



CERTIFICATE OF AUTHENTICITY

THIS IS TO CERTIFY THAT THE FOLLOWING ELECTRONIC RECORDS ARE TRUE AND ACCURATE REPRODUCTIONS OF THE ORIGINAL RECORDS OF JAMES CITY COUNTY GENERAL SERVICES DEPARTMENT- STORMWATER DIVISION; WERE SCANNED IN THE REGULAR COURSE OF BUSINESS PURSUANT TO GUIDELINES ESTABLISHED BY THE LIBRARY OF VIRGINIA AND ARCHIVES; AND HAVE BEEN VERIFIED IN THE CUSTODY OF THE INDIVIDUAL LISTED BELOW.

BMP NUMBER: MC005

DATE VERIFIED: December 6, 2012

QUALITY ASSURANCE TECHNICIAN: Leah Hardenbergh

Leah Hardenbergh

LOCATION: WILLIAMSBURG, VIRGINIA



Stormwater Division

MEMORANDUM

Date: March 28, 2012
To: Michael J. Gillis, Virginia Correctional Enterprises Document Management Services
From: Leah Hardenbergh
PO: 110426
Re: Files Approved for Scanning

General File ID or BMP ID: MC005
PIN: 4711300001
Owner Name (if known): JOHN TYLER INVESTMENT GROUP
Legal Property Description: L-1 JOHN TYLER COMM
Site Address: 4556 JOHN TYLER HGWY

(For internal use only):

Box # 3

Agreements (in file as of scan date): N Book or Doc #:

MC-005

Contents for Stormwater Management Facilities As-built Files

Each file is to contain:

1. As-built plan
2. Completed construction certification
- ③ Construction Plan
- ④ Design Calculations
5. Watershed Map
6. Maintenance Agreement
7. Correspondence with owners
8. Inspection Records
9. Enforcement Actions

T.B.M. COR. CONC. PAD VIA. FORWARD TRANSMITTER Q. PRINTED PINK FIRE HYDRANT
ELEV. = 65.95'

LABEL	RADIUS	CENTRAL ANGLE	ARC LENGTH	CHORD LENGTH	CHORD BEARING	TAN. LENGTH
C1	1185.92	01° 17' 08"	26.61	26.61	N 89° 48' 24" W	13.31
C2	145.00	05° 08' 02"	12.99	12.99	S 01° 43' 50" E	6.50



BASIN "A"
 A - 0.3 AC.
 C - 0.7
 I - 7.2 IN/HR
 Q - 1.5 CFS

BASIN "B"
 A - 1.1 AC.
 C - 0.9
 I - 7.2
 Q - 7.1 CFS

BASIN "F"
 A - 0.3 AC
 C - 0.95
 I - 7.2
 Q - 2.1 CFS

BASIN "C"
 A - 0.8 AC.
 C - 0.3
 I - 6.7
 Q - 1.6 CFS

BASIN "E"
 A - 0.7 AC.
 C - 0.3
 I - 7.2 IN/HR
 Q - 1.5 CFS

BASIN "G"
 A - 0.2 AC.
 C - 0.95
 I - 7.2
 Q - 1.4 CFS

BASIN "D"
 A - 0.3 AC
 C - 0.4
 I - 7.2
 Q - 0.9 CFS



LIMITS OF 25% SLOPE
 FOR REVIEW ONLY, NOT TO BE USED FOR CONSTRUCTION

SHEET INDEX

NO.	DESCRIPTION	DATE
1.	SITE PLAN	
2.	NOTES AND DETAILS	
3.	LANDSCAPE PLAN	



Langley and McDonald
 A PROFESSIONAL CORPORATION
 ENGINEERS • PLANNERS • SURVEYORS
 VIRGINIA BEACH - WILLIAMSBURG, VIRGINIA

DES. CRO	HTB
DWN	CHK
DATE	3/30/14

CUSTOM BUILDER SUPPLY
 DRAINAGE AREA MAP
 FOR
JOHN TYLER INVESTMENT GROUP
 VIRGINIA
 JAMES CITY COUNTY

PROJ. NO.	94021-3
SCALE	1"=20'
SHEET	1 OF 1
DWG.	5254W

SP-56-94

LABEL	RADIUS	CENTRAL ANGLE	ARC LENGTH	CHORD LENGTH	CHORD BEARING	TAN. LENGTH
C1	1185.92	01° 17' 08"	26.61	26.61	N 89° 48' 24" W	13.31
C2	145.00	05° 08' 02"	12.99	12.99	S 01° 43' 50" E	6.50



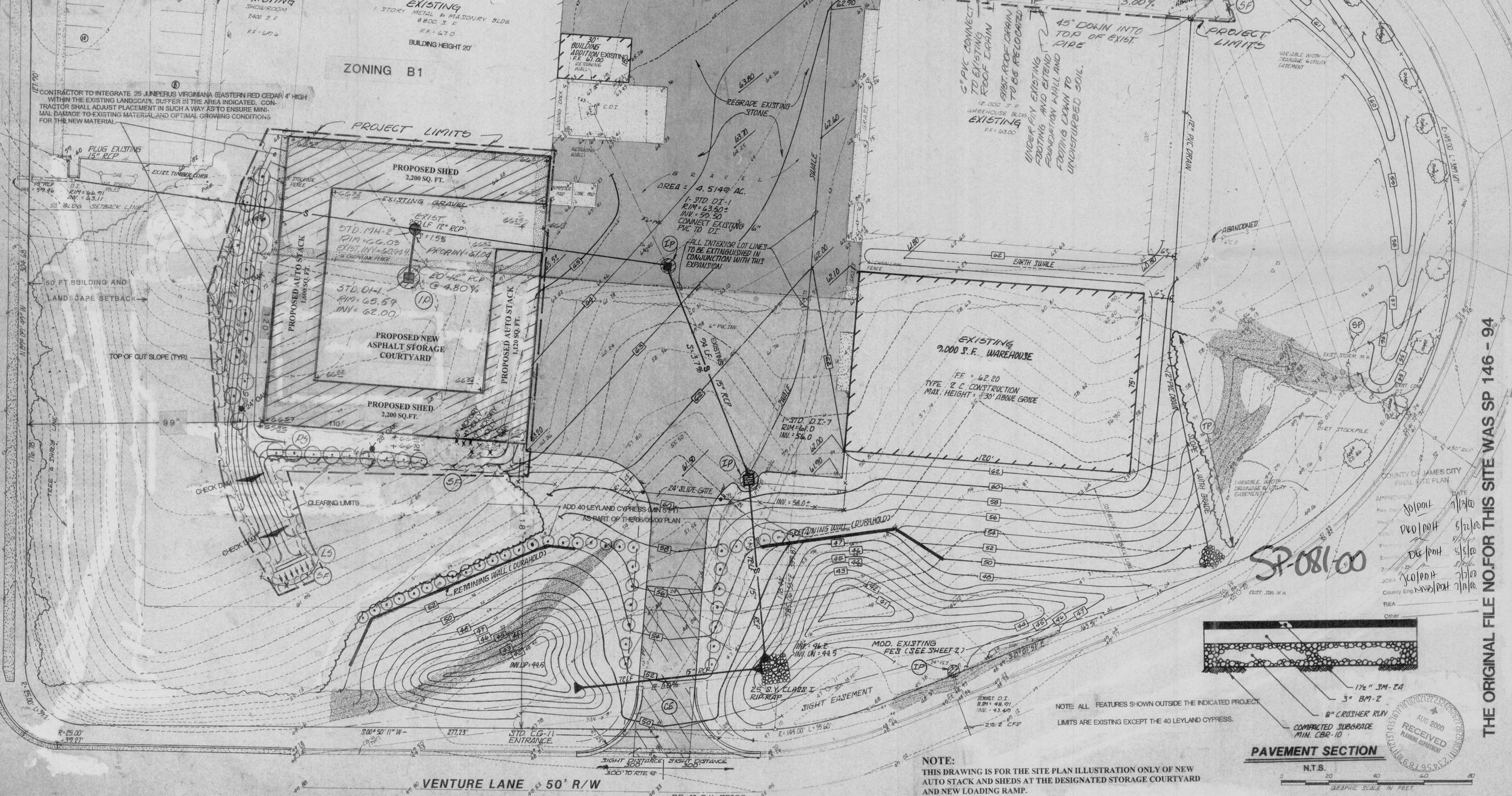
COMMONWEALTH OF VIRGINIA
STEPHEN A. ROMEO
No. 1448-B
LAND SURVEYOR

SITE STATISTICAL DATA

PARKING: 1,250 S.F. RETAIL OFFICE SPACE

FLOOR AREA	(S.F.)	% OF PARCEL	MAX. ALLOWED %
EXISTING	32,740	16.6	25
PROPOSED	7,200	3.7	8.4
TOTAL	39,940	20.3	25

IMPERVIOUS AREA	(S.F.)	% OF PARCEL	MAX. ALLOWED %
EXISTING	87,780	44.6	60
PROPOSED	8,740	4.4	15.4
TOTAL	96,520	49.0	60



VICINITY MAP SCALE: 1"=2000'

LANDMARK DESIGN GROUP
Engineers • Planners • Surveyors
Landscape Architects • Environmental Consultants

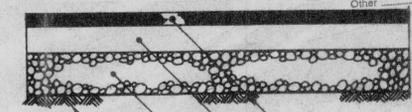
DES. DEW	DWN. DEW	CHK.	DATE
			06/05/00

CUSTOM BUILDER SUPPLY
SITE PLAN FOR STORAGE RACKS, SHEDS AND LOADING RAMP
FOR
JOHN TYLER INVESTMENT GROUP
JAMES CITY COUNTY
VIRGINIA

PROJ. NO.	1940021-000.15
SCALE	1"=20'
SHEET	1 OF 2
DWG.	5257 BW

THE ORIGINAL FILE NO. FOR THIS SITE WAS SP 146 - 94

SP-081-00



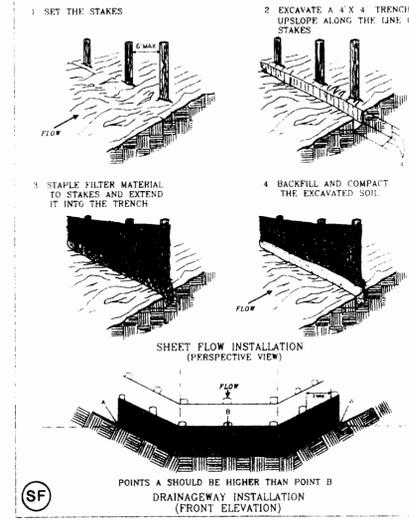
PAVEMENT SECTION

NOTE: ALL FEATURES SHOWN OUTSIDE THE INDICATED PROJECT LIMITS ARE EXISTING EXCEPT THE 40 LEYLAND CYPRESS.

NOTE: THIS DRAWING IS FOR THE SITE PLAN ILLUSTRATION ONLY OF NEW AUTO STACK AND SHEDS AT THE DESIGNATED STORAGE COURTYARD AND NEW LOADING RAMP.

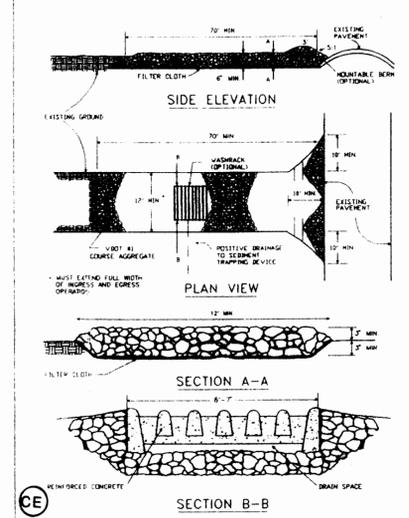


CONSTRUCTION OF A SILT FENCE (WITHOUT WIRE SUPPORT)



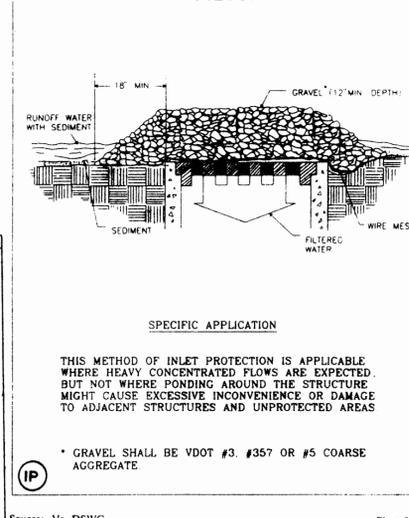
Source: Adapted from Installation of Straw and Fabric Filter Barriers for Sediment Control, Sherwood and Wyatt Plate 3.05-2

STONE CONSTRUCTION ENTRANCE



Source: Adapted from 1983 Maryland Standards for Soil Erosion and Sediment Control, and VA DSWC Plate 3.02-1

GRAVEL AND WIRE MESH DROP INLET SEDIMENT FILTER



Source: Va. DSWC Plate 3.07-2

LANDSCAPE PLANTING NOTES

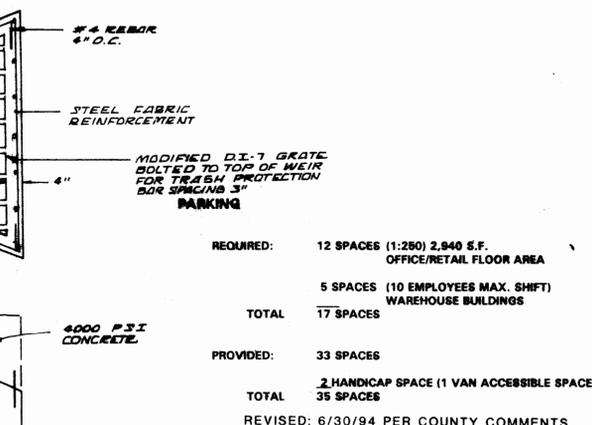
THE CONTRACTOR SHALL PROVIDE ALL LABOR, MATERIALS, ETC. NECESSARY TO COMPLETE ALL WORK SHOWN ON THE DRAWINGS... A LIST OF PLANTS, INCLUDING SPECIES, QUANTITIES AND OTHER REQUIREMENTS, IS SHOWN ON THE DRAWINGS... THE CONTRACTOR IS RESPONSIBLE FOR VERIFYING THE IDENTIFICATION OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE MAINTENANCE OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PROTECTION OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE REMOVAL OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE REPLACEMENT OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE WATERING OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE FERTILIZATION OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PRUNING OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE MULCHING OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE WEEDING OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PROTECTION OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE REMOVAL OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE REPLACEMENT OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE WATERING OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE FERTILIZATION OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PRUNING OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE MULCHING OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE WEEDING OF PLANTS...

2.2.2. A3 HORIZONS SHALL BE MINERAL HORIZONS IN WHICH THE FEATURE EMPHASIZED IS LOSS OF CLAY, IRON OR ALUMINUM WITH HEAVY METALS... 2.3 "A" HORIZON TOPSOIL CONTENT: "A" HORIZON TOPSOIL SHALL BE IN ACCORDANCE WITH THE FOLLOWING MATERIALS BY PERCENTAGE OF VOLUME... 3.0 TOPSOIL FOR PLANTING PLANTS SHALL HAVE A pH IN THE RANGE OF 6.0 TO 7.0 PRIOR TO MIXING WITH AMENDMENTS... 3.1 BALLED AND BURLAPPED PLANTS ("BALL") SHALL BE DUG WITH FIRM NATURAL BALLS OF EARTH OF SUFFICIENT DIAMETER AND DEPTH TO ENCOMPASS THE PLANT... 3.2 THE CONTRACTOR SHALL BE NOTIFIED BY THE OWNER WHEN OTHER DIVISIONS OF THE WORK HAVE PROCEEDED SUFFICIENTLY TO COMMENCE PLANTING OPERATIONS... 3.3 NEW PLANTINGS SHALL BE LOCATED WHERE SHOWN ON THE PLAN EXCEPT WHERE OTHERWISE INDICATED... 3.4 PRIOR TO EXCAVATION OF PLANT PIT, AN AREA EQUAL TO TEN TIMES THE DIAMETER OF THE ROOT BALL SHALL BE ROTO-TILLED TO A DEPTH EQUAL TO THE DEPTH OF THE ROOT BALL... 3.5 THE DIAMETER OF PITS FOR TREES AND SHRUBS SHALL BE AT LEAST TWICE THE DIAMETER OF THE BALL OR SHRUB... 3.6 NECESSARY QUANTITIES OF TOPSOIL SHALL BE SUPPLIED BY THE CONTRACTOR AND APPROVED BY THE OWNER... 3.7 CLASS A TOPSOIL SHALL BE STOCKPILED TOPSIDE THAT HAS BEEN SALVAGED IN ACCORDANCE WITH SECTION 3.02.04 (A) OF THE VDOT SPECIFICATIONS... 3.8 CLASS B TOPSOIL SHALL BE TOPSOIL FURNISHED FROM SOURCES OUTSIDE THE PROJECT LIMITS AND HAVE THE QUALITY OF THE SOIL PROFILE FORMED UNDER NATURAL CONDITIONS... 3.9 THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PROTECTION OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE REMOVAL OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE REPLACEMENT OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE WATERING OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE FERTILIZATION OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PRUNING OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE MULCHING OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE WEEDING OF PLANTS...

2.2.2. A3 HORIZON SHALL BE MINERAL HORIZONS IN WHICH THE FEATURE EMPHASIZED IS LOSS OF CLAY, IRON OR ALUMINUM WITH HEAVY METALS... 2.3 "A" HORIZON TOPSOIL CONTENT: "A" HORIZON TOPSOIL SHALL BE IN ACCORDANCE WITH THE FOLLOWING MATERIALS BY PERCENTAGE OF VOLUME... 3.0 TOPSOIL FOR PLANTING PLANTS SHALL HAVE A pH IN THE RANGE OF 6.0 TO 7.0 PRIOR TO MIXING WITH AMENDMENTS... 3.1 BALLED AND BURLAPPED PLANTS ("BALL") SHALL BE DUG WITH FIRM NATURAL BALLS OF EARTH OF SUFFICIENT DIAMETER AND DEPTH TO ENCOMPASS THE PLANT... 3.2 THE CONTRACTOR SHALL BE NOTIFIED BY THE OWNER WHEN OTHER DIVISIONS OF THE WORK HAVE PROCEEDED SUFFICIENTLY TO COMMENCE PLANTING OPERATIONS... 3.3 NEW PLANTINGS SHALL BE LOCATED WHERE SHOWN ON THE PLAN EXCEPT WHERE OTHERWISE INDICATED... 3.4 PRIOR TO EXCAVATION OF PLANT PIT, AN AREA EQUAL TO TEN TIMES THE DIAMETER OF THE ROOT BALL SHALL BE ROTO-TILLED TO A DEPTH EQUAL TO THE DEPTH OF THE ROOT BALL... 3.5 THE DIAMETER OF PITS FOR TREES AND SHRUBS SHALL BE AT LEAST TWICE THE DIAMETER OF THE BALL OR SHRUB... 3.6 NECESSARY QUANTITIES OF TOPSOIL SHALL BE SUPPLIED BY THE CONTRACTOR AND APPROVED BY THE OWNER... 3.7 CLASS A TOPSOIL SHALL BE STOCKPILED TOPSIDE THAT HAS BEEN SALVAGED IN ACCORDANCE WITH SECTION 3.02.04 (A) OF THE VDOT SPECIFICATIONS... 3.8 CLASS B TOPSOIL SHALL BE TOPSOIL FURNISHED FROM SOURCES OUTSIDE THE PROJECT LIMITS AND HAVE THE QUALITY OF THE SOIL PROFILE FORMED UNDER NATURAL CONDITIONS... 3.9 THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PROTECTION OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE REMOVAL OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE REPLACEMENT OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE WATERING OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE FERTILIZATION OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PRUNING OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE MULCHING OF PLANTS... THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE WEEDING OF PLANTS...

INSPECTION OF THE WORK TO DETERMINE COMPLETION OF PLANTINGS, EXCLUSIVE OF THE POSSIBLE REPLACEMENT OF PLANTINGS, WILL BE MADE BY THE OWNER AT THE CONCLUSION OF THE INSTALLATION PERIOD... NURSERY STOCK SHALL BE FULLY GUARANTEED FOR 1 FULL YEAR... LANDSCAPING WILL NOT BE MEASURED, BUT SHALL INCLUDE ALL STOCK, PLANTS, MULCH, TESTING, MAINTENANCE, AND GUARANTEES... TREE PROTECTION NOTES: 1. THE LINES OF CLEARING SHALL BE DETERMINED BY THE LOCATION AND PLACEMENT OF PROTECTIVE FENCING MARKING THE AREAS OF THE SITE TO BE UNDISTURBED... 2. PROTECTIVE FENCING: UNDISTURBED AREAS SHALL BE IDENTIFIED BY BRIGHT BRIGHT ORANGE FENCING... 3. PROTECTIVE FENCING MATERIAL SHALL BE IN PLACE PRIOR TO THE COMMENCEMENT OF ANY WORK ON THE SITE... 4. EQUIPMENT OPERATION AND STORAGE: HEAVY EQUIPMENT, VEHICULAR TRAFFIC, AND MATERIALS SHALL NOT BE PERMITTED WITHIN THE PROTECTIVE FENCING... 5. SOIL PROTECTION: UNDISTURBED AREAS SHALL BE IDENTIFIED BY BRIGHT BRIGHT ORANGE FENCING... 6. ALL TREE LIMBS DAMAGED DURING BUILDING OR LAND LEVELING OR OTHERWISE SHALL BE REPAIRED OR REPLACED... 7. THE EXACT HORIZONTAL AND VERTICAL LOCATION OF ALL EXISTING UTILITIES SHALL BE VERIFIED BY EXCAVATION AND ESTABLISHING THE EXACT HORIZONTAL AND VERTICAL LOCATION... 8. THE VIRGINIA DEPARTMENT OF TRANSPORTATION IS TO RECEIVE WRITTEN NOTIFICATION BY THE CONTRACTOR, 48 HOURS PRIOR TO STARTING ANY WORK... 9. ALL DIMENSIONS ARE TO BACK OF CURB, FACE OF BUILDING, EDGE OF PAVEMENT, UNLESS OTHERWISE INDICATED... 10. ALL STORM SEWER PIPES AND DROP INLETS TO BE CLEANED OF DEBRIS AND ERODED MATERIAL AT LAST STAGES OF CONSTRUCTION... 11. ALL DROP INLETS, WITHIN VIRGINIA DEPARTMENT OF TRANSPORTATION RIGHT-OF-WAYS OR EASEMENTS, SHALL BE CAST IN PLACE OR APPROVED PRE-CAST UNITS... 12. SURFACE DRAINAGE SHALL NOT BE ALLOWED TO ENTER SANITARY SEWER SYSTEM AT ANY TIME... 13. THE CONTRACTOR SHALL BE RESPONSIBLE FOR REPLACING, WITH MATCHING MATERIALS, ANY PAVEMENT, DRIVEWAYS, WALKS, CURBS, ETC. THAT MUST BE CUT OR THAT ARE DAMAGED DURING CONSTRUCTION... 14. ALL CONCRETE TO BE VDOT CLASS "A-3" (MIN.)... 15. THE CONTRACTOR SHALL BE RESPONSIBLE FOR SECURING ALL PERMITS NECESSARY FOR CONSTRUCTION OF THIS PROJECT... 16. UNSUITABLE MATERIAL ENCOUNTERED DURING THE COURSE OF CONSTRUCTION SHALL BE REMOVED AND REPLACED WITH SUITABLE MATERIAL AT THE DIRECTION OF THE OWNER... 17. THE CONTRACTOR SHALL PROVIDE COMPACTION REPORTS TO THE OWNER ON ALL BACKFILL OF UTILITIES, STORM SEWERS, BUILDING SLABS, AND PARKING AREAS BY A CERTIFIED MATERIALS TESTING COMPANY...

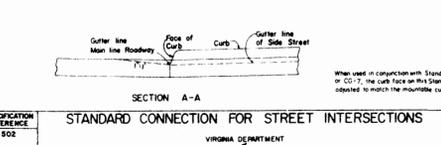
Table with 4 columns: Description, Area, Percentage, and Notes. Includes rows for Total Lot Area (196,669 SQ.FT.), Existing Bldg. Area (23,200 SQ.FT.), Proposed Warehouse (9,000 SQ.FT.), Total Bldg. Area (49,167 SQ.FT.), Existing Paved Area (42,320 SQ.FT.), Proposed Paved Area (13,350 SQ.FT.), Total Impervious Post Expansion (65,520 SQ.FT.), Total Impervious Post Expansion (87,870 SQ.FT.), Total Open Space (108,800 SQ.FT.).



REVISIONS: 6/30/94 PER COUNTY COMMENTS

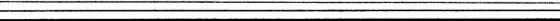
Advertisement for Langley and McDonald, P.C., Engineers • Surveyors • Planners • Landscape Architects • Environmental Consultants. Includes contact information for Williamsburg, Virginia Beach, and James City County. Also includes a logo for JOHN TYLEY INVESTMENT GROUP.

THE PURPOSE OF THE EROSION CONTROL MEASURES SHOWN ON THESE PLANS SHALL BE TO PRECLUDE THE TRANSPORT OF ALL WATERBORNE SEDIMENTS RESULTING FROM CONSTRUCTION ACTIVITIES FROM ENTERING ONTO ADJACENT PROPERTIES OR STATE WATERS... 1. ALL EROSION AND SEDIMENT CONTROL MEASURES SHALL BE INSTALLED AND MAINTAINED IN ACCORDANCE WITH THE "VIRGINIA EROSION AND SEDIMENT CONTROL HANDBOOK", 3RD EDITION, 1992... 2. ALL POINTS OF CONSTRUCTION INGRESS AND EGRESS SHALL BE PROTECTED BY A TEMPORARY CONSTRUCTION ENTRANCE... 3. SEDIMENT BASINS AND TRAPS, PERIMETER DIKES, SEDIMENT BARRIERS AND OTHER MEASURES INTENDED TO TRAP SEDIMENT ON-SITE MUST BE CONSTRUCTED AS A FIRST STEP IN GRADING... 4. MAINTENANCE OF ALL EROSION AND SEDIMENT CONTROL MEASURES SHALL INCLUDE THE REPAIR OF MEASURES DAMAGED BY ANY CONSTRUCTION INCLUDING THOSE OF THE PUBLIC UTILITY COMPANIES... 5. SURFACE FLOWS OVER CUT AND FILL SLOPES SHALL BE CONTROLLED BY EITHER REDIRECTING FLOWS THROUGH TRAVERSING THE SLOPES OR BY INSTALLING MECHANICAL DEVICES... 6. SEDIMENT CONTROL MEASURES MAY REQUIRE MINOR FIELD ADJUSTMENTS AT TIME OF CONSTRUCTION... 7. THE CONTRACTOR SHALL PLACE SOIL STOCKPILES AT THE LOCATIONS SHOWN ON THIS PLAN... 8. THE CONTRACTOR SHALL COMPLETE DRAINAGE FACILITIES WITHIN 30 DAYS FOLLOWING COMPLETION OF ROUGH GRADING... 9. PERMANENT OR TEMPORARY SOIL STABILIZATION MUST BE APPLIED TO ALL DENUDED AREAS WITHIN 7 DAYS AFTER FINAL GRADE IS REACHED... 10. NO MORE THAN 300 FEET OF SANITARY SEWER, STORM SEWER, WATERLINES, OR UNDERGROUND UTILITY LINES ARE TO BE INSTALLED AT ONE TIME... 11. IF DISTURBED AREA STABILIZATION IS TO BE ACCOMPLISHED DURING THE MONTHS OF DECEMBER, JANUARY, OR FEBRUARY... 12. THE TERM SEEDING, FINAL VEGETATIVE COVER OR STABILIZATION, ON THIS PLAN SHALL MEAN THE SUCCESSFUL GERMINATION AND ESTABLISHMENT OF A STABLE GRASS COVER... 13. ALL SLOPES STEEPER THAN 3:1 SHALL REQUIRE THE USE OF EROSION CONTROL BLANKETS... 14. INLET PROTECTION IN ACCORDANCE WITH SPECIFICATION 3.07 SHALL BE PROVIDED FOR ALL STORM DRAIN INLETS AS SOON AS PRACTICAL... 15. TEMPORARY LINERS, SUCH AS POLYETHYLENE SHEETS, SHALL BE PROVIDED FOR ALL PAVED DITCHES UNTIL THE PERMANENT CONCRETE LINER IS INSTALLED... 16. PAVED DITCHES SHALL BE REQUIRED WHEREVER EROSION IS EVIDENT... 17. TEMPORARY EROSION CONTROL MEASURES ARE NOT TO BE REMOVED UNTIL ALL DISTURBED AREAS ARE STABILIZED... 18. OFF-SITE WASTE OR BORROW AREAS SHALL BE APPROVED BY THE OFFICE OF CODE COMPLIANCE... 19. ALL PAVED AND/OR PIPED OUTFALLS WILL BE CONSTRUCTED BEFORE ROAD GRADING AND UTILITY INSTALLATION BEGINS...



Source: VIRGINIA DEPARTMENT OF TRANSPORTATION

CONSTRUCTION OPERATIONS RELATIVE TO THE LOCATION OF PROTECTED TREES



PAVEMENT SECTION



Table with 4 columns: PPE, SIZE, CONC, CONC MATERIAL. Includes rows for 12\"/>

GENERAL NOTES: D1-7 - No gutter... D1-7B - Double gutter when drop inlet is in a sag between two grades... SHEET 2 OF 3

**CHESAPEAKE BAY NARRATIVE
FOR
CUSTOM BUILDER SUPPLY
SITE PLAN SUBMITTAL**

Due to the fact that existing development occurs on the site, the three step, ten point system is difficult to apply to the proposed additional development. Consequently, the Chesapeake Bay Compliance review is based upon an analysis of existing pollutant loading versus the pollutant loading after the new development occurs. The basis of that review is the loading equation set forth in the Chesapeake Bay Local Assistance Manual. Page 1 of the accompanying calculations indicates that the total impervious area, including the new building and pavement area and the existing building and pavement area, is 1.9 acres total. The total pervious area is calculated on Page 1 by adding up each of the drainage basin areas as shown on the accompanying drainage map and subtracting from the total area draining to the basin the impervious acreage. This calculation indicates that a total of 1.8 acres of the site will be pervious after development. The post-development impervious percentage is calculated at the bottom of Page 1 to be 51.3%.

Page 2 of the calculations presents the pre and post-development loading calculations. The pre-development impervious percentage is 33.3%. The pre-development pollutant loading is indicated to be 3.67 pounds per year, under current conditions. A second calculation is provided showing the current pollutant loading using the Chesapeake Bay default value of 16% impervious. That loading is indicated to be 2.04 pounds per year.

Page 2 shows that the post-development loading, based upon a 44.7% impervious value, after the new development, is equal to 4.75 pounds per year. The removal requirement, based upon the current 33.3% impervious value, is 1.08 pounds per year. Based upon the Chesapeake Bay 16% default value, the removal requirement is indicated to be 2.71 pounds per year.

sewer
1) submerge pipe
min. of 0.45'

$$\therefore 46.2 - 1.25 - .45 = 44.5$$

recommend min slope of 0.5%

Page 1

2) check outlet cond. from basin
- 24" pipe maybe control

Page 3 of the calculations indicates that a 2.5 V_r wet pond will be used to meet the pollutant removal requirements. The Chesapeake Bay Local Assistance Manual indicates that such a facility removes 40% to 45% of the pollutant loading flowing to the facility. The runoff volume from the mean storm flowing to the BMP is shown in the middle of Page 3 to be 3,082 cubic feet. The required storage volume for a 2.5 V_r basin is shown to be 7,700 cubic feet. The calculation at the bottom of Page 3 shows that, based upon 3.7 acres flowing to the basin, a total of 4.41 pounds per year of pollutant loading occurs. Based upon a basin efficiency of 45%, 2 pounds per year are removed by the 2.5 V_r basin. The calculation at the bottom of Page 3 compares the 2 pound per year removal with the 1.08 pound per year removal requirement based upon the current site condition of 33.3% impervious.

Page 4 of the calculations provides the current, pre-development, and post-development runoff coefficients for determining flow attenuation requirements of the proposed BMP facility. The pre-development peak runoff rates, based upon the indicated parameters, are shown at the bottom of Page 4. These are as follows:

Pre-Development Q_2 = 12.8 cfs

Pre-Development Q_{10} = 15.8 cfs

Pre-Development Q_{25} = 18.0 cfs

Pre-Development Q_{100} = 21.4 cfs

The computer generated data following Page 4 provides the hydrograph and flood routing information for the proposed BMP. The flood routing is based upon the Modified Rational Hydrograph. The routing also assumes that a total of 4.51 acres flows to the basin in both the pre-development and post-development condition. Pages 5 through 8 show the allowable outflow from the basin, based upon the current "c" of 0.50. These pages also show the required storage based upon the post-development "c" of 0.56. The allowable basin outflows for the 2, 10, 25 and 100 year storms are 12.80 cfs, 15.80 cfs, 18.0 cfs and 21.40 cfs respectively. Page 9 of the calculations show a summary of the various storms modeled. These show the allowable outflows and the storage required

to meet those allowable outflows. This summary also shows the parameters used in calculating the peak discharges after the proposed site development.

Page 10 of the calculations shows the characteristics of the basin and show that at the proposed rim elevation of the outlet structure of 46.2, the storage provided is 12,583 cubic feet. This should be compared to the 7,700 cubic foot volume requirement for a 2.5 V_r basin, as shown on Page 3. The additional capacity is provided in the basin to accommodate uncertain future development. Page 11 shows the characteristics of the outlet structure. As shown on the plans, the outlet structure is in reality a modified 24-inch flared end section. The modification provides a weir that is equal in length to a 3.5 foot diameter circular standpipe. Page 12 shows the outflow summary for the structure at various elevations.

Page 13 through Page 16 shows the routing of the 10 year post-development flow. The peak outflow for the 10 year post-development storm is 9.29 cfs, with a peak elevation of 46.62 feet. This should be compared with the peak flow from the 10 year storm under existing conditions of 15.8 cfs, as shown on Page 4. Pages 17 through 20 show the routing of the 100 year post-development storm. Page 19 shows that the peak outflow for 100 post-development storm is 12.92 cfs with a peak elevation of 46.72 feet. This should be compared with the peak 100 year storm flow of 21.4 cfs under existing conditions, as shown on Sheet 4.

The peak 100 year flood elevation is shown to be elevation 46.72 feet. This still leaves 2.14 feet of differential between the peak 100 year flood elevation and the top of curb at the low point near the structure outlet.



Langley and McDonald
A PROFESSIONAL CORPORATION
ENGINEERS • PLANNERS • SURVEYORS
VIRGINIA BEACH • WILLIAMSBURG, VIRGINIA

Subject CUSTOM BUILDER
GIES. BAY
Computed By NHM Checked By _____

Project No. 94-21-3
Client _____
Date 4/28/94 Sheet No. 1

AREA TO PONDS

TOTAL AREA IMPERVIOUS

NEW BLDG. & PVMT. = ~~9000 SF~~ + 13,350 SF = 22,350 SF

EXIST BLDG & PVMT. = 23,200 SF + 37,520 S.F. = 60,720 SF

22,350 + 60,720 = 1.9 AC. IMPERVIOUS
43560

TOTAL AREA PERVIOUS

TOTAL DRAINAGE BASINS TO PONDS

BASIN A = 0.3 AC

B = 1.1 AC

C = 0.8 AC

D = 0.3 AC

E = 0.7 AC

F = 0.3 AC

G = 0.2 AC

3.7 AC. TOTAL

LESS ABOVE IMPERVIOUS AREA

3.7 AC - 1.9 = 1.8 AC. PERVIOUS

IMPERVIOUS PERCENT OF POST-DEV. AREA DRAINING TO PONDS

1.9 AC IMPERVIOUS = 51.3% ✓
1.9 AC + 1.8 AC. of drainage area



Langley and McDonald
A PROFESSIONAL CORPORATION
ENGINEERS • PLANNERS • SURVEYORS
VIRGINIA BEACH - WILLIAMSBURG, VIRGINIA

Subject CUSTOM BUILDER
CHES. BAY
Computed By NHM Checked By _____

Project No. 94-21-3
Client _____
Date 4/28/94 Sheet No. 2

PRE-DEV. LOAD

$I_{PRE} = 33.3\%$ ACTUAL IMPERVIOUS VALUE

(USING DEFAULT VALUE) LOAD = $[0.05 + 0.009(16)] \times 4.51 \text{ Ac.} \times 2.33 = 2.04 \text{ \# / yr.}$
↑ DEFAULT VALUE site area

(USING ACTUAL VALUE = 33.3%) LOAD = $[0.05 + 0.009(33.3)] \times 4.51 \times 2.33 = 3.67 \text{ \# / yr.}$
↑ ACTUAL VALUE

POST-DEV. LOAD

$I_{POST} = 44.7\%$

LOAD = $[0.05 + 0.009(44.7)] \times 4.51 \times 2.33 = 4.75 \text{ \# / yr.}$
↑ 5.48 #/yr

REMOVAL REQMT. = $4.75 - 2.04 = 2.71 \text{ \# / yr.}$ USING 16% DEFAULT VALUE FOR PRE-DEV.
 $4.75 - 3.67 = 1.08 \text{ \# / yr.}$ USING ACTUAL PRE-DEV. 33.3% IMPERVIOUS

VOLUME OF STORAGE REQ'D. FOR 45% RUNOFF REDUCTION

USE 2.5 V_p WET POND

AREA TO POND = 3.7 AC

$R_v = 0.05 + 0.009 I$

$R_v = 0.05 + 0.009 (51.3)$ (SEE BOTTOM OF PG. 1)

$R_v = 0.51'$

$Vol. = \frac{(R_v)(R_m)}{12} (Ac)$

$Vol. = \frac{(0.51)(0.45'')}{12} 3.7 AC$

$Vol. = 0.07 AC \cdot FT. = 3082 C.F.$

STORAGE VOL. REQ'D. = 2.5 X 3082 = 7700 C.F.

4.51 ac, 44.7% I ⇒ ~~2.4~~ = 2.5 V_p = 8300 CF .19 AC/FT

ACTUAL REMOVAL WITH 3.7 AC. DRAINING TO PONDS, WITH PERCENT IMPERVIOUS = 51.3%

$[0.05 + 0.009 (51.3)] (3.7 AC) (2.33) = 4.41 LB/YR.$

COLLECTION OF OTHER TERMS IN LOADING EQUATION

ACTUAL REMOVAL = 4.41 LB/YR X 45% REMOVAL = 2.0 LB/YR.

REMOVAL REQMT. W/ DEFAULT VALUE = 2.71 LB/YR

REMOVAL REQMT. W/ ACTUAL PRE-DEV. 33.3% IMPERV. = 1.08 LB/YR



PRE-DEV

$$4.51 \times 0.333 = 1.5 \text{ AC. IMPERV.}$$

$$4.51 - 1.5 = 3.0 \text{ AC. GRASS/WOODS}$$

Comp. "C"

$$1.5 \times 0.9 = 1.35$$

$$3.0 \times 0.3 = 0.90$$

$$2.25 \div 4.51 = 0.50$$

POST-DEV

$$4.51 \times 0.447 = 2.0 \text{ AC. IMPERV.}$$

$$4.51 - 2.0 = 2.5 \text{ AC. GRASS/WOODS}$$

Comp. "C"

$$2.0 \times 0.9 = 1.8$$

$$2.5 \times 0.3 = 0.75$$

$$2.55 \div 4.51 = 0.56$$

PRE-DEV. STORMS

$$C = 0.50$$

$$T_c = 5 \text{ MIN}$$

$$A = 4.51 \text{ AC.}$$

$$Q_2 = (4.51)(0.50)(3.7) = 13.8 \text{ c.f.s.}$$

$$Q_{10} = (4.51)(0.50)(7) = 15.8$$

$$Q_{25} = (4.51)(0.50)(8) = 18.0$$

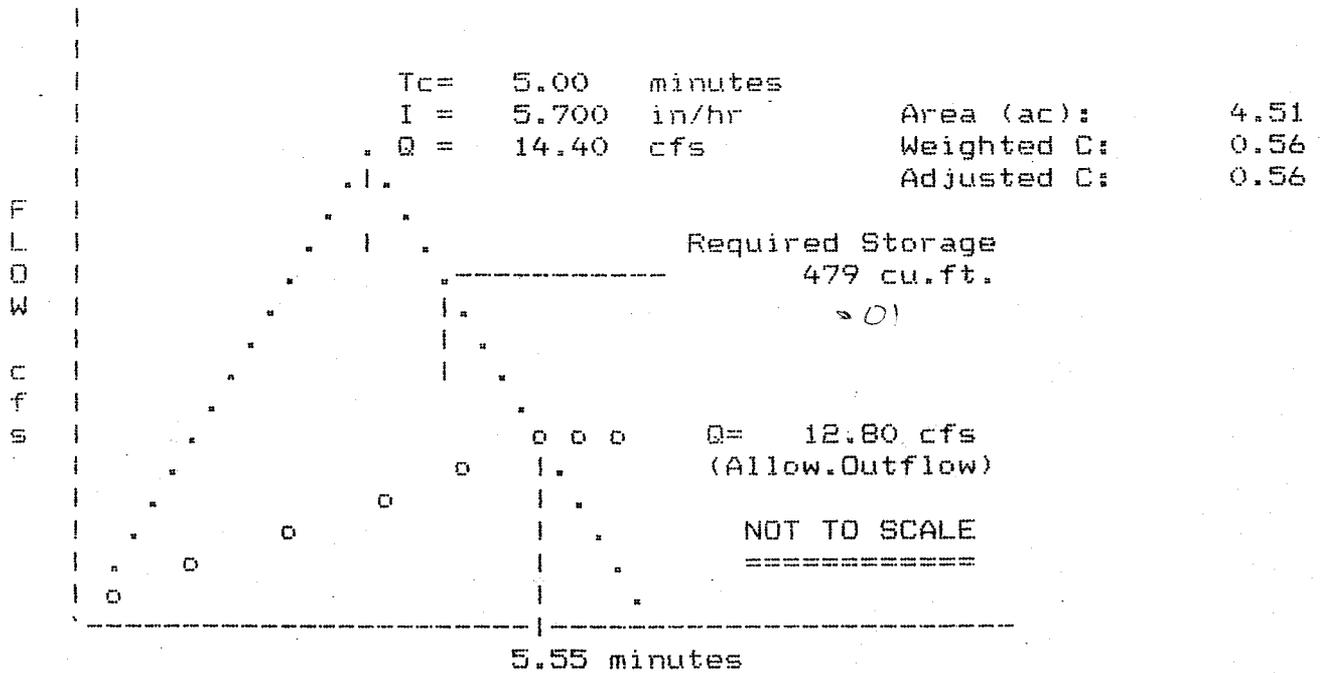
$$Q_{100} = (4.51)(0.50)(9.5) = 21.4$$

MODIFIED RATIONAL METHOD
 ----- Graphical Summary for Maximum Required Storage -----

CUSTOM BUILDER SUPPLY

```

*****
*
* RETURN FREQUENCY: 2 yr | Allowable Outflow: 12.80 cfs *
* 'C' Adjustment: 1.000 | Required Storage: 479 cu.ft. *
*
* STORM DURATION = Tc for Max.Storage *
*-----*
* Peak Inflow: 14.40 cfs Inflow .HYD stored: 2OUT .HYD *
*****
    
```



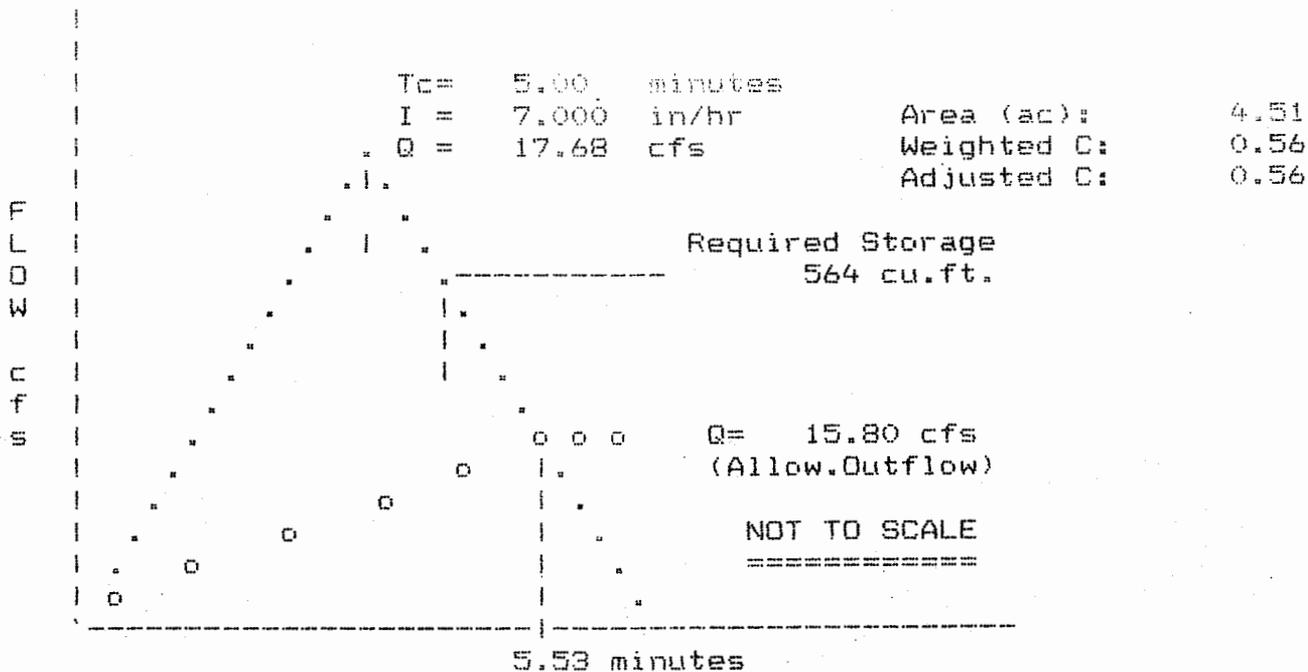


MODIFIED RATIONAL METHOD
 -----< Graphical Summary for Maximum Required Storage -----

CUSTOM BUILDER SUPPLY

```

*****
*
* RETURN FREQUENCY: 10 yr | Allowable Outflow: 15.80 cfs *
* 'C' Adjustment: 1.000 | Required Storage: 564 cu.ft. *
*
* STORM DURATION = Tc for Max.Storage *
*-----*
* Peak Inflow: 17.68 cfs Inflow .HYD stored: 100UT .HYD *
*****
    
```

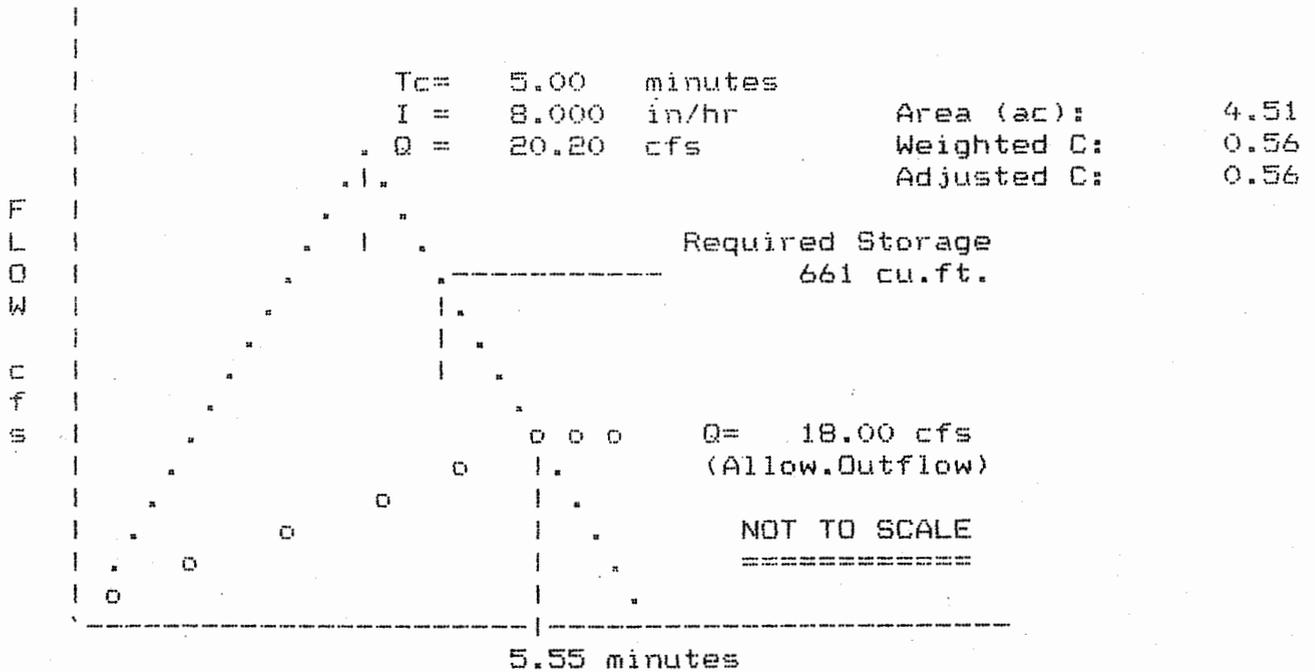


MODIFIED RATIONAL METHOD
 ---- Graphical Summary for Maximum Required Storage ----

CUSTOM BUILDER SUPPLY

```

*****
*
* RETURN FREQUENCY: 25 yr | Allowable Outflow: 18.00 cfs *
* 'C' Adjustment: 1.000 | Required Storage: 661 cu.ft. *
*
* STORM DURATION = Tc for Max.Storage *
*-----*
* Peak Inflow: 20.20 cfs Inflow .HYD stored: 250UT .HYD *
*****
    
```



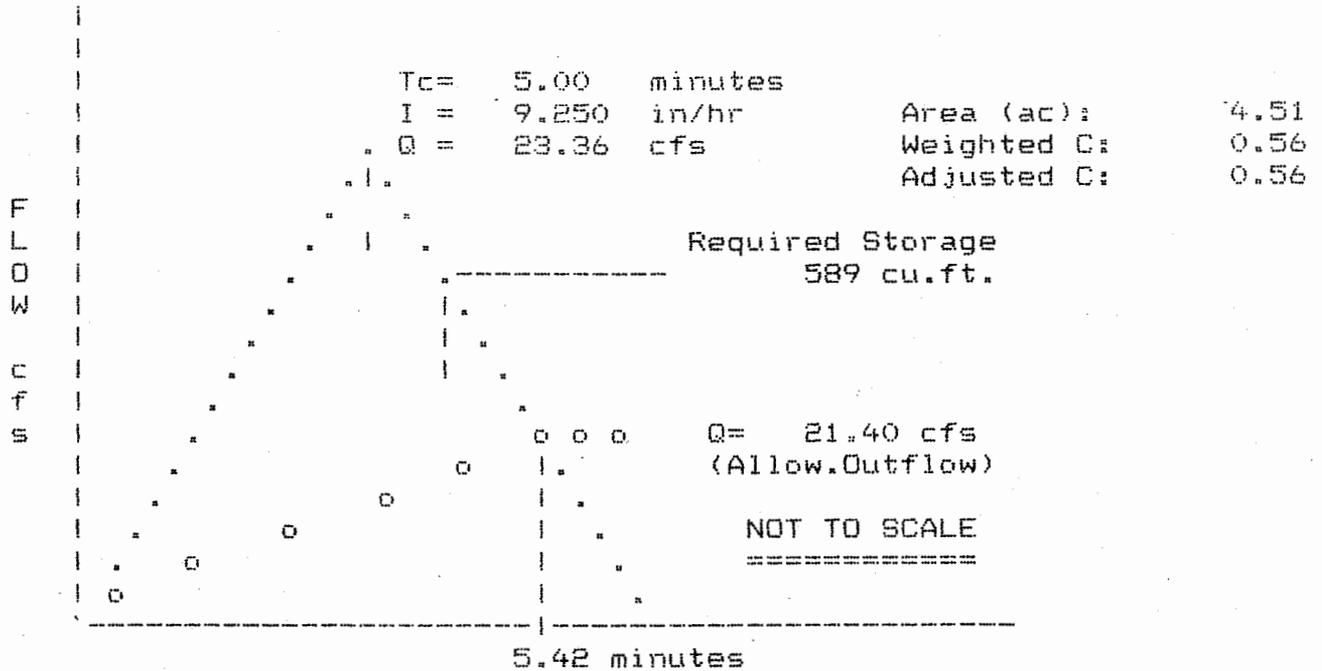
MODIFIED RATIONAL METHOD
 ---- Graphical Summary for Maximum Required Storage ----

(B)

CUSTOM BUILDER SUPPLY

```

*****
*                                     |                                     *
* RETURN FREQUENCY: 100 yr          | Allowable Outflow: 21.40 cfs *
* 'C' Adjustment: 1.000            | Required Storage: 589 cu.ft. *
*                                     |                                     *
* STORM DURATION = Tc for Max.Storage |                                     *
*-----*-----*-----*-----*-----*-----*-----*-----*-----*
* Peak Inflow: 23.36 cfs           | Inflow .HYD stored: 100OUT .HYD *
*****
  
```



10.

POND-2 Version: 5.17
S/N: 1295130250

CUSTOM BUILDER SUPPLY

CALCULATED 05-03-1994 11:55:02
DISK FILE: b:CBS1 .VOL

Planimeter scale: 1 inch = 20 ft.

Elevation (ft)	Planimeter (sq.in.)	Area (sq.ft)	A1+A2+sqr(A1*A2) (sq.ft)	* Volume (cubic-ft)	Volume Sum (cubic-ft)
41.00	0.60	240	0	0	0
42.00	1.50	600	1,219	406	406
43.00	3.20	1,280	2,756	919	1,325
44.00	6.20	2,480	5,542	1,847	3,173
45.00	10.50	4,200	9,907	3,302	6,475
45.80	*I*	5,366	14,314	3,817	10,292
46.00	14.20	5,680	14,764	4,921	11,396
46.20	*I*	6,188	17,797	1,186	12,583
47.00	21.10	8,440	21,044	7,015	18,411

I ---> Interpolated area from closest two planimeter readings.

* Incremental volume computed by the Conic Method for Reservoir Volumes.

*Yes ✓ Does this include both sides
of road - basin*

11.

Outlet Structure File: CBS1 .STR

POND-2 Version: 5.17

S/N: 1295130250

Date Executed:

Time Executed:

CUSTOM BUILDER SUPPLY

>>>>> Structure No. 1 <<<<<<
(Input Data)

STAND PIPE

Stand Pipe with weir or orifice flow

E1 elev.(ft)? 46.2 ✓
E2 elev.(ft)? 47.001
Crest elev.(ft)? 46.2
Diameter (ft)? 3.5
Weir coefficient? 3.1
Orifice coefficient? 0.6
Start transition elev.(ft) @ ?
Transition height (ft)?

Outlet Structure File: CBS1 .STR

POND-2 Version: 5.17

S/N: 1295130250

Date Executed:

Time Executed:

CUSTOM BUILDER SUPPLY

Outflow Rating Table for Structure #1
STAND PIPE Stand Pipe with weir or orifice flow

***** INLET CONTROL ASSUMED *****

Elevation (ft)	Q (cfs)	Computation	Messages
46.20	0.0	Weir:	H = 0.0
46.30	1.1	Weir:	H = .1
46.40	3.0	Weir:	H = .2
46.50	5.6	Weir:	H = .3
46.60	8.6	Weir:	H = .4
46.70	12.1	Weir:	H = .5
46.80	15.8	Weir:	H = .6
46.90	20.0	Weir:	H = .7
47.00	24.4	Weir:	H = .8

Weir Cw = 3.1 Weir length = 10.99557 ft
Orifice Co = .6 Orifice area = 9.621128 sq.ft.
 $Q (cfs) = (Cw * L * H^{1.5})$ or $(Co * A * \text{sqr}(2 * g * H))$
No transition used, transition height = 0.0
Weir equation = Orifice equation @ elev. = 47.55907 ft

13

```
*****
*
* CUSTOM BUILDER SUPPLY 10 year post dev outflow *
*
*
*
*
*****
```

Inflow Hydrograph: b:100OUT .HYD
 Rating Table file: b:CBS1 .PND

----INITIAL CONDITIONS----
 Elevation = 46.20 ft
 Outflow = 0.00 cfs
 Storage = 12,583 cu-ft

GIVEN POND DATA			INTERMEDIATE ROUTING COMPUTATIONS	
ELEVATION (ft)	OUTFLOW (cfs)	STORAGE (cu-ft)	2S/t (cfs)	2S/t + 0 (cfs)
46.20	0.0	12,583	419.3	419.3
46.30	1.1	13,215	440.4	441.5
46.40	3.0	13,873	462.4	465.4
46.50	5.6	14,559	485.2	490.8
46.60	8.6	15,272	509.0	517.6
46.70	12.1	16,013	533.7	545.8
46.80	15.8	16,783	559.3	575.1
46.90	20.0	17,582	586.0	606.0
47.00	24.4	18,411	613.6	638.0

Time increment (t) = 1.0 min.

*check also 24" pipe
 to see which controls*

14

Pond File: b:CBS1 .PND
 Inflow Hydrograph: b:100OUT .HYD
 Outflow Hydrograph: b:OUT .HYD

INFLOW HYDROGRAPH

ROUTING COMPUTATIONS

TIME (min)	INFLOW (cfs)	I1+I2 (cfs)	2S/t - 0 (cfs)	2S/t + 0 (cfs)	OUTFLOW (cfs)	ELEVATION (ft)
0.0	0.00	-----	419.3	419.3	0.00	46.20
1.0	3.54	3.5	422.5	422.9	0.18	46.22
2.0	7.07	10.6	431.8	433.1	0.68	46.26
3.0	10.61	17.7	446.0	449.4	1.73	46.33
4.0	14.14	24.8	463.6	470.7	3.55	46.42
5.0	17.68	31.8	483.2	495.5	6.12	46.52
6.0	14.14	31.8	498.4	515.0	8.32	46.59
7.0	10.61	24.8	504.6	523.1	9.29	46.62
8.0	7.07	17.7	503.9	522.2	9.18	46.62
9.0	3.54	10.6	498.0	514.5	8.26	46.59
10.0	0.00	3.5	487.9	501.5	6.80	46.54

15

***** SUMMARY OF ROUTING COMPUTATIONS *****

Pond File: b:CBS1 .PND
Inflow Hydrograph: b:100OUT .HYD
Outflow Hydrograph: b:OUT .HYD

Starting Pond W.S. Elevation = 46.20 ft

***** Summary of Peak Outflow and Peak Elevation *****

Peak Inflow = 17.68 cfs
Peak Outflow = 9.29 cfs
Peak Elevation = 46.62 ft

***** Summary of Approximate Peak Storage *****

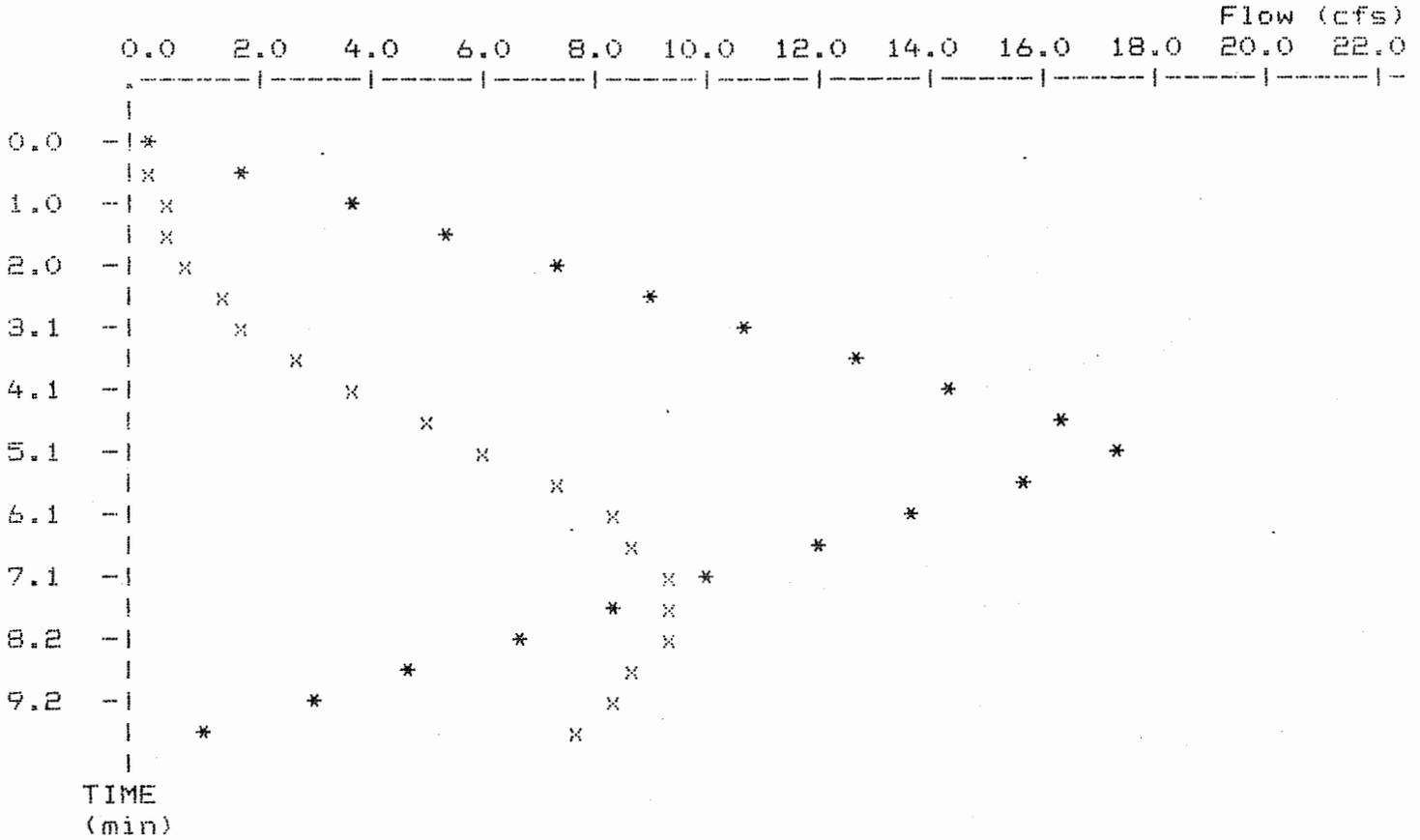
Initial Storage = 12,583 cu-ft
Peak Storage From Storm = 2,836 cu-ft

Total Storage in Pond = 15,419 cu-ft

Pond File: b:CBS1 .PND
Inflow Hydrograph: b:100OUT .HYD
Outflow Hydrograph: b:OUT .HYD

EXECUTED: 05-03-1994
12:16:59

Peak Inflow = 17.68 cfs
Peak Outflow = 9.29 cfs
Peak Elevation = 46.62 ft



x File: b:100OUT .HYD Qmax = 9.3 cfs
* File: b:OUT .HYD Qmax = 17.7 cfs

17

```
*****
*
*   CUSTOM BUILDER SUPPLY 100 yr post dev outflow *
*
*
*
*
*
*****
```

Inflow Hydrograph: b:100OUT .HYD
 Rating Table file: b:CBS1 .PND

-----INITIAL CONDITIONS-----
 Elevation = 46.20 ft
 Outflow = 0.00 cfs
 Storage = 12,583 cu-ft

GIVEN POND DATA			INTERMEDIATE ROUTING COMPUTATIONS	
ELEVATION (ft)	OUTFLOW (cfs)	STORAGE (cu-ft)	2S/t (cfs)	2S/t + O (cfs)
46.20	0.0	12,583	419.3	419.3
46.30	1.1	13,215	440.4	441.5
46.40	3.0	13,873	462.4	465.4
46.50	5.6	14,559	485.2	490.8
46.60	8.6	15,272	509.0	517.6
46.70	12.1	16,013	533.7	545.8
46.80	15.8	16,783	559.3	575.1
46.90	20.0	17,582	586.0	606.0
47.00	24.4	18,411	613.6	638.0

Time increment (t) = 1.0 min.

Pond File: b:CBS1 .PND
 Inflow Hydrograph: b:100OUT .HYD
 Outflow Hydrograph: b:OUT .HYD

18

INFLOW HYDROGRAPH

ROUTING COMPUTATIONS

TIME (min)	INFLOW (cfs)	I1+I2 (cfs)	2S/t - 0 (cfs)	2S/t + 0 (cfs)	OUTFLOW (cfs)	ELEVATION (ft)
0.0	0.00	---	419.3	419.3	0.00	46.20
1.0	4.67	4.7	423.5	424.0	0.23	46.22
2.0	9.34	14.0	435.7	437.6	0.90	46.28
3.0	14.02	23.4	454.1	459.1	2.50	46.37
4.0	18.69	32.7	476.4	486.8	5.19	46.48
5.0	23.36	42.1	501.0	518.5	8.71	46.60
6.0	18.69	42.1	519.6	543.1	11.77	46.69
7.0	14.02	32.7	526.4	552.3	12.92	46.72
8.0	9.34	23.4	524.6	549.8	12.61	46.71
9.0	4.67	14.0	516.2	538.6	11.21	46.67
10.0	0.00	4.7	502.8	520.8	9.01	46.61

19

***** SUMMARY OF ROUTING COMPUTATIONS *****

Pond File: b:CBS1 .PND
Inflow Hydrograph: b:100OUT .HYD
Outflow Hydrograph: b:OUT .HYD

Starting Pond W.S. Elevation = 46.20 ft

***** Summary of Peak Outflow and Peak Elevation *****

Peak Inflow = 23.36 cfs
Peak Outflow = 12.92 cfs
Peak Elevation = 46.72 ft

***** Summary of Approximate Peak Storage *****

Initial Storage = 12,583 cu-ft
Peak Storage From Storm = 3,601 cu-ft

Total Storage in Pond = 16,184 cu-ft

5/18/94

D Cook

Custom Builder Supply

Discharge for culvert between the 2 pond sections

$$Q = C a \sqrt{2gh}$$

$$C = \left(1.1 + \frac{0.026 L}{d^{1.2}} \right)^{-1/2} = \left(1.1 + \frac{0.026 (72)}{1.23} \right)^{-1/2} = 0.63$$

$$Q = (0.63)(1.23) \sqrt{2 \cdot 32.2 \cdot 1} = 6.2 \text{ cfs}$$

Determine head losses

$$H_v = \frac{V^2}{2g} = \frac{25}{64.4} = 0.39'$$

$$H_e = 0.15 \times \frac{V^2}{2g} = \frac{0.06}{0.45'}$$

$$Q = VA =$$

$$V = \frac{Q}{A} = \frac{6.2}{1.23} = 5' / \text{sec}$$

$$46.2 - 1.25 - 0.45 = 44.5'$$