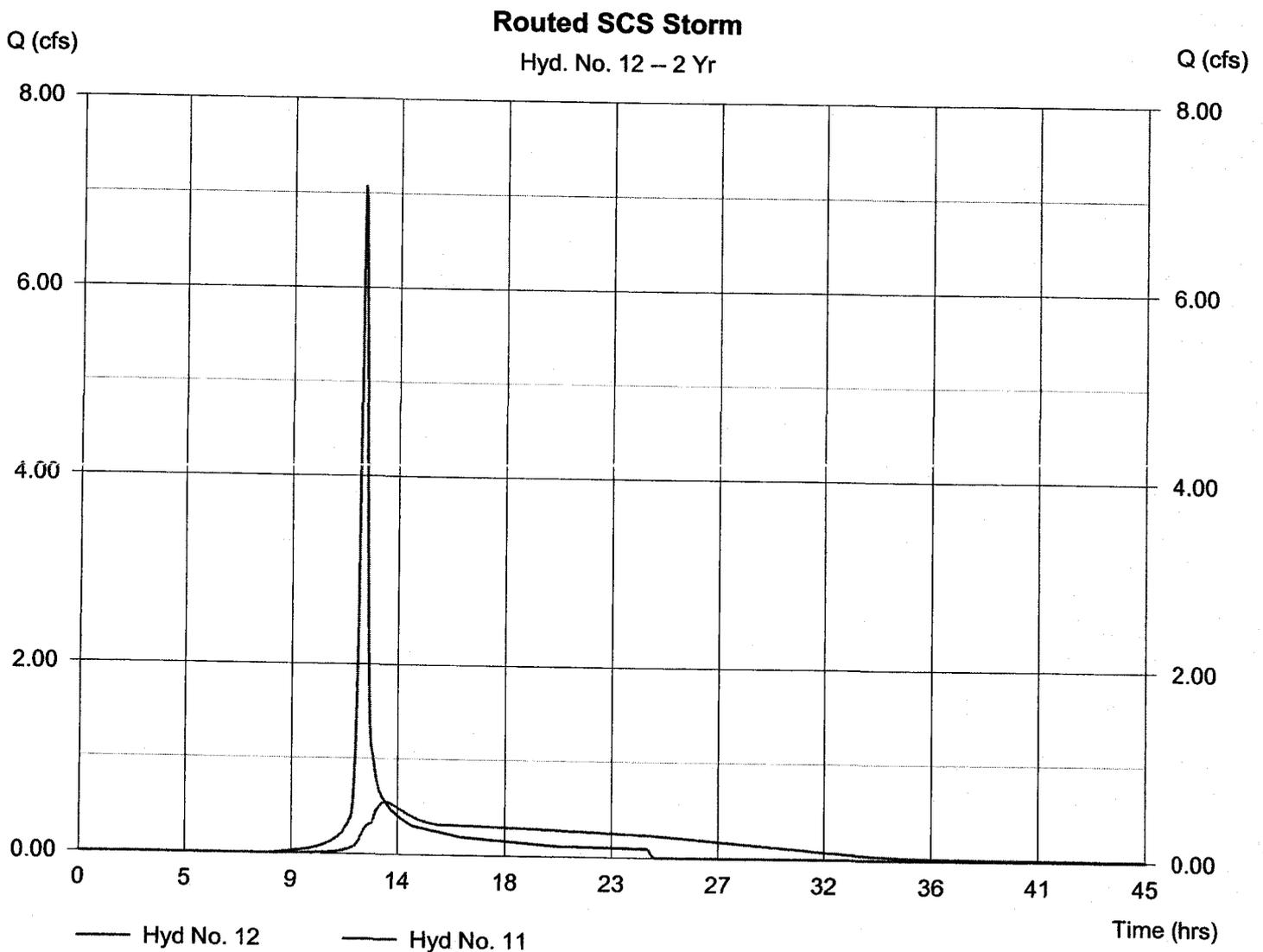
Routed SCS Storm

Hydrograph type = Reservoir  
Storm frequency = 2 yrs  
Inflow hyd. No. = 11  
Reservoir name = JRBC Pond

Peak discharge = 0.54 cfs  
Time interval = 3 min  
Max. Elevation = 86.00 ft  
Max. Storage = 16,483 cuft

Storage indication method used. Wet pond routing start elevation = 84.00 ft.

Hydrograph Volume = 19,137 cuft



# Pond Report

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:44 PM

## Pond No. 1 - JRBC Pond

### Pond Data

Pond storage is based on known contour areas. Average end area method used.

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	81.00	1,044	0	0
1.00	82.00	1,464	1,254	1,254
2.00	83.00	1,940	1,702	2,956
3.00	84.00	4,362	3,151	6,107
4.00	85.00	5,910	4,772	10,879
4.90	85.90	5,910	4,991	15,869
5.00	86.00	6,023	597	16,466
5.90	86.90	6,910	5,820	22,286
6.00	87.00	6,996	695	22,981

### Culvert / Orifice Structures

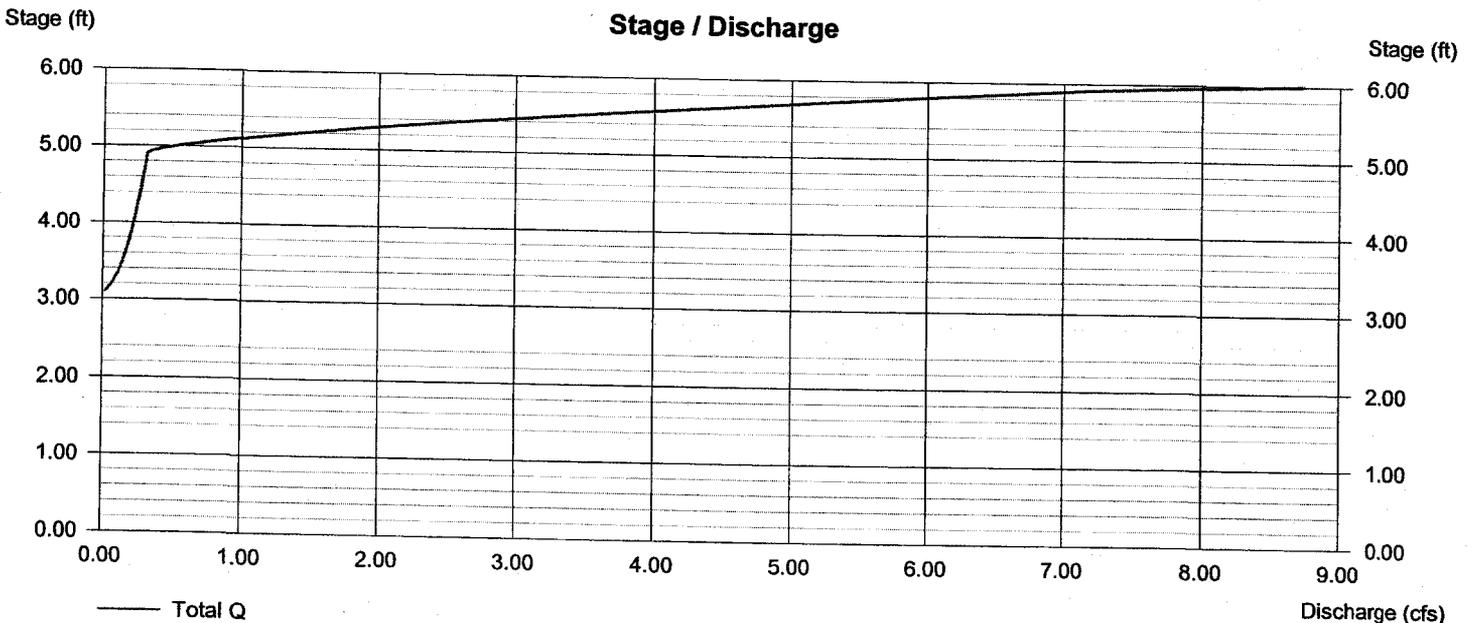
	[A]	[B]	[C]	[D]
Rise (in)	= 15.00	3.00	0.00	0.00
Span (in)	= 15.00	3.00	0.00	0.00
No. Barrels	= 1	1	0	0
Invert El. (ft)	= 80.20	84.00	0.00	0.00
Length (ft)	= 30.00	0.00	0.00	0.00
Slope (%)	= 0.50	0.00	0.00	0.00
N-Value	= .013	.013	.000	.000
Orif. Coeff.	= 0.60	0.60	0.00	0.00
Multi-Stage	= n/a	Yes	No	No

### Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 2.00	8.00	0.00	0.00
Crest El. (ft)	= 85.90	86.90	0.00	0.00
Weir Coeff.	= 3.33	2.60	3.33	0.00
Weir Type	= Riser	Broad	—	—
Multi-Stage	= Yes	Yes	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:42 PM

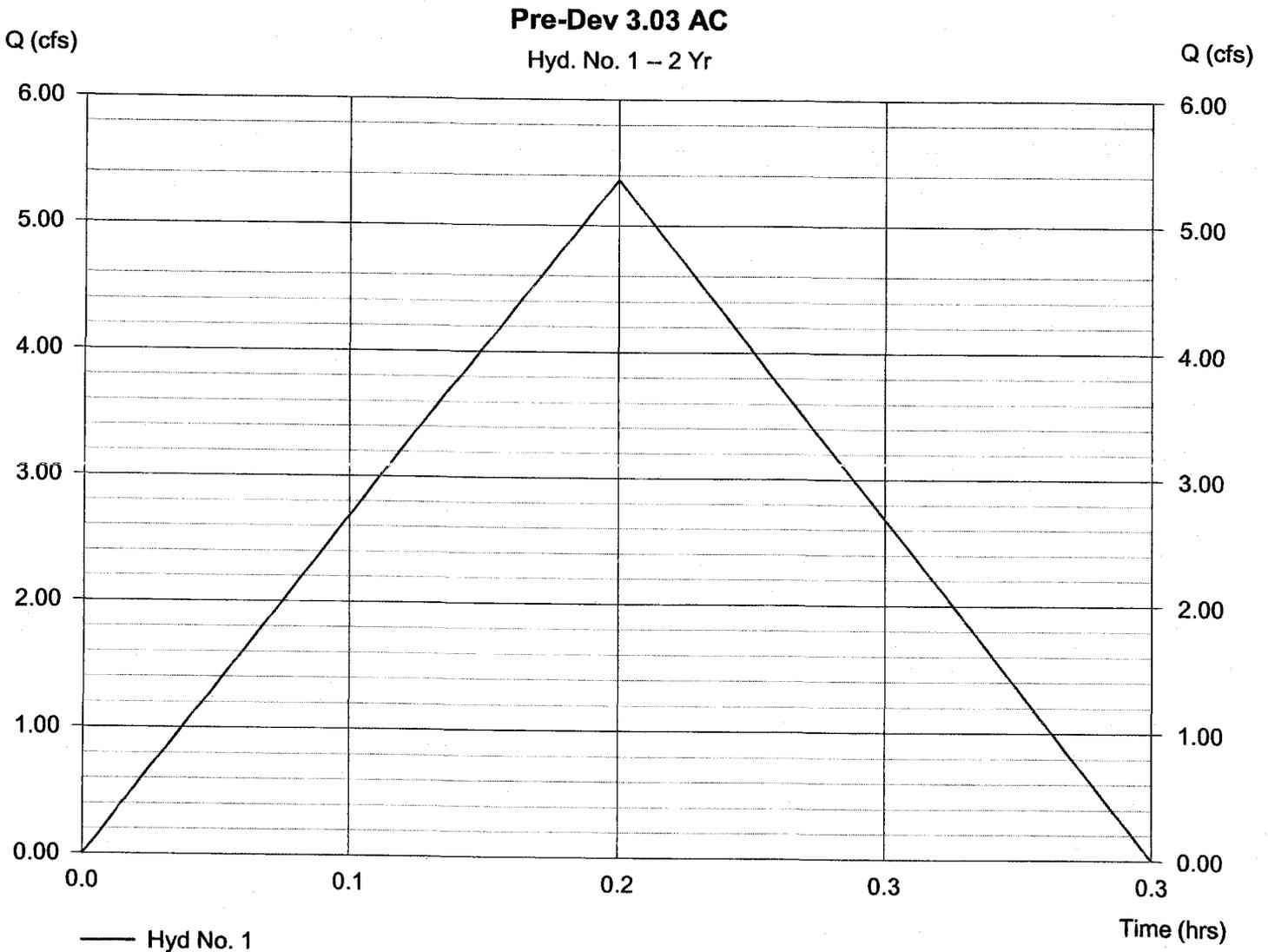
## Hyd. No. 1

Pre-Dev 3.03 AC

Hydrograph type = Mod. Rational  
Storm frequency = 2 yrs  
Drainage area = 3.0 ac  
Intensity = 4.660 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 5.37 cfs  
Time interval = 1 min  
Runoff coeff. = 0.38  
Tc by User = 10 min  
Storm duration = 1 x Tc

Hydrograph Volume = 3,220 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:42 PM

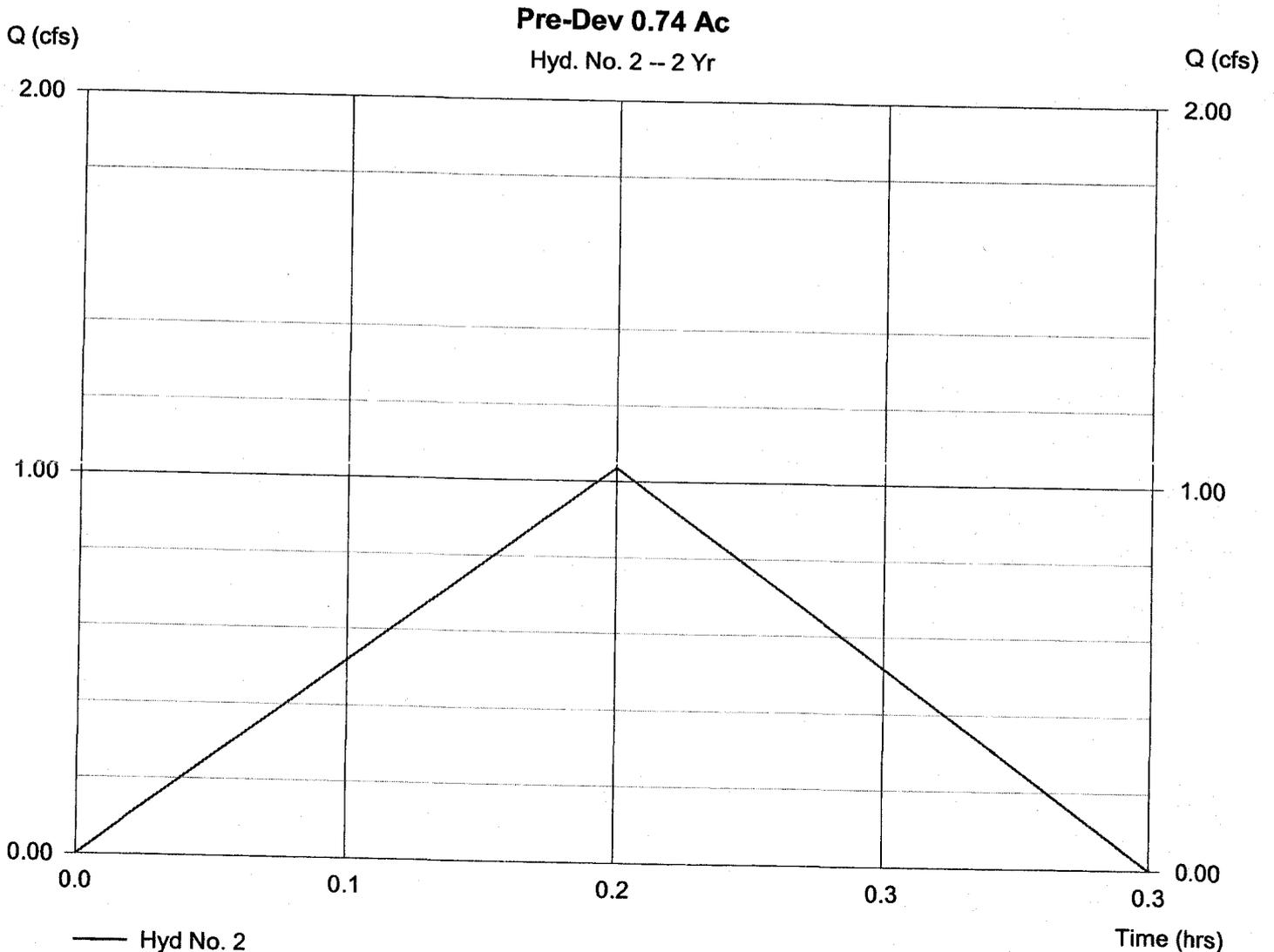
## Hyd. No. 2

Pre-Dev 0.74 Ac

Hydrograph type = Rational  
Storm frequency = 2 yrs  
Drainage area = 0.7 ac  
Intensity = 4.660 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 1.03 cfs  
Time interval = 1 min  
Runoff coeff. = 0.3  
Tc by TR55 = 10 min  
Asc/Rec limb fact = 1/1

Hydrograph Volume = 621 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:43 PM

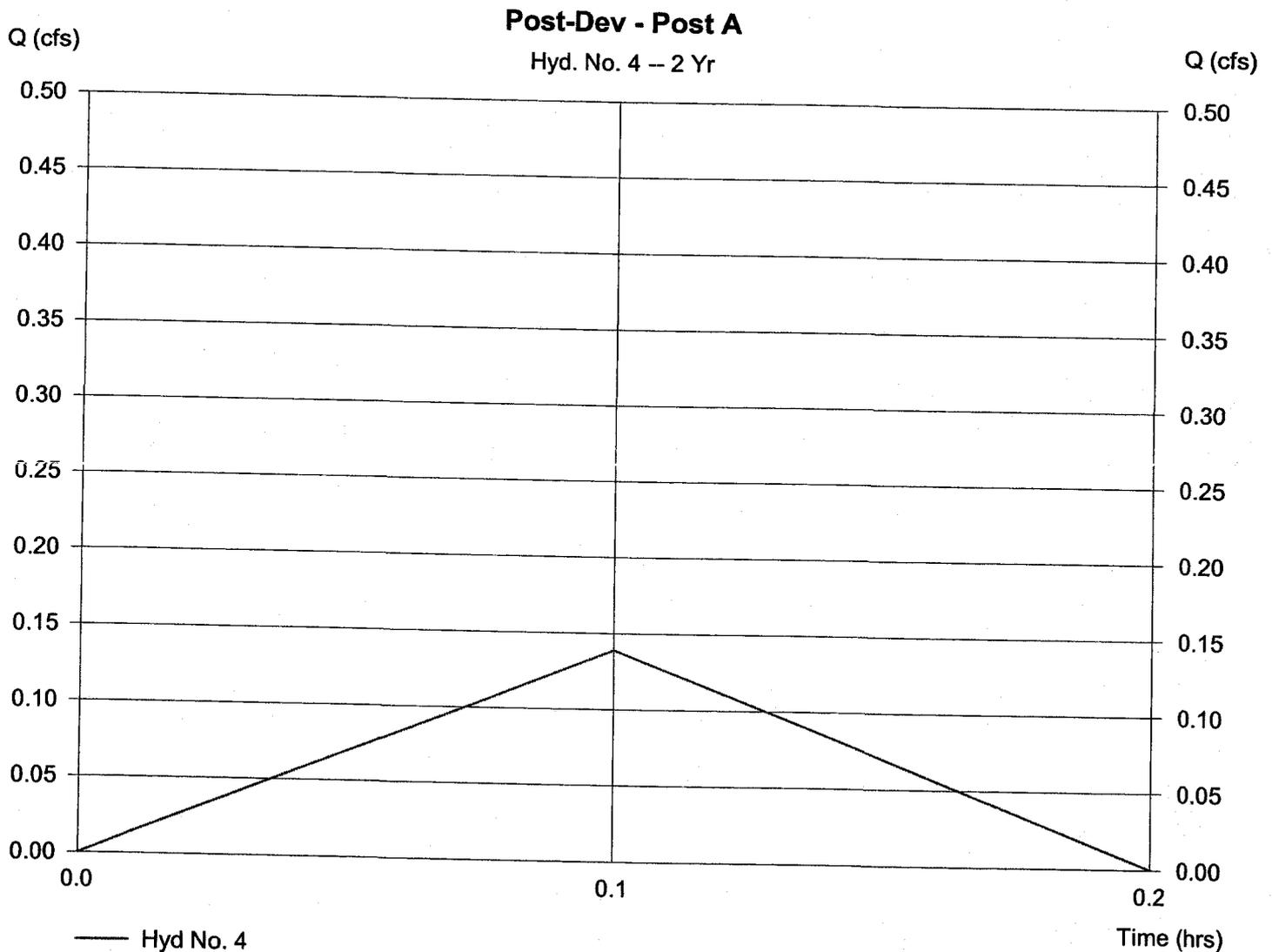
## Hyd. No. 4

Post-Dev - Post A

Hydrograph type = Rational  
Storm frequency = 2 yrs  
Drainage area = 0.1 ac  
Intensity = 5.783 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 0.14 cfs  
Time interval = 1 min  
Runoff coeff. = 0.3  
Tc by User = 5 min  
Asc/Rec limb fact = 1/1

Hydrograph Volume = 42 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:43 PM

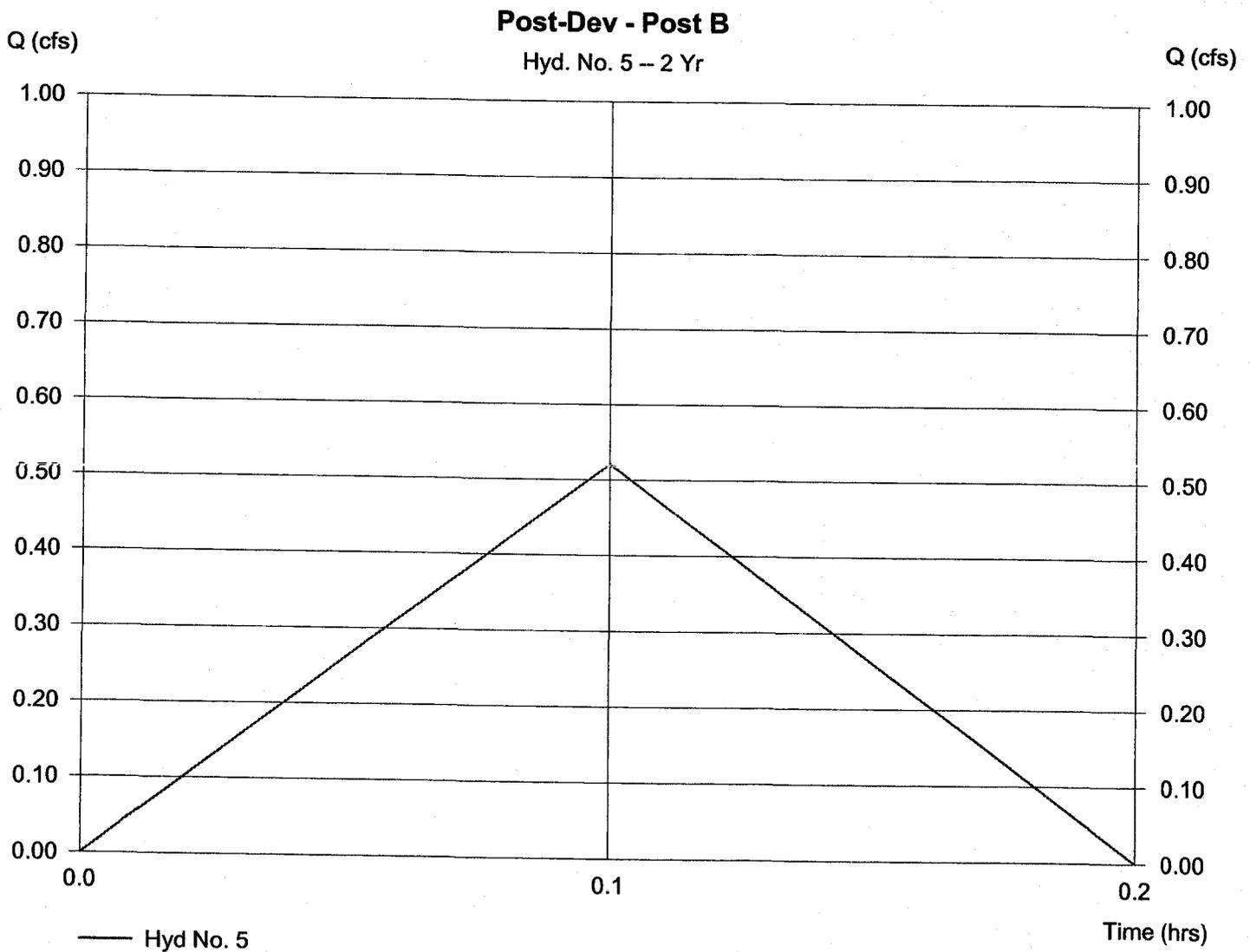
## Hyd. No. 5

Post-Dev - Post B

Hydrograph type = Rational  
Storm frequency = 2 yrs  
Drainage area = 0.3 ac  
Intensity = 5.783 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 0.52 cfs  
Time interval = 1 min  
Runoff coeff. = 0.3  
Tc by User = 5 min  
Asc/Rec limb fact = 1/1

Hydrograph Volume = 156 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:43 PM

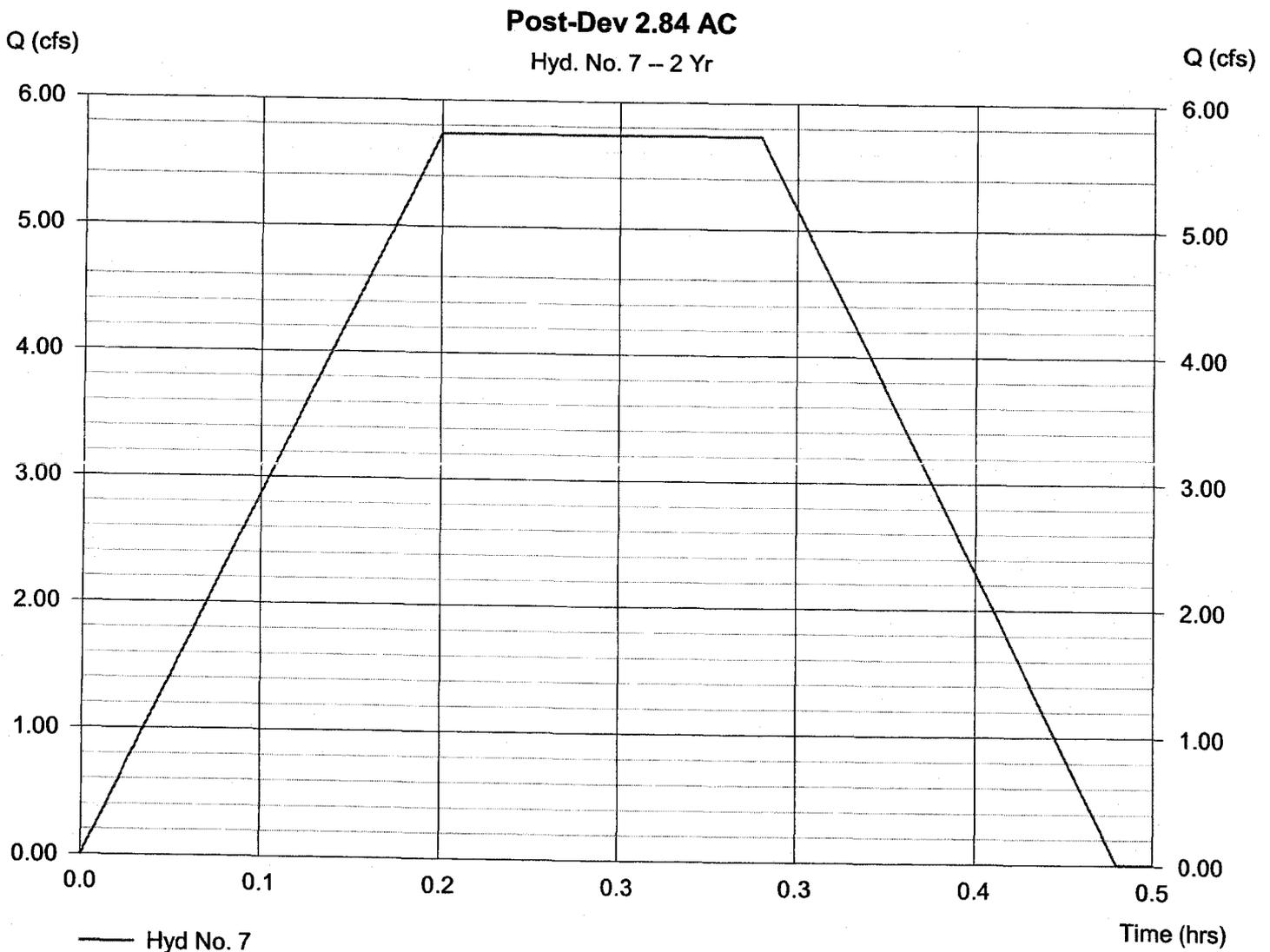
## Hyd. No. 7

Post-Dev 2.84 AC

Hydrograph type = Mod. Rational  
Storm frequency = 2 yrs  
Drainage area = 2.8 ac  
Intensity = 3.422 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 5.73 cfs  
Time interval = 1 min  
Runoff coeff. = 0.59  
Tc by User = 10 min  
Storm duration = 1.97 x Tc

Hydrograph Volume = 6,777 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:43 PM

## Hyd. No. 8

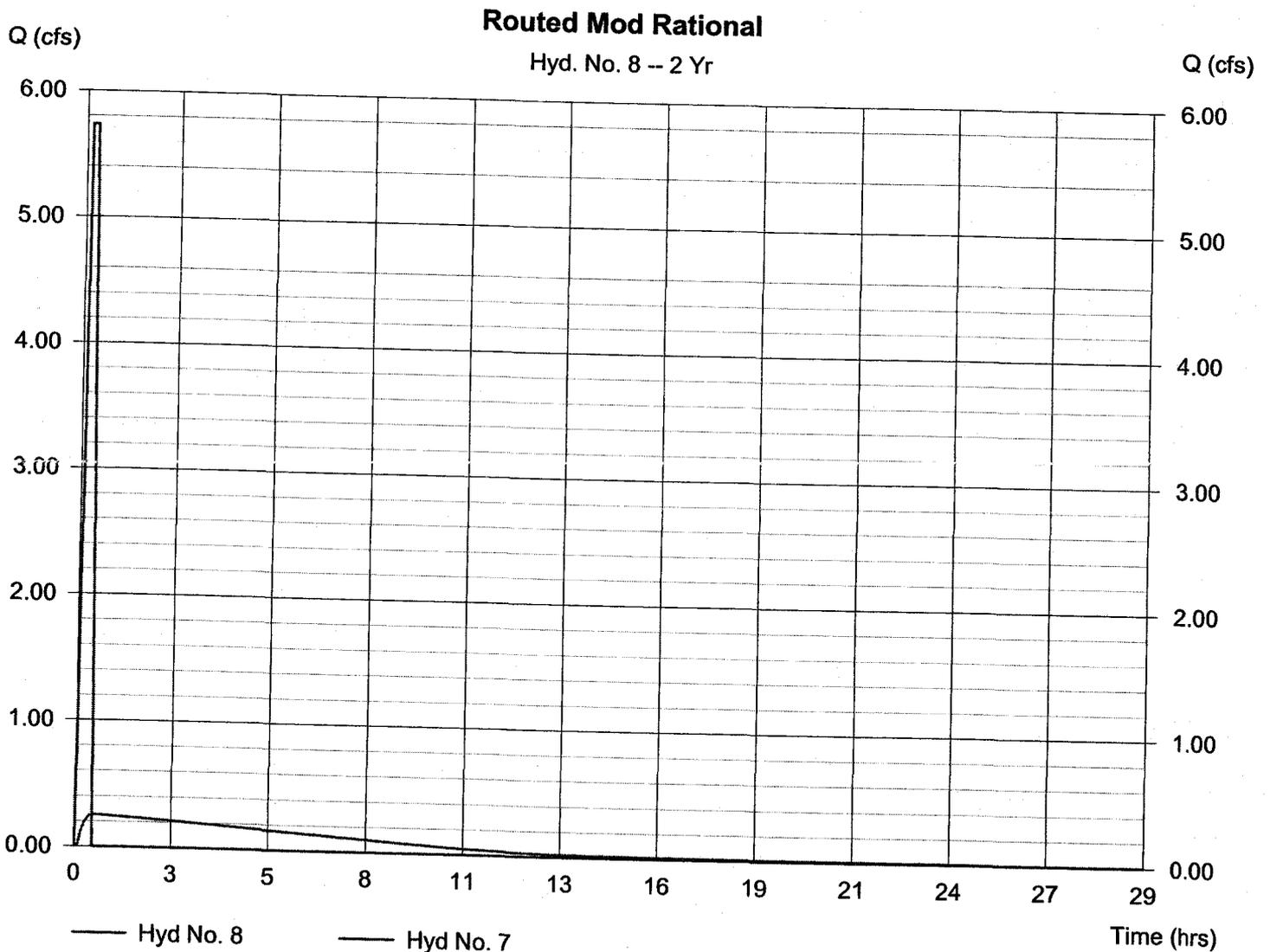
Routed Mod Rational

Hydrograph type = Reservoir  
Storm frequency = 2 yrs  
Inflow hyd. No. = 7  
Reservoir name = JRBC Pond

Peak discharge = 0.25 cfs  
Time interval = 1 min  
Max. Elevation = 85.27 ft  
Max. Storage = 12,384 cuft

Storage Indication method used. Wet pond routing start elevation = 84.00 ft.

Hydrograph Volume = 6,512 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:42 PM

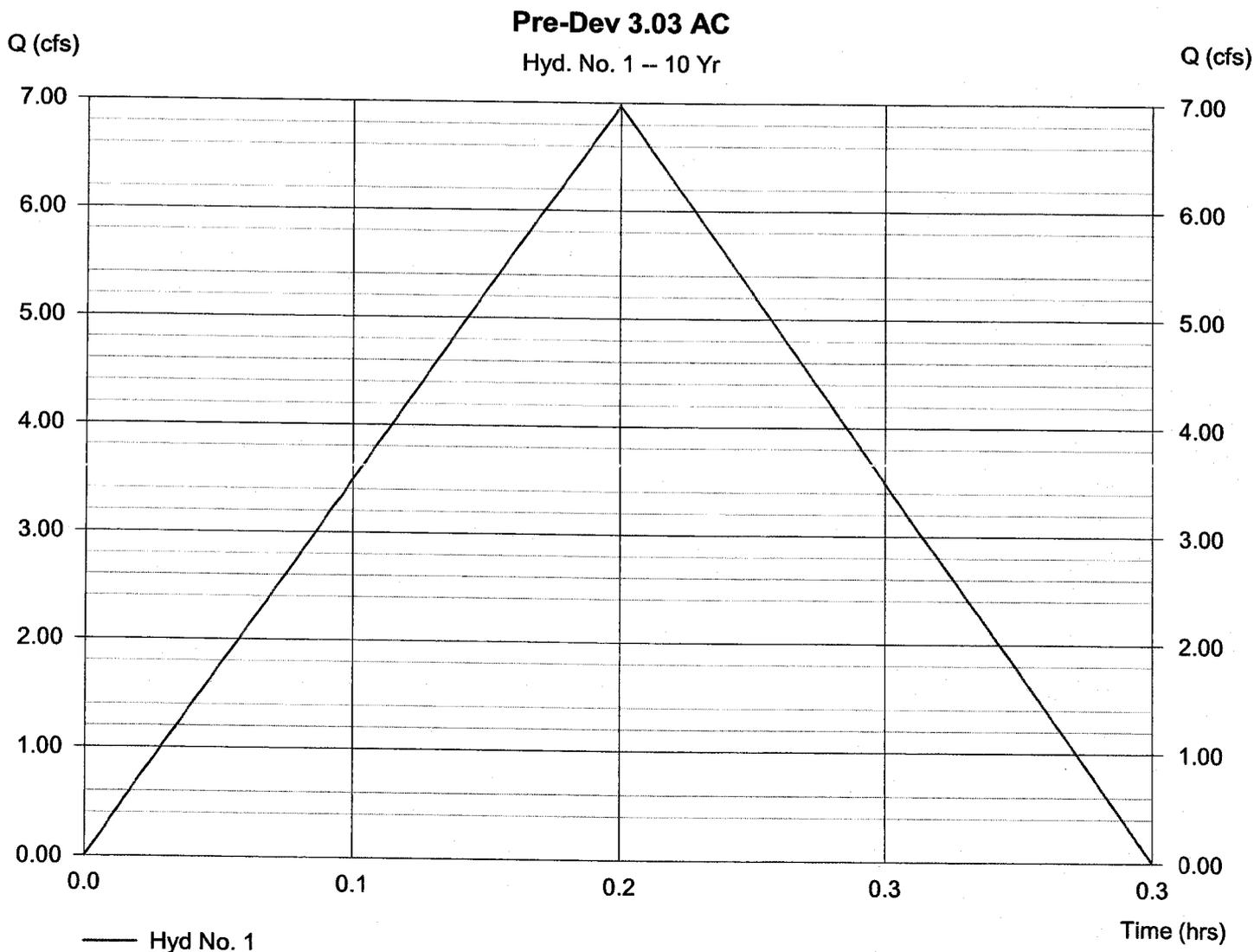
## Hyd. No. 1

Pre-Dev 3.03 AC

Hydrograph type = Mod. Rational  
Storm frequency = 10 yrs  
Drainage area = 3.0 ac  
Intensity = 6.059 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 6.98 cfs  
Time interval = 1 min  
Runoff coeff. = 0.38  
Tc by User = 10 min  
Storm duration = 1 x Tc

Hydrograph Volume = 4,186 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:42 PM

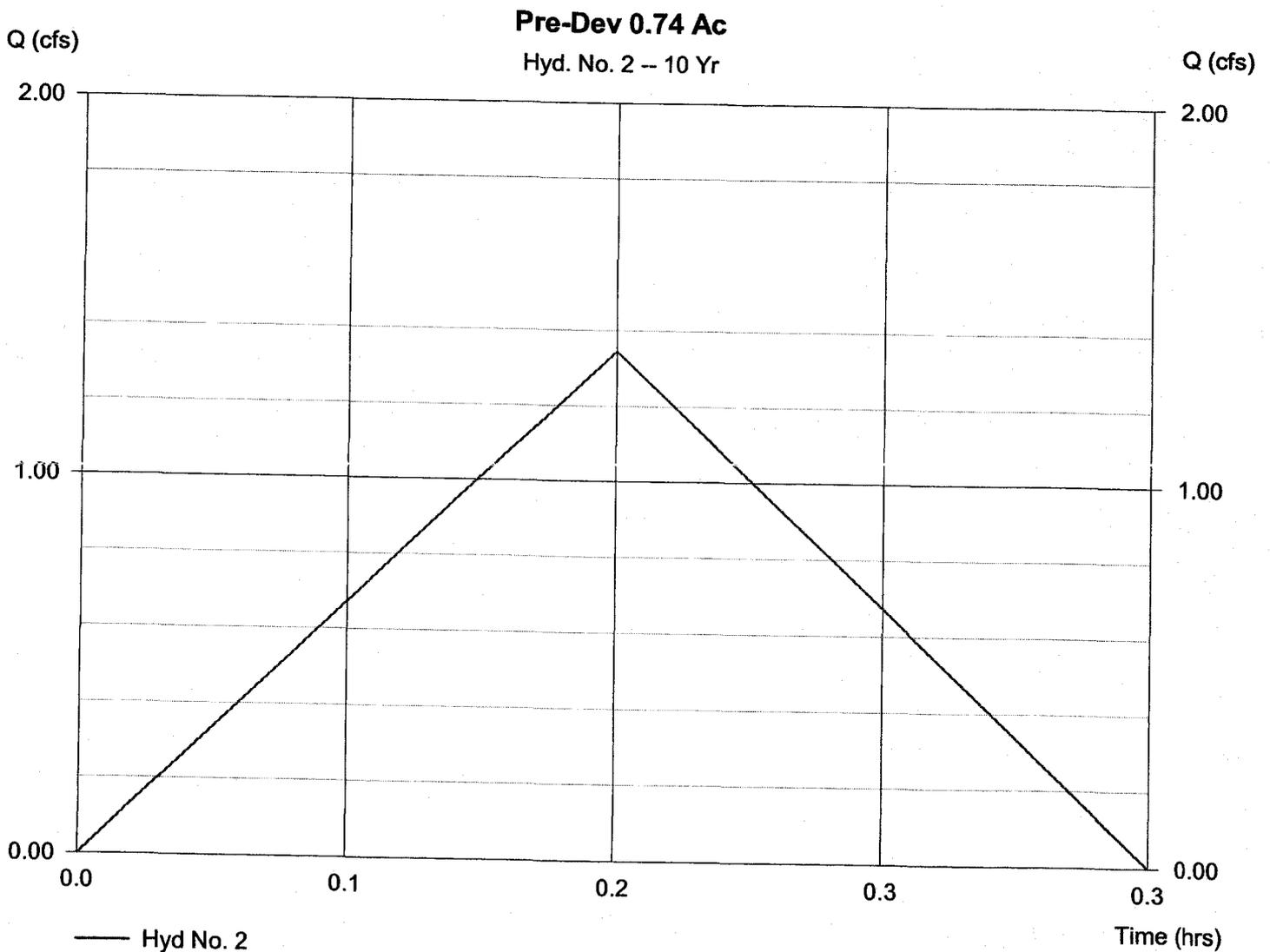
## Hyd. No. 2

Pre-Dev 0.74 Ac

Hydrograph type = Rational  
Storm frequency = 10 yrs  
Drainage area = 0.7 ac  
Intensity = 6.059 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 1.35 cfs  
Time interval = 1 min  
Runoff coeff. = 0.3  
Tc by TR55 = 10 min  
Asc/Rec limb fact = 1/1

Hydrograph Volume = 807 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intellisolve

Tuesday, Aug 22 2006, 7:43 PM

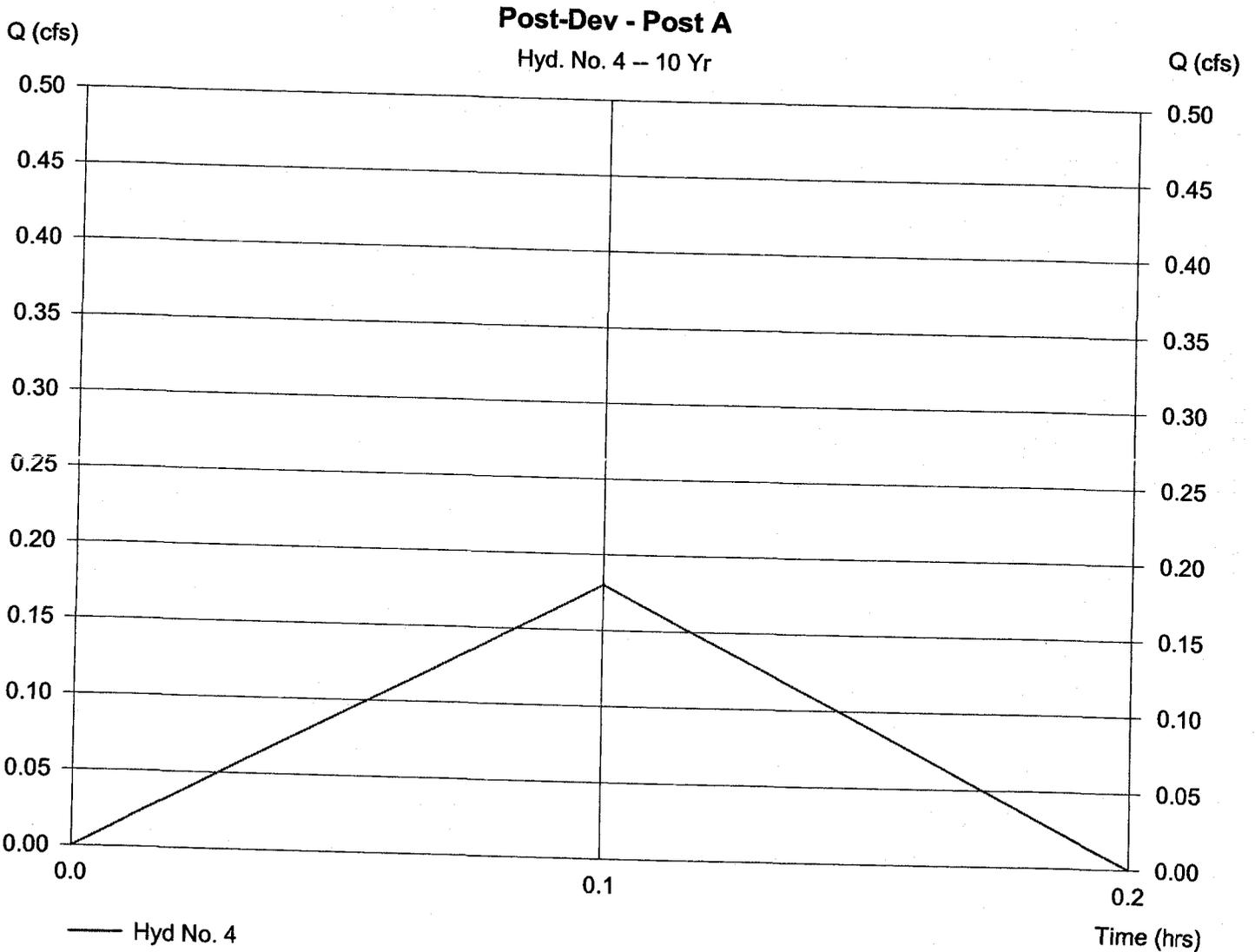
## Hyd. No. 4

Post-Dev - Post A

Hydrograph type = Rational  
Storm frequency = 10 yrs  
Drainage area = 0.1 ac  
Intensity = 7.496 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 0.18 cfs  
Time interval = 1 min  
Runoff coeff. = 0.3  
Tc by User = 5 min  
Asc/Rec limb fact = 1/1

Hydrograph Volume = 54 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:43 PM

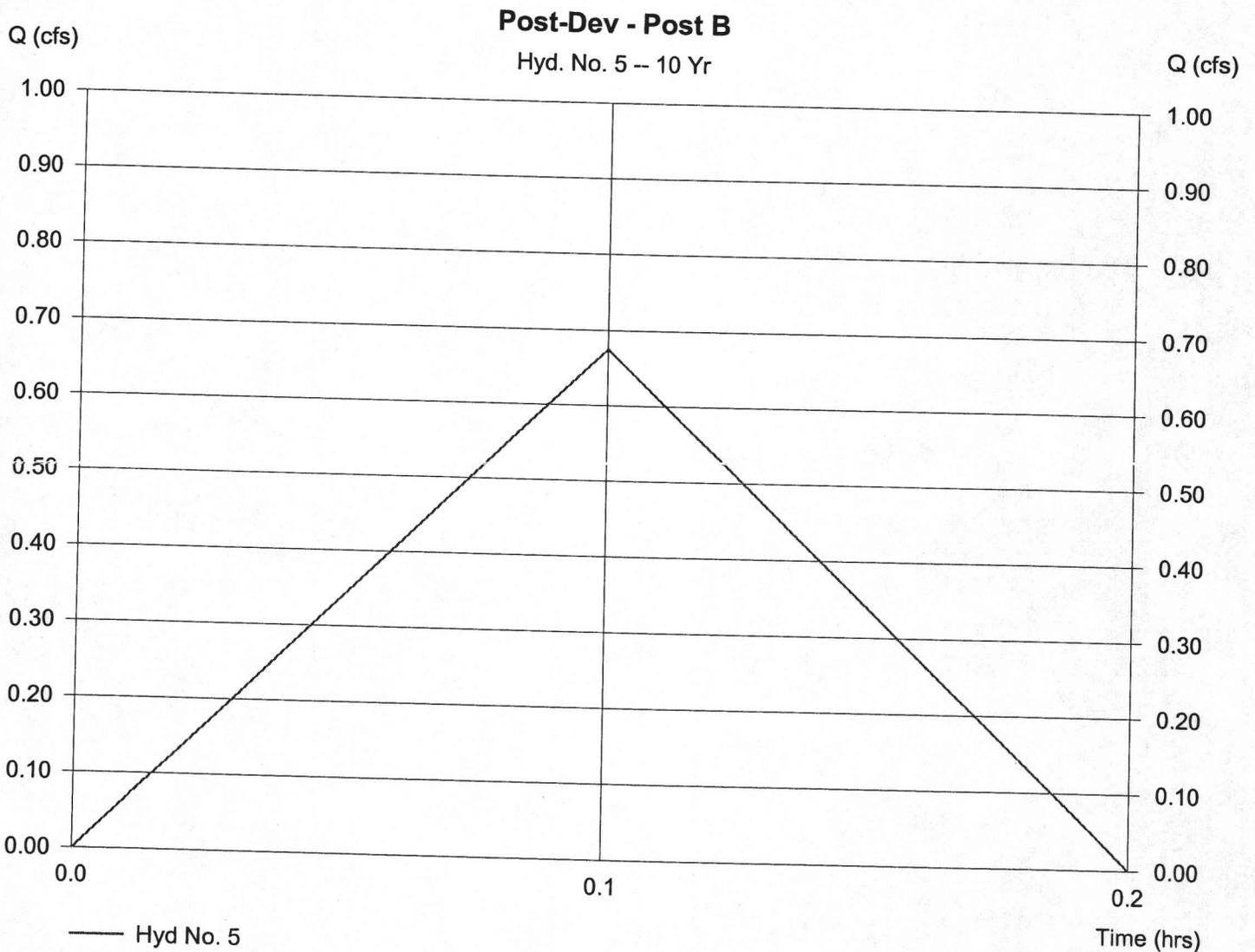
## Hyd. No. 5

Post-Dev - Post B

Hydrograph type = Rational  
Storm frequency = 10 yrs  
Drainage area = 0.3 ac  
Intensity = 7.496 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 0.67 cfs  
Time interval = 1 min  
Runoff coeff. = 0.3  
Tc by User = 5 min  
Asc/Rec limb fact = 1/1

Hydrograph Volume = 202 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:43 PM

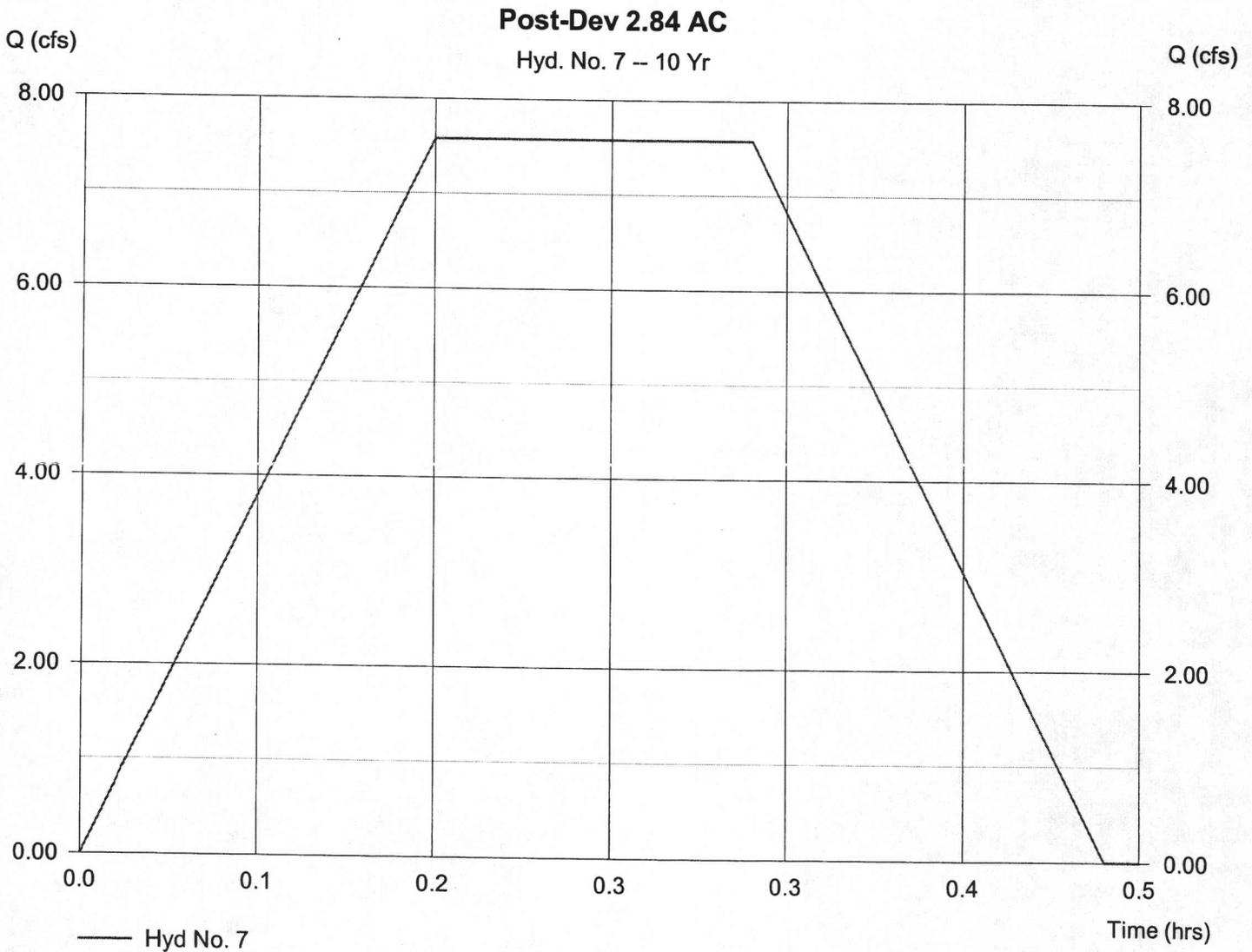
## Hyd. No. 7

Post-Dev 2.84 AC

Hydrograph type = Mod. Rational  
Storm frequency = 10 yrs  
Drainage area = 2.8 ac  
Intensity = 4.522 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 7.58 cfs  
Time interval = 1 min  
Runoff coeff. = 0.59  
Tc by User = 10 min  
Storm duration = 1.97 x Tc

Hydrograph Volume = 8,956 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:43 PM

## Hyd. No. 8

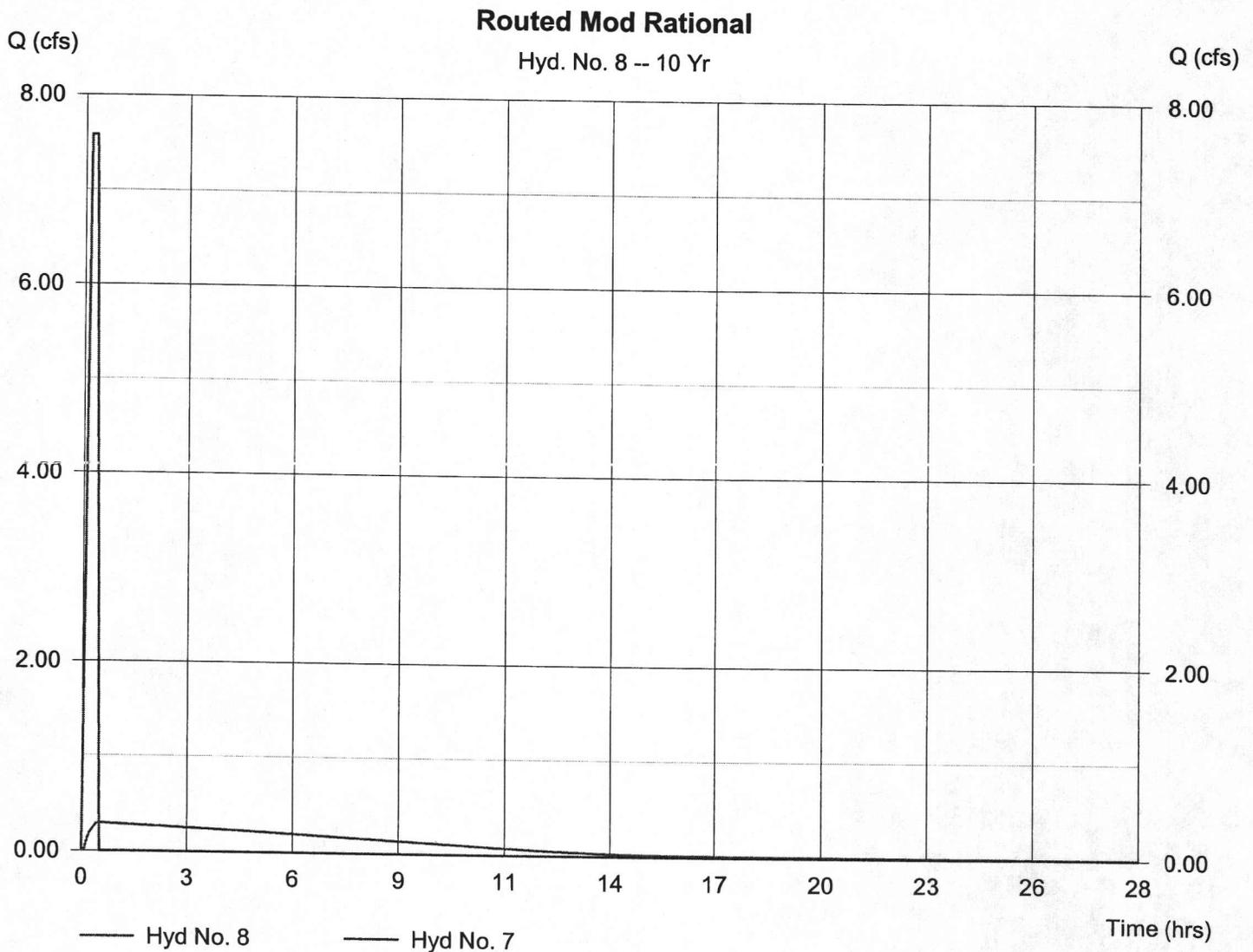
Routed Mod Rational

Hydrograph type = Reservoir  
Storm frequency = 10 yrs  
Inflow hyd. No. = 7  
Reservoir name = JRBC Pond

Peak discharge = 0.29 cfs  
Time interval = 1 min  
Max. Elevation = 85.64 ft  
Max. Storage = 14,440 cuft

Storage Indication method used. Wet pond routing start elevation = 84.00 ft.

Hydrograph Volume = 8,614 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:42 PM

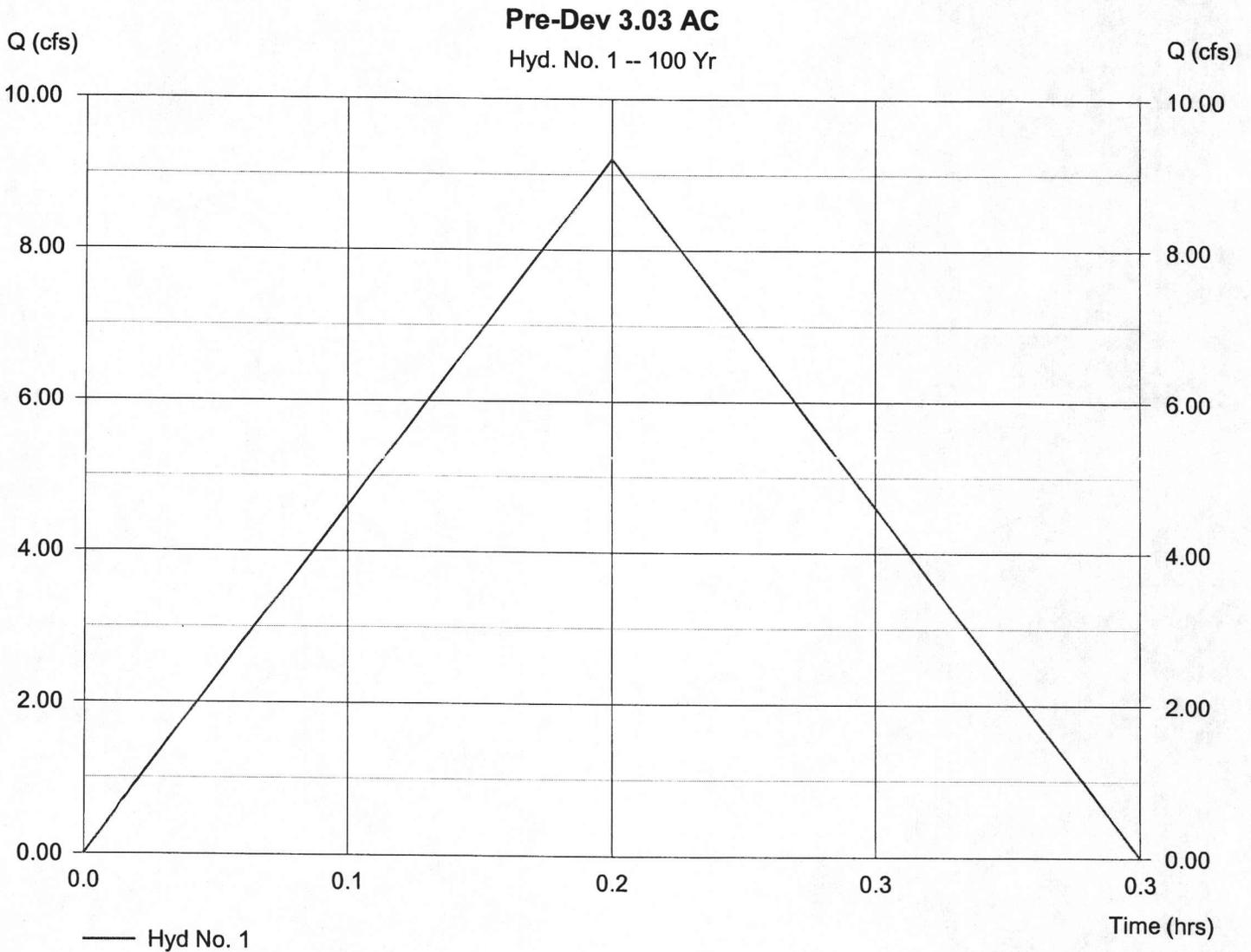
## Hyd. No. 1

Pre-Dev 3.03 AC

Hydrograph type = Mod. Rational  
Storm frequency = 100 yrs  
Drainage area = 3.0 ac  
Intensity = 7.996 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 9.21 cfs  
Time interval = 1 min  
Runoff coeff. = 0.38  
Tc by User = 10 min  
Storm duration = 1 x Tc

Hydrograph Volume = 5,524 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:42 PM

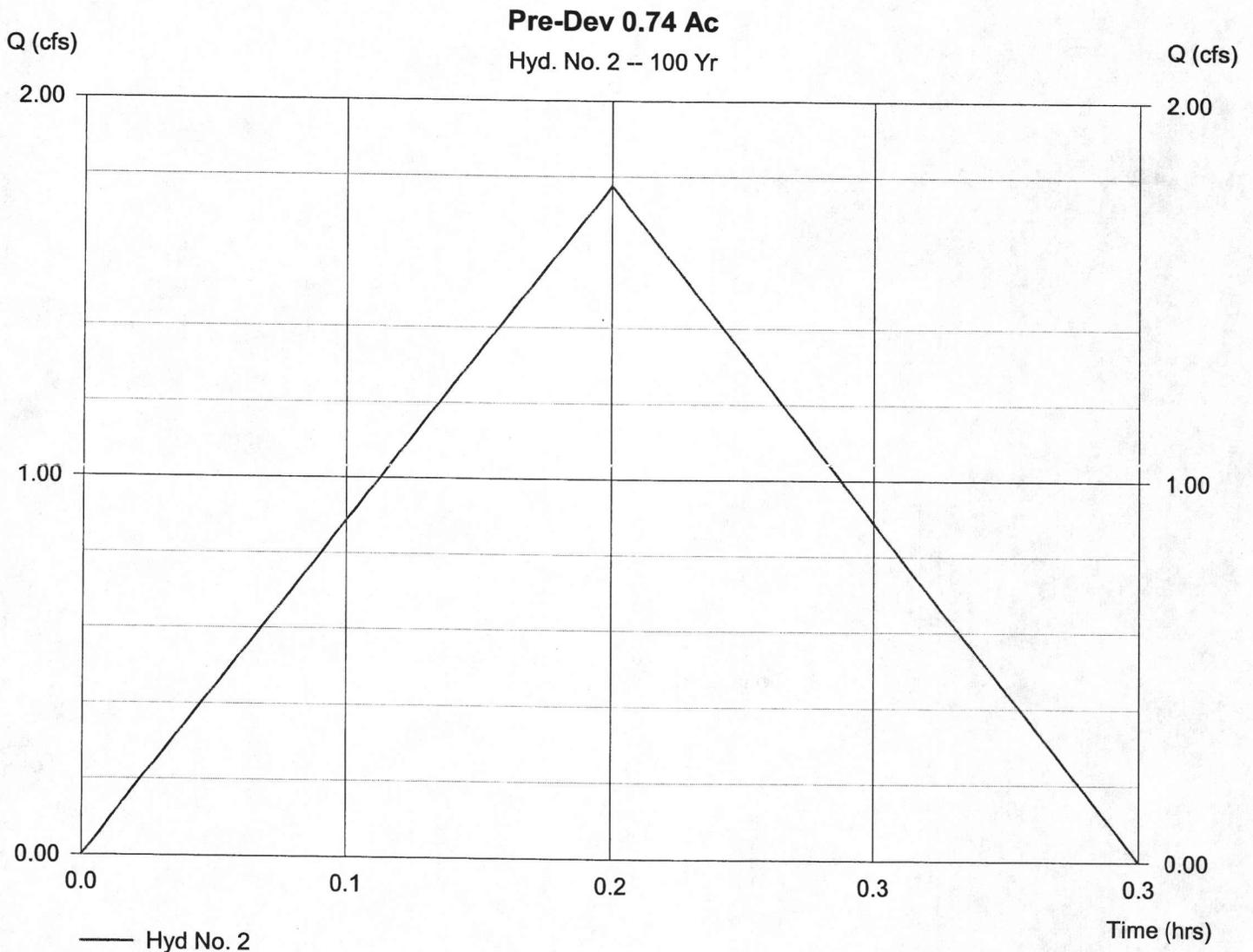
## Hyd. No. 2

Pre-Dev 0.74 Ac

Hydrograph type = Rational  
Storm frequency = 100 yrs  
Drainage area = 0.7 ac  
Intensity = 7.996 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 1.78 cfs  
Time interval = 1 min  
Runoff coeff. = 0.3  
Tc by TR55 = 10 min  
Asc/Rec limb fact = 1/1

Hydrograph Volume = 1,065 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:43 PM

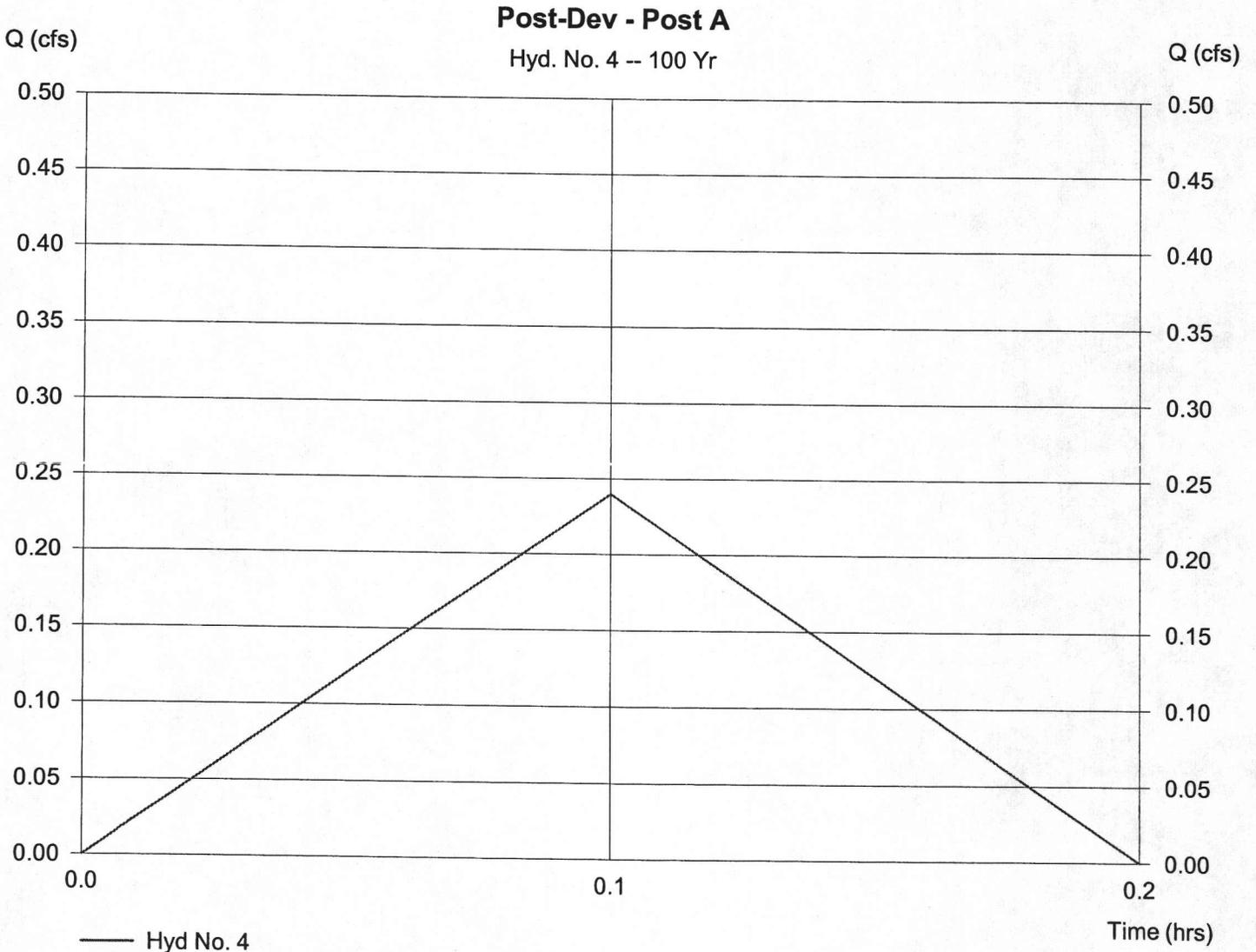
## Hyd. No. 4

Post-Dev - Post A

Hydrograph type = Rational  
Storm frequency = 100 yrs  
Drainage area = 0.1 ac  
Intensity = 9.988 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 0.24 cfs  
Time interval = 1 min  
Runoff coeff. = 0.3  
Tc by User = 5 min  
Asc/Rec limb fact = 1/1

Hydrograph Volume = 72 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:43 PM

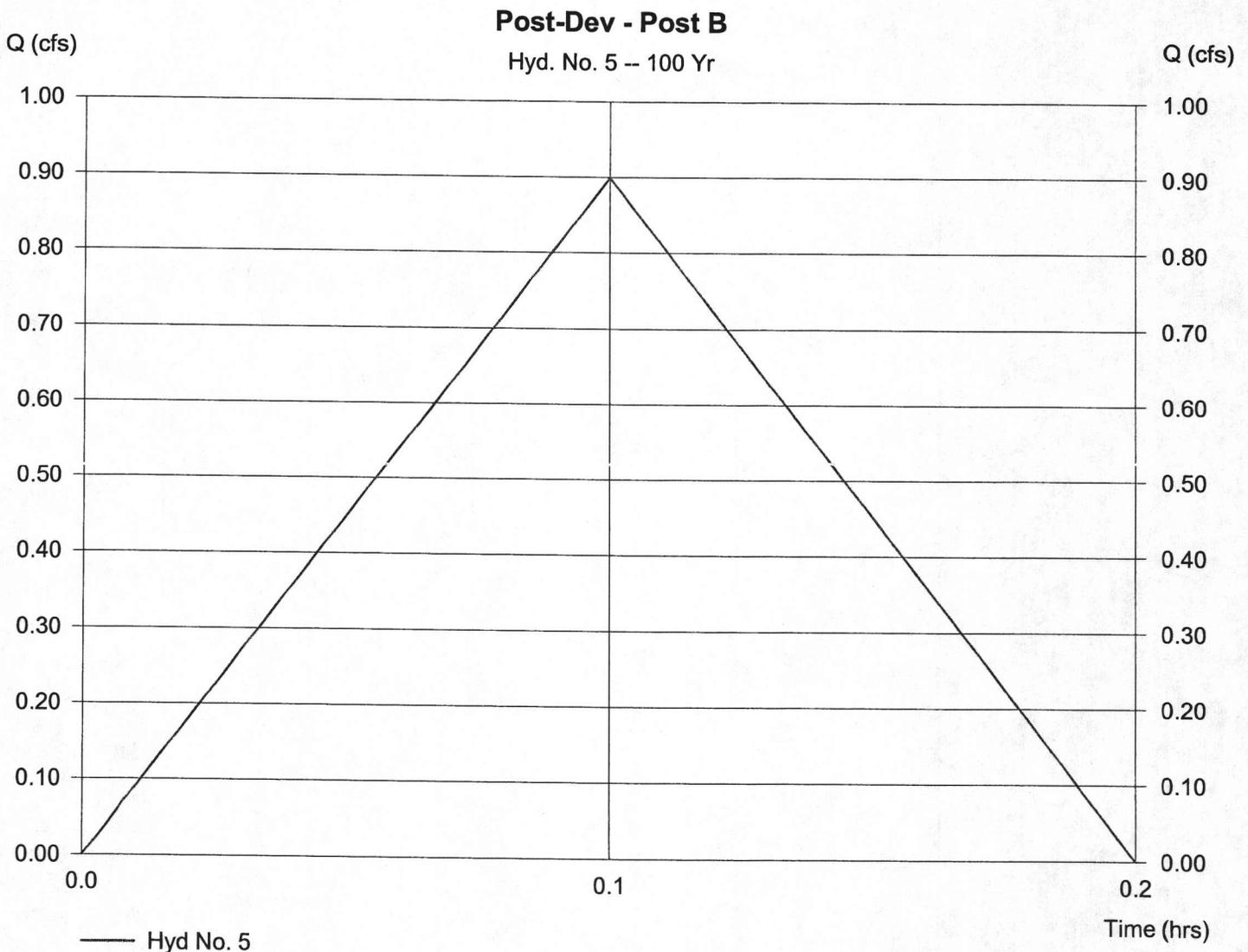
## Hyd. No. 5

Post-Dev - Post B

Hydrograph type = Rational  
Storm frequency = 100 yrs  
Drainage area = 0.3 ac  
Intensity = 9.988 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 0.90 cfs  
Time interval = 1 min  
Runoff coeff. = 0.3  
Tc by User = 5 min  
Asc/Rec limb fact = 1/1

Hydrograph Volume = 270 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:43 PM

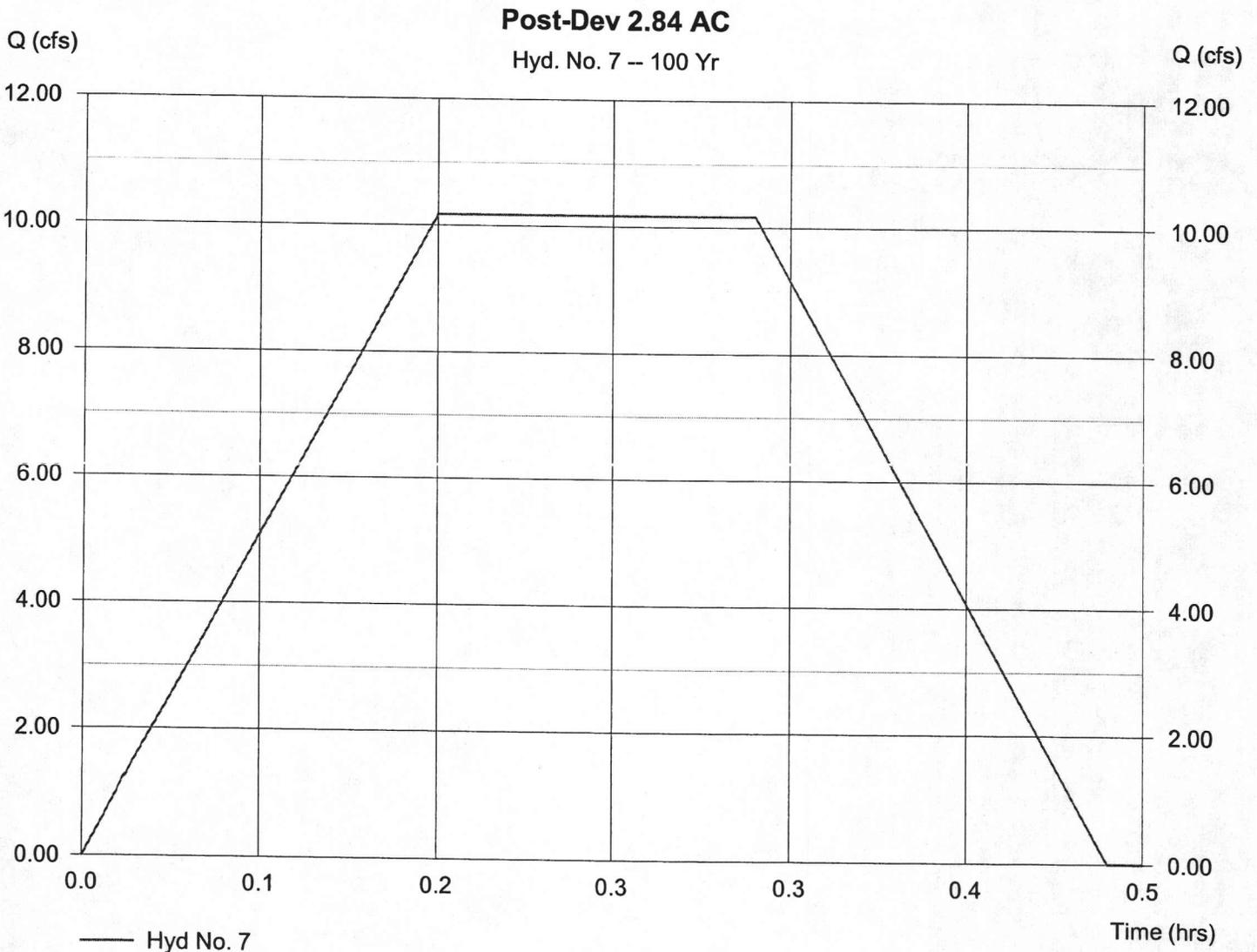
## Hyd. No. 7

Post-Dev 2.84 AC

Hydrograph type = Mod. Rational  
Storm frequency = 100 yrs  
Drainage area = 2.8 ac  
Intensity = 6.069 in/hr  
IDF Curve = JamesCity-NW-14.IDF

Peak discharge = 10.17 cfs  
Time interval = 1 min  
Runoff coeff. = 0.59  
Tc by User = 10 min  
Storm duration = 1.97 x Tc

Hydrograph Volume = 12,020 cuft



# Hydrograph Plot

Hydraflow Hydrographs by Intellisolve

Tuesday, Aug 22 2006, 7:43 PM

## Hyd. No. 8

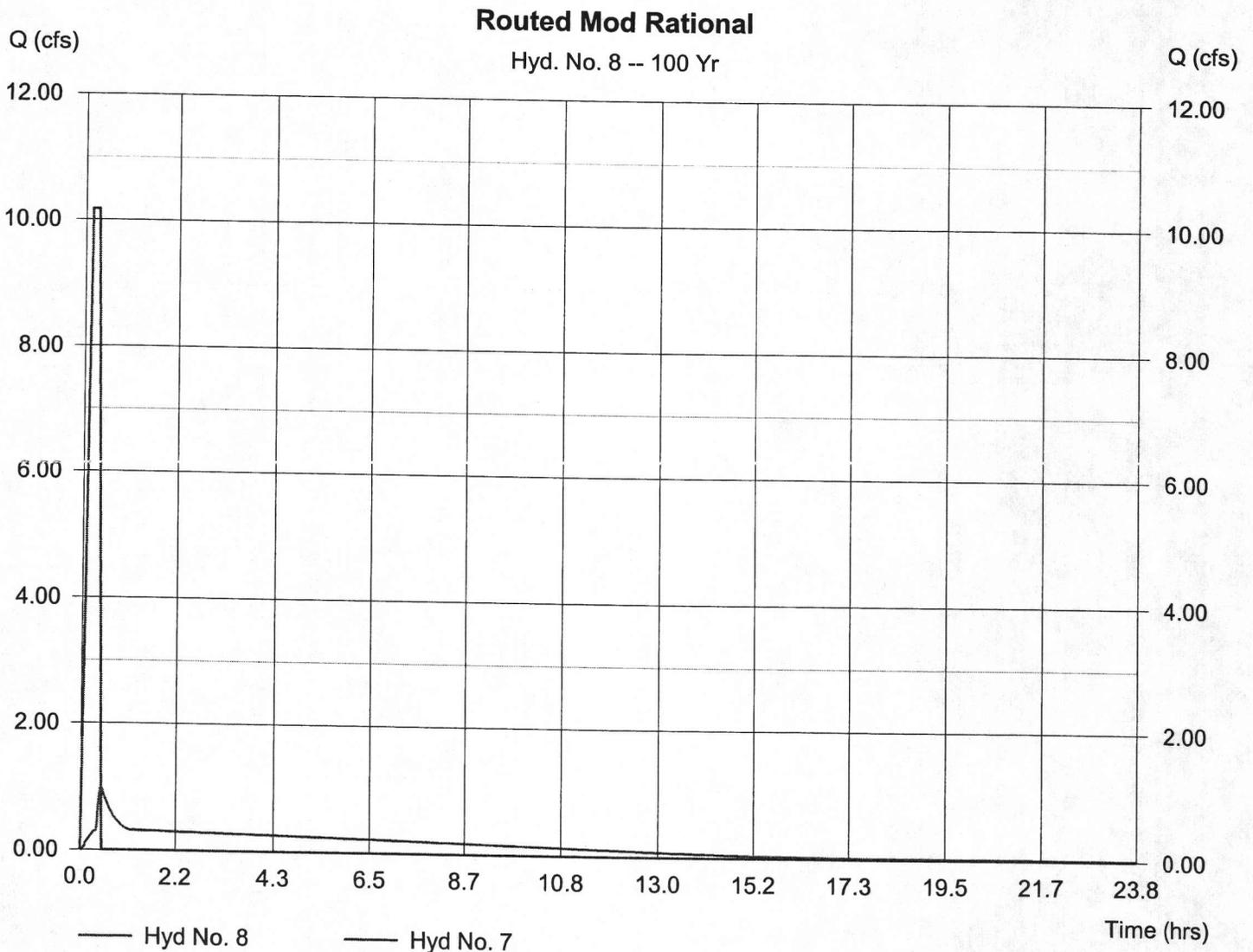
Routed Mod Rational

Hydrograph type = Reservoir  
Storm frequency = 100 yrs  
Inflow hyd. No. = 7  
Reservoir name = JRBC Pond

Peak discharge = 0.99 cfs  
Time interval = 1 min  
Max. Elevation = 86.11 ft  
Max. Storage = 17,184 cuft

Storage Indication method used. Wet pond routing start elevation = 84.00 ft.

Hydrograph Volume = 11,570 cuft



# Pond Report

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 22 2006, 7:43 PM

## Pond No. 1 - JRBC Pond

### Pond Data

Pond storage is based on known contour areas. Average end area method used.

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	81.00	1,044	0	0
1.00	82.00	1,464	1,254	1,254
2.00	83.00	1,940	1,702	2,956
3.00	84.00	4,362	3,151	6,107
4.00	85.00	5,181	4,772	10,879
4.90	85.90	5,910	4,991	15,869
5.00	86.00	6,023	597	16,466
5.90	86.90	6,910	5,820	22,286
6.00	87.00	6,996	695	22,981

### Culvert / Orifice Structures

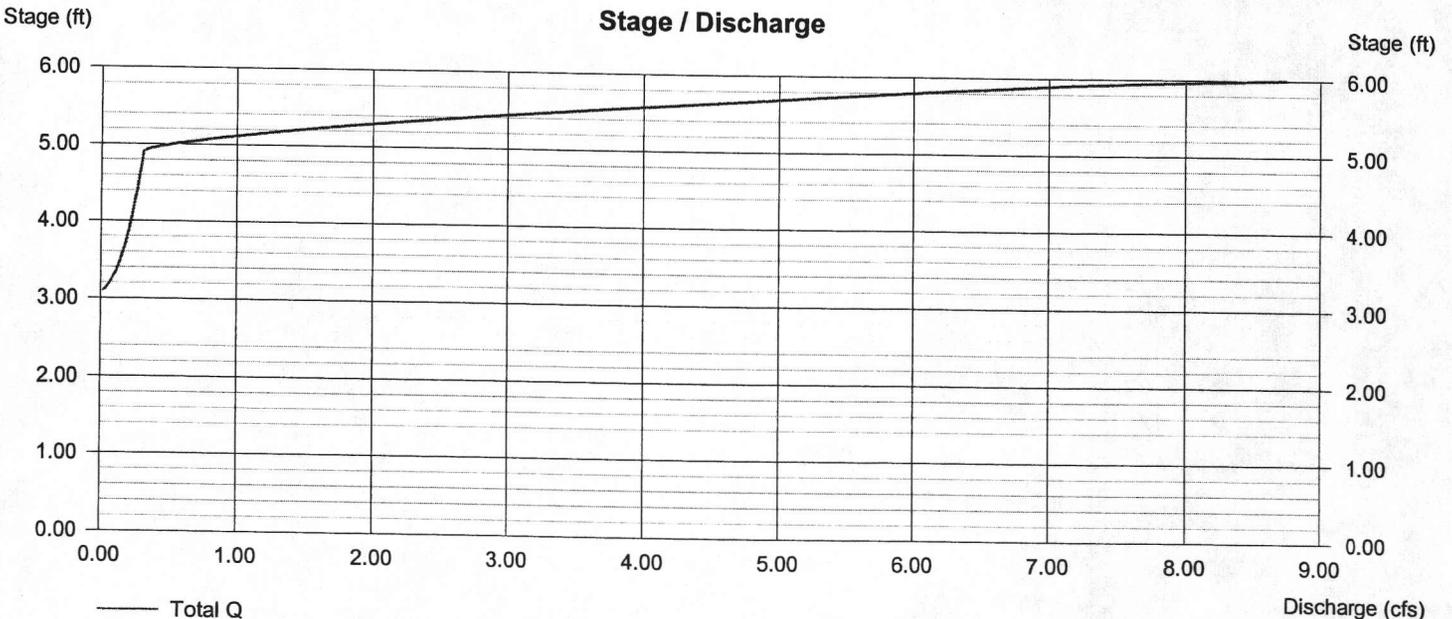
	[A]	[B]	[C]	[D]
Rise (in)	= 15.00	3.00	0.00	0.00
Span (in)	= 15.00	3.00	0.00	0.00
No. Barrels	= 1	1	0	0
Invert El. (ft)	= 80.20	84.00	0.00	0.00
Length (ft)	= 30.00	0.00	0.00	0.00
Slope (%)	= 0.50	0.00	0.00	0.00
N-Value	= .013	.013	.000	.000
Orif. Coeff.	= 0.60	0.60	0.00	0.00
Multi-Stage	= n/a	Yes	No	No

### Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 2.00	8.00	0.00	0.00
Crest El. (ft)	= 85.90	86.90	0.00	0.00
Weir Coeff.	= 3.33	2.60	3.33	0.00
Weir Type	= Riser	Broad	---	---
Multi-Stage	= Yes	Yes	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

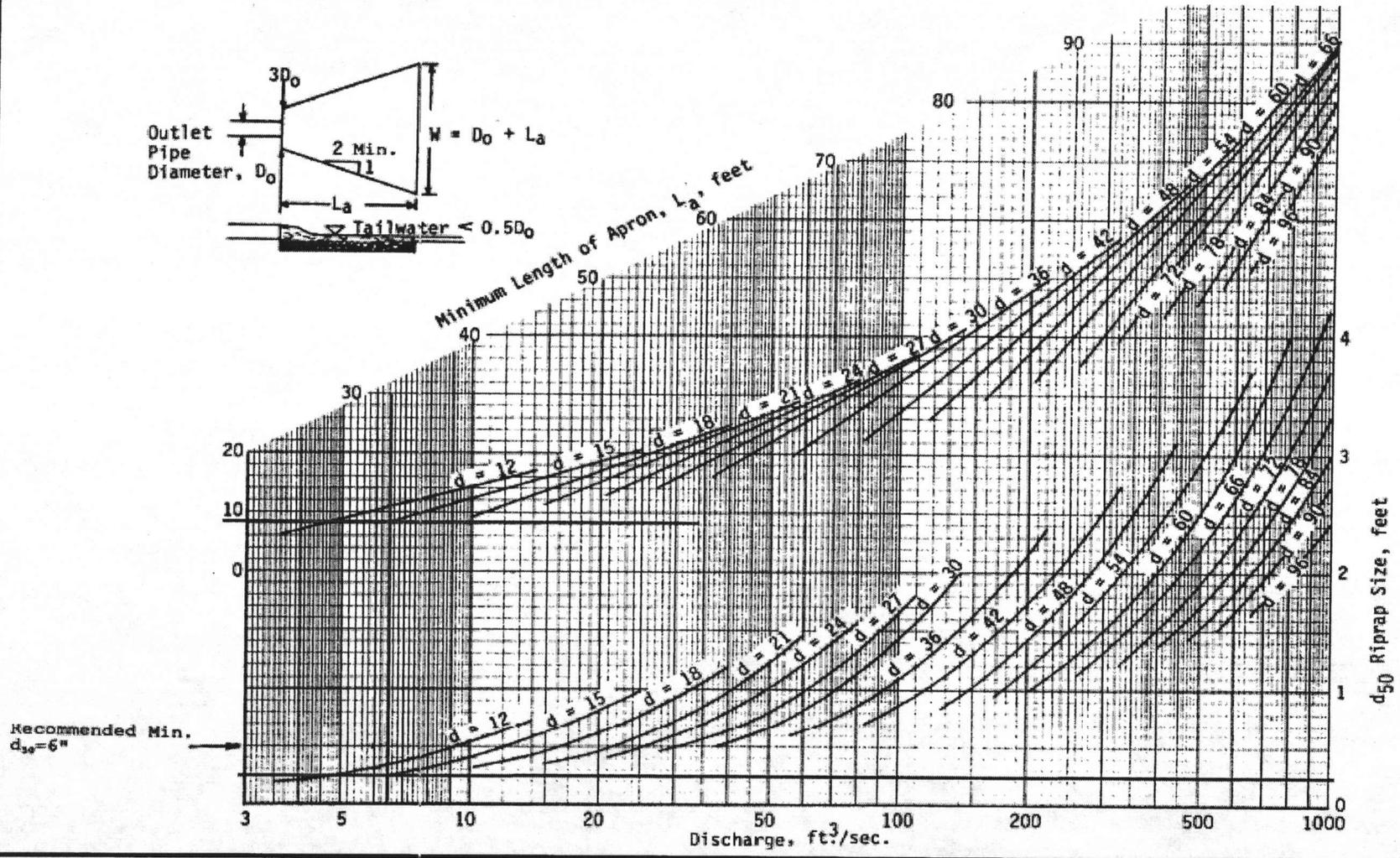
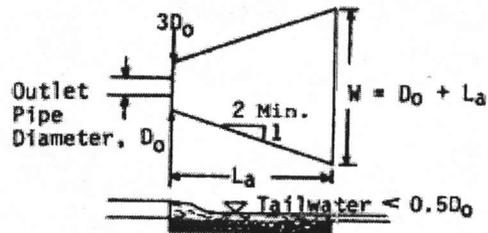
Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.



### Outlet Location: BMP Outfall ( 15" RCP )

DESIGN OF OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL  
 MINIMUM TAILWATER CONDITION ( $T_w < 0.5$  DIAMETER)

Source: USDA-SCS



III - 164

Plate 3.18-3

1992

3.18

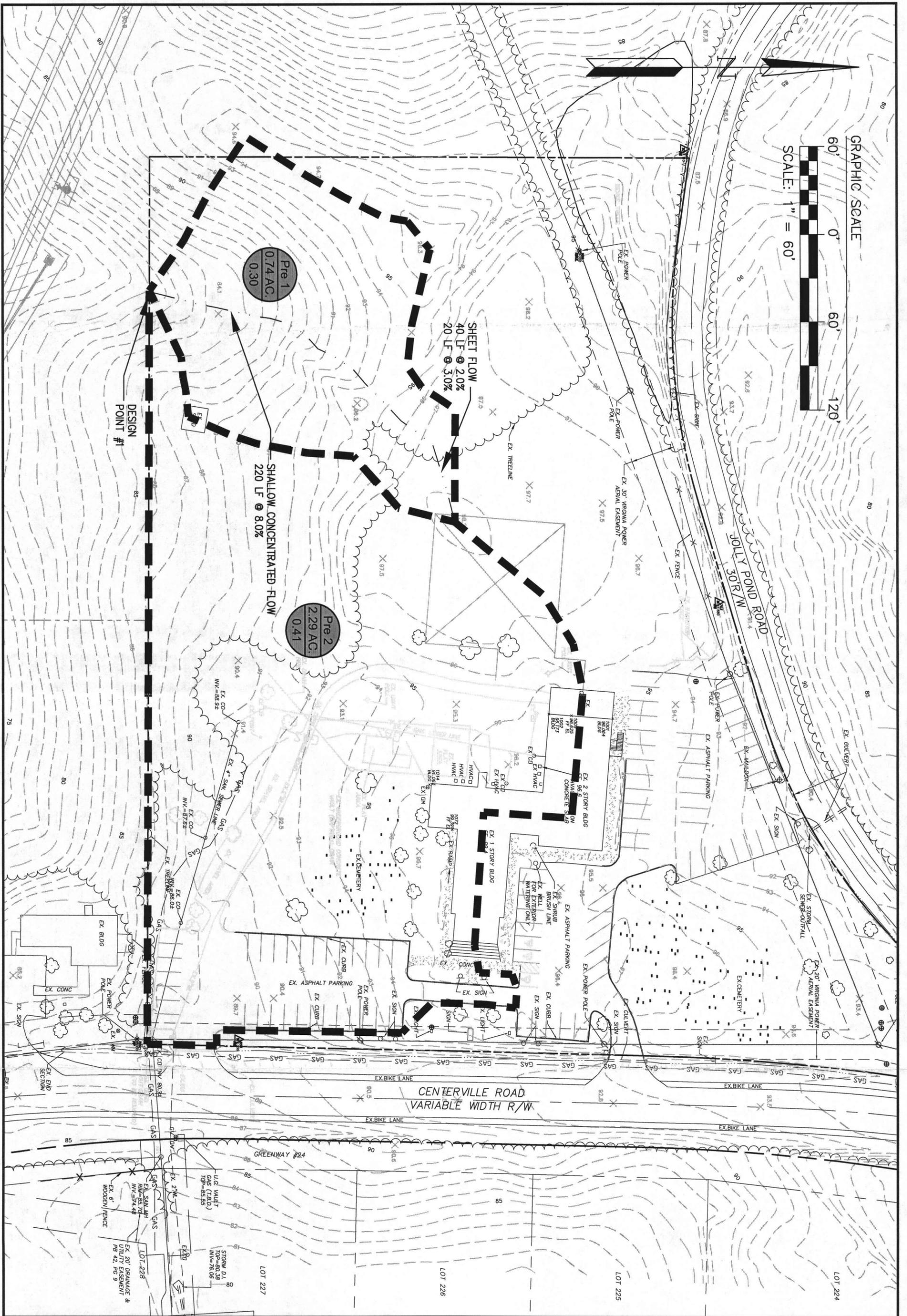
$Q = 6.5$  cfs  
 $D_0 = 15$  in

$3D_0 = 45$  in  
 $L_a = 9$  ft

$W = 10$  ft  
 $d_{50} = 1.1$  ft

Depth = 2.5 ft

**DRAINAGE AREA MAPS**



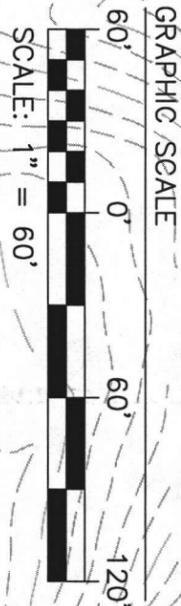
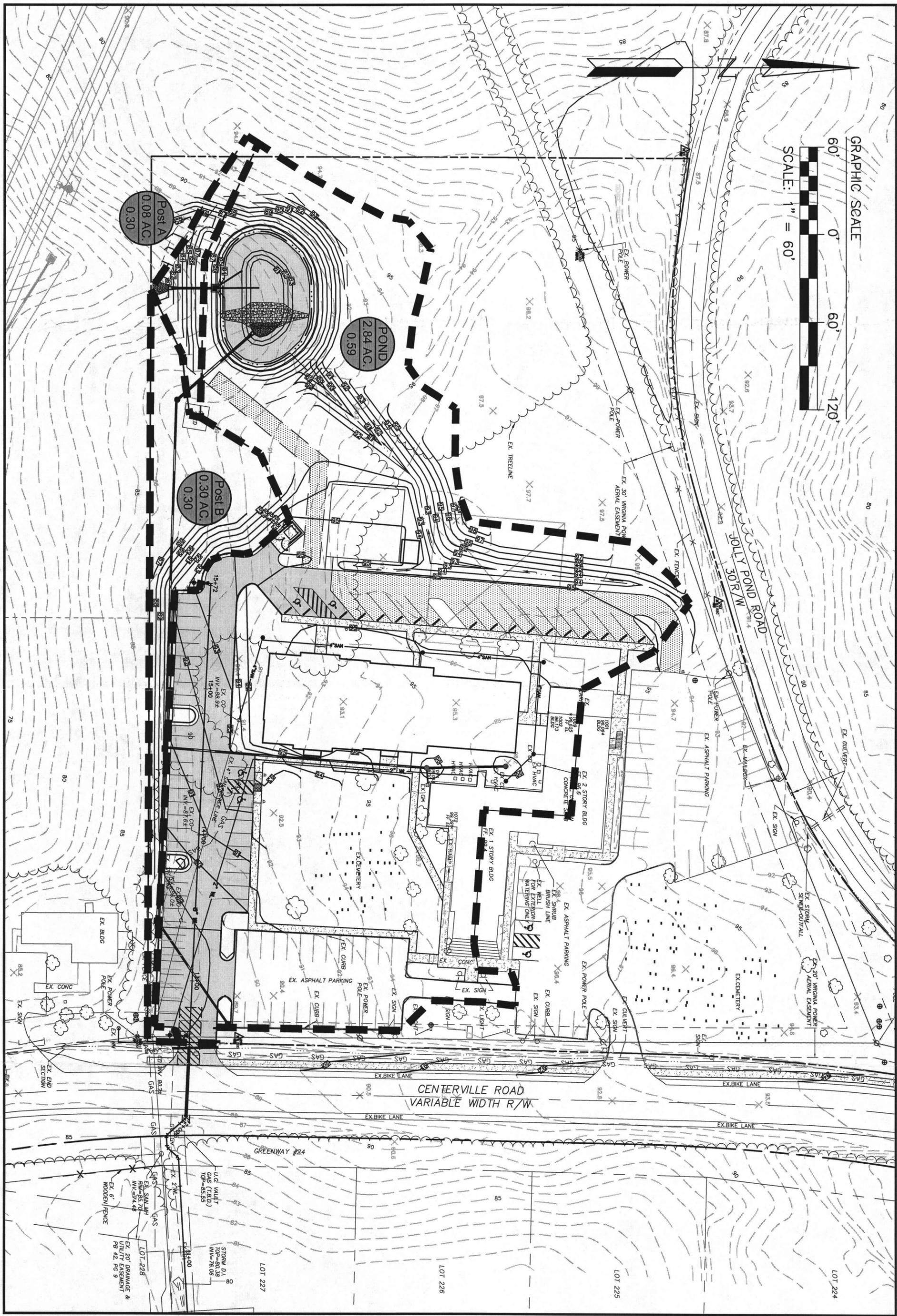
**PRE-DEVELOPMENT**  
**MULTI-MINISTRY BUILDING**  
**JAMES RIVER BAPTIST CHURCH**  
 POWHATAN DISTRICT    JAMES CITY COUNTY    VIRGINIA

**ES**  
**CONSULTING ENGINEERS**  
 WILLIAMSBURG • RICHMOND • GLOUCESTER

5248 Olde Towne Road, Suite 1  
 Williamsburg, Virginia 23188  
 (757) 253-0040  
 Fax (757) 220-8994

No.	DATE	REVISION / COMMENT / NOTE	REVISION BY	REVIEWED BY

Designed NB Scale 1"=60' Project No. 9552-00 Drawing No. 1	Drawn LBA Date 8/23/06
---	---------------------------------



POST-DEVELOPMENT	
MULTI-MINISTRY BUILDING	
JAMES RIVER BAPTIST CHURCH	
POWhatan DISTRICT	JAMES CITY COUNTY VIRGINIA
Designed NB	Drawn LBA
Scale 1"=60'	Date 8/22/06
Project No. 9552-00	
Drawing No. 2	



5248 Olde Towne Road, Suite 1  
 Williamsburg, Virginia 23188  
 (757) 253-0040  
 Fax (757) 220-8994

No.	DATE	REVISION / COMMENT / NOTE	REVIEWED BY	DESIGNED BY



**INLET DRAINAGE AREAS**  
**MULTI-MINISTRY BUILDING**  
**JAMES RIVER BAPTIST CHURCH**

POWHATAN DISTRICT    JAMES CITY COUNTY    VIRGINIA

Designed NB	Drawn LBA	Date 8/23/06	
Scale 1"=60'	Project No. 9352-00	Drawing No. 3	

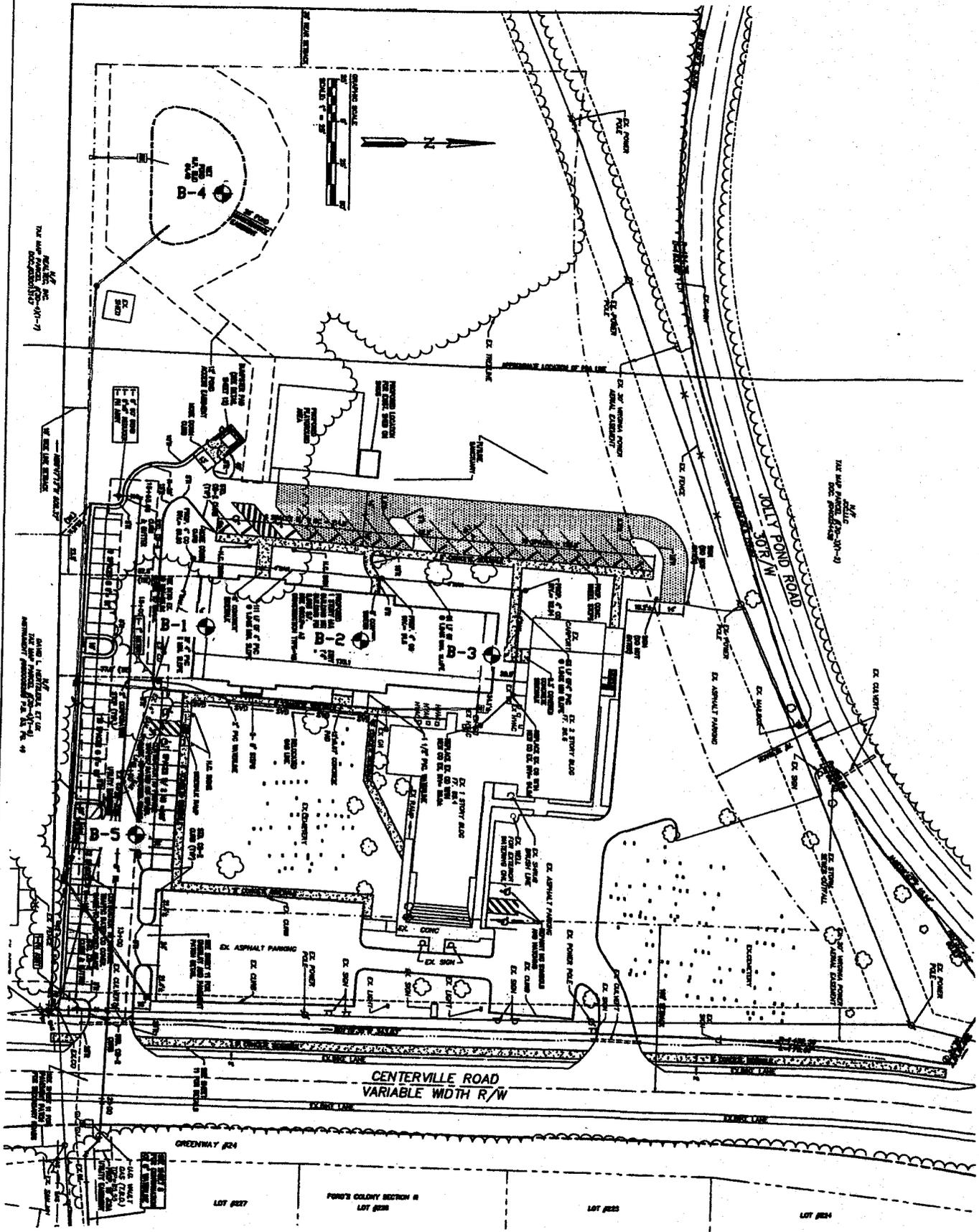
**ES**  
**CONSULTING ENGINEERS**

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 Williamsburg, Virginia 23188  
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 Fax (757) 220-8994

No.	DATE	REVISION / COMMENT / NOTE	REVISED BY	REVIEWED BY

**APPENDIX I**  
**BORING LOCATION PLAN**



**LEGEND:**

⊙ - APPROX BORING LOCATION

\*Base Plan provided by AES Consulting Engineers, Inc.

DATE	07/23/06
SHEET	1
PROJECT NO.	8494
SCALE	NTS
ENGINEER	DAWSON
ARCHITECT	RNL
DATE	
REVISIONS	

**BORING  
LOCATION PLAN**



**James River Baptist  
Additions  
James City County, Virginia**

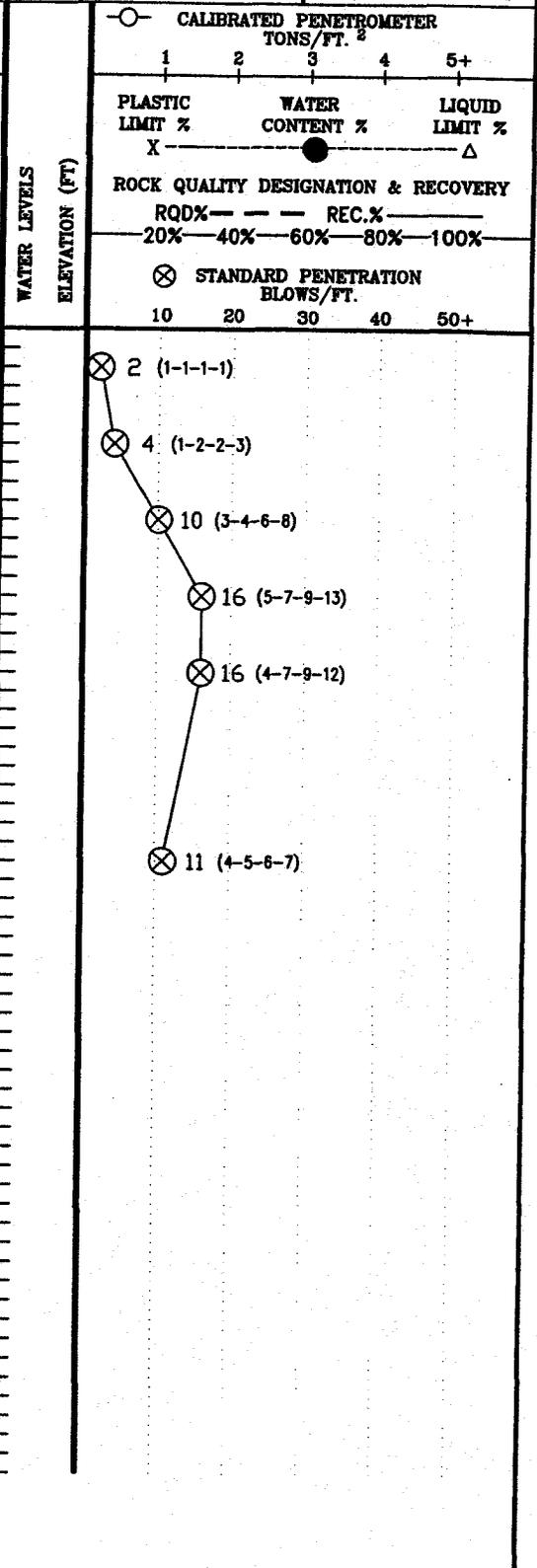
**APPENDIX II**  
**SOIL TEST BORING LOGS**

CLIENT <b>AES</b>	JOB # <b>8494</b>	BORING # <b>B-1</b>	SHEET <b>1 OF 1</b>
PROJECT NAME <b>James River Baptist Additions</b>		ARCHITECT-ENGINEER	



SITE LOCATION  
**James City County, Virginia**

DEPTH (FT)	SAMPLE NO.	SAMPLE TYPE	SAMPLE DISTANCE (IN)	RECOVERY (IN)	DESCRIPTION OF MATERIAL
					ENGLISH UNITS
0					SURFACE ELEVATION
0	1	SS	24	24	TOPSOIL DEPTH 2"
1	2	SS	24	24	Fine to Medium Clayey SAND, Brown to Orange-Brown, Moist, Very Loose to Loose, (SC)
2					
3	3	SS	24	24	Sandy CLAY, Orange-Brown, Moist, Very Stiff, (CL)
4	4	SS	24	24	
5	5	SS	24	24	
15	6	SS	24	24	Fine to Medium Clayey SAND, Orange-Brown with Light Brown Mottling, Moist, Medium Dense, (SC)
END OF BORING @ 15.00'					



RNL (07-05-06) RNL (07-05-06) RNL (07-05-06) RNL (07-25-06)

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES IN-SITU THE TRANSITION MAY BE GRADUAL

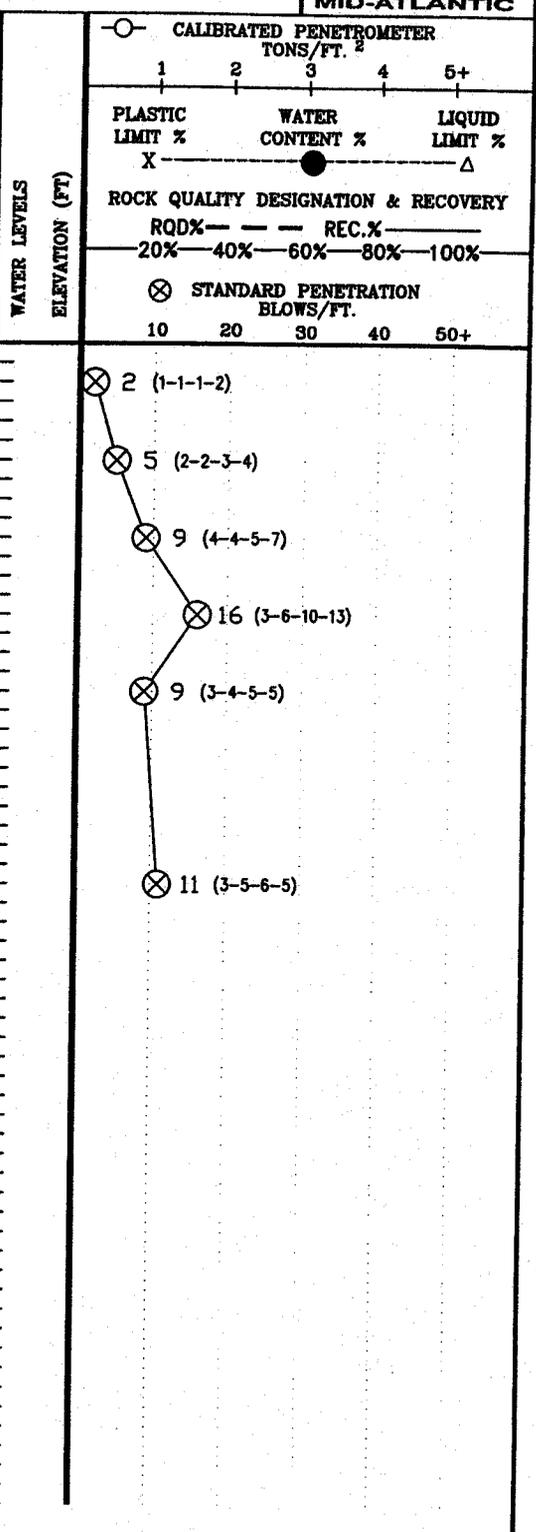
∇ WL DRY ∇ WL(AB) DRY    ∇ WL(AC) DRY ∇ WL	WS OR (ID) BORING STARTED <b>6/21/06</b> BORING COMPLETED <b>6/21/06</b> RIG ATV                      FOREMAN SDS	CAVE IN DEPTH ● 15.0 DRILLING METHOD AUGER
--	--	---

CLIENT <b>AES</b>	JOB # <b>8494</b>	BORING # <b>B-2</b>	SHEET <b>1 OF 1</b>
PROJECT NAME <b>James River Baptist Additions</b>		ARCHITECT-ENGINEER	



SITE LOCATION  
**James City County, Virginia**

DEPTH (FT)	SAMPLE NO.	SAMPLE TYPE	SAMPLE DISTANCE (IN)	RECOVERY (IN)	DESCRIPTION OF MATERIAL
					ENGLISH UNITS
0					SURFACE ELEVATION
0	1	SS	24	24	TOPSOIL DEPTH 2"
1	2	SS	24	24	Fine to Medium Clayey SAND, Brown, Moist, Very Loose, (SC)
2	3	SS	24	24	Sandy CLAY, Orange-Brown, Moist, Medium Stiff, (CL)
3	4	SS	24	24	Fine to Medium Clayey SAND, Orange-Brown with Red-Brown Mottling, Moist, Loose, (SC)
4	5	SS	24	24	Sandy CLAY, Orange-Brown with Red-Brown Mottling, Moist, Very Stiff, (CL)
5					Fine to Medium Clayey SAND, Orange-Brown, Moist, Medium Dense, (SC)
6	6	SS	24	24	Sandy CLAY, Light Brown with Gray Mottling, Moist, Stiff, (CL)
15					END OF BORING @ 15.00'



RNL (07-05-06) RNL (07-05-06) RNL (07-05-06) RNL (07-05-06) RNL (07-05-06)

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES IN-SITU THE TRANSITION MAY BE GRADUAL

▽ WL DRY	WS OR <b>TD</b>	BORING STARTED	<b>6/21/06</b>
▽ WL(AB) DRY	▽ WL(AC) DRY	BORING COMPLETED	<b>6/21/06</b>
▽ WL	RIG ATV	FOREMAN SDS	DRILLING METHOD AUGER

CAVE IN DEPTH @ 15.0

CLIENT <b>AES</b>	JOB # <b>8494</b>	BORING # <b>B-3</b>	SHEET <b>1 OF 1</b>	<b>ECS LLC</b> MID-ATLANTIC
PROJECT NAME <b>James River Baptist Additions</b>	ARCHITECT-ENGINEER			

SITE LOCATION  
**James City County, Virginia**

○ CALIBRATED PENETROMETER  
TONS/FT.<sup>2</sup>

1 2 3 4 5+

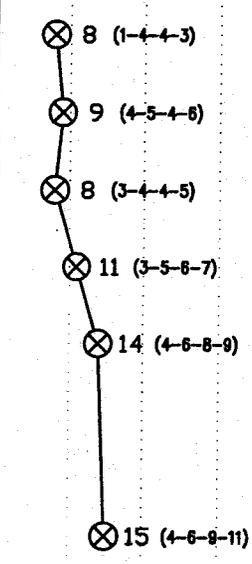
PLASTIC LIMIT % WATER CONTENT % LIQUID LIMIT %  
X ● Δ

ROCK QUALITY DESIGNATION & RECOVERY  
RQD% — — — REC.% — — —  
20% 40% 60% 80% 100%

⊗ STANDARD PENETRATION BLOWS/FT.  
10 20 30 40 50+

DEPTH (FT)	SAMPLE NO.	SAMPLE TYPE	SAMPLE DISTANCE (IN)	RECOVERY (IN)	DESCRIPTION OF MATERIAL
					ENGLISH UNITS
0					SURFACE ELEVATION
0	1	SS	24	18	TOPSOIL DEPTH 2"
0	2	SS	24	20	Fine to Medium Clayey SAND, Trace Fine Gravel, Light Brown, Moist, Loose, (SC)
5	3	SS	24	24	Sandy CLAY, Light Brown to Light Brown with Orange-Brown Mottling, Moist, Medium Stiff to Stiff, (CL)
5	4	SS	24	24	
10	5	SS	24	24	Fine Medium Clayey SAND, Brown with Red-Brown Mottling, Moist, Medium Dense, (SC)
15	6	SS	24	24	Sandy CLAY, Orange-Brown with Gray and Red-Brown, Moist, Very Stiff, (CL)
15	END OF BORING @ 15.00'				

WATER LEVELS  
ELEVATION (FT)



RNL (07-05-06) RNL (07-05-06) RNL (07-05-06) RNL (07-25-06)

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES IN-SITU THE TRANSITION MAY BE GRADUAL

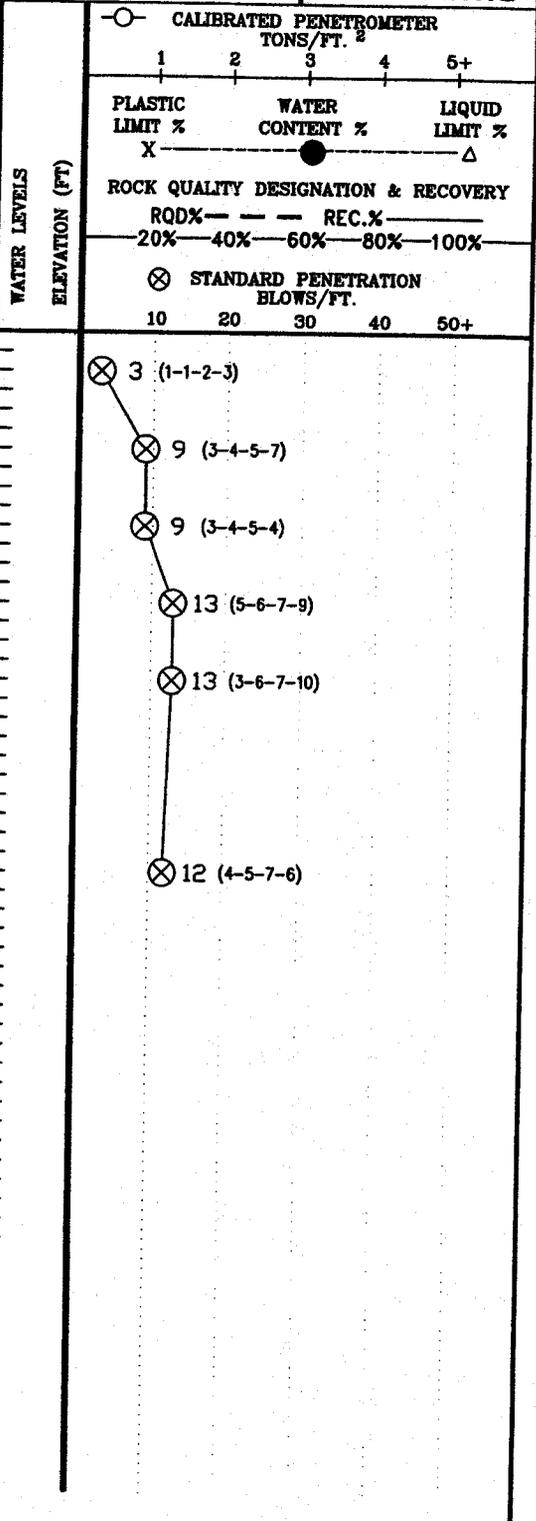
▽WL DRY	WS OR (TD)	BORING STARTED	6/21/06	
▽WL(AB) DRY	▽WL(AC) DRY	BORING COMPLETED	6/21/06	CAVE IN DEPTH @ 15.0
▽WL		RIG ATV	FOREMAN SDS	DRILLING METHOD AUGER

CLIENT <b>AES</b>	JOB # <b>8494</b>	BORING # <b>B-4</b>	SHEET <b>1 OF 1</b>
PROJECT NAME <b>James River Baptist Additions</b>	ARCHITECT-ENGINEER		



SITE LOCATION  
**James City County, Virginia**

DEPTH (FT)	SAMPLE NO.	SAMPLE TYPE	SAMPLE DISTANCE (IN)	RECOVERY (IN)	DESCRIPTION OF MATERIAL
					ENGLISH UNITS
					SURFACE ELEVATION
0	1	SS	24	24	TOPSOIL DEPTH 3"
	2	SS	24	24	Fine to Medium Clayey SAND, Light Brown with Dark Brown Mottling to Light Brown, Very Loose to Loose, (SC)
	3	SS	24	24	
5	4	SS	24	24	
	5	SS	24	24	Sandy CLAY, Light Brown with Orange-Brown Mottling to Orange-Brown with Gray and Red-Brown Mottling, Moist, Stiff, (CL)
10	6	SS	24	24	
15	END OF BORING @ 15.00'				



RNL (07-05-06) RNL (07-05-06) RNL (07-05-06) RNL (07-25-06)

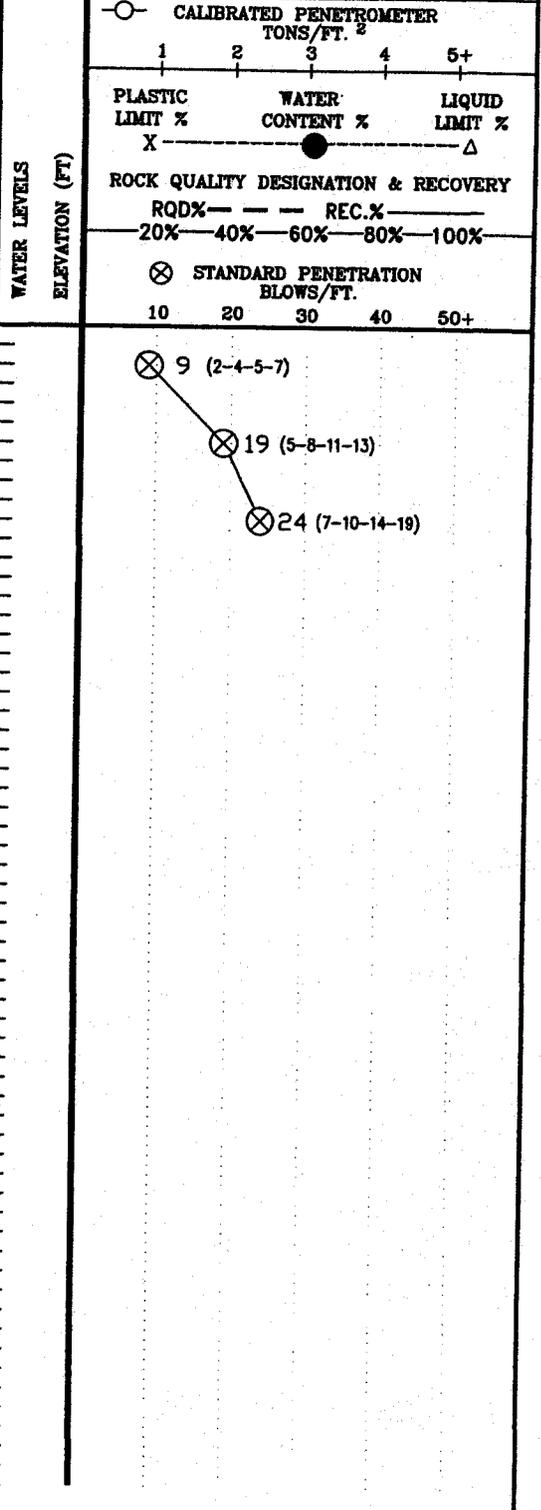
THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES IN-SITU THE TRANSITION MAY BE GRADUAL

∇ WL DRY	WS OR (D)	BORING STARTED	6/21/06	
∇ WL(AB) DRY	∇ WL(AC) DRY	BORING COMPLETED	6/21/06	CAVE IN DEPTH ● 15.0
∇ WL		RIG ATV	FOREMAN SDS	DRILLING METHOD AUGER

CLIENT <b>AES</b>	JOB # <b>8494</b>	BORING # <b>B-5</b>	SHEET <b>1 OF 1</b>	<b>ECS LLC</b> MID-ATLANTIC
PROJECT NAME <b>James River Baptist Additions</b>	ARCHITECT-ENGINEER			

SITE LOCATION  
**James City County, Virginia**

DEPTH (FT)	SAMPLE NO.	SAMPLE TYPE	SAMPLE DISTANCE (IN)	RECOVERY (IN)	DESCRIPTION OF MATERIAL
					ENGLISH UNITS
0					SURFACE ELEVATION
0	1	SS	24	24	TOPSOIL DEPTH 1"
2	2	SS	24	21	Sandy CLAY, Orange-Brown with Gray and Red-Brown Mottling, Moist, Medium Stiff to Very Stiff, (CL)
5	3	SS	24	24	
6.00	END OF BORING @ 6.00'				



RNL (07-05-06) RNL (07-05-06) RNL (07-05-06) RNL (07-25-06)

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES IN-SITU THE TRANSITION MAY BE GRADUAL

▽ WL DRY	WS OR (D)	BORING STARTED	6/21/06	
▽ WL(AB) DRY	▽ WL(AC) DRY	BORING COMPLETED	6/21/06	CAVE IN DEPTH ● 15.0
▽ WL		RIG ATV	FOREMAN SDS	DRILLING METHOD AUGER

**APPENDIX III**

**LABORATORY TEST SUMMARY**

# **POOR QUALITY**

**ORIGINAL(S) FOLLOW**

**THIS IS THE BEST COPY  
AVAILABLE**

***VCE  
DOCUMENT  
CONVERSION***



**APPENDIX IV**

**UNIFIED SOIL CLASSIFICATION SYSTEM AND  
REFERENCE NOTES FOR BORING LOGS**

**POOR  
QUALITY**

**ORIGINAL(S)  
FOLLOW**

**THIS IS THE BEST  
COPY AVAILABLE**

**VCE DOCUMENT CONVERSION**

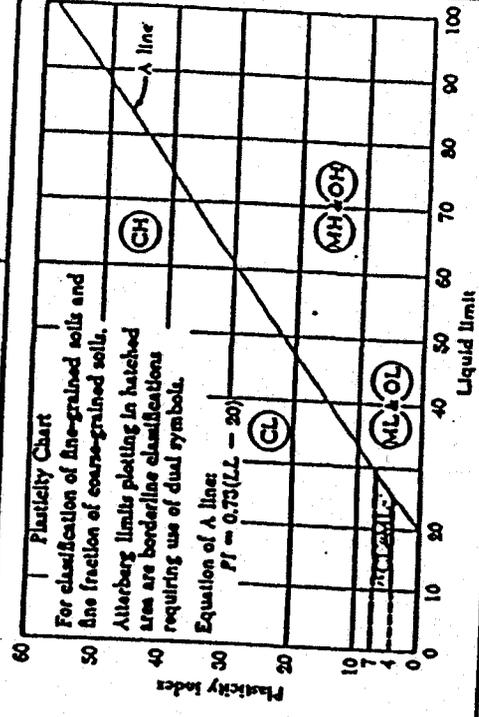
# UNIFIED SOIL CLASSIFICATION SYSTEM (USCS)

Table Unified System of Classification.

Major divisions		Group symbols	Typical names
Coarse-Grained Soils More than 50% retained on No. 200 sieve	Gravels 50% or more of coarse fraction retained on No. 4 sieve	Clean Gravels	Well-graded gravels and gravel-sand mixtures, little or no fines
		Gravels with Fines	Poorly graded gravels and gravel-sand mixtures, little or no fines
Fine-Grained Soils 50% or more passes No. 200 sieve	Sands More than 50% of coarse fraction passes No. 4 sieve	Clean Sands	Silty sands, gravel-sand-silt mixtures
		Sands with Fines	Clayey sands, gravel-sand-clay mixtures
	Sils and Clays Liquid limit 50% or less	ML	Well-graded sands and gravelly sands, little or no fines
		CL	Poorly graded sands and gravelly sands, little or no fines
Sils and Clays Liquid limit greater than 50%	Sils and Clays Liquid limit 50% or less	SM	Silty sands, sand-silt mixtures
		SC	Clayey sands, sand-clay mixtures
	Highly Organic Soils	MH	Inorganic silts, very fine sands, rock flour, silty or clayey fine sands
		ML, OL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays
Highly Organic Soils	Highly Organic Soils	MH, OH	Organic silts and organic silty clays of low plasticity
		HO	Inorganic silts, micaceous or diatomaceous fine sands or silts, elastic silts
Highly Organic Soils	Highly Organic Soils	CH	Inorganic clays of high plasticity, fat clays
		OH	Organic clays of medium to high plasticity
Highly Organic Soils	Highly Organic Soils	UL	Peat, muck, and other highly organic soils
		UL	Peat, muck, and other highly organic soils

Table (Continued)

Classification on basis of percentages of fines		Classification criteria	
Less than 5% pass No. 200 sieve GW, GP, SW, SP More than 15% pass No. 200 sieve GM, GC, SM, SC 5% to 15% pass No. 200 sieve Borrowline classification requiring use of dual symbols	Classification on basis of percentages of fines	$C_u = D_{60}/D_{10}$ Greater than 4	Classification criteria
		$C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Between 1 and 3	$C_u = D_{60}/D_{10}$ Greater than 4 $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Between 1 and 3
Not meeting both criteria for CW	Not meeting both criteria for CW	Atterberg limits plot below "A" line or plasticity index less than 4	Atterberg limits plotting in hatched area are borderline classifications requiring use of dual symbols
		Atterberg limits plot above "A" line and plasticity index greater than 7	Atterberg limits plotting in hatched area are borderline classifications requiring use of dual symbols
Not meeting both criteria for SW	Not meeting both criteria for SW	Atterberg limits plot below "A" line or plasticity index less than 4	Atterberg limits plotting in hatched area are borderline classifications requiring use of dual symbols
		Atterberg limits plot above "A" line and plasticity index greater than 7	Atterberg limits plotting in hatched area are borderline classifications requiring use of dual symbols



Visual-manual identification, see ASTM Designation D2488.

## REFERENCE NOTES FOR BORING LOGS

### I. Drilling and Sampling Symbols:

SS - Split Spoon Sampler	RB - Rock Bit Drilling
ST - Shelby Tube Sampler	BS - Bulk Sample of Cuttings
RC - Rock Core: NX, BX, AX	PA - Power Auger (no sample)
PM - Pressuremeter	HSA - Hollow Stem Auger
DC - Dutch Cone Penetrometer	WS - Wash Sample

Standard Penetration (Blows/Ft) refers to the blows per foot of a 140 lb. hammer falling 30 inches on a 2 in. O.D. splitspoon sampler, as specified in ASTM D-1586. The blow count is commonly referred to as the N value.

### II. Correlation of Penetration Resistances to Soil Properties:

<u>Relative Density-Sands, Silts</u>		<u>Consistency of Cohesive Soils</u>	
<u>SPT-N</u>	<u>Relative Density</u>	<u>Unconfined Compressive Strength, Op. tsf</u>	<u>Consistency</u>
0 - 3	Very Loose	Under 0.25	Very Soft
4 - 9	Loose	0.25 - 0.49	Soft
10 - 29	Medium Dense	0.50 - 0.99	Firm
30 - 49	Dense	1.00 - 1.99	Stiff
50 - 80	Very Dense	2.00 - 3.99	Very Stiff
over 80	Extremely Dense	4.00 - 8.00	Hard
		over 8.00	Very Hard

### III. Unified Soil Classification Symbols:

GP - Poorly Graded Gravel	ML - Low Plasticity Silts
GW - Well Graded Gravel	MH - High Plasticity Silts
GM - Silty Gravel	CL - Low Plasticity Clays
GC - Clayey Gravels	CH - High Plasticity Clays
SP - Poorly Graded Sands	OL - Low Plasticity Organics
SW - Well Graded Sands	OH - High Plasticity Organics
SM - Silty Sands	CL-ML - Dual Classification
SC - Clayey Sands	(Typical)

### IV. Water Level Measurement Symbols:

WL - Water Level	BCR - Before Casing Removal
WS - While Sampling	ACR - After Casing Removal
WD - While Drilling	WCI - Wet Cave In
	DCI - Dry Cave In

The water levels are those water levels actually measured in the borehole at the times indicated by the symbol. The measurements are relatively reliable when augering, without adding fluids, in a granular soil. In Clays and Plastic Silts the accurate determination of water levels may require several days for the water level to stabilize. In such cases additional methods of measurement are generally applied.

ECS MID-ATLANTIC, LLC  
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(757) 229-6677

**AES CONSULTING ENGINEERS**  
**Engineering, Surveying, and Planning**  
 5248 Olde Towne Road, Suite 1  
 Williamsburg, VA 23188

**Phone: (757) 253-0040**  
**Fax: (757) 220-8994**

# LETTER OF TRANSMITTAL

**ATTN: Tina Cooke/Bill Cain**  
 JCC Environmental Division  
 Environmental Inspector

**CO.:** \_\_\_\_\_  
 101-E Mounts Bay Road  
 P.O Box. 8784  
**Address:** Williamsburg, Virginia 23187-8784

**cc:** \_\_\_\_\_  
 Joe Salama – S-Works

<b>DATE</b> 8/26/2008	<b>JOB NO.</b> 9552-01
<b>FROM:</b> Matt Good	
<b>RE</b> James River Baptist Church BMP Record Drawings	



WE ARE SENDING YOU THE FOLLOWING ITEMS:

- Attached  
 Under separate cover via  
 Original(s)     Print(s)     Plan(s)     Specification(s)     Change Order  
 Copy of letter(s)     Other:

COPIES	DATE	No. of Pages	DESCRIPTION
2	7/31/08	3	James River Baptist Church BMP Record Drawings
1		3	BMP Certification

THESE ARE TRANSMITTED as checked below:

- For your approval     For your signature     For review and comment  
 For your use     As you requested     As requested by:  
 Other:

REMARKS:

VIA:  Hand Deliver     UPS Ground     UPS Next Day Air     USPS Mail     Other:

*If enclosures are not as noted, kindly notify us at once.*

## Tina Cooke

---

**From:** s-works construction [joe@s-works-gc.com]  
**Sent:** Tuesday, December 02, 2008 8:41 AM  
**To:** Tina Cooke; 'Chris Cuthbertson'  
**Cc:** 'Abbott, Bruce'; dreed903@aol.com; WJR24@MSN.COM; 'Jeff Clark'  
**Subject:** RE: Bond Status For James River Baptist Church

Tina:

Thank you for your prompt response! In talking with Wayne Reed this AM he is aware of these issues and he is correcting them ALL today and will schedule a re-inspection with you prior to the end of this week. Again thank you for addressing our bond release as you have done here

Joseph D. Salama  
President

---

### S-Works Construction Corp.

---

310 Barlow Rd.  
Williamsburg, VA 23188  
O (757) 565-7377  
C (703) 774-4727  
F (757) 565-7378  
[www.s-works-gc.com](http://www.s-works-gc.com)



---

**From:** Tina Cooke [mailto:TCooke@james-city.va.us]  
**Sent:** Tuesday, December 02, 2008 6:27 AM  
**To:** 'Chris Cuthbertson'  
**Cc:** 's-works construction'; 'Abbott, Bruce'; dreed903@aol.com; 'WJR24@MSN.COM'  
**Subject:** RE: Bond Status For James River Baptist Church

Chris,

Wayne Reed requested the final inspection on 11/20/08 and upon inspection I found the following minor issues that need to be addressed prior to bond release;

- The valve in the drainage structure needs to be closed completely. Otherwise, we may have a issue with seepage.
- Erosion was present at the rip rap channel. Rip rap is placed prior to the filter fabric (approximately 1') and water is cutting beneath the rip rap. I suggested that they place the rip rap on the fabric and stabilize the channel to prevent this erosion issue.
- A small place within the drainage channel to the BMP is holding water for more than 48 hours and needs to be re-graded and stabilized.

I spoke to Wayne about these needs and he indicated that he would call for re-inspection once these issues were addressed. Should you have any additional questions, feel free to contact me for clarification.

*Tina Cooke*  
*Environmental Inspector*  
*James City Environmental Division*  
*(757) 253-6743*

---

**From:** Chris Cuthbertson [mailto:chris@s-works-gc.com]  
**Sent:** Monday, December 01, 2008 5:10 PM  
**To:** Tina Cooke  
**Cc:** 's-works construction'  
**Subject:** Bond Status For James River Baptist Church

Tina,

Joe asked me to send you an email in regard to James River Baptist Church project. He would like to know what the status is on the bond for the erosion control. If you could let us know we would greatly appreciate it. Thanks and I hope you had a nice Thanksgiving holiday.

Chris Cuthbertson  
Project Manager

---

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## Tina Cooke

---

**From:** Tina Cooke  
**Sent:** Thursday, March 13, 2008 3:51 PM  
**To:** 's-works construction'  
**Cc:** Joe Buchite  
**Subject:** RE: S-WORKS PROJECT #2706 JRBC PROJECT COMPLETION DATE

Mr. Salama,

I conducted a preliminary inspection today and have listed the site needs below that will be necessary prior to bond release.

- Site stabilization – this includes the area adjacent to the sidewalk (VDOT ROW), utility disturbance areas, and around the building.
- Landscaping completed according to approved plan.
- Construction certifications & record drawings submitted to our office for review – Basin needs to be converted from trap mode – refer to sheet 7 on approved plan for details.
- Removal of E&S control measures after you have achieved site stabilization.

Should you have any questions, please contact my office for clarification.

*Tina Cooke*  
*Environmental Inspector*  
*James City Environmental Division*  
*(757) 253-6743*

---

**From:** s-works construction [mailto:joe@s-works-gc.com]  
**Sent:** Wednesday, March 12, 2008 3:30 PM  
**To:** Tina Cooke; Tom Coghill; Joe Basilone  
**Subject:** FW: S-WORKS PROJECT #2706 JRBC PROJECT COMPLETION DATE

WJCC team FYI please see below

Joseph D. Salama  
President

---

**S-Works Construction Corp.**

---

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---

**From:** s-works construction [mailto:joe@s-works-gc.com]

**Sent:** Tuesday, March 11, 2008 3:31 PM

**To:** 'Grant Owens'; 'Herbert Rowe'; 'Butch Duell'; 'Steve Haerbig'

**Cc:** 'Michael Cooke'; 'judith'; 'danyelle@s-works-gc.com'; 'dreed903@aol.com'; 'dreed903@msn.com'; 'Denley Brown'; 'Peters370@aol.com'; 'Bill Ahl'; 'jglazier@urbannabuilders.com'; 'motox8@cavtel.net'; 'motox8@verizon.net'; 'Jeff McManigal'; 'dan@dudleyroofingcorp.com'; 'meunice@cablefirst.com'; 'LaFlam, Shanan'; 'mnissen@pella386.com'; 'Glenn Davis'; 'alex@vanarcop.hrcoxmail.com'

**Subject:** S-WORKS PROJECT #2706 JRBC PROJECT COMPLETION DATE

S-Works Subcontractor Project Team:

First of all thank you for a project that is shaping up and looking great (a project we can ALL be proud of!) especially from Centerville Road! **Our project Completion date goal is 04-30-2008** project complete with CofO and bonds released! Please check in with Project Superintendent Mike Cooke to ensure we can meet this date for the church! This completion is critical because the church has a very important ceremony due to the church anniversary of 105 years! This completion is NOT unrealistic any issue must be raised NOW that would prevent us from making this date!

FAX TO FL HAZLEWOOD

Sincerely:

Joseph D. Salama  
President

---

**S-Works Construction Corp.**

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PC145

PC079

PC197

GC008



**REPORT OF  
SUBSURFACE EXPLORATION  
AND GEOTECHNICAL ENGINEERING ANALYSIS**

**JAMES RIVER BAPTIST ADDITIONS  
JAMES CITY COUNTY, VIRGINIA**

**FOR**

**Mr. Bruce Abbitt**

**July 28, 2006**

**ECS Project No. 07:8494**



## **ECS MID-ATLANTIC, LLC**

**Geotechnical • Construction Materials • Environmental • Facilities**

July 28, 2006

Mr. Bruce Abbitt  
James River Baptist Church  
4931 Centerville Road  
Williamsburg, VA 23188

ECS Project No. 07:8494

Reference: Subsurface Exploration and Geotechnical Engineering Analysis  
James River Baptist Additions  
James City County, Virginia

Dear Mr. Price,

ECS Mid-Atlantic, LLC has completed a subsurface exploration and engineering evaluation of the above referenced project. This report presents the results of the subsurface exploration and engineering analyses for the proposed building, BMP and associated parking areas. This portion of the project has been completed in accordance with our proposal No. 07:12445 dated May 16, 2006, and authorized by you.

### **Introduction**

The project site is located at 4931 Centerville Road in Williamsburg, Virginia. We understand the project will consist of the construction of a new 9,683 sf single story Multi Ministry Building at the existing church complex, a new BMP, and parking areas. The area within the proposed building footprint is grass covered, the parking area is grass covered with small trees and shrubs, and the BMP is in a moderately to heavily wooded area. Building loads have not been provided to us at the time of writing of this report, therefore we have assumed that column and wall foundation loadings will not exceed 75 kips and 4 kips per linear foot, respectively.

The purpose of this exploration was to explore the soil and groundwater conditions at the site and to develop soils-related engineering recommendations to guide design and construction of the planned buildings, and associated parking areas. Our investigation included drilling five (5) soil test borings within the at the site to explore the subsurface soil and groundwater conditions, performing a site reconnaissance to observe general topography, and analyzing field data to develop appropriate geotechnical engineering recommendations regarding the planned construction. A Boring Location Plan is included in Appendix I.

### **Field Exploration Procedures**

Three (3) soil test borings were drilled within the proposed building (B-1 through B-3), one (1) soil test boring was drilled within the proposed BMP (B-4), and one (1) soil test boring was drilled within the proposed parking areas. No subsurface bulk samples were taken for CBR testing within the access and parking areas. However, we have provided a pavement design section within this report based on visual classification, regional California Bearing Ratio test results, as well as our general engineering experience, and nearby soil borings performed within the building areas. The soil test borings were performed with an ATV mounted drill rig utilizing continuous flight augering techniques.

Representative soil samples were obtained by means of the split-barrel sampling procedure in accordance with ASTM Specification D-1586. In this procedure, a 2-inch outside diameter split-barrel sampler is driven into the soil a distance of 24 inches by a 140-pound hammer falling 30 inches. After a 6-inch seating interval, the number of blows required to drive the sampler through the next 12-inch interval is termed the Standard Penetration Test (SPT) value and is indicated for each sample on the boring log. This value can be used as a qualitative indication of the in-place relative density and relative consistency of non-cohesive soils and cohesive soils, respectively. This indication is qualitative, since many factors can significantly affect the standard penetration resistance value and prevent a direct correlation between drill crews, drill rigs, drilling procedures, and hammer-rod-sampler assemblies.

Field logs of the soils encountered in the borings were maintained by the drill crew. After recovery, each sample was removed from the sampler and visually classified. Representative portions of each sample were sealed in glass jars and delivered to our laboratory in Williamsburg, Virginia, for further visual examination and laboratory testing.

### **Subsurface Conditions**

Experienced personnel from our office classified each soil sample in accordance with the Unified Soil Classification System (USCS). Select samples from the test borings were subjected to classification testing to confirm our visual classifications. The group symbols for each soil type are indicated in parentheses following the soil descriptions on the boring logs. The geotechnical engineer grouped the various soil types into the major zones noted on the boring logs. The stratification lines designating the interfaces between earth materials on the boring logs are approximate; in situ, the transitions may be gradual. A brief explanation of the USCS and a Reference Notes for Boring Log sheet is provided in Appendix IV of this report.

Our subsurface exploration and site reconnaissance determined that the site is covered with 1 to 3 inches of topsoil. Underlying the near surface soils, we encountered interbedded deposits of soft to very stiff consistency Sandy CLAYS (CL), and very loose to medium density Clayey SAND

(SC). This stratum extended to boring termination depths of 6 to 15 feet below ground surface (bgs). The Standard Penetration Test (SPT) N-values recorded for these layers ranged from 2 to 24 blows-per-foot (bpf).

Groundwater was not encountered at the boring locations. Considering the fine-grained soils encountered, a perched ground water condition could be encountered. Please note that groundwater levels are influenced by seasonal conditions and by periods of significant precipitation or prolonged drought. If ground water is encountered, we recommend it be pumped from sumps located below the bottom of foundation elevation.

### **Subgrade Preparation and Earthwork Operations**

The depth of topsoil recorded in the test borings ranged between 1 to 3 inches. However, stripping topsoil typically disturbs soils to a depth greater than the actual topsoil thickness. Therefore, for project planning purposes, we anticipate a 4 inch stripping depth for this site to remove topsoil, and associated organic matter. Isolated areas may require further cuts of an additional 12 to 18 inches or more due to tree stumps and heavy root mat from existing trees or thicker pavement sections. We recommend stripping of any organic or unstable material. The stripping depth should be evaluated at the time of construction by representatives of the Geotechnical Engineer. If additional stripping becomes necessary, suitable methods should be employed to determine additional stripping depths beyond the contract depth (such as elevations determined before and after additional stripping, etc.). If undercuts are recommended and extend into large areas, the undercut volume could be reduced by the use of geotextiles or geogrids. The use of geosynthetic reinforcement should be evaluated by the geotechnical engineer. Cut and fill operations should extend a minimum of 5 feet beyond the project limits.

After stripping or cutting to the desired grade, and prior to fill placement, subgrades should be observed by the Geotechnical Engineer. In an effort to densify any loose surficial subgrade soils, the stripped area should be proofrolled with a smooth drum roller with a minimum of two passes in two perpendicular directions, provided in-situ moisture contents are within  $\pm 3\%$  of optimum in order to facilitate compaction.

Any soft or unsuitable materials encountered, which cannot be stabilized by reworking the soil, should be removed and replaced with an approved structural fill. Undercut volumes should be determined by cross-sectioning the area before and after undercut. We have found that calculating undercut volumes by truck counts is less accurate and generally results in additional expense to the owner. In order to minimize undercutting and issues during earthwork activities, we recommend earthwork operations be performed during the drier times of the year.

We recommend the contract documents include an allowance for undercutting and/or reworking soft near surface soils (if encountered) and replacement with engineered fill. Add/deduct unit prices should also be established so adjustment for the actual volume of undercut can be made.

Generally, the on-site soils are considered suitable for reuse as compacted structural fill provided they classify as CL, ML, SM, SM-SP, SP, SC or better. Any soils classifying as CH are not considered suitable as compacted fill in structural areas within the building, floor slab, or parking lots, due to their moisture sensitivity and shrink-swell potential. On-site soils to be re-used as structural fill and all proposed select fill soils should be submitted to the geotechnical engineer for approval prior to their use on the project. We recommend imported engineered fill (select) material consisting of approved inorganic material classified as SM, SM-SP, SP, SC or better containing less than about 40% by weight Silt or Clay and free of debris. This material should be placed in horizontal lifts not exceeding 8 inches in loose thickness, moisture conditioned to within +/- 3% of the optimum moisture content, and compacted to a minimum of 95% of the maximum dry density obtained in accordance with VTM-1, Standard Proctor method. Select fill slopes should be no greater than 3 horizontal to 1 vertical.

### **Foundations**

Based on the results of our exploration and analysis, it is our opinion that the proposed building can be supported by shallow spread footings bearing on suitable natural soils or in properly compacted select fill extending to stable, undisturbed subgrade. For footings placed on suitable natural soils or compacted engineered fill, we recommend that a net allowable soil bearing pressure of 3000 psf be utilized for proportioning the foundations. The base of the footings should be a minimum of 24 inches wide for wall footings and 30 inches square for column footings to minimize potential failure of the bearing soils by local or punching shear action. The near-surface natural soils are variable across the site with respect to shrink-swell issues. The sands are considered low shrink-swells while the clays are considered high. However, considering the estimated building loads are believed to be substantial enough to counter act the soils swell pressure, we recommend foundations be embedded a minimum of 24 inches below site grades for shrink-swell, frost protection, and bearing capacity considerations.

Select controlled fill should be compacted to at least 95% of the material's maximum dry density as determined by the Standard Proctor method (ASTM D-698). Spread footing foundations should be evaluated as an independent system which are not rigidly connected to the floor slab-on-grade. In addition, we recommend that all continuous (strip type) footings be adequately reinforced and be of sufficient thickness so as to better distribute the foundation structural loading and to span soft zones or other inconsistencies in the subgrade bearing soils.

The net allowable soil bearing pressure refers to that pressure which may be transmitted to the foundation bearing soils in excess of the final minimum surrounding overburden pressure. Based on foundations designed and constructed herein utilizing a net allowable bearing pressure of 3000 psf, the total long term settlement for the building is estimated to not exceed one inch, with differential settlements between adjacent columns estimated to not exceed one-half inch.

### **Seismic Design**

We have evaluated the seismic site coefficient in accordance with IBC 2003. We consider the soils to match Site-Class Type E based on the IBC 2003 "Site Class Definitions", Section 1615.1.1.

If this project can benefit from a Site Class "D" seismic site class coefficient, we recommend a site specific seismic evaluation be performed utilizing the seismic cone penetrometer (CPT).

### **Floor Slab Design**

The building pad subgrade and fill placement should be prepared and placed as recommended in the previous subgrade preparation and earthwork section of this report. In conditioned office areas, we recommend the slab-on-grade be directly supported by a minimum of 4 inches of a well graded, clean granular material (porous fill) having a maximum aggregate size of 1.5 inch and no more than 15% passing the #200 Sieve (GM, GW, GP, SM, SW, SP). Both VDOT No. 57 stone and VDOT Grade A Fine Aggregate meet the criteria for porous fill.

These granular layers below the floor slab will facilitate the fine grading of the subgrade, provide more uniform bearing conditions, and help minimize the rise of water to the bottom of the slab via capillary action. The slab should also be directly underlain by a suitable polyethylene vapor retarder to minimize moisture intrusion into the slab. Provided the design and construction recommendations discussed herein are followed, the slab may be designed assuming a Modulus of Subgrade Reaction,  $K_s$ , of 200 psi per inch.

### **Pavements**

Once the design pavement subgrade elevation is reached, the subgrade should be proofrolled and carefully observed at the time of construction in order to aid in identifying any localized soft or unsuitable materials. An outcome of the proofrolling may be a recommendation to scarify, aerate, and recompact the soils at near the soil's optimum moisture content. Soils which are still unstable will require undercutting and replacement with structural fill material under the direction of the geotechnical engineer. If site work is performed during the wetter winter months, we anticipate that slightly cohesive and moisture-sensitive subgrade soils subjected to wet conditions and/or ponding water will become unstable and require undercuts and replacement with dryer, suitable material. Ideally, site work should be performed during the dryer late summer and early fall months to minimize potential undercuts due to moisture intrusion and facilitate compaction. Exposed subgrade soils should be graded to drain surface moisture, and covered as soon as possible with full design depths of select materials that are

compacted in accordance with project design criteria. Construction traffic should be confined to specific stabilized construction roads, and not allowed to degrade the pavement subgrade or new pavement section once it is placed.

An important consideration with the design and construction of new pavements is surface and subsurface drainage. Where standing water develops, either on the pavement surface or within the base course layer, softening of the subgrade and other problems related to the deterioration of the pavement can be expected. Furthermore, good drainage should minimize the possibility of the subgrade materials becoming saturated over a long period of time. Based upon the results of the soil test borings, the groundwater table should not significantly affect the performance of pavements; however, surface runoff water that is trapped during construction on the exposed subgrade soils could create localized deterioration of the soil's bearing capacity. Standing water that may develop on the surface of the pavement may be minimized by adequate design (surface graded to control runoff to desired locations - catch basins, drain inlets, gutters, etc.), adequate compaction of each lift of pavement material (to minimize localized settlements that result in ponding), and accurate fine grading of each lift of pavement material (to achieve the desired design grades). Standing water that tends to develop within the base course layer may be minimized by installing temporary weep holes in drainage structures, construction of drainage swales and diversion ditches, and proper backfill and grading behind curbs to minimize water intrusion from behind the curbs.

There were no subgrade samples taken in the parking areas. The pavement recommendations presented herein are being based on the one (1) soil test boring performed within the parking area, and our experience in the area on regional soil types. We encountered Sandy CLAY (CL) soils in the parking area. Typically, soaked CBR values for this soil type range between 4 and 8. We therefore recommend a design CBR value of 4 for pavement design. A Resiliency Factor (RF) of 2.0 and the resulting Soil Support Value (SSV) of 8 should also be used in this design.

The following pavement sections are based on VDOT minimum section requirements and our local experience in the project area. We recommend the following pavement sections for the main drive lanes and parking spaces:

#### **Flexible Pavement – Light Duty (Parking Spaces)**

- |                   |  |
|-------------------|--|
| Asphalt Surface   | - 2.0 inches Asphalt Concrete Surface Mix, Type SM-9.5.  |
| Aggregate Subbase | - 8.0 inches untreated Aggregate Base Material, Type I, Size 21A/B.  |
| Subgrade          | - Stable and compacted to a dry density of at least 95% of the soil's Standard Proctor maximum dry density (ASTM D698) |

Dam

We recommend that any dumpster pad area's (including the area the collection truck will be on while emptying the dumpster) be a rigid pavement. We recommend that concrete pavements be comprised of a minimum of 6 inches of Portland cement concrete having a minimum 28-day compression strength of 4000 psi. The concrete should be air entrained and should be reinforced with welded wire mesh-type reinforcement or Fibermesh concrete should be used. Construction joints or sawcut joints should be provided at a maximum spacing of 12 feet. Four inches of untreated aggregate base material, Type I - Size 21A/B, are recommended beneath exterior concrete pavements.

Compaction testing may be waived by the Geotechnical Engineer based on the results of the proofrolling operations. It should be noted that pavement sections recommended herein are considered to be minimums with regard to recognized pavement design practices, and any reductions in the pavement sections could result in less than satisfactory pavement performance.

### **Earthen Embankments and Slope Stability:**

Existing elevations across the site were not provided. However, the bottom of pond elevation is approximately 84.40 ft, msl. Generally, we encountered Clayey SAND (SC) that extended from the ground surface to 6 ft below ground surface, and Sandy CLAY (CL) that extended from 6 ft bgs to the depths explored at 20 feet below site grades. We did not encounter ground water.

The soils located within the base of the pond area consist of Sandy CLAY (CL) materials. Generally, these soils would be considered suitable for reuse as the dam core material. We recommend the core of the dam be constructed with a lower permeability clay material. Clay core material should classify as CL or CH material. This material should be placed in horizontal lifts not exceeding 8 inches in loose thickness, moisture conditioned to within -1% to +3% of the optimum moisture content, and compacted to a minimum 95% of the maximum dry density obtained in accordance with ASTM Specification D-698, Standard Proctor method. Slopes should be constructed no greater than 3 horizontal to 1 vertical. Also, the side slopes should be seeded to promote vegetation growth and further add to the stability of the slopes.

### **Infiltration**

The soils encountered at boring location B-4 from the ground surface to the depth of 6 feet bgs, appeared to match Hydrologic Soil Group designations of B to C (Sandy Loam to Sandy Clay Loam), with estimated infiltration rates of approximately 1.02 to 0.17 inches per hour. The soils encountered between 6 to 20 feet at B-4 appeared to match Hydrologic Soil Group designations of D (Silty Clay Loam to Silty Clay), with estimated infiltration rates of approximately 0.06 to 0.04 inches per hour.

Based on the soils encountered at the other B-4, these soils are expected to provide marginal to good water retention characteristics. However, if the conditions do not allow for a fixed permanent pool elevation to be maintained, additional steps to minimize seepage losses may be necessary. Typically, soils with the Hydrologic Soil Group designations of A and B are considered suitable for SWMP's that may utilize on-site filtration in their designs. Some soils designated as C type soils are considered suitable for infiltration practices but these soils would need to be evaluated on a case specific basis. Soils with group designations of D are considered suitable for a wet pond, if required.

### **Construction Considerations:**

The existing slopes generally ranged between 3H:1V to as steep as 1H:1V throughout the planned pond areas. All topsoil and organics should be removed to suitable natural soils within the construction area. The stripping depth should extend up the slopes to at least the 100 year flood elevation. As such, some of the side slopes may need to be reconstructed. The slopes should be reconstructed utilizing engineered fill placed in controlled, compacted lifts that are benched into the existing slopes. On-site sandy or clayey soils are considered suitable for engineered fill to regrade the slopes. This material should be placed in horizontal lifts not exceeding 8 inches in loose thickness, moisture conditioned to within +/-3% of the optimum moisture content, and compacted to a minimum 95% of the maximum dry density obtained in accordance with ASTM Specification D-698, Standard Proctor method. Slopes should be constructed no greater than 3:1. Also, the side slopes should be seeded to promote vegetation growth and further add to the stability of the slopes.

The subgrade materials are moisture sensitive, and exposure to the environment may weaken the soils at the footing bearing level if the foundation excavations remain open for too long a time; therefore, foundation concrete (or flowable fill) should be placed the same day that foundations are excavated. If the bearing soils are softened by surface water intrusion or exposure, the softened soils must be removed from the foundation excavation bottom immediately prior to placement of concrete. If the excavation must remain open overnight, or if rainfall becomes imminent while the bearing soils are exposed, we recommend that a 1- to 3-inch thick "mud mat" of lean concrete be placed on the bearing soils before the placement of reinforcing steel.

In a dry and undisturbed state, the soil at the site will provide good subgrade support for fill placement and construction operations; however, when wet, this soil will degrade quickly with disturbance from contractor operations. Good site drainage should be maintained during earthwork operations which would help maintain the integrity of the soil.

Proper compaction control of fill is an important aspect of this project. Therefore, we recommend that all fill operations be observed full-time by a qualified soil technician to determine if minimum compaction requirements are being met.

We did not encounter groundwater during drilling of the borings. As such, we do not anticipate that ground water will impact foundation construction. If ground water is encountered, we expect that dewatering in shallow trenches could be accomplished by pumping from sumps adjacent to the construction excavations. The specifications should, however, alert the contractor to the potential presence of subsurface water, and it should be incumbent on the contractor to provide the means by which to satisfactorily dewater the site.

**General Comments:**

This report has been prepared in order to aid in the evaluation of this site and to assist the Contractor, Architect and Engineer in the design and planning of the project. The report scope is limited to the specific project and location described, and the project description represents our understanding of the significant aspects relevant to soil and foundation characteristics.

We have appreciated being of service to you during the design phase of this project and look forward to its successful construction. If you should have any questions regarding the information and recommendations contained in this report or if we can be of any further assistance, please contact our office.

Respectfully,

ECS MID-ATLANTIC, LLC.



David Gordinier, E.I.T.  
Project Engineer



Michael J. Galli, P.E.  
Principal Engineer

RNL/DJG/MJG:abf

- Appendix:
- I. Boring Location Plan (1)
  - II. Soil Test Boring Logs (5)
  - III. Laboratory Test Summary (1)
  - IV. Unified Soil Classification System/  
Reference Notes for Boring Logs (2)



**James City County Environmental Division  
Stormwater Management / BMP Inspection Report  
Detention and Retention Pond Facilities**

County BMP ID Code (if known): GC.008  
 Name of Facility: James River Baptist BMP No.: 1 of 1 Date: 6/25/08  
 Location: 4931 Centerville Rd  
 Name of Owner: James River Baptist  
 Name of Inspector: Tina Cooke  
 Type of Facility: Wet pond  
 Weather Conditions: Sunny Type:  Final Inspection  County BMP Inspection Program  Owner Inspection

If an inspection item is not applicable, mark NA, otherwise mark the appropriate column.

- O.K. - The item checked is in adequate condition and the maintenance program is currently satisfactory. No action required.
- Routine - The item checked requires attention, but does not present an immediate threat to the function/integrity of the BMP.
- Urgent - The item checked requires immediate attention to keep the BMP operational and to prevent damage to the facility.

Provide an explanation and details in the comment column, if routine or urgent are marked.

Facility Item	O.K.	Routine	Urgent	Comments
<b>Embankments and Side Slopes:</b>				
Grass Height		✓		Completed 12/3/08 most of grass is either dead or dying.
Vegetation Condition		✓		
Tree Growth	✓			
Erosion			✓	rip rap channel - erosion at/under filter fabric
Trash & Debris	✓			Completed on 12/3/08
Seepage	✓			
Fencing or Benches		✓		See below
<b>Interior Landscaping/Planted Areas:</b> <input type="checkbox"/> None <input type="checkbox"/> Constructed Wetland/Shallow Marsh <input type="checkbox"/> Naturally Established Vegetation				
Vegetated Conditions		✓		
Trash & Debris	✓			
Floating Material	✓			
Erosion	✓			minor
Sediment	✓			
Dead Plant		✓		aquatic bench plantings (need 122) either dead or missing
Aesthetics	✓			
Other				
Notes:				

May be reduced to \$10,000<sup>00</sup> in current state. Bond Exp 8/10

Facility Item	O.K.	Routine	Urgent	Comments
<b>Water Pools:</b> <input checked="" type="checkbox"/> Permanent Pool (Retention Basin) <input type="checkbox"/> Shallow Marsh (Detention Basin) <input type="checkbox"/> None, Dry (Detention Basin)				
Shoreline Erosion	/			
Algae	/			
Trash & Debris	/			
Sediment	/			
Aesthetics	/			
Other				
<b>Inflows (Describe Types/Locations):</b>				
Condition of Structure	/			
Erosion	/			
Trash and Debris	/			
Sediment	/			
Outlet Protection				
Other <i>Asbuilts</i>				<i>(SSI-1)</i> <i>3LF Short</i> / <i>reverse slope</i> <i>PIPE 2' short</i>
<b>Principal Flow Control Structure - Riser, Intake, etc. (Describe Type):</b>				
Condition of Structure	/			
Corrosion	/			
Trash and Debris	/			
Sediment	/			
Vegetation	/			
Other <i>Asbuilts</i>				<i>see above</i>
<b>Principal Outlet Structure - Barrel, Conduit, etc. :</b>				
Condition of Structure				
Settlement	/			
Trash & Debris	/			
Erosion/Sediment	/			
Outlet Protection	/			
Other <i>Asbuilts</i>				<i>1' longer (31')</i>
<b>Emergency Spillway (Overflow):</b>				
Vegetation	/			
Lining	/			
Erosion	/			
Trash & Debris	/			
Other				
Notes:				

*OKAY Dec Biol*

Facility Item	O.K.	Routine	Urgent	Comments
<b>Nuisance Type Conditions:</b>				
Mosquito Breeding	/			
Animal Burrows	✓			
Graffiti	/			
Other				
<b>Surrounding Perimeter Conditions:</b>				
Land Uses A-1	/			7/8/08 topsoil, seeded, & straw - no veg yet
Vegetation		/		seed straw applied / limited topsoil
Trash & Debris	/			clay & sand conditions not conducive to seed germination
Aesthetics	/			
Access / Maintenance Roads or Paths		/		6" stone required on access road. Completed
Other				
<b>Remarks:</b> Need record drawing certification on BMP cert forms not just record drawings. resubmitted by AES				
Overall Environmental Division Internal Rating: <u>3</u>				
Signature: <u>Vina Cooke</u>				Date: <u>6/25/08</u>
Title: <u>Environmental Inspector</u>				



**JAMES CITY COUNTY - ENVIRONMENTAL DIVISION**

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From: Lina Cook

James City County  
P O Box 8784  
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Facsimile Number: 220-89014

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From: Tina Cooke

James City County  
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Williamsburg VA 23187-8784

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The last page is the record drawing certification we discussed.

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DATE SENT: 6/25/08

Name: Wayne Reed  
Firm or Company: Reed Ent.  
Facsimile Number: (757) 282-2468  
Number of pages including this transmittal: 4  
From: Tim Cooke

James City County  
P O Box 8784  
Williamsburg VA 23187-8784

Comments: Not on BMP Field Insp form:

① The silt fence & tree protection must also be removed once the site is stabilized. — 7/8/08 — already removed??

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