



CERTIFICATE OF AUTHENTICITY

THIS IS TO CERTIFY THAT THE FOLLOWING ELECTRONIC RECORDS ARE TRUE AND ACCURATE REPRODUCTIONS OF THE ORIGINAL RECORDS OF JAMES CITY COUNTY GENERAL SERVICES DEPARTMENT- STORMWATER DIVISION; WERE SCANNED IN THE REGULAR COURSE OF BUSINESS PURSUANT TO GUIDELINES ESTABLISHED BY THE LIBRARY OF VIRGINIA AND ARCHIVES; AND HAVE BEEN VERIFIED IN THE CUSTODY OF THE INDIVIDUAL LISTED BELOW.

BMP NUMBER: WC072

DATE VERIFIED: July 11, 2012

QUALITY ASSURANCE TECHNICIAN: Leah Hardenbergh



LOCATION: WILLIAMSBURG, VIRGINIA



Stormwater Division

MEMORANDUM

DATE: March 12, 2010
TO: Michael J. Gillis, Virginia Correctional Enterprises Document Management Services
FROM: Jo Anna Ripley, Stormwater
PO: 270712
RE: Files Approved for Scanning

General File ID or BMP ID: WC072

PIN: 0520400001A

Subdivision, Tract, Business or Owner

Name (if known):

Stonehouse

Property Description:

Bent Tree Common Area Section 3

Site Address:

(For internal use only)

Box 20

Drawer: 8

Agreements: (in file as of scan date)

Y

Book or Doc#:

010018060

Page:

990026872

Comments

DECLARATION OF COVENANTS

DRAFT

INSPECTION/MAINTENANCE OF DRAINAGE SYSTEM

THIS DECLARATION, made this 25th day of SEPTEMBER, 2001,
 between STONEHOUSE, LLC,
 and all successors in interest, hereinafter referred to as the "COVENANTOR(S)," owner(s) of the
 following property: SECTION Y-B ("BENT TREE" - SECTION 3),
 Deed Book _____, Page No. _____ or Instrument No. 99-0026872,
 and James City County, Virginia, hereinafter referred to as the "COUNTY."

WITNESSETH:

We, the COVENANTOR(S), with full authority to execute deeds, mortgages, other covenants, and all rights, titles and interests in the property described above, do hereby covenant with the COUNTY as follows:

1. The COVENANTOR(S) shall provide maintenance for the drainage system including any runoff control facilities, conveyance systems and associated easements, hereinafter referred to as the "SYSTEM," located on and serving the above-described property to ensure that the SYSTEM is and remains in proper working condition in accordance with approved design standards, and with the law and applicable executive regulations. The SYSTEM shall not include any elements located within any Virginia Department of Transportation rights-of-way.
2. If necessary, the COVENANTOR(S) shall levy regular or special assessments against all present or subsequent owners of property served by the SYSTEM to ensure that the SYSTEM is properly maintained.
3. The COVENANTOR(S) shall provide and maintain perpetual access from public right-of-ways to the SYSTEM for the COUNTY, its agent and its contractor.
4. The COVENANTOR(S) shall grant the COUNTY, its agent and its contractor a right of entry to the SYSTEM for the purpose of inspecting, operating, installing, constructing, reconstructing, maintaining or repairing the SYSTEM.
5. If, after reasonable notice by the COUNTY, the COVENANTOR(S) shall fail to maintain the SYSTEM in accordance with the approved design standards and with the law and applicable executive regulations, the COUNTY may perform all necessary repair or maintenance work, and the COUNTY may assess the COVENANTOR(S) and/or all property served by the SYSTEM for the cost of the work and any applicable penalties.
6. The COVENANTOR(S) shall indemnify and save the COUNTY harmless from any and all claims for damages to persons or property arising from the installation, construction, maintenance, repair, operation or use of the SYSTEM.
7. The COVENANTOR(s) shall promptly notify the COUNTY when the COVENANTOR(S) legally transfers any of the COVENANTOR(S)' responsibilities for the SYSTEM. The COVENANTOR(S)' shall supply the COUNTY with a copy of any document of transfer, executed by both parties.
8. The covenants contained herein shall run with the land and shall bind the COVENANTOR(S) and the COVENANTOR(S)' heirs, executors, administrators, successors and assignees, and shall bind all present and subsequent owners of property served by the SYSTEM.
9. This COVENANT shall be recorded in the County Land Records.

Instrument # 010018060

Recorded on Oct. 4, 2001

IN WITNESS WHEREOF, the COVENANTOR(S) have executed this DECLARATION OF COVENANTS as of this 25TH day of SEPTEMBER, 19 2001

COVENANTOR(S)

James H. Bennett

Print Name/Title

JAMES H. BENNETT
VICE PRESIDENT

ATTEST:

COVENANTOR(S)

Print Name/Title

ATTEST:

COMMONWEALTH OF VIRGINIA
CITY/COUNTY OF James City

I hereby certify that on this 25th day of September, 19 2001, before the subscribed, a Notary Public of the State of Virginia, and for the City/County of James City, aforesaid personally appeared James H. Bennett and did acknowledge the foregoing instrument to be their Act.

IN WITNESS WHEREOF, I have hereunto set my hand and official seal this 25th day of September, 19 2001.

Joan Stalberger
Notary Public

My Commission expires: 9/25/04

Approved as to form:

Lee P. Rogers
Deputy County Attorney

This Declaration of Covenants prepared by:

JAMES H. BENNETT
(Print Name)

VICE PRESIDENT
(Title)

9701 MILL POND RUN
(Address)

TOANO VA 23168
(City) (State) (Zip)

drainage.pre
Revised 2/97

S-68-01
S-81-99

Handwritten signature



**James City County Environmental Division
Stormwater Management/BMP Record Drawing &
Construction Certification Review
Tracking Form**

Project Name: Storehouse Bent Tree sec 5B Ph 3
County Plan No.: 6-81-99 S-68-01
Stormwater Management Facility: BMP # 5.4 Dry Pond
BMP Phase #: I II III
 Information Package Received. Date/By: 10/12/04 AES

Completeness Check:
 Record Drawing Date/By: 2/13/06 AES
 Construction Certification Date/By: 2/17/06 GET
 RD/CC Standard Forms (Required for all BMPs after Feb 1st 2001 Only)
 Insp/Maint Agreement # / Date: # 01018060 Oct 04 2004
 BMP Maintenance Plan Location: Sheet 17
 Other: N

Standard E&SC Note on Approved Plan Requiring RD/CC or County comment in plan review
 Yes No Location: Note # 19 on Sheet 15
 Assign County BMP ID Code #: Code: WC 072

Preliminary Input/Log into Division's "As-Built Tracking Log"
 Add Location to GIS Map. Obtain basic site information (GPIN, Owner, Address, etc.)
 Preliminary Log into Access Database (BMP ID #, Plan No., GPIN, Project Name, etc.)
 Active Project File Review (correspondence, H&H, design computations, etc.)
 Initial As-Built File setup (File label, folder, copy plan/details/design information, etc.)
 Inspector Check of RD/CC (forward to Inspector using transmittal for cursory review).
 Pre-Inspection Drawing Review of Approved Plan (Quick look prior to Field Inspection).
 Final Inspection (FI) Performed Date: 1/13/05 SJT
 Record Drawing (RD) Review Date: 02/12/06 SJT
 Construction Certification (CC) Review Date: 02/12/06 SJT

Actions:
 No comments.
 Comments. Letter Forwarded. Date: _____
 Record Drawing (RD)
 Construction Certification (CC)
 Construction-Related (CR) much - list completed. Insp 1/13/05
 Site Issues (SI)
 Other: _____

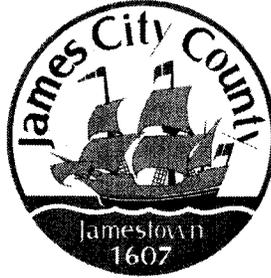
Second Submission:
 Reinspection (if necessary): 5/30/06 SJT
 Acceptable for SWM Purposes (RD/CC/CR/Other). Ok to proceed with bond release.
 Complete "Surety Request Form".
 Check/Clean active file of any remaining material and finish "As-Built" file.
 Add to County BMP Inventory/Inspection schedule (Phase I, II or III).
 Copy Final Inspection Report into County BMP Inspection Program file.
 Obtain Digital Photographs of BMP and save into County BMP Inventory.
 Request mylar/reproducible from As-Built plan preparer.
 Complete "As-built Tracking Log".
 Last check of BMP Access Database (County BMP Inventory).
 Add BMP to JCC Hydrology & Hydraulic database (optional).
 Add BMP to Municipal BMP list (if a County-owned facility)
 Add BMP to PRIDE BMP ratings database.

Final Sign-Off

Plan Reviewer: *[Signature]*

Date: 02/13/07

*** See separate checklist, if needed.



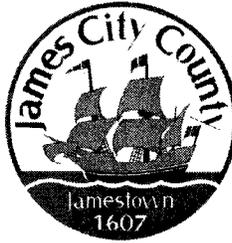
James City County, Virginia
Environmental Division

Stormwater Management / BMP Facilities Record Drawing and Construction Certification

Standard Forms & Instructions

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Issue Date
February 1, 2001



James City County, Virginia
Environmental Division

Stormwater Management / BMP Facilities
Record Drawing and Construction Certification Forms

(Note: In accordance with the requirements of the Chesapeake Bay Preservation Ordinance, Chapter 23, Section 23-10(4), BMP's shall be designed and constructed in accordance with the manual entitled James City County Guidelines for Design and Construction of Stormwater Management BMP's. Erosion and sediment control policy and approved plans generally require that at the completion of the project and prior to release of surety, an "as-built" plan prepared by a registered Professional Engineer or Certified Land Surveyor must be provided for the drainage system for the project, including any Best Management Practice (BMP) facilities. In addition, for BMP facilities involving the construction of an impounding structure or dam embankment, certification is required by a Professional Engineer who has inspected the structure during its construction. Currently there are over 20 water quality type BMP's accepted by the County.)

Section 1 – Site Information:

Project Name: Stonehouse - Section V-B (Bent Tree Phase 3)
Structure/BMP Name: BMP #5.4
Project Location: Stonehouse - Bent Tree
BMP Location: Off Private Drive at end of Sapling Drive
County Plan No.: JCC Case No. S - 81 - 99

Project Type: Residential Business Tax Map/Parcel No.: (6-4) (1-1)
 Commercial Office BMP ID Code (if known): WC072
 Institutional Industrial Zoning District: PUD-R
 Public Roadway Land Use: Residential
 Other Site Area (sf or acres): 20.86

Brief Description of Stormwater Management/BMP Facility: Dry Pond

Nearest Visible Landmark to SWM/BMP Facility: Private Drive at end of Sapling Drive

Nearest Vertical Ground Control (if known):
 JCC Geodetic Ground Control USGS Temporary Arbitrary Other
Station Number or Name: 303
Datum or Reference Elevation: NGVD 1929
Control Description: NAD 27
Control Location from Subject Facility: 3.5 miles south

Section 2 – Stormwater Management / BMP Facility Construction Information:

PreConstruction Meeting Held for Construction of SWM/BMP Facility: Yes No Unknown
Approx. Construction Start Date for SWM/BMP Facility: September 2001
Facility Monitored by County Representative during Construction: Yes No Unknown
Name of Site Work Contractor Who Constructed Facility: George Nice & Sons, Inc.
Name of Professional Firm Who Routinely Monitored Construction: _____
Date of Completion for SWM/BMP Facility: October 2002
Date of Record Drawing/Construction Certification Submittal: 11/07/02

(Note: Record Drawing and Construction Certifications are required within thirty (30) days of the completion of Stormwater Management and/or BMP facility construction. Record Drawings and Construction Certifications must be reviewed and approved by the James City County Environmental Division prior to final inspection, acceptance and bond or surety release.)

Section 3 – Owner / Designer / Contractor Information:

Owner/Developer: *(Note: Site Owner or Applicant responsible for development of the project.)*

Name: Stonehouse Development Company
Mailing Address: 9701 Mill Pond Run
Toano, VA 23168
Business Phone: 757-234-5000 Fax: 757-234-5091
Contact Person: Jerry Moore Title: President

Design Professional: *(Note: Professional Engineer or Certified Land Surveyor responsible for the design and preparation of plans and specifications for the Stormwater Management / BMP facility.)*

Firm Name: AES Consulting Engineers
Mailing Address: 5248 Olde Towne Road, Suite 1
Williamsburg, VA 23188
Business Phone: 757-253-0040
Fax: 757-220.8994
Responsible Plan Preparer: Marc Bennett
Title: Senior Project Manager
Plan Name: Stonehouse - Development Area One, Phase 1- Section V-B, "Bent Tree" - Phase 3
Firm's Project No. 8878-00
Plan Date: March 2, 2001
Sheet No.'s Applicable to SWM/BMP Facility: 7 / 13 / 14 / 17 /

BMP Contractor: *(Note: Site Work Contractor directly responsible for construction of the Stormwater Management / BMP facility.)*

Name: George Nice & Sons, Inc.
Mailing Address: 143 Skimino Road
Williamsburg, VA 23188-2229
Business Phone: (757) 565-2885
Fax: (757) 565-1526
Contact Person: Ray Nice P. E.
Site Foreman/Supervisor: _____
Specialty Subcontractors & Purpose (for BMP Construction Only):

Section 4 – Professional Certifications:

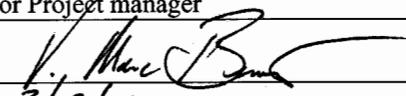
Certifying Professionals: *(Note: A Registered Professional Engineer of Certified Land Surveyor is responsible for preparation of a Record Drawing, sometimes referred to as an As-Built plan, for the drainage system for the project including any Stormwater Management/BMP Facilities. A Registered Professional Engineer is responsible for the inspection, monitoring and certification of Stormwater Management / BMP facilities during its construction.)*

Record Drawing and Construction Certifications for Stormwater Management / BMP Facilities

Record Drawing Certification

Firm Name: AES Consulting Engineers
Mailing Address: 5248 Olde Towne Road, Suite 1
Williamsburg, VA 23188
Business Phone: 757-253-0040
Fax: 757-220-8994

Name: Marc Bennett
Title: Senior Project manager

Signature: 
Date: 2/13/06

I hereby certify to the best of my knowledge and belief that this record drawing represents the actual condition of the Stormwater Management / BMP facility. The facility appears to conform with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.

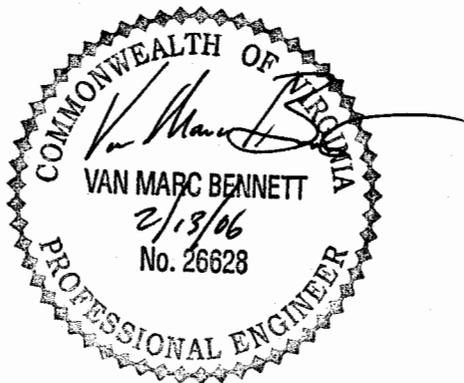
Construction Certification

Firm Name: _____
Mailing Address: _____
Business Phone: _____
Fax: _____

Name: _____
Title: _____

Signature: _____
Date: _____

I hereby certify to the best of my knowledge and belief that this Stormwater Management / BMP facility was monitored and constructed in accordance with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.



 (Seal)

Virginia Registered Professional Engineer
Or Certified Land Surveyor

_____ (Seal)

Virginia Registered
Professional Engineer

Section 4 – Professional Certifications:

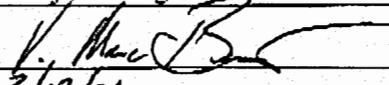
Certifying Professionals: *(Note: A Registered Professional Engineer or Certified Land Surveyor is responsible for preparation of a Record Drawing, sometimes referred to as an As-Built plan, for the drainage system for the project including any Stormwater Management/BMP Facilities. A Registered Professional Engineer is responsible for the inspection, monitoring and certification of Stormwater Management / BMP facilities during its construction.)*

Record Drawing and Construction Certifications for Stormwater Management / BMP Facilities

Record Drawing Certification

Firm Name: AES Consulting Engineers
Mailing Address: 5248 Olde Towne Road, Suite 1
Williamsburg, VA 23188
Business Phone: 757-253-0040
Fax: 757-220-8994

Name: Marc Bennett
Title: Senior Project manager

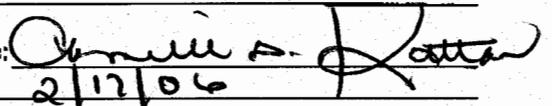
Signature: 
Date: 2/13/06

I hereby certify to the best of my knowledge and belief that this record drawing represents the actual condition of the Stormwater Management / BMP facility. The facility appears to conform with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.

Construction Certification

Firm Name: _____
Mailing Address: _____
Business Phone: _____
Fax: _____

Name: _____
Title: _____

Signature: 
Date: 2/17/06

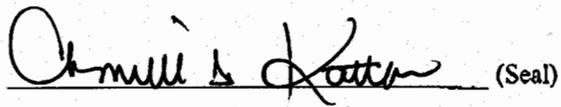
I hereby certify to the best of my knowledge and belief that this Stormwater Management / BMP facility was monitored and constructed in accordance with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.



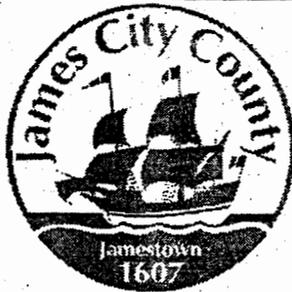
 (Seal)

Virginia Registered Professional Engineer
Or Certified Land Surveyor



 (Seal)

Virginia Registered
Professional Engineer



**James City County, Virginia
Environmental Division**

**Erosion and Sediment Control and
Stormwater Management Design Plan Checklists**

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GENERAL INFORMATION

Project Name: BENT TREE - PHASE 3 (STONEHOUSE)
 Owner / Applicant: STONEHOUSE DEVELOPMENT COMPANY, LLC
 Plan Preparer: AES CONSULTING ENG. Email: _____
 Project Location: ADJACENT TO BENT TREE - PHASE 1 (NORTH OF Mill Pond Road)
 Tax Map / Parcel: _____
 County Plan No. (if known): _____
 County BMP Type: EXTENDED DETENTION DET. POND (F-2)

Other information submitted in addition to this checklist (Check all that apply):

- Design or Construction Drawings (Plans, Profiles, Details, etc.).
- Erosion & Sediment Control Plan (Plans, Details, etc.).
- Erosion & Sediment Control Plan Design Report.
- Stormwater Management Design Plan (Plans, Profiles, Details, etc.).
- Stormwater Management Design Report.
- Other, List: _____

*SA
REVIEW
04-10-01*

**Issue Date
March 1, 2001**

**JAMES CITY COUNTY, VIRGINIA
ENVIRONMENTAL DIVISION**

EROSION AND SEDIMENT CONTROL PLAN CHECKLIST

I. GENERAL:

Yes No N/A

- FAMILIARITY** with current versions of Chapter 8, Erosion and Sedimentation Control and Chapter 23, Chesapeake Bay Preservation ordinances of the Code of James City County, Virginia and the Virginia Erosion and Sediment Control Handbook (VESCH).
- LAND DISTURBING PERMIT AND SILTATION AGREEMENT** with surety are required for the project.
- VARIANCE** if necessary, requested in writing, for the plan approving authority to waive or modify any of the minimum standards and specifications of the VESCH deemed inappropriate based on site conditions specific to this review case only. Variances which are approved shall be properly documented in the plan and become part of the approved erosion and sediment control plan for the site. *25% SLOPE WAIVER REQUEST.*

II. SITE PLAN:

Yes No N/A

- VICINITY MAP** locating the site in relation to the surrounding area. Include any major landmarks which might assist in physically locating the site.
- INDICATE NORTH** direction in relation to the site.
- LIMITS OF CLEARING AND GRADING** for the site including that required for implementation of erosion and sediment controls, stockpile areas and utilities.
- DISTURBED AREA ESTIMATES** in acres or square feet for the project.
- EXISTING TOPOGRAPHY** or contours for the site at no more than 5 foot contour interval.
- FINAL TOPOGRAPHY**, contours or proposed site grading in accordance with the design plan which indicates changes to existing topography and drainage patterns at no more than 2 foot contour interval (or 1 foot contours where required).
- EXISTING AND PROPOSED SPOT ELEVATIONS** to supplement existing and proposed contours, topography or site grading information. Spot elevations may replace final contours in some instances, especially if terrain is in a low lying area or relatively flat.
- EXISTING VEGETATION** including existing tree lines, grassed or unique vegetation areas.

Yes No N/A

EXISTING SITE FEATURES including roads, buildings, homes, utilities, streams, fences, structures and other important surface features of the site.

SOILS MAP with soil symbols, boundaries and legend in accordance with the current Soil Survey of James City and York Counties and the City of Williamsburg, Virginia.

ENVIRONMENTAL INVENTORY in accordance with Section 23-10(2) of the Chesapeake Bay Preservation Ordinance of James City County. Inventory generally includes: tidal shores and wetlands, non-tidal wetlands, resource protection area, hydric soils and slopes steeper than 25 percent. For wetlands, provide a copy of issued permits or satisfactory evidence that appropriate permits are being pursued for the entire project.

WE HAVE REQUESTED
COPY OF WETLANDS
PERMIT FROM CORPS.

100-YEAR FLOODPLAIN LIMITS or any special flood hazard areas or flood zones based on appropriate Federal Management Agency Flood Insurance Rate Maps (FIRMs) or Flood Hazard Boundary Maps (FHBMs) of James City County, Virginia. *ZONE A NOT SHOWN.*

DRAINAGE AREAS for offsite and onsite areas, existing or proposed as applicable. Include drainage divides and directional labels for all subareas at points of interest and size (in acres), weighted runoff coefficient or curve number and times of concentration for each subarea.

CRITICAL EROSION AREAS which require special consideration or unique erosion and sediment control measures. Refer to the VESCH, Chapter 6 for criteria.

DEVELOPMENT PLAN for the site showing all improvements such as buildings, structures, parking areas, access roadways, above and below ground utilities, stormwater management and drainage facilities, trails or sidewalks, proposed vegetation and landscaping, amenities, etc.

LOCATION OF PRACTICES proposed for erosion and sediment control, tree protection and temporary stormwater management due to land disturbance activities at the site. Use standard abbreviations, labels and symbols consistent for plan views based on minimum standards and specifications in Chapter 3 of the VESCH.

TEMPORARY STOCKPILE AREAS or staging and equipment storage areas as required for onsite or offsite construction activities or indicate that none are anticipated for this project. *NOT ADDRESSED*

OFFSITE LAND DISTURBING AREAS including borrow sites, waste areas, utility extensions, etc. and required erosion and sediment controls. If none are anticipated for the project, then indicate on the plans by general or erosion and sediment control notes.

DETAILS or alternately, appropriate reference to current minimum standards and specifications of the VESCH for each measure proposed for the project. Non-modified, standard duplicated details (silt fence, diversion dikes, etc.) may be referenced to the current version of the VESCH. Specific dimensional or modified standards (basins, traps, outlet protections, check dams, etc.) require presentation on detail sheets. Schedules or tables may be used for multiple site measures such as sediment traps, basins, channels, slope drains, etc. Any modification to standard details should be clearly defined, explained and illustrated.

Yes No N/A

MAINTENANCE PLAN or alternately, appropriate reference to current minimum standards and specifications of the VESCH, outlining the inspection frequency and maintenance requirements for all erosion and sediment control measures proposed for the project.

TRENCH DEWATERING methods and erosion and sediment controls, if anticipated for the project.

CONSTRUCTION SEQUENCE outlining the anticipated sequence for installation of erosion and sediment controls and site, grading and utility work to be performed for the project by the site contractor.

PHASING PLAN if required for larger project sites that are to be developed in stages or phases.

STANDARD COUNTY NOTES are required to be placed on the erosion and sediment control plan. Refer to the standard James City County Erosion and Sediment Control Notes dated May 5, 1999.

PROFESSIONAL SEAL AND SIGNATURE required on final and complete approved plans, drawings, technical reports and specifications.

NOT on Design report for BMP & storm drainage.

III.

NARRATIVE:

WHERE?

Yes No N/A

PROJECT DESCRIPTION briefly describing the nature and purpose of the land disturbing activity and the acreage to be disturbed.

EXISTING SITE CONDITIONS description of existing topography, land use, cover and drainage patterns at the site.

ADJACENT AREA descriptions of neighboring onsite or offsite areas such as streams, lakes, property, roads, etc. and potential impacts due to concentrated flow or runoff from the land disturbing activity.

OFFSITE DISTURBED AREA descriptions of proposed borrow sites, waste or surplus areas, utility extensions and erosion and sediment controls to be implemented.

SOILS DESCRIPTION briefly summarizing site, disturbed area and drainage basin soils including name, unit, hydrologic soil group (HSG) classification, surface runoff potential, erodibility, permeability, depth, texture, structure, erosion hazards, shrink-swell potential, limitations for use and anticipated depths to bedrock and the seasonal water table, as applicable.

CRITICAL AREAS on the site which may have potentially serious erosion and sediment control problems and special considerations required (ie. steep slopes, hydric soils, channels, springs, sinkholes, water supply reservoirs, groundwater recharge areas, etc.)

Yes No N/A

?

PROPOSED EROSION & SEDIMENT CONTROL MEASURES inclusive to the specific erosion and sediment control plan as proposed for the land disturbing activity. Measures should be consistent with those proposed on the site drawings. Address general use, installation, limitations, sequencing and maintenance requirements for each control measure.

?

STABILIZATION MEASURES required for the site, either temporary or permanent, and during and following construction including temporary and permanent seeding and mulching, paving, stone, soil stabilization blankets and matting, sodding, landscaping or special stabilization techniques to be utilized at the site.

?

STORMWATER MANAGEMENT CONSIDERATIONS for the site, either of temporary or permanent nature, and strategies, sequences and measures required for control. May reference the stormwater management plan for the site, if prepared, for permanent stormwater management facilities and control of drainage once the site is stabilized.

IV. CALCULATIONS:

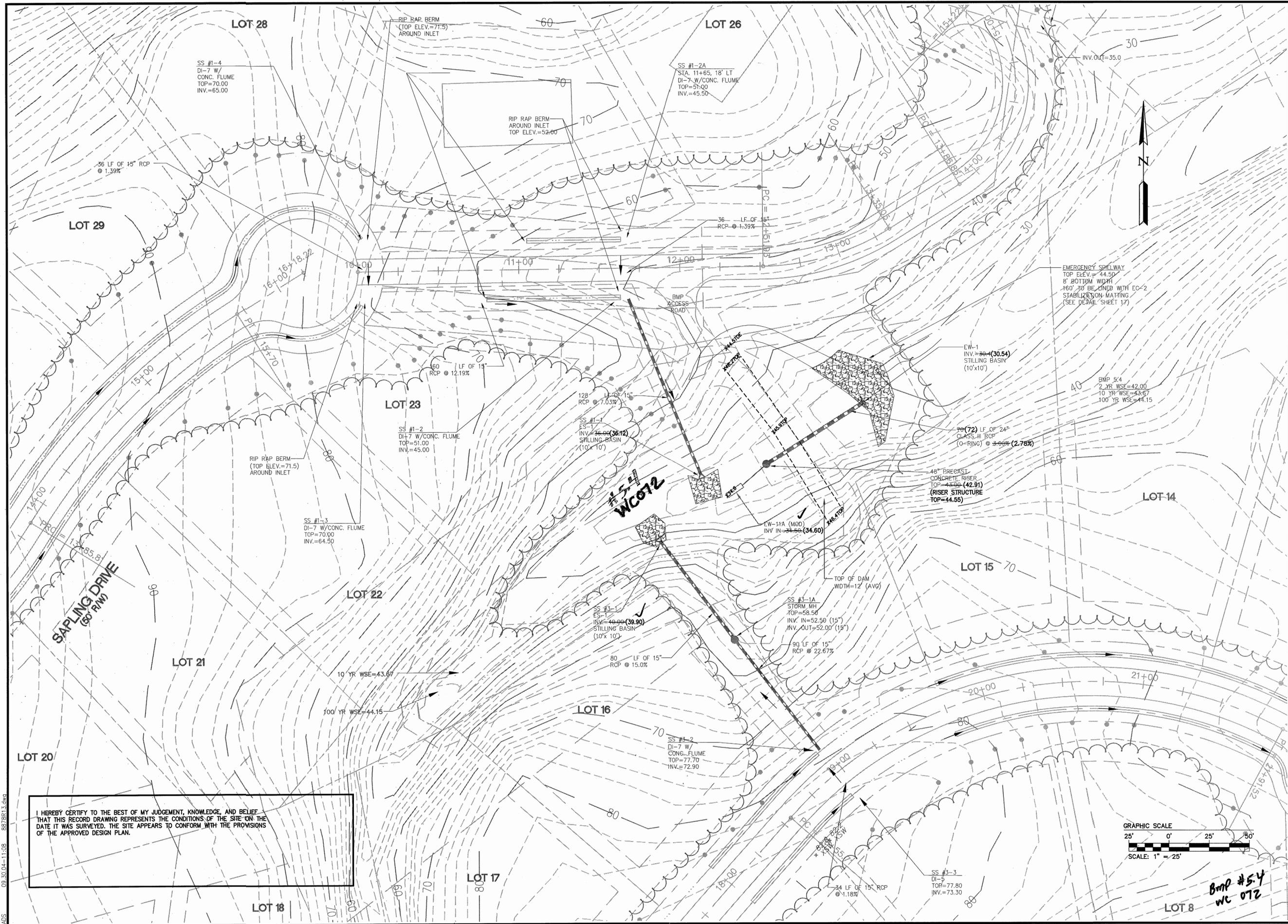
Yes No N/A

CALCULATIONS AND COMPUTATIONS associated with hydrology, hydraulics and design of proposed temporary and permanent erosion and sediment control measures including: sediment traps and basins, diversions, stormwater conveyance channels, culverts, slope drains, outlet protections, etc. Computations are not required on the construction plan and may be attached in a supplemental erosion and sediment control plan design report, if presented in a clear and organized format.

○

TEMPORARY SEDIMENT BASIN DESIGN DATA SHEET submitted for each basin along with schematic or sketch cross-section showing applicable design and construction data, storage volumes (wet-dry), dimensions and elevations. Peak design runoff to be based on the 2- or 25-year design storm event based on maximum disturbed site conditions (existing, interim or proposed conditions) in accordance with Minimum Standard 3.14 of the VESCH.

Need for sed BASIN #1 & #2



I HEREBY CERTIFY TO THE BEST OF MY JUDGEMENT, KNOWLEDGE, AND BELIEF THAT THIS RECORD DRAWING REPRESENTS THE CONDITIONS OF THE SITE ON THE DATE IT WAS SURVEYED. THE SITE APPEARS TO CONFORM WITH THE PROVISIONS OF THE APPROVED DESIGN PLAN.

NO.	DATE	REVISION / COMMENT / NOTE	BY
4	11/20/03	BMP #5.4 RECORD DRAWING	RED
3	10/25/01	REVISED PER JCSA AND JCC COMMENTS	REW
2	10/24/01	REVISED PER JCC AND JCC COMMENTS	REW
1	10/22/01	REVISED PER JCC AND JCC COMMENTS	REW

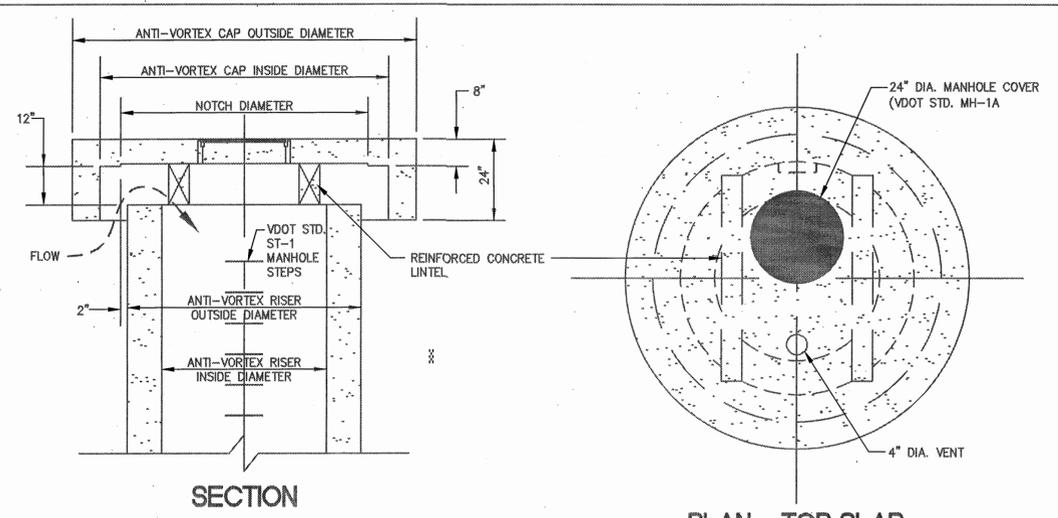


5248 Old Towne Road, Suite 1
Williamsburg, Virginia 23188
(757) 253-0040
Fax (757) 220-8994



RECORD DRAWING
& BMP #5.4
SECTION V-B 'BENT TREE' - PHASE 3
AT STONEHOUSE
FOR
STONEHOUSE DEVELOPMENT COMPANY, L.L.C.
STONEHOUSE DISTRICT
JAMES CITY COUNTY, VIRGINIA

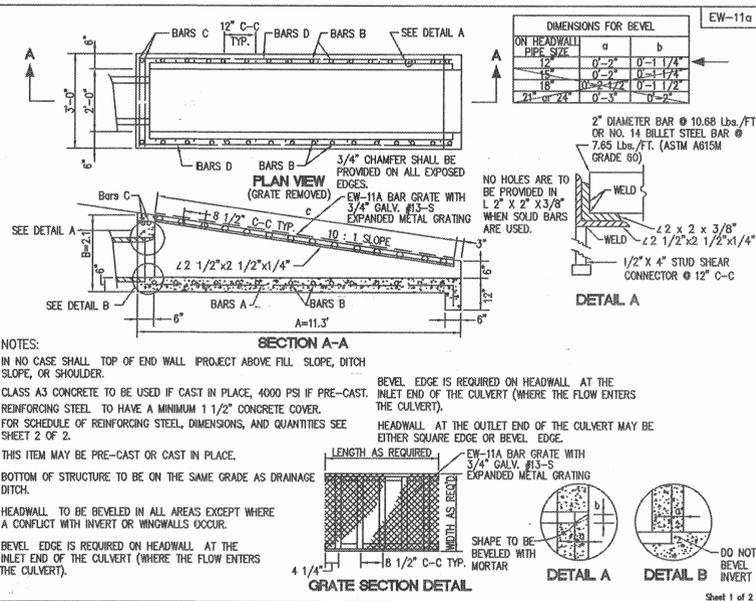
DESIGNED	DRAWN
RED	RED
SCALE	DATE
1" = 25'	1/29/03
PROJECT NO.	8878-00
DRAWING NO.	R13(B)



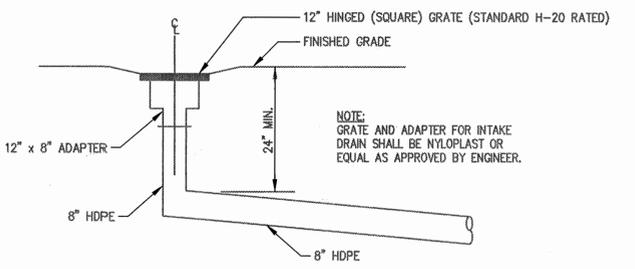
RISER		ANTI-VORTEX CAP		NOTCH DIAMETER	APPROXIMATE CAP WEIGHT
I.D.	O.D.	I.D.	O.D.		
48"	58"	84"	100"	62"	4.27 T

- ANTI-VORTEX DEVICE (CAP AND RISER) MANUFACTURED IN ACCORDANCE WITH ASTM C478.
- DIMENSIONS SUBJECT TO PERMISSIBLE VARIATIONS OF ASTM C478.
- INLET AREA (AREA BETWEEN DEVICE I.D. AND RISER O.D.) IS GREATER THAN OUTLET AREA (AREA OF RISER I.D.).
- SLAB REINFORCEMENT TO BE ASTM A615 #4 BARS @ 8" E.W. CIRCUMFERENTIAL.

ANTI-VORTEX DETAIL
NOT TO SCALE



PIPE ENDWALL WITH LOAD - CARRYING GRATE



INLINE DRAIN AT COMMON DRIVES

GENERAL NOTES FOR CONSTRUCTION OF STORMWATER BASINS

- THE CONTRACTOR SHALL PROVIDE ALL WORK AND MATERIALS NEEDED TO CONSTRUCT THE STORMWATER BASIN, STORMWATER MANAGEMENT PONDS, BEST MANAGEMENT PRACTICES, SEDIMENT BASINS AND SEDIMENT TRAPS. THE WORK SHALL INCLUDE ALL LABOR, MATERIALS, EQUIPMENT AND MATERIALS NEEDED FOR THE COMPLETION OF GRADING AND EARTHWORK ASSOCIATED WITH THE CONSTRUCTION.
- THE CONTRACTOR SHALL CONSULT AND PROVIDE FOR THE SERVICES OF A GEOTECHNICAL ENGINEER. THE GEOTECHNICAL ENGINEER SHALL PROVIDE TEST RESULTS ON PLACED DAM MATERIALS, IDENTIFYING SOIL CLASSIFICATION, PERMEABILITY, PLASTICITY INDEX, AND COMPACTION. ALL TESTS SHALL BE IN CONFORMANCE WITH ASTM STANDARDS. THE COST OF THE SERVICES OF THE GEOTECHNICAL ENGINEER SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR. SATISFACTORY GEOTECHNICAL RESULTS ARE NEEDED PRIOR TO FINAL APPROVAL.
- ALL INSPECTIONS REQUIRED FOR THE WORK SHALL BE PERFORMED BY A GEOTECHNICAL ENGINEER AT THE EXPENSE OF THE GENERAL CONTRACTOR.
- ON-SITE EXCAVATED MATERIAL, IF DETERMINED SUITABLE FOR USE IN DAM CONSTRUCTION BY A GEOTECHNICAL ENGINEER, MAY BE USED FOR DAM CONSTRUCTION. SHOULD ADDITIONAL MATERIAL BE REQUIRED, THE CONTRACTOR SHALL IDENTIFY THE NEED FOR MATERIAL TO THE OWNER, AS ADDITIONAL BORROW MATERIAL MAY BE AVAILABLE ON THE STONEHOUSE PROPERTY. ALL EXCAVATED MATERIAL DETERMINED BY THE GEOTECHNICAL ENGINEER TO BE UNSUITABLE SHALL BE DISPOSED OF PROPERLY AT THE CONTRACTOR'S EXPENSE. ALL EXCAVATED MATERIAL NOT REQUIRED FOR BACKFILLING SHALL EITHER BE DEPOSITED ON SITE AND SPREAD BY THE CONTRACTOR, OR SHALL BE DEPOSITED IN AN AREA ON THE STONEHOUSE PROPERTY AS DIRECTED BY THE GEOTECHNICAL ENGINEER. MEASURES NEEDED TO CONTROL AS PER THE VESCH THIRD EDITION.
- UNDERCUT FOR THE FOUNDATION OF THE DAM EMBANKMENT SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATION. THE FOUNDATION SHALL BE BACKFILLED WITH SOILS CLASSIFIED AS SM, SC, OR CL UNDER THE UNIFIED SOIL CLASSIFICATION SYSTEM. SOILS SHALL HAVE A MINIMUM OF 15% BY WEIGHT FINES, HAVING A PLASTICITY INDEX <math>PI < 30</math> AND A PERMEABILITY OF 0.0004 IN./SEC. OR LESS. FILL SHALL BE COMPACTED IN 12-INCH LIFTS, OR AS DIRECTED BY THE GEOTECHNICAL ENGINEER, TO A DRY DENSITY OF 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY (ASTM D-698). EXCAVATION FOR THE DAM KEY SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATION. HEIGHT, DEPTH, AND WIDTH OF THE KEY SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS. THE KEY SHALL BE FORMED USING SOILS CLASSIFIED AS SC OR CL, WITH A PERMEABILITY OF 0.0004 IN./SEC. OR LESS.
- THE DAM CORE SHALL BE AS CONSTRUCTED WITH NON-EXPANSIVE SC OR CL CLAYEY MATERIAL WITH PERMEABILITY OF 0.0004 IN./SEC. OR LESS. THE FILL OF THE CORE SHALL BE MADE IN 12-INCH LIFTS, OR AS DIRECTED BY THE GEOTECHNICAL ENGINEER, TO AT LEAST 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY (ASTM D-698). SIZE, SHAPE, WIDTH, DEPTH, AND HEIGHT OF THE DAM CORE SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS. TO COVER THE DAM CORE, A SILTY FINE SAND OR CLAYEY SOIL (SM, SC, OR CL) SHALL BE PLACED. A VEGETATIVE COVER USING VDOT EC-2 EROSION CONTROL BLANKETS SHALL BE PLACED ON DAM SLOPES AND CREST TO PREVENT EROSION.
- UPON COMPLETION, THE CONSTRUCTION OF THE DAM WILL BE CERTIFIED BY A GEOTECHNICAL ENGINEER WHO HAS INSPECTED THE STRUCTURE DURING CONSTRUCTION.

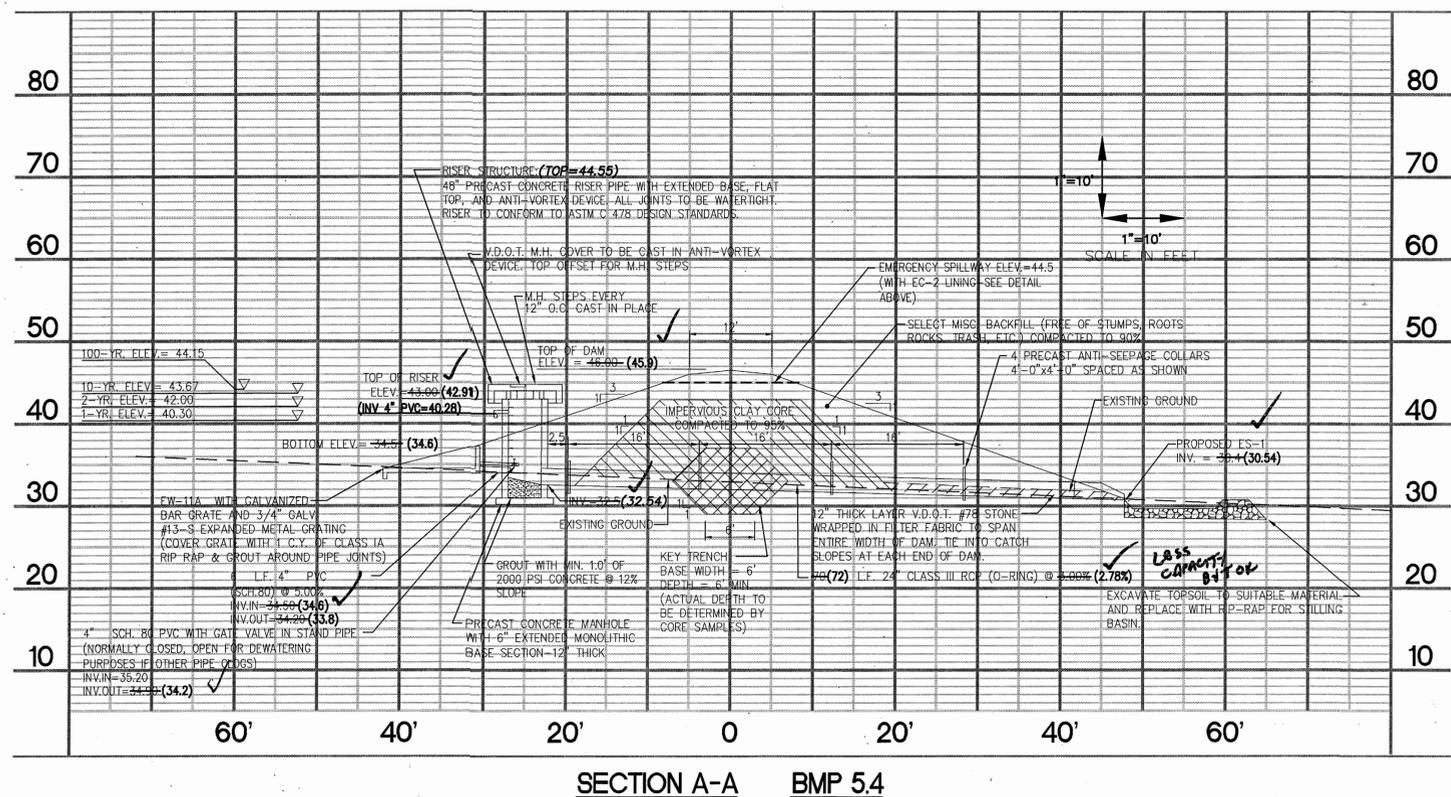
STORMWATER MANAGEMENT/ BMP FACILITY MAINTENANCE PLAN

PROPER MAINTENANCE OF THIS FACILITY IS ENCOURAGED TO PREVENT THE INTRODUCTION OF DEBRIS AND SEDIMENT IN TO THE FACILITY, SPILLWAY(S) AND DOWNSTREAM WATERWAYS. FOLLOWING INSTALLATION OF THE FACILITY AND ESTABLISHMENT OF VEGETATION IN DISTURBED AREAS, INSPECTIONS FOR SEDIMENT BUILDUP WILL BE PERFORMED AT LEAST QUARTERLY. IT IS ANTICIPATED THAT UNDER NORMAL CONDITIONS, SEDIMENT REMOVAL FROM THE FACILITY WILL BE REQUIRED ONCE EVERY 10 YEARS. IF OTHER CONSTRUCTION OR RELATED ACTIVITIES ARE PERFORMED ON UPLAND PARCELS, ADEQUATE PROTECTION SHOULD BE PROVIDED AND INSPECTIONS PERFORMED AT LEAST ONCE WEEKLY OF THESE NEWLY DISTRIBUTED AREAS AS WELL AS INSPECTIONS FOR ACCUMULATED SEDIMENTS AT TWO BMP FACILITY.

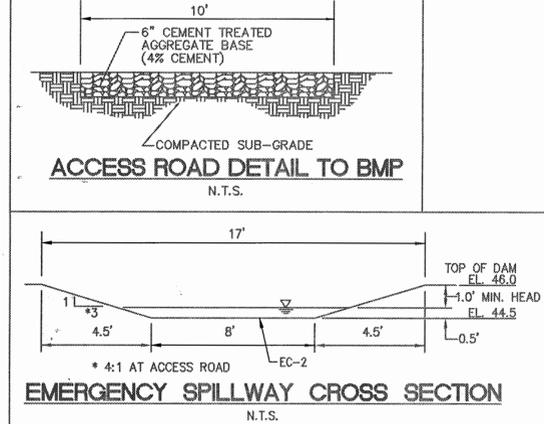
A DESIGNATED REPRESENTATIVE OF THE OWNER WILL INSPECT THE BMP STRUCTURE AFTER EACH SIGNIFICANT RAINFALL EVENT OR THE FOLLOWING WORKING DAY IF A WEEKEND OR HOLIDAY OCCURS. A SIGNIFICANT RAINFALL FOR THIS STRUCTURE IS DEFINED AS ONE (1) INCH OR MORE OF GAUGED RAINFALL WITHIN A 24 HOUR PERIOD. ONCE PER YEAR, A REPRESENTATIVE OF THE COUNTY MAY JOINTLY INSPECT THE STRUCTURE. APPROPRIATE ACTION, PERFORMED AT THE COST OF THE OWNER, WILL BE TAKEN TO ENSURE APPROPRIATE MAINTENANCE. KEYS TO LOCKED ACCESS PORTS SHALL BE MADE AVAILABLE TO COUNTY INSPECTION PERSONNEL UPON REQUEST.

INSPECTION AND MAINTENANCE OF THE FACILITY WILL CONSIST OF THE FOLLOWING ADDITIONAL MEASURES:

- THE INSPECTION FOR SEDIMENT BUILDUP WILL BE PERFORMED BY VISUAL INSPECTION AND A PHYSICAL DETERMINATION OF SEDIMENT DEPTH WITHIN THE STORAGE AREA. SEDIMENT REMOVAL IS REQUIRED USING A RUBBER-WHEELED BACKHOE AT THE SAME TIME, OR AT LEAST ONCE PER YEAR, THE RISER BOTTOM AND OUTLET PIPE SHALL BE CLEANED OF ACCUMULATED SEDIMENTS. DISPOSE OF SEDIMENTS REMOVED FROM THE FACILITY AT AN ACCEPTABLE DISPOSAL AREA. SEDIMENT SHALL NOT BE ALLOWED TO ACCUMULATE IN DEPTHS GREATER THAN 1-FOOT. NO SEDIMENT SHALL BE ALLOWED TO ACCUMULATE TO PREVENT THE PROPER FUNCTION OF ANY PIPE OR CULVERT.
- PERFORM MAINTENANCE MOWING OF GRASSED AREAS AT LEAST TWICE EACH YEAR. GRASSES SUCH AS TALL FESCUE SHOULD BE MOWED IN EARLY SUMMER AFTER EMERGENCE OF THE HEADS ON COOL SEASON GRASSES AND IN LATE FALL TO PREVENT SEEDS OF ANNUAL WEEDS FROM MATURING. MOWING OF LEGUMES CAN BE LESS FREQUENT TREES AND SHRUBS SHOULD NOT BE PERMITTED TO GROW ON ANY PART OF THE GRADED EMBANKMENT.
- PERFORM SOIL SAMPLING ON STABILIZED BMP SOIL AREAS ONCE EVERY FOUR (4) YEARS. SOIL SAMPLING AND TESTING SHOULD BE PERFORMED BY A QUALIFIED INDEPENDENT TESTING LABORATORY. APPLY ADDITIONAL LIME AND FERTILIZER IN ACCORDANCE WITH TEST RECOMMENDATIONS.
- IN STABILIZED BMP AREAS, IF VEGETATION COVERS LESS THAN 40% OF SOIL SURFACES, LIME FERTILIZE AND SEED IN ACCORDANCE WITH RECOMMENDATIONS FOR NEW SEEDLINGS, AS LISTED IN DAM CONSTRUCTION NOTES. IF VEGETATION COVERS MORE THAN 40% BUT LESS THAN 70% OF SOIL SURFACES, LIME FERTILIZE AND OVERSEED IN ACCORDANCE WITH CURRENT SEEDLING RECOMMENDATIONS.
- PERFORM QUARTERLY INSPECTIONS OF THE RELEASE STRUCTURES, RISER SECTION AND CREST OF SPILLWAY FOR THE OBSERVANCE OF COLLECTED DEBRIS. IMMEDIATELY REMOVE ANY DEBRIS TO MAINTAIN THE INTEGRITY OF THE STRUCTURE AND PROVIDE AN ATTRACTIVE APPEARANCE. DURING QUARTERLY INSPECTIONS, THE POND DRAIN VALVE, USUALLY LEFT IN THE VALVE "CLOSED" POSITION, SHALL BE INSPECTED AND OPERATED THROUGH TWO COMPLETE FULL-OPEN TO FULL-CLOSE TO FULL-OPEN CYCLES.
- PERFORM YEARLY STRUCTURAL INSPECTIONS OF THE FACILITY FOR DAMAGE. STRUCTURAL INSPECTION SHALL BE PERFORMED ON THE CONCRETE RISER, ANTI-VORTEX DEVICE, TRASH RACK, ORIFICE/WEIRS, OUTLET BARREL AND POND EMBANKMENT. IF DAMAGE IS EVIDENT, FURTHER INVESTIGATION BY A PROFESSIONAL ENGINEER MAY BE REQUIRED TO ASSESS THE CONTINUED INTEGRITY OF THE STRUCTURE.
- PERFORM QUARTERLY INSPECTIONS OF THE GRADED SIDE SLOPES OF THE FACILITY FOR SIGNS OF ANNUAL / ROCKET BORROWS OR SLOPE EROSION. IMMEDIATELY PERFORM NECESSARY REPAIRS, REPLANTING OR RESEEDING AS APPROPRIATE.
- RECORD KEEPING. THE LANDOWNER OR DESIGNATED REPRESENTATIVE SHALL KEEP REASONABLE, ACCURATE WRITTEN RECORDS OR INSPECTIONS PERFORMED FOR THE STRUCTURE. RECORDS SHALL DOCUMENT ROUTINE MAINTENANCE AND/OR REPAIRS PERFORMED. COPIES SHALL BE PROVIDED TO THE COUNTY UPON REQUEST.
- THE FACILITY SHALL NOT BE MODIFIED IN ANY WAY WITHOUT PRIOR CONSENT/ APPROVAL OF THE COUNTY.



SECTION A-A BMP 5.4



EMERGENCY SPILLWAY CROSS SECTION

I HEREBY CERTIFY TO THE BEST OF MY JUDGEMENT, KNOWLEDGE, AND BELIEF THAT THIS RECORD DRAWING REPRESENTS THE CONDITIONS OF THE SITE ON THE DATE IT WAS SURVEYED. THE SITE APPEARS TO CONFORM WITH THE PROVISIONS OF THE APPROVED DESIGN PLAN.

REV	DATE	BY	REVISION / COMMENT
1	1/30/03	RED	REVISED PER JCCS AND JCC COMMENTS
2	3/25/03	RED	REVISED PER JCC AND VDOT COMMENTS
3	8/27/03	RED	REVISED PER JCC AND VDOT COMMENTS
4	1/30/03	RED	BMP 5.4 RECORD DRAWING



5248 Olde Towne Road, Suite 1
Williamsburg, Virginia, 23188
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Fax (757) 220-8894



ASBUILT DAM SECTION AND DETAILS
SECTION V-B 'BENT TREE' - PHASE 3
AT STONEHOUSE
FOR
STONEHOUSE DEVELOPMENT COMPANY, L.L.C.
STONEHOUSE DISTRICT
JAMES CITY COUNTY
VIRGINIA

Designed RGW	Drawn RED
Scale NOTED	Date 3/2/01
Project No. 8878-00	
Drawing No. R17	

SEQUENCE OF CONSTRUCTION

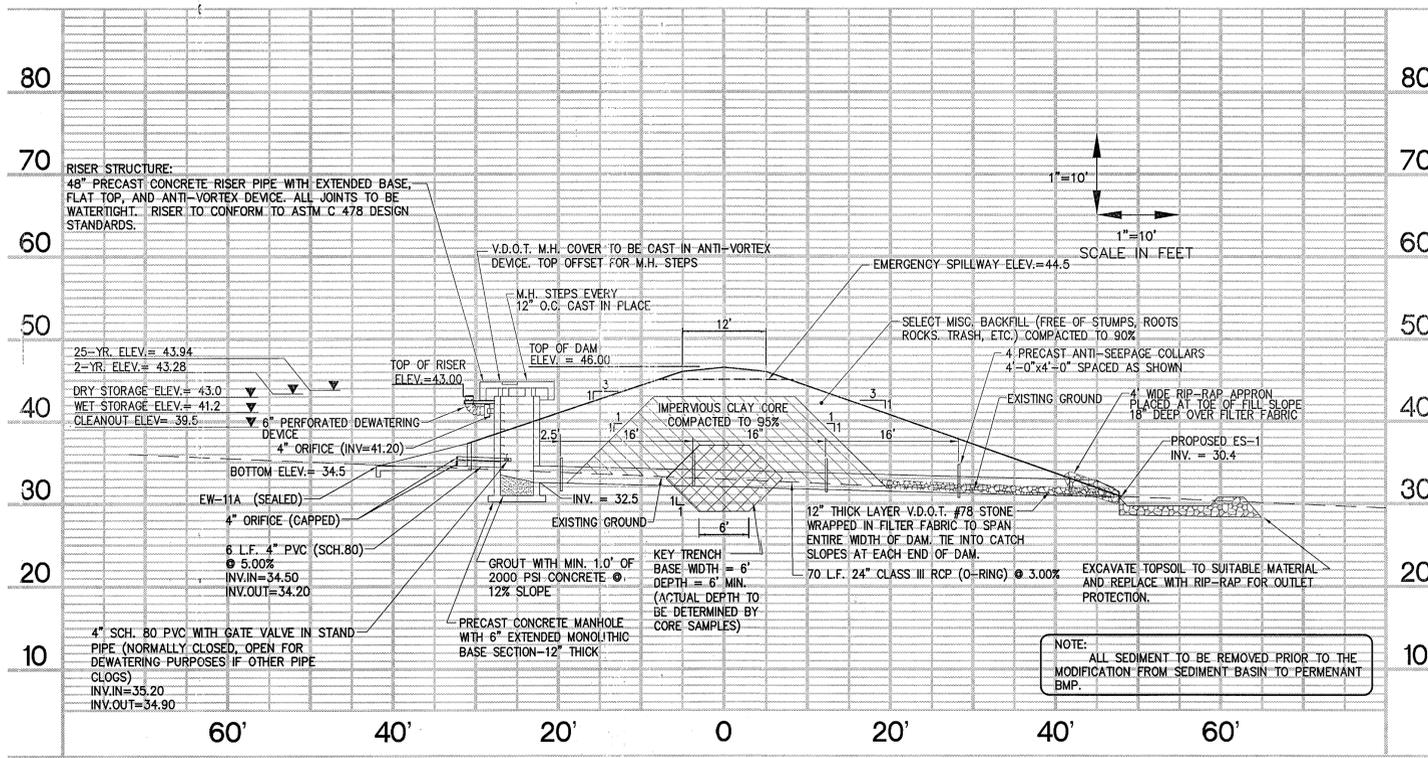
PHASE 1

- 1 - INSTALL STONE CONSTRUCTION ENTRANCES (SPLITWOOD ROAD, SApLING DRIVE, AND WINDY BRANCH DRIVE).
- 2 - CLEAR PERIMETER EXCEPT FOR TEMPORARY STOCKPILE AREA.
- 3 - INSTALL CULVERT AND ROAD FILL BEFORE CLEARING AND USING TEMPORARY STOCKPILE AREA.
- 4 - CONSTRUCT SEDIMENT BASIN #1 AND SEDIMENT TRAP #2
- 5 - INSTALL TREE PROTECTION, SILT FENCE, CHECK DAMS, OUTLET PROTECTION, AND DIVERSION DIKES AS SHOWN ON THIS SHEET.
- 6 - CLEAR AND GRUB REMAINING AREAS.
- 7 - STRIP TOPSOIL FROM CLEARED AREAS FOR EARTHWORK OPERATIONS.

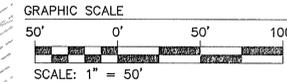
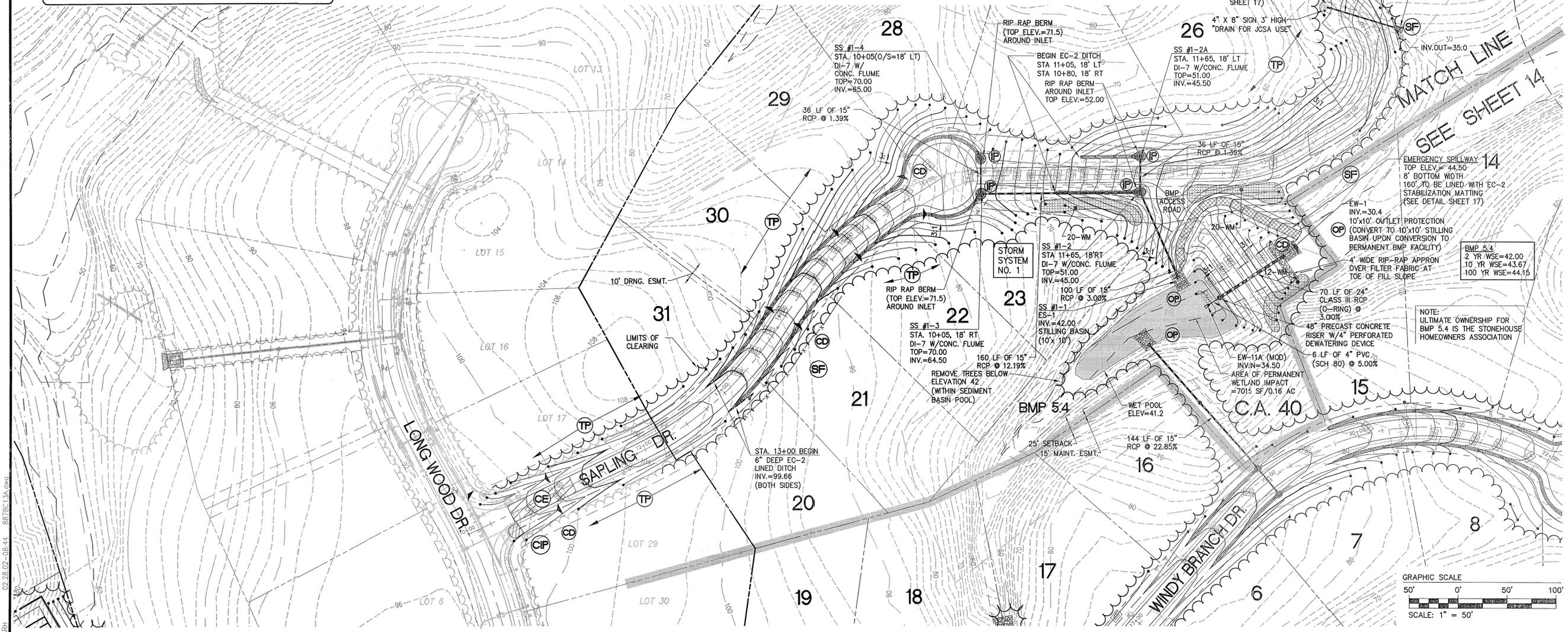
PHASE 2

- 1 - INSTALL DITCHES, CULVERTS, & STORM SEWER WITH CHECK DAMS, INLET, & TEMP. OUTLET PROTECTION.
- 2 - SEED AND MULCH DISTURBED AREAS ONCE FINISHED GRADE IS ACHIEVED.
- 3 - OFF-SITE GRADING ACTIVITIES INCLUDE FILL SECTIONS FOR THE FUTURE EXTENSION OF SPLITWOOD ROAD, AND A TEMPORARY STOCKPILE. NO OTHER OFF-SITE GRADING ACTIVITIES ARE ANTICIPATED.
- 4 - BEGIN UNDERGROUND UTILITY CONSTRUCTION (WATER AND SEWER NETWORKS). CONNECT SYSTEMS TO EXISTING FACILITIES AT THE PRESENT END OF SPLITWOOD DRIVE AND AT INTERSECTIONS OF SApLING AND WINDY BRANCH DRIVES WITH EXISTING LONGWOOD DRIVE.
- 5 - COMPLETE ROADWAY CONSTRUCTION WITH FINE GRADING, STONE AGGREGATE AND BASE COURSE.
- 6 - CONSTRUCT CONCRETE DITCHES.
- 7 - TOPSOIL DENuded AREAS AND PERMANENTLY SEED.
- 8 - REMOVE ALL ACCUMULATED SEDIMENT FROM SEDIMENT TRAP #2 AND TEMPORARY SEDIMENT BASIN #1. REMOVE SEDIMENT TRAP #2.
- 9 - MODIFY SEDIMENT BASIN #1 BY REMOVING DEWATERING DEVICE AND GROUTING UNDER OPEN ORIFICE. UNCOVER PERMANENT ORIFICES AND REMOVE CAPS AND REPLACE SCREEN ON EW-11.
- 10 - REMOVE REMAINING EROSION CONTROL MEASURES UPON SITE STABILIZATION.
- 11 - INSTALL ALL PERMANENT STILLING BASINS, AFTER OBTAINING J.C.C. ENVIRONMENTAL DIVISION APPROVAL.

PURPOSE AND INTENT OF AMENDED PLAN SHEET 13A IS TO SHOW THE REDESIGN OF BMP 5.4 INTO A SEDIMENT BASIN. THIS WILL ELIMINATE THE NEED FOR THE UPHILL SEDIMENT TRAP PREVENTING EXCESSIVE CLEARING AND GRADING ACTIVITIES ON STEEP SLOPES.



SECTION A-A SEDIMENT BASIN 1



NO.	DATE	REVISION / COMMENT / NOTE
1	8/22/01	REVISED PER JCC AND ROOT COMMENTS
2	8/24/01	REVISED PER JCC AND ROOT COMMENTS
3	9/25/01	REVISED PER JCSA AND JCC COMMENTS
4	3/5/02	MODIFIED FOR BMP CHANGES



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 Williamsburg, Virginia 23188
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 Fax (757) 220-8994



AMENDED DRAINAGE, GRADING AND E&S CONTROL PLAN SECTION V-B 'BENT TREE' AT STONEHOUSE FOR STONEHOUSE DEVELOPMENT COMPANY, L.L.C. JAMES CITY COUNTY, VIRGINIA

DESIGNED: VMB/JAG
 DRAWN: JAG
 SCALE: 1" = 50'
 DATE: 3/5/02
 PROJECT NO.: 8878-00
 DRAWING NO.: 13 A

EROSION AND SEDIMENTATION CONTROL LEGEND

-  SILT FENCE (SPEC. 3.05)
-  INLET PROTECTION (SPEC. 3.07)
-  CONSTRUCTION ENTRANCE (SPEC. 3.02)
-  CHECK DAM (SPEC. 3.20)
-  TEMPORARY DIVERSION DIKE (SPEC. 3.09)
-  OUTLET PROTECTION (SPEC. 3.18)
-  CULVERT INLET PROTECTION (SPEC. 3.08-1 WITH STONE COMBIN. INSTEAD OF SILT FENCE)
-  TEMPORARY SEDIMENT TRAP (SPEC. 3.13)
-  PERMANENT SEEDING (SPEC. 3.32)
-  TEMPORARY SEDIMENT BASIN (SPEC. 3.14)
-  TREE PROTECTION (SPEC. 3.38)
-  TEMPORARY SLOPE DRAIN (SPEC. 3.15)

NOTE:
SEE VIRGINIA EROSION & SEDIMENT CONTROL HANDBOOK FOR EROSION CONTROL SPECIFICATIONS (SPEC.) AND DETAILS.

SOIL No.	SOIL NAME	TYPICAL SLOPES	EROSION FACTOR (K)	EROSION FACTOR (T)
11C	GRAVEN-UCHEE COMPLEX	6-10%	0.32-0.37	3
14B	EMPORIA	2-6%	0.20-0.28	4
15F	EMPORIA COMPLEX	25-60%	0.20-0.28	4
17	JOHNSTON COMPLEX	-	0.17-0.20	5
19B	KEMPSVILLE-EMPORIA FINE SANDY LOAM	2-6%	0.24-0.32	3
25B	NORFOLK FINE SANDY LOAM	2-6%	0.17-0.24	5

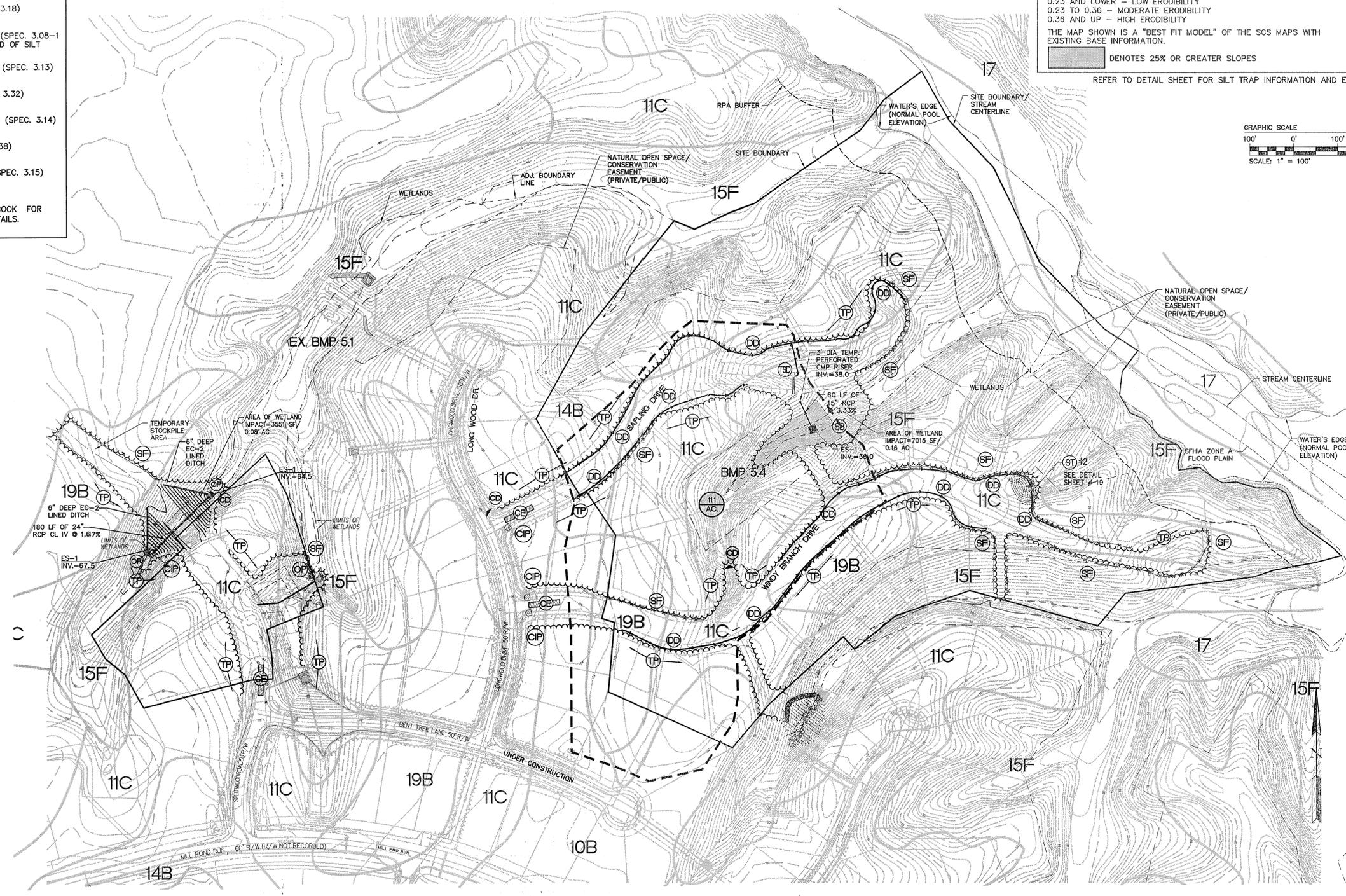
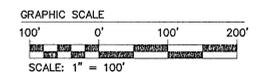
INFORMATION TAKEN FROM "SOIL SURVEY OF JAMES CITY AND YORK COUNTIES AND THE CITY OF WILLIAMSBURG, VIRGINIA" ISSUED IN APRIL, 1985, BY THE UNITED STATES DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE IN COOPERATION WITH VIRGINIA POLYTECHNIC INSTITUTE AND STATE UNIVERSITY.

SOIL SUSCEPTIBILITY TO EROSION CLASSIFICATION (K)
0.23 AND LOWER - LOW ERODIBILITY
0.23 TO 0.36 - MODERATE ERODIBILITY
0.36 AND UP - HIGH ERODIBILITY

THE MAP SHOWN IS A "BEST FIT MODEL" OF THE SCS MAPS WITH EXISTING BASE INFORMATION.

 DENOTES 25% OR GREATER SLOPES

REFER TO DETAIL SHEET FOR SILT TRAP INFORMATION AND E & S NARRATIVE.



No.	DATE	REVISION / COMMENT / NOTE	BY
4	3/5/02	BMP MODIFICATION	WMB
3	9/25/01	REVISED PER JCSA AND JCC COMMENTS	RGW
2	8/24/01	REVISED PER JCC AND VDOT COMMENTS	RGW
1	6/22/01	REVISED PER JCC AND VDOT COMMENTS	RGW



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Williamsburg, Virginia 23188
(757) 253-0040
Fax (757) 220-8994



AMENDED ENVIRONMENTAL INVENTORY AND PH. 1 & S CONTROL SECTION V-B "BENT TREE" - PHASE 3 AT STONEHOUSE FOR STONEHOUSE DEVELOPMENT COMPANY, L.L.C. STONEHOUSE DISTRICT, JAMES CITY COUNTY, VIRGINIA

Designed RGW	Drawn ARH
Scale 1"=100'	Date 3/5/01
Project No. 8878-00	
Drawing No. 16A	



STORM SEWER DRAINAGE AREA MAP
SECTION VB "BENT TREE" - PHASE 3
AT STONEHOUSE
FOR
STONEHOUSE L.L.C.
 STONEHOUSE DISTRICT JAMES CITY COUNTY VIRGINIA

1 OF 1

D-1

GRAPHIC SCALE IN FEET
 1" = 50'

0 50 100 150 200

Project Number: 1960038-11173
 Dwg. File No.: 10507W
 Drawing Number: D-1

Drawn: CMJ
 Checked: SAG/RSP
 Designed: SAG/RSP
 Date: 7/30/1999
 Scale: 1"=50'

CADD File name: DRAINAGE-READING

COUNTY APPROVAL
 1st Submitted: []
 2nd Submitted: []
 3rd Submitted: []
 Approved: []

DRAWING STATUS
 Interoffice Review: []
 Client for Review: []
 Pre-Approved Bidding: []
 NOTE: []

No.	Date	Comment
1	2/21/00	REVISED PER COUNTY COMMENTS

By: CMJ

REVISIONS:

Langley and McDonald, Inc.
 Engineers • Surveyors • Planners
 Landscape Architects • Environmental Consultants
 WILLIAMSBURG
 VIRGINIA BEACH

5544 Greenleaf Road - Suite 100
 Williamsburg, VA 23186
 Tel: (757) 265-2979
 Fax: (757) 225-0048
 Email: @langley.com

COMMONWEALTH OF VIRGINIA
 JAMES H. PHILIP
 No. 023853
 PROFESSIONAL SEAL

VIRGINIA STATE PLANE COORDINATE SYSTEM (SOUTH ZONE) (NAD 83)

5-000-01
5-68-01

E PLAN FOR NEHOUSE

DEVELOPMENT COMPANY, L.L.C.

AREA ONE, PHASE I BENT TREE" - PHASE 3 Y COUNTY, VIRGINIA

INDEX OF SHEETS

SHEET NUMBER	DESCRIPTION
1	COVER SHEET
2	OVERALL PLAN OF DEVELOPMENT
3	PRELIMINARY PLAT - SAPLING DRIVE
4	PRELIMINARY PLAT - WINDY BRANCH DRIVE
5	PRELIMINARY PLAT - SPLITWOOD ROAD
6	MASTER UTILITY PLAN
7	ROAD AND UTILITY PLAN - SAPLING DRIVE
8	ROAD AND UTILITY PLAN - WINDY BRANCH DRIVE
9	ROAD AND UTILITY PLAN - SPLITWOOD ROAD
10	ROAD AND UTILITY PROFILE
11	ROAD AND UTILITY PROFILE
12	OVERALL DRAINAGE PLAN
13	DRAINAGE, GRADING AND E & S CONTROL PLAN
14	DRAINAGE, GRADING AND E & S CONTROL PLAN
15	DRAINAGE, GRADING AND E & S CONTROL PLAN
16	ENVIRONMENTAL INVENTORY & PH. 1 E & S CONTROL
17	DAM PROFILE, NOTES AND DETAILS
18	NOTES AND DETAILS
19	NOTES AND DETAILS
20	NOTES AND DETAILS

SITE DATA:

TAX MAP PARCEL No.	(6-4) (1-1)
ZONING:	PUD-R
PROJECT AREA:	35.07 ACRES / 1,527,769 SF
DISTURBED AREA:	8.81 ACRES / 383,774 SF
NUMBER OF LOTS (PHASE 3):	34
FLOOD HAZARD MAP:	FEMA PANEL NUMBER 510201 0010 B - SFHA ZONE A

OWNER INFORMATION:

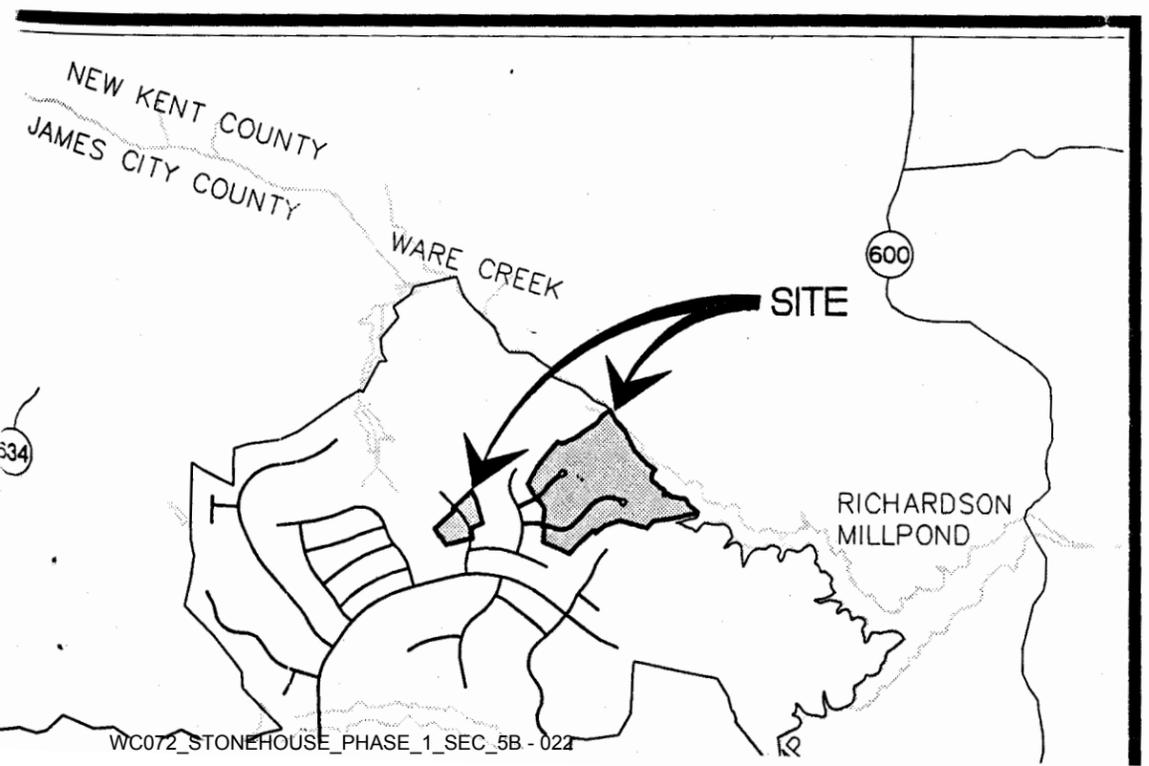
STONEHOUSE DEVELOPMENT COMPANY, L.L.C.
ATTENTION: MR. JAMES H. BENNETT
P.O. BOX 759
9701 MILL POND RUN
TOANO, VIRGINIA. 23168

RESPONSIBLE LAND DISTURBER

MR. JAMES H. BENNETT, P.E.
(757) 234-5000

NOTES:

- OWNERS OF LOTS WHICH REQUIRE A GRINDER PUMP FOR SANITARY SEWER SERVICE ARE REQUIRED TO HAVE A GRINDER PUMP MAINTENANCE CONTRACT.



BILITY COMPANY
I-R
810
3-97

WATER'S EDGE
(NORMAL POOL
ELEVATION)

SITE BOUNDARY

ADJ. BOUNDARY
LINE

RPA BUFFER

SITE BOUNDARY/ STREAM CENTERLINE

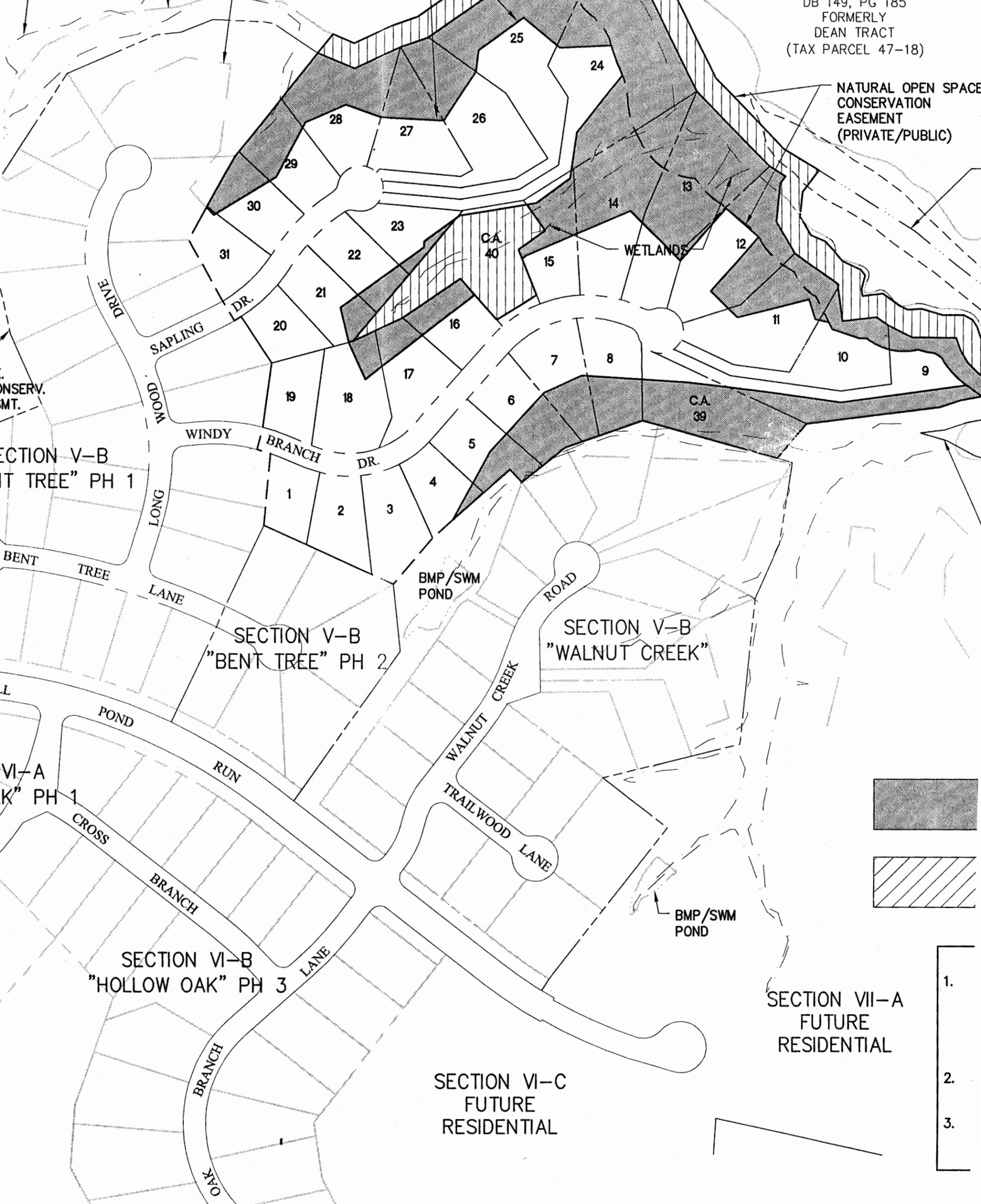
COMMON AREA (C.A.)
41

STONEHOUSE INC.
DB 149, PG 185
FORMERLY
DEAN TRACT
(TAX PARCEL 47-18)

WETLANDS

NATURAL OPEN SPACE/
CONSERVATION
EASEMENT
(PRIVATE/PUBLIC)

NATURAL OPEN SPACE/
CONSERVATION
EASEMENT
(PRIVATE/PUBLIC)



ONSERV.
SMT.

SECTION V-B
"BENT TREE" PH 1

SECTION V-B
"BENT TREE" PH 2

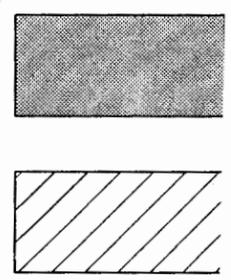
SECTION V-B
"WALNUT CREEK"

VI-A
"HOLLOW OAK" PH 1

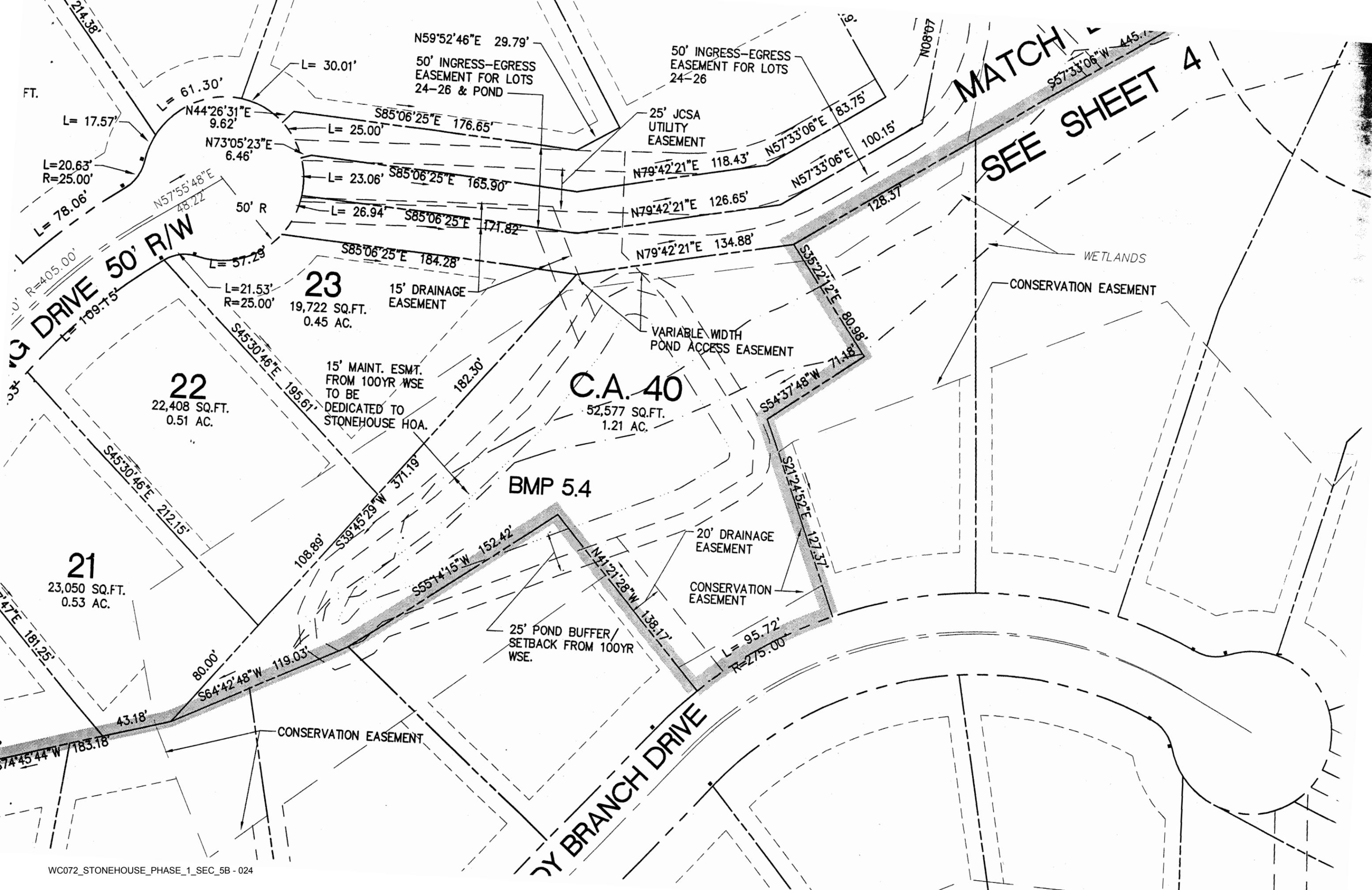
SECTION VI-B
"HOLLOW OAK" PH 3

SECTION VI-C
FUTURE
RESIDENTIAL

SECTION VII-A
FUTURE
RESIDENTIAL



- 1.
- 2.
- 3.



FT.

MATCH
SEE SHEET 4

DRIVE 50' R/W

Y BRANCH DRIVE

23

22

21

C.A. 40

BMP 5.4

15' DRAINAGE EASEMENT

15' MAINT. ESMT. FROM 100YR WSE TO BE DEDICATED TO STONEHOUSE HOA.

VARIABLE WIDTH POND ACCESS EASEMENT

20' DRAINAGE EASEMENT

CONSERVATION EASEMENT

25' POND BUFFER/SETBACK FROM 100YR WSE.

WETLANDS

CONSERVATION EASEMENT

N59°52'46"E 29.79'
50' INGRESS-EGRESS EASEMENT FOR LOTS 24-26 & POND

50' INGRESS-EGRESS EASEMENT FOR LOTS 24-26

25' JCSA UTILITY EASEMENT

L=17.57'

L=20.63'
R=25.00'

L=78.06'

R=405.00'

L=109.15'

L=61.30'

N44°26'31"E 9.62'

N73°05'23"E 6.46'

N57°55'48"E 48.22'

50' R

L=57.23'

L=21.53'
R=25.00'

S45°30'46"E 195.87'

S45°30'46"E 212.15'

L=30.01'

L=25.00'

L=23.06'

L=26.94'

L=57.23'

L=21.53'
R=25.00'

S45°30'46"E 195.87'

S45°30'46"E 212.15'

S85°06'25"E 176.65'

S85°06'25"E 165.90'

S85°06'25"E 171.82'

S85°06'25"E 184.28'

N79°42'21"E 118.43'

N79°42'21"E 126.65'

N79°42'21"E 134.88'

N79°42'21"E 126.65'

N57°33'06"E 83.75'

N57°33'06"E 100.15'

N57°33'06"E 128.37'

N57°33'06"E 100.15'

N79°42'21"E 118.43'

N79°42'21"E 126.65'

N79°42'21"E 134.88'

N79°42'21"E 126.65'

N57°33'06"E 83.75'

N57°33'06"E 100.15'

N57°33'06"E 128.37'

N57°33'06"E 100.15'

N79°42'21"E 118.43'

MA
SEE SHEET

14

EMERGENCY SPILLWAY
TOP ELEV.= 44.50
8' BOTTOM WIDTH
160' TO BE LINED WITH EC-2
STABILIZATION MATTING
(SEE DETAIL SHEET 17)

BMP 5.4
2 YR WSE=42.00
10 YR WSE=43.67
100 YR WSE=44.15

NOTE:
ULTIMATE OWNERSHIP FOR
BMP 5.4 IS THE STONEHOUSE
HOMEOWNERS ASSOCIATION

EW-1
INV.=30.4
STILLING BASIN
(10'x10')

70 LF OF 24"
CLASS III RCP
(O-RING) @
3.00%

AREA OF WETLAND
IMPACT=5051 SF/
0.12 AC

15

48" PRECAST
CONCRETE RISER

6 LF OF 4" PVC
(SCH 80) @ 5.00%

EW-11A (MOD)
INV.IN=34.50

C.A. 40

100 YR WSE

144 LF OF 15"
RCP @ 22.85%

16

25' SETBACK
15' MAINT. ESMT.

128 LF OF 15"
RCP @ 7.03%

SS #1-1
ES-1
INV.=36.00
STILLING BASIN
(10'x 10')

BMP 5.4

160 LF OF 15"
RCP @ 12.19%

SS #1-3
STA. 10+05, 18' RT
DI-7 W/CONC. FLUME
TOP=70.00
INV.=64.50

22

RIP RAP BERM
(TOP ELEV.=71.5)
AROUND INLET

STORM
SYSTEM
NO. 1

23

SS #1-2
STA 11+65, 18' RT
DI-7 W/CONC. FLUME
TOP=51.00
INV.=45.00

ST
#1

BRANCH DR.

7

8

17

21

29

36 LF OF 15"
RCP @ 1.39%

STA. 10+05 (O/S=18' LT)
DI-7 W/
CONC. FLUME
TOP=70.00
INV.=65.00

BEGIN EC-2 DITCH
STA 11+05, 18' LT
STA 10+80, 18' RT
RIP RAP BERM
AROUND INLET
TOP ELEV.=52.00

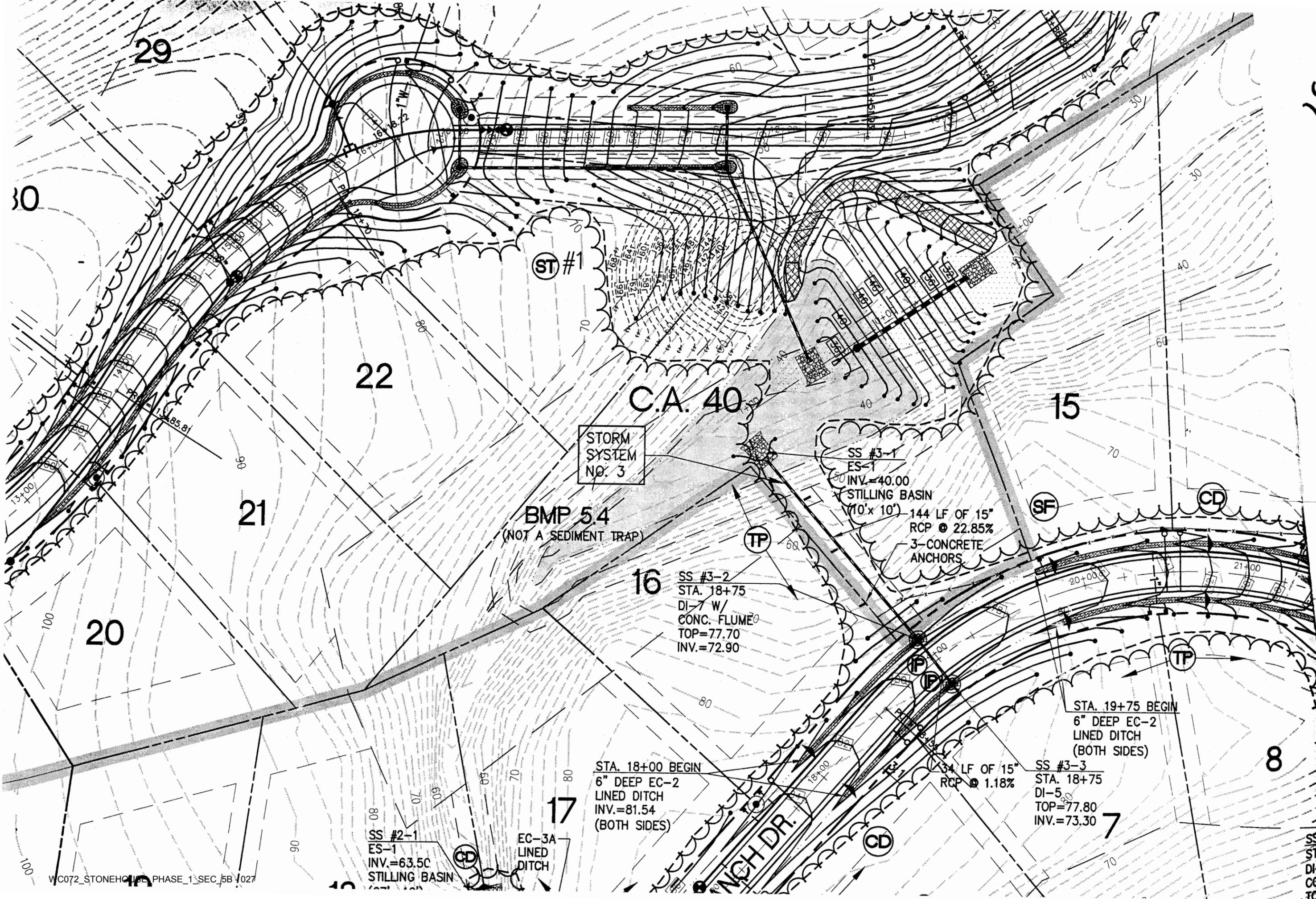
STA 11+65, 18' LI
DI-7 W/CONC. FLUME
TOP=51.00
INV.=45.50

36 LF OF 15"
RCP @ 1.39%

13+00 BEGIN
DEEP EC-2
DITCH
=99.66
(TH SIDES)

20

Stonehouse Bent Tree



29

30

22

21

20

C.A. 40

15

STORM SYSTEM NO. 3

BMP 5.4 (NOT A SEDIMENT TRAP)

SS #3-1
ES-1
INV.=40.00
STILLING BASIN
(10'x 10')
144 LF OF 15" RCP @ 22.85%
3- CONCRETE ANCHORS

16
SS #3-2
STA. 18+75
DI-7 W/
CONC. FLUME
TOP=77.70
INV.=72.90

STA. 19+75 BEGIN
6" DEEP EC-2
LINED DITCH
(BOTH SIDES)

STA. 18+00 BEGIN
6" DEEP EC-2
LINED DITCH
INV.=81.54
(BOTH SIDES)

34 LF OF 15" RCP @ 1.18%
SS #3-3
STA. 18+75
DI-5
TOP=77.80
INV.=73.30

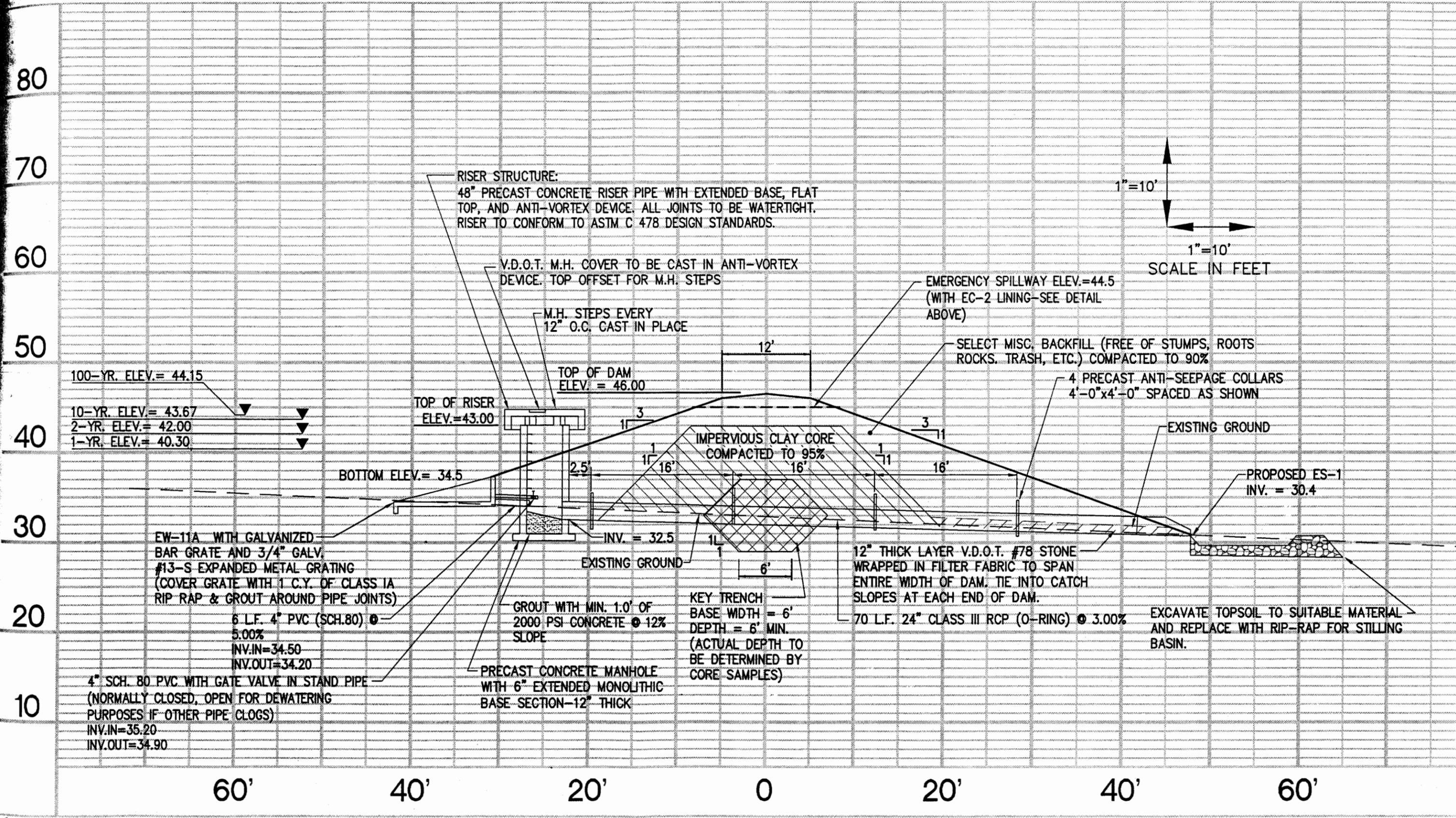
SS #2-1
ES-1
INV.=63.5C
STILLING BASIN

EC-3A
LINED
DITCH

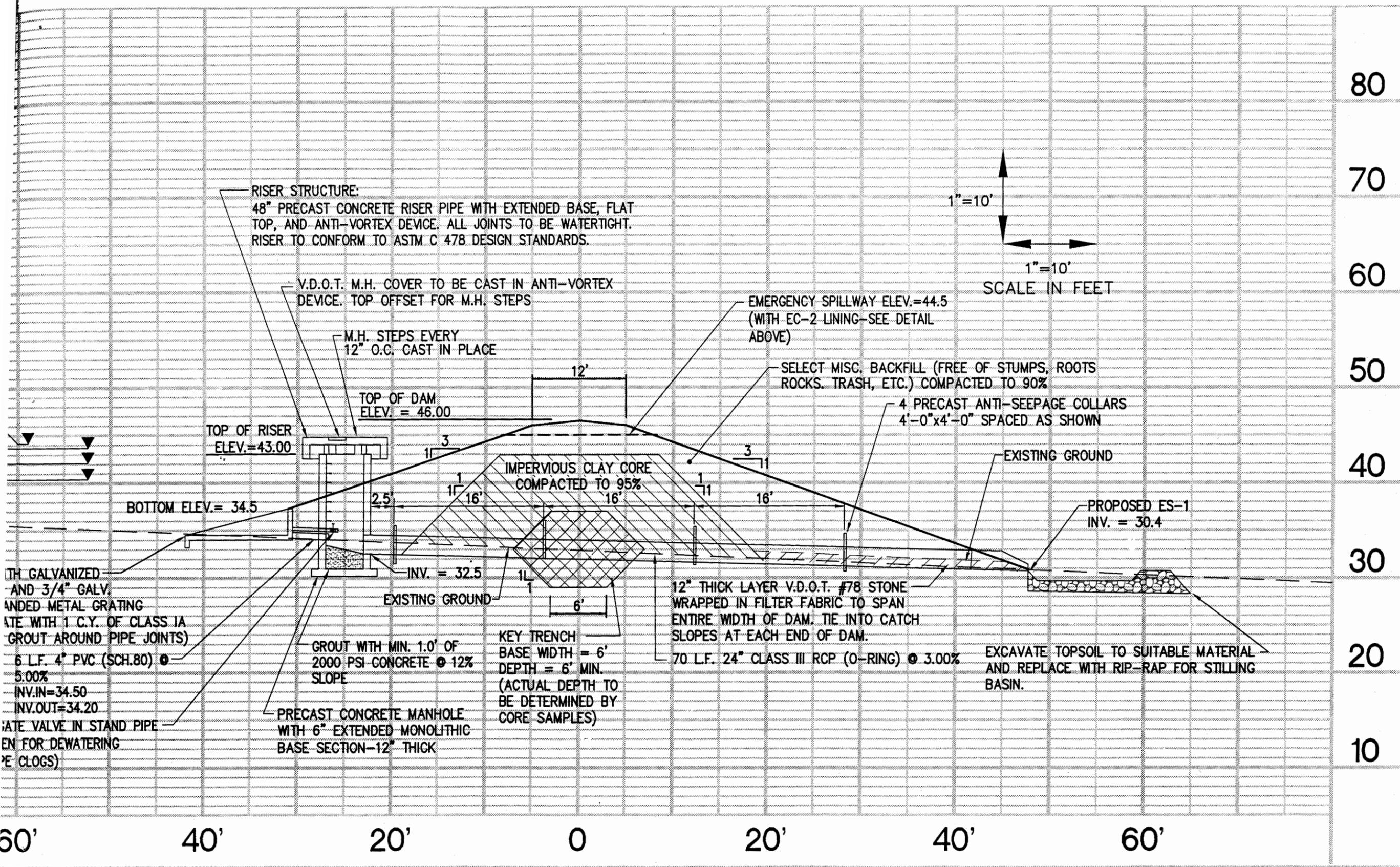
8

7

SS
STA.
DI-
CON
TOP



SECTION A-A BMP 5.4



RISER STRUCTURE:
 48" PRECAST CONCRETE RISER PIPE WITH EXTENDED BASE, FLAT TOP, AND ANTI-VORTEX DEVICE. ALL JOINTS TO BE WATERTIGHT. RISER TO CONFORM TO ASTM C 478 DESIGN STANDARDS.

V.D.O.T. M.H. COVER TO BE CAST IN ANTI-VORTEX DEVICE. TOP OFFSET FOR M.H. STEPS

M.H. STEPS EVERY 12" O.C. CAST IN PLACE

TOP OF DAM ELEV. = 46.00

TOP OF RISER ELEV. = 43.00

BOTTOM ELEV. = 34.5

EMERGENCY SPILLWAY ELEV. = 44.5 (WITH EC-2 LINING-SEE DETAIL ABOVE)

SELECT MISC. BACKFILL (FREE OF STUMPS, ROOTS, ROCKS, TRASH, ETC.) COMPACTED TO 90%

4 PRECAST ANTI-SEEPAGE COLLARS 4'-0" x 4'-0" SPACED AS SHOWN

EXISTING GROUND

PROPOSED ES-1 INV. = 30.4

1/2" GALVANIZED AND 3/4" GALV. ANODIZED METAL GRATING (1 C.Y. OF CLASS IA GROUT AROUND PIPE JOINTS)
 6 L.F. 4" PVC (SCH.80) @ 5.00%
 INV. IN = 34.50
 INV. OUT = 34.20
 GATE VALVE IN STAND PIPE (FOR DEWATERING PIPE CLOGS)

GROUT WITH MIN. 1.0' OF 2000 PSI CONCRETE @ 12% SLOPE

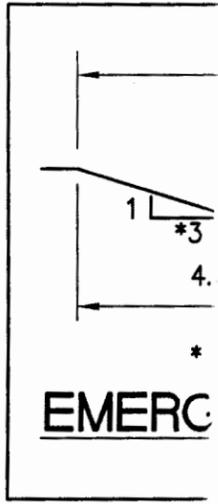
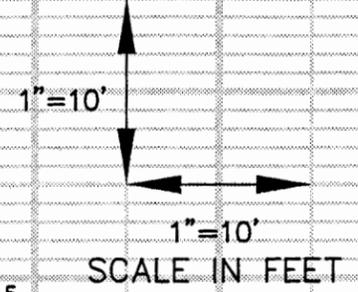
PRECAST CONCRETE MANHOLE WITH 6" EXTENDED MONOLITHIC BASE SECTION-12" THICK

KEY TRENCH
 BASE WIDTH = 6'
 DEPTH = 6' MIN.
 (ACTUAL DEPTH TO BE DETERMINED BY CORE SAMPLES)

12" THICK LAYER V.D.O.T. #78 STONE WRAPPED IN FILTER FABRIC TO SPAN ENTIRE WIDTH OF DAM. TIE INTO CATCH SLOPES AT EACH END OF DAM.

70 L.F. 24" CLASS III RCP (O-RING) @ 3.00%

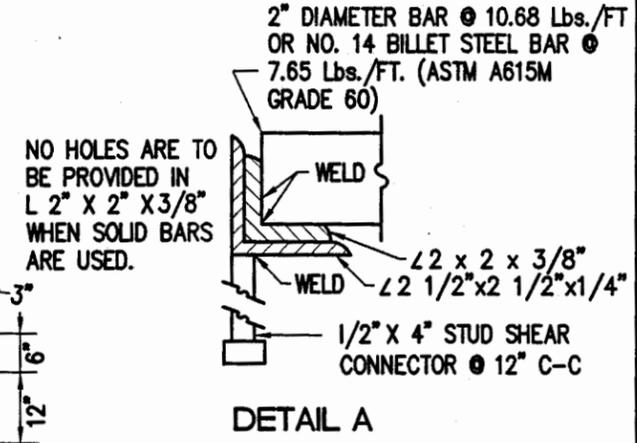
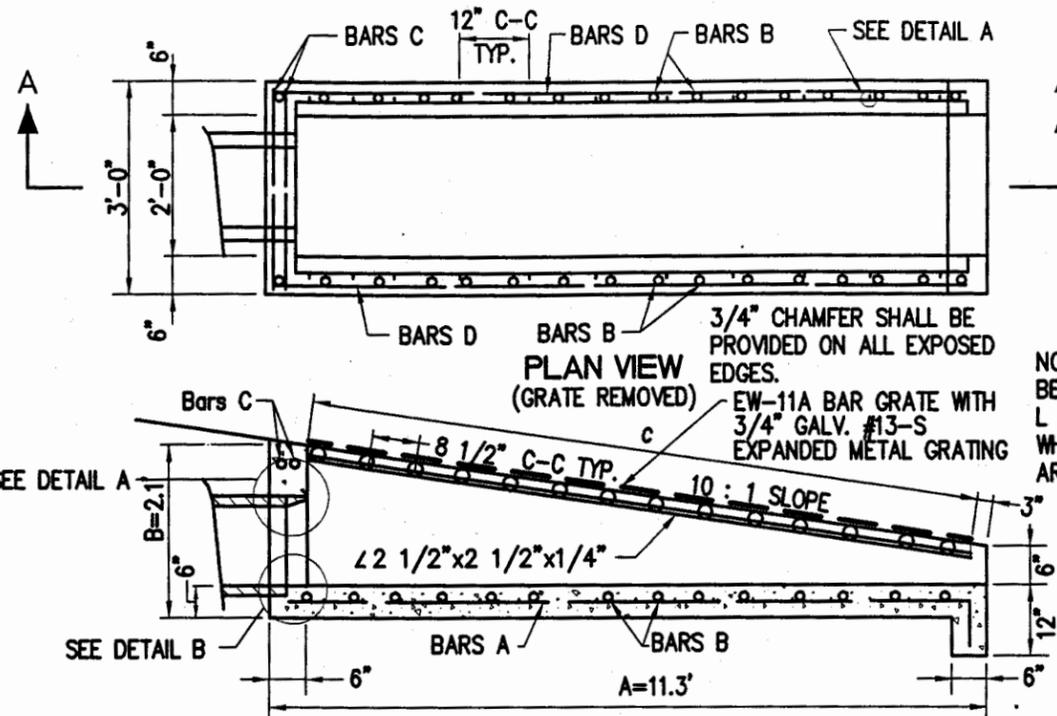
EXCAVATE TOPSOIL TO SUITABLE MATERIAL AND REPLACE WITH RIP-RAP FOR STILLING BASIN.



EMERC

SECTION A-A BMP 5.4

DIMENSIONS FOR BEVEL		
ON HEADWALL PIPE SIZE	a	b
12"	0'-2"	0'-1 1/4"
15"	0'-2"	0'-1 1/4"
18"	0'-2 1/2"	0'-1 1/2"
21" or 24"	0'-3"	0'-2"

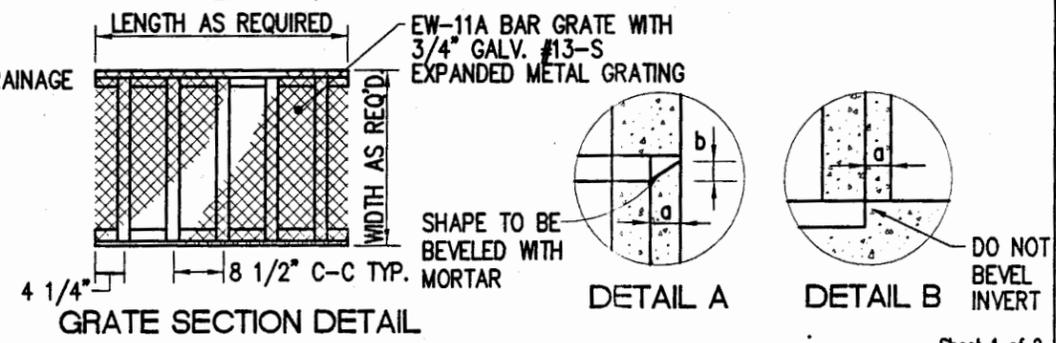


NOTES:

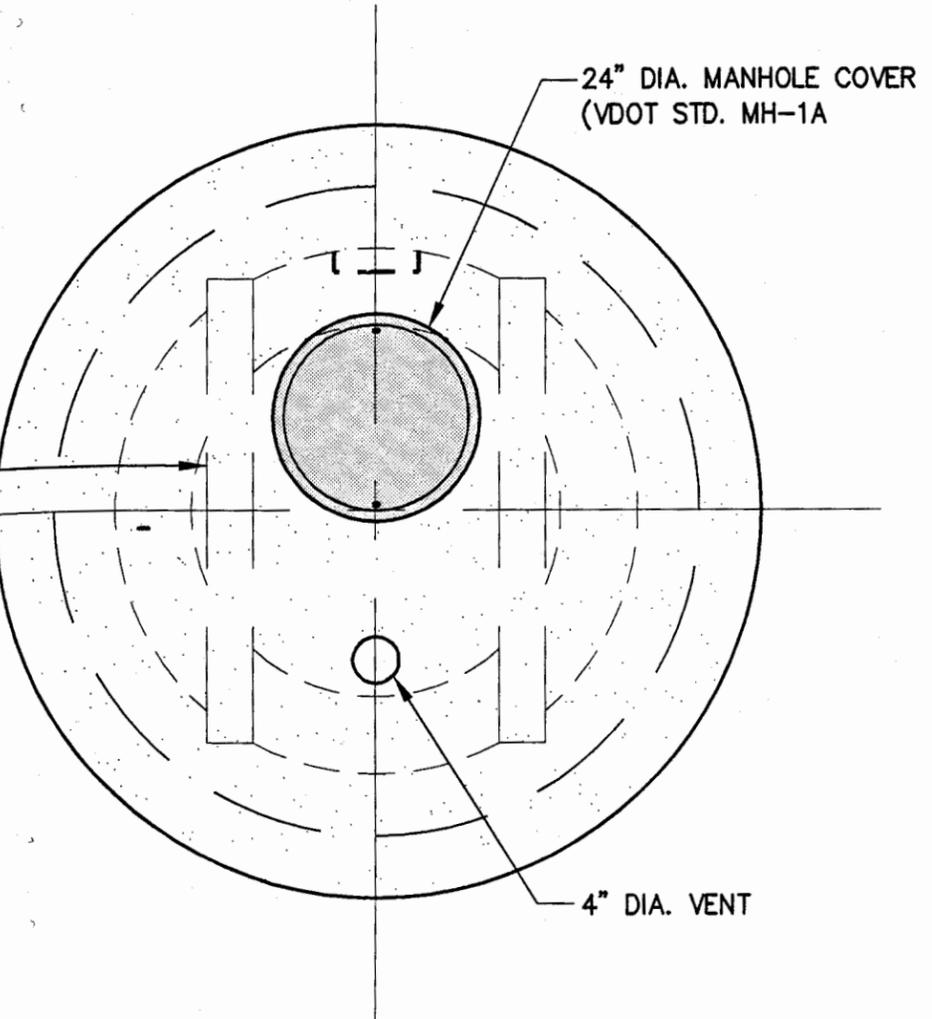
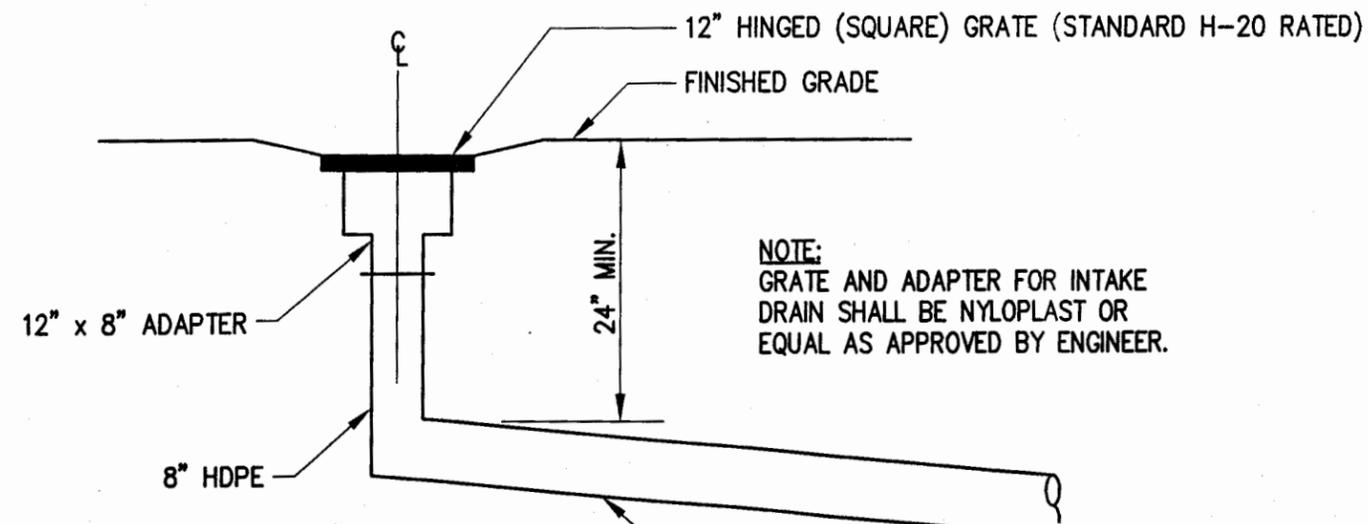
- IN NO CASE SHALL TOP OF END WALL PROJECT ABOVE FILL SLOPE, DITCH SLOPE, OR SHOULDER.
- CLASS A3 CONCRETE TO BE USED IF CAST IN PLACE, 4000 PSI IF PRE-CAST.
- REINFORCING STEEL TO HAVE A MINIMUM 1 1/2" CONCRETE COVER.
- FOR SCHEDULE OF REINFORCING STEEL, DIMENSIONS, AND QUANTITIES SEE SHEET 2 OF 2.
- THIS ITEM MAY BE PRE-CAST OR CAST IN PLACE.
- BOTTOM OF STRUCTURE TO BE ON THE SAME GRADE AS DRAINAGE DITCH.
- HEADWALL TO BE BEVELED IN ALL AREAS EXCEPT WHERE A CONFLICT WITH INVERT OR WINGWALLS OCCUR.
- BEVEL EDGE IS REQUIRED ON HEADWALL AT THE INLET END OF THE CULVERT (WHERE THE FLOW ENTERS THE CULVERT).

BEVEL EDGE IS REQUIRED ON HEADWALL AT THE INLET END OF THE CULVERT (WHERE THE FLOW ENTERS THE CULVERT).

HEADWALL AT THE OUTLET END OF THE CULVERT MAY BE EITHER SQUARE EDGE OR BEVEL EDGE.



PIPE ENDWALL WITH LOAD - CARRYING GRATE



PLAN - TOP SLAB

1. ANTI-VORTEX DEVICE (CAP AND RISER) MANUFACTURED IN ACCORDANCE WITH ASTM C478.
2. DIMENSIONS SUBJECT TO PERMISSIBLE VARIATIONS OF ASTM C478
3. INLET AREA (AREA BETWEEN DEVICE I.D. AND RISER O.D.) IS GREATER THAN OUTLET AREA (AREA OF RISER I.D.)
4. SLAB REINFORCEMENT TO BE ASTM A615 #4 BARS @ 8" E.W. CIRCUMFERENTIAL.

ANTI-VORTEX DETAIL
NOT TO SCALE

PROVIDE PROPER STABILIZATION, AND EROSION AND SEDIMENT CONTROL MEASURES NEEDED TO CONTROL AS PER THE VESCH THIRD EDITION.

5. UNDERCUT FOR THE FOUNDATION OF THE DAM EMBANKMENT SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATION. THE FOUNDATION SHALL BE BACKFILLED WITH SOILS CLASSIFIED AS SM, SC, OR CL UNDER THE UNIFIED SOIL CLASSIFICATION SYSTEM. SOILS SHALL HAVE A MINIMUM OF 15% BY WEIGHT FINES, HAVING A PLASTICITY INDEX OF 30% AND A PERMEABILITY OF 0.0004 IN./SEC. OR LESS. FILL SHALL BE COMPACTED IN 12-INCH LIFTS, OR AS DIRECTED BY THE GEOTECHNICAL ENGINEER, TO A DRY DENSITY OF 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY (ASTM D-698). EXCAVATION FOR THE DAM KEY SHALL BE IN ACCORDANCE TO THE GEOTECHNICAL ENGINEER'S RECOMMENDATION. HEIGHT, DEPTH, AND WIDTH OF THE KEY SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS. THE KEY SHALL BE FORMED USING SOILS CLASSIFIED AS SC OR CL, WITH A PERMEABILITY OF 0.0004 IN./SEC. OR LESS.

6. THE DAM CORE SHALL BE AS CONSTRUCTED WITH NON-EXPANSIVE SC OR CL CLAYEY MATERIAL WITH PERMEABILITY OF 0.0004 IN./SEC. OR LESS. THE FILL OF THE CORE SHALL BE MADE IN 12-INCH LIFTS, OR AS DIRECTED BY THE GEOTECHNICAL ENGINEER, TO AT LEAST 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY (ASTM D-698). SIZE, SHAPE, WIDTH, DEPTH, AND HEIGHT OF THE DAM CORE SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS. TO COVER THE DAM CORE, A SILTY FINE SAND OR CLAYEY SOIL (SM, SC, OR CL) SHALL BE PLACED. A VEGETATIVE COVER USING VDOT EC-2 EROSION CONTROL BLANKETS SHALL BE PLACED ON DAM SLOPES AND CREST TO PREVENT EROSION.

7. UPON COMPLETION, THE CONSTRUCTION OF THE DAM WILL BE CERTIFIED BY A GEOTECHNICAL ENGINEER WHO HAS INSPECTED THE STRUCTURE DURING CONSTRUCTION.

STORMWATER MANAGEMENT/ BMP FACILITY MAINTENANCE PLAN

PROPER MAINTENANCE OF THIS FACILITY IS ENCOURAGED TO PREVENT THE INTRODUCTION OF DEBRIS AND SEDIMENT IN TO THE FACILITY, SPILLWAY(S) AND DOWNSTREAM WATERWAYS. FOLLOWING INSTALLATION OF THE FACILITY AND ESTABLISHMENT OF VEGETATION IN DISTURBED AREAS, INSPECTIONS FOR SEDIMENT BUILDUPS WILL BE PERFORMED AT LEAST QUARTERLY. IT IS ANTICIPATED THAT UNDER NORMAL CONDITIONS, SEDIMENT REMOVAL FROM THE FACILITY WILL BE REQUIRED ONCE EVERY 10 YEARS. IF OTHER CONSTRUCTION OR RELATED ACTIVITIES ARE PERFORMED ON UPSLOPE PARCELS, ADEQUATE PROTECTION SHOULD BE PROVIDED AND INSPECTIONS PERFORMED AT LEAST ONCE WEEKLY OF THESE NEWLY DISTRIBUTED AREAS AS WELL AS INSPECTIONS FOR ACCUMULATED SEDIMENTS AT TWO BMP FACILITY.

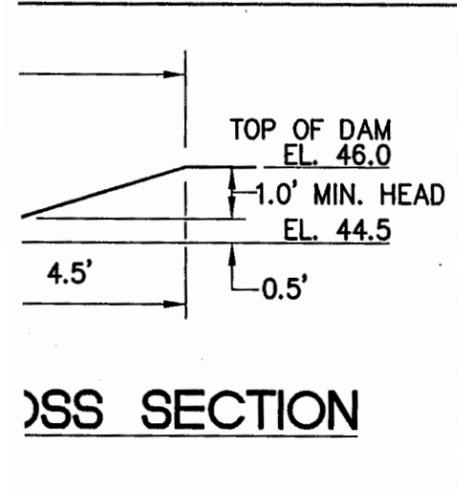
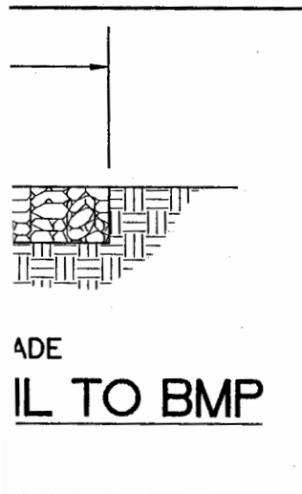
A DESIGNATED REPRESENTATIVE OF THE OWNER WILL INSPECT THE BMP STRUCTURE AFTER EACH SIGNIFICANT RAINFALL EVENT OR THE FOLLOWING WORKING DAY IF A WEEKEND OR HOLIDAY OCCURS. A SIGNIFICANT RAINFALL FOR THIS STRUCTURE IS DEFINED AS ONE (1) INCH OR MORE OF GAUGED RAINFALL WITHIN A 24 HOUR PERIOD. ONCE PER YEAR, A REPRESENTATIVE OF THE COUNTY MAY JOINTLY INSPECT THE STRUCTURE. APPROPRIATE ACTION, PERFORMED AT THE COST OF THE OWNER, WILL BE TAKEN TO ENSURE APPROPRIATE MAINTENANCE. KEYS TO LOCKED ACCESS POINTS SHALL BE MADE AVAILABLE TO COUNTY INSPECTION PERSONNEL UPON REQUEST.

INSPECTION AND MAINTENANCE OF THE FACILITY WILL CONSIST OF THE FOLLOWING ADDITIONAL MEASURES:

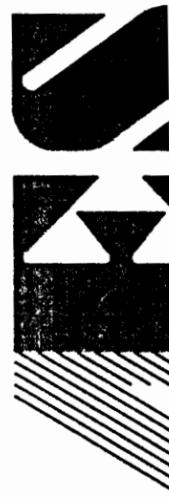
1. THE INSPECTION FOR SEDIMENT BUILDUP WILL BE PERFORMED BY VISUAL INSPECTION AND A PHYSICAL DETERMINATION OF SEDIMENT DEPTH WITHIN THE STORAGE AREA. SEDIMENT REMOVAL IS REQUIRED USING A RUBBER-WHEELED BACKHOE. AT THE SAME TIME, OR AT LEAST ONCE PER YEAR, THE RISER BOTTOM AND OUTLET PIPE SHALL BE CLEANED OF ACCUMULATED SEDIMENTS. DISPOSE OF SEDIMENTS REMOVED FROM THE FACILITY AT AN ACCEPTABLE DISPOSAL AREA. SEDIMENT SHALL NOT BE ALLOWED TO ACCUMULATE IN DEPTHS GREATER THAN 1-FOOT. NO SEDIMENT SHALL BE ALLOWED TO ACCUMULATE TO PREVENT THE PROPER FUNCTION OF ANY PIPE OR CULVERT.
2. PERFORM MAINTENANCE MOWING OF GRASSED AREAS AT LEAST TWICE EACH YEAR. GRASSES SUCH AS TALL FESCUE SHOULD BE MOWED IN EARLY SUMMER AFTER EMERGENCE OF THE HEADS ON COOL SEASON GRASSES AND IN LATE FALL TO PREVENT SEEDS OF ANNUAL WEEDS FROM MATURING. MOWING OF LEGUMES CAN BE LESS FREQUENT TREES AND SHRUBS SHOULD NOT BE PERMITTED TO GROW ON ANY PART OF THE GRADED EMBANKMENT.
3. PERFORM SOIL SAMPLING ON STABILIZED BMP SOIL AREAS ONCE EVERY FOUR (4) YEARS. SOIL SAMPLING AND TESTING SHOULD BE PERFORMED BY A QUALIFIED INDEPENDENT TESTING LABORATORY. APPLY ADDITIONAL LIME AND FERTILIZER IN ACCORDANCE WITH TEST RECOMMENDATIONS.
4. IN STABILIZED BMP AREAS, IF VEGETATION COVERS LESS THAN 40% OF SOIL SURFACES, LIME FERTILIZE AND SEED IN ACCORDANCE WITH RECOMMENDATIONS FOR NEW SEEDLINGS, AS LISTED IN DAM CONSTRUCTION NOTES. IF VEGETATION COVERS MORE THAN 40% BUT LESS THAN 70% OF SOIL SURFACES, LIME FERTILIZE AND OVERSEED IN ACCORDANCE WITH CURRENT SEEDLING RECOMMENDATIONS.
5. PERFORM QUARTERLY INSPECTIONS OF THE RELEASE STRUCTURES, RISER SECTION AND CREST OF SPILLWAY FOR THE OBSERVANCE OF COLLECTED DEBRIS. IMMEDIATELY REMOVE ANY DEBRIS TO MAINTAIN THE INTEGRITY OF THE STRUCTURE AND PROVIDE AN ATTRACTIVE APPEARANCE. DURING QUARTERLY INSPECTIONS, THE POND DRAIN VALVE, USUALLY LEFT IN THE VALVE "CLOSED" POSITION, SHALL BE INSPECTED AND OPERATED THROUGH TWO COMPLETE FULL-OPEN TO FULL-CLOSE TO FULL-OPEN CYCLES.
6. PERFORM YEARLY STRUCTURAL INSPECTIONS OF THE FACILITY FOR DAMAGE. STRUCTURAL INSPECTION SHALL BE PERFORMED ON THE CONCRETE RISER, ANTI-VORTEX DEVICE, TRASH RACK, ORIFICE/ WEIR(S), OUTLET BARREL AND POND EMBANKMENT. IF DAMAGE IS EVIDENT, FURTHER INVESTIGATION BY A PROFESSIONAL ENGINEER MAY BE REQUIRED TO ASSESS THE CONTINUED INTEGRITY OF THE STRUCTURE.
7. PERFORM QUARTERLY INSPECTIONS OF THE GRADED SIDE SLOPES OF THE FACILITY FOR SIGNS OF ANIMAL/ RODENT BORROWS OR SLOPE EROSION. IMMEDIATELY PERFORM NECESSARY REPAIRS, REFILLING OR RESEEDING AS APPROPRIATE.
8. RECORD KEEPING. THE LANDOWNER OR DESIGNATED REPRESENTATIVE SHALL KEEP REASONABLE, ACCURATE WRITTEN RECORDS OR INSPECTIONS PERFORMED FOR THE STRUCTURE. RECORDS SHALL DOCUMENT ROUTINE MAINTENANCE AND/OR REPAIRS PERFORMED. COPIES SHALL BE PROVIDED TO THE COUNTY UPON REQUEST.

DO NOT BEVEL INVERT
Sheet 1 of 2

ATED)



5248 Olde Towne Road, Suite 1
Williamsburg, Virginia 23188
(757) 253-0040



DAM SECTION AND DETAILS
SECTION V-B "BENT TREE" - PHASE 3
AT STONEHOUSE
FOR

Designed RGW	Drawn
Scale NOTED	Date 3/
Project No. 8878-00	

JAMES CITY COUNTY, VIRGINIA
ENVIRONMENTAL DIVISION

STORMWATER MANAGEMENT DESIGN PLAN CHECKLIST

I. GENERAL:

Yes No N/A

FAMILIARITY with current versions of the James City County Guidelines for Design and Construction of Stormwater Management BMPs manual; Chapter 8, Erosion and Sediment Control and Chapter 23, Chesapeake Bay Preservation ordinances of the Code of James City County, Virginia; the Virginia Erosion and Sediment Control Handbook (VESCH); and the Virginia Stormwater Management Handbook (VSMH).

WAIVER OR EXCEPTION if necessary, requested in writing, for the plan approving authority to waive or except the requirements of Chapter 23, Chesapeake Bay Preservation ordinance in accordance with procedure established in Sections 23-14 through 23-17 of the ordinance. Applies to this review case only.

VARIANCE REQUEST if necessary, requested in writing for the plan approving authority to waive or modify any of the minimum standards and specifications of the VESCH deemed inappropriate based on site conditions specific to this review case only. Variances which are approved shall be properly documented in the plan and become part of the approved erosion and sediment control plan for the site.

PROFESSIONAL SEAL AND SIGNATURE required on final and complete approved stormwater management plans, drawings, technical reports and specifications. *NOT ON REPORTS.*

WORKSHEET FOR BMP POINT SYSTEM to ensure the stormwater management plan for the project attains at least 10 BMP points (New Development) or traditional pollutant load reduction computations per the Chesapeake Bay Local Assistance Manual (Redevelopment Only). *NOT PROVIDED.*

PROPOSED CONSERVATION EASEMENT AREAS for any natural open space points claimed in the BMP worksheet.

INSPECTION/MAINTENANCE AGREEMENT is required to be prepared and executed with the County for the project.

FEMA FIRM PANEL reference with designated special flood hazard areas or zone designations associated with the site, as applicable. *MISSING REF. TO COMP A*

DRAINAGE AREA MAP at a maximum scale of 1"=200' scale showing drainage area boundaries for pre- and postdevelopment conditions and associated time of concentration flow paths. Labels to include drainage area size, runoff coefficient or curve number and time of concentration for each subarea shown on the map.

Yes No N/A

SOILS MAP with soil symbols, boundaries and legend in accordance with the current Soil Survey of James City and York Counties and the City of Williamsburg, Virginia with approximate locations of the project site, BMPs and applicable drainage basins.

None
Provided

STORMWATER MANAGEMENT NARRATIVE in a brief and simple format which describes the project; location; site and drainage basin soil characteristics; receiving water or drainage facility; existing site and drainage basin conditions (topography, land use, cover, slopes, etc.); proposed site development; proposed stormwater management and drainage plan including County BMP type selected; summary of hydrology and hydraulics; maintenance program; and any special assumptions utilized for development of the stormwater management and drainage design plan or computations.

TEMPORARY STORMWATER MANAGEMENT (if applicable) for control of stormwater runoff encountered during construction activities in addition to measures provided in the erosion and sediment control plan or stormwater management/drainage plan for the site. Adequate protection measures or sequencing provided.

None
For
BMP #54

MODIFICATION PLAN clearly defined for temporary sediment control structures which will be converted to permanent SWM/BMP structures. Includes appropriate hydrologic and hydraulic computations, conversions, sequencing and cleanout information or details. Normally related to primary control structures associated with dry detention or wet retention ponds. Normally not permitted for Group C or D categories such as bioretention, infiltration and filtering system facilities.

STORMWATER MANAGEMENT and DRAINAGE DESIGN REPORT in a bound 8-1/2 x 11 inch size format. Report shall generally include a title sheet, date, project identification, owner and preparer information, table of contents, narrative, summaries and computations as required. Computations may include: backwater, closed conduit, headwater, hydraulic, hydraulic grade line, hydrology, inlet, open channel, storm sewer, water quality, extended detention or stream channel protection and multi-stage storm routing calculations, as applicable, for the project. Computation data may include hand or computer generated computations, maps or schematics. All information should be presented in a clear, easy to follow format and should closely match construction plan information.

PLAN VIEW at 1 inch = 50 ft. scale or less (1" = 40', 1" = 30', etc.)

North arrow and plan legend.

Property lines.

Adjacent property information.

Existing site features and existing impervious cover areas.

Impervious cover tabulations.

Existing drainage facilities (natural or manmade).

Existing environmentally sensitive areas (RPA, wetlands, floodplain, steep slopes, critical soils, buffers, etc.).

Existing and proposed contours (1' or 2' contour interval) and spot elevations as necessary to define high and low topography.

Existing and proposed easement locations.

Yes No N/A

- Proposed site improvements and proposed impervious cover areas.
- Proposed stormwater conveyance, drainage and management facilities with appropriate labeled construction data and information.
- Proposed landscaping and seeding plans (disturbed areas, pond interior, etc.).
- Proposed slope stabilization areas (riprap, blankets, mattings, walls, etc.).
- Delineation of permanent pools and the 1-, 2-, 10- and 100-year Design Water Surface Elevations.
- Delineation of ponding, headwater, surcharge or backwater areas which may affect adjacent existing or proposed buildings, structures or upstream adjacent properties.
- Test boring locations with reference surface elevations (if known).
- Risers, barrels, underdrains, overflows and outlet protections.
- Emergency spillway level section and outlet channel.
- Existing and proposed site utilities and protection measures.
- Erosion and sediment control measures (for site or BMP).
- Maintenance or access corridors to permanent stormwater management, BMP or drainage facilities.

II. STORMWATER CONVEYANCE SYSTEMS:

Yes No N/A

- PLAN VIEWS**
 - Storm drain lengths, sizes, types, classes and slopes for all segments. Label directly on plan or use structure/pipe schedule.
 - Access structure (inlets, manholes, junctions, etc.) rim elevations, inverts, type and required grate or top unit and lengths labeled.
 - All structure numbers labeled.
 - Adequate horizontal clearance from other site utilities or structures.
- PROFILES** generally are not required but are encouraged to expedite review. If not provided, ensure all pipe segments have adequate minimum cover, do not exceed maximum depths of cover for the type/class of pipe specified and do not conflict with other site utilities or excavation areas.
- DETAILS**
 - Typical storm drain bedding details or reference note. *√007.*
 - Standard details or reference note for all proposed access structure types (inlets, manholes, junctions, etc.).
 - Inlet shaping detail or applicable reference note.
 - Step detail or applicable reference note (if depth 4 ft. or more).
 - Typical open channel details with designation, location, shape, type, bottom width, top width, lining, slope, length, side slope, and installation depth required for construction. Channel design data as necessary may also be included.
 - Outlet protections at all pipe outfalls.

Yes No N/A

STORMWATER CONVEYANCE SYSTEM COMPUTATIONS

- Storm Sewer Design computations based on 10-year design event.
- Hydraulic Grade Line computations based on 10-year design event.
- Inlet computations based on current VDOT procedure for spread, ponding depth and grate size required.
- Culvert Headwater computations. Design based on 10-year design storm event and check only for 100-year storm event.
- Open Channel computations based on 2-year design event for velocity and 10-year design event for capacity.
- Standard outlet protection or special energy dissipators.
- Pipe thickness design computations, as required, for selected pipe type (live load, minimum cover, maximum height of cover, etc.).
- Adequate channel computations for receiving channels (based on field measured channel section data).

III. STORMWATER MANAGEMENT / BMP FACILITIES:

Yes No N/A

HYDROLOGY - An SCS based methodology is required for the design of stormwater management/BMP facilities with watersheds exceeding 20 acres. Under 20 acres, other generally accepted methodologies such as the modified rational, critical storm are allowable. Refer to Chapter 5 of the VESCH or Chapter 5 of the VSMH.

- Runoff Curve Number or Coefficient determinations: predeveloped and ultimate development land use scenarios.
- Time of concentration: predeveloped and ultimate development indicating overland, shallow concentrated, and channel flow components (200 ft. maximum length for overland flow).
- Hydrograph generation (tabular or graphical): pre- and postdevelopment conditions for the 1-, 2-, 10-, and 100-year design storm events.

FACILITY CONFIGURATION and MINIMUM SEPARATIONS

- Screening and layout consistent with Section 24-98(d) of the Chapter 24 Zoning ordinance (landscaping, screening, visibility, etc.).
- Basic considerations for safety and unauthorized entry.
- Proper length to width ratio (Typically 2H:1V).
- Facilities with deep pools (4 feet or more in depth) provided with two benches. Fifteen (15) ft. safety bench outward from normal pool at maximum 6 percent slope and aquatic bench inward from normal shoreline below normal pool. Narrower widths may be considered on a case-by-case basis.
- Pond buffer minimum 25 feet outward from maximum design WSEL. Additional setbacks may be required to permanent structures.
- No trees, shrubs or woody plants within 15 feet of embankment toe or 25 feet from principal spillway structure.

Not Provided
15' Buffer
Shown

Yes No N/A

Infiltration and filtering system facilities generally located at least 100 feet horizontally from any water supply well; 100 feet from any downslope building; and 25 feet from any upslope buildings, unless site specific investigation allows for reduced separation.

Yes No N/A

HYDRAULIC COMPUTATIONS

- Elevation- or Stage- Storage curve and/or tabular data.
- Weir / Orifice Control - Extended Detention.
- Weir / Orifice Control - riser 1-year control for channel protection.
- Weir / Orifice Control - riser 2-year control for quantity (if required).
- Weir / Orifice Control - riser 10-year control for quantity (if required).
- Inlet / Outlet (barrel) control - (All Storms).
- Check for barrel control prior to riser orifice flow to prevent slug flow-water hammer conditions.
- Emergency spillway capacity and depth of flow.
- Elevation - Discharge (Outlet Rating) curve and/or table. Provide all supporting calculations and/or design assumptions.
- Adequate channel computations for receiving channel. May be waived if facility is designed based on current Stream Channel Protection criteria.

POND or RESERVOIR ROUTING

- Storage-Indication Routing of postdeveloped inflow hydrographs for the 1-, 2-, 10-, and 100-year design storms. Preference is for structure to discharge up to the 10-year storm through the principal spillway and pass the 100-year storm with a minimum 1 foot of freeboard through a combination principal and emergency spillways. If no emergency spillway is provided, riser must be large enough to pass the design high water flow and trash without overtopping the facility, have 3 square feet or more of cross-sectional area, contain a hood type inlet and have a minimum freeboard of 2 feet. Token spillways with minimum 8 ft. width are also recommended at or above the design 100-year storm elevation.
- Downstream hydrographs at established study points, if conditions warrant (ie. facility discharge combined with uncontrolled bypass).

MISCELLANEOUS COMPUTATIONS

- Water quality volume for permanent pool based on selected BMP treatment volume (WQv).
- Water quality volume for extended detention based on selected BMP treatment volume (WQv) with drawdown computations.
- Drawdown computations for the 1-year, 24 hour detention for stream channel protection criteria.
- Pond drain computations (within 24 hours). *WHY DRY DET*
- Anti-seep collar design (concrete preferred) or match material type.
- Filter diaphragm design (or alternative method of controlling seepage).

?

Yes No N/A

- Riser / base structure flotation analyses. FS = 1.25 minimum.
- Downstream danger reach study and/or emergency action plan (if conditions warrant).
- Upstream backwater analyses onto offsite adjacent property (if conditions warrant).
- 100 year floodplain impacts (if conditions warrant).

Yes No N/A

GEOTECHNICAL REQUIREMENTS

- Geotechnical Report with recommendations specific to BMP facility type selected. Report prepared by a registered professional engineer. Requires submission, review and approval prior to issuance of Land Disturbance Permit.
- Initial Feasibility Testing requirements satisfied as per Appendix E of the James City County Guidelines for Design and Construction of Stormwater Management BMPs manual. (Infiltration, Bioretention and Filtering System BMP types only).
- Concept Design Testing requirements satisfied as per Appendix E of the James City County Guidelines for Design and Construction of Stormwater Management BMPs manual. (Infiltration, Bioretention and Filtering System BMP types only).
- Minimum Boring locations: borrow area, pool area, principal control structure, top of facility near one abutment and emergency spillway if provided.
- Boring logs with Unified Soil Classification (ASTM D2487), soils descriptions and depths to bedrock and the seasonal water table indicated.
- Standard County Record Drawing/Construction Certification note provided on plan. *Note: It is understood that preparation of record drawings and construction certifications as required for project facilities may not necessarily be performed by the plan preparer. These components may be performed by others.*

Yes No N/A

PRINCIPAL SPILLWAY PROFILE AND ASSOCIATED DETAILS

- EXISTING GROUND AND PROPOSED GRADE**
 - Embankment or excavation side slopes labeled (3H:1V maximum).
 - Minimum top width labeled (per VESCH or VSMH requirements).
 - Removal of unsuitable material under proposed facility (per Geotechnical Report requirements).

Yes No N/A

CORE TRENCH

- Material (per plan or Geotechnical Report).
- Bottom width (4' minimum or greater as dictated by Geotechnical Report recommendations).
- Side slopes (1:1 maximum steepness)
- Depth (4' minimum or greater as dictated by Geotechnical Report).

ASTM C361 PIPE
OR
ASTM C478 MH

PRINCIPAL CONTROL STRUCTURE. RISER OR SIMILAR STRUCTURE (DETAILS REQUIRED FOR ALL ITEMS)

- Durable, watertight, resistant material (concrete preferred).
- Riser diameter is at least 1.25 times larger than barrel diameter.
- All pertinent dimensions and elevations shown.
- Control orifice or weir dimensions and elevations shown.
- Trash rack - removable - for each release.
- Anti-vortex device, baffle or plate.
- Riser base structure with dimensions and embedment specifications (concrete preferred).
- Interior access (steps, ladders, etc.) for maintenance for structures over 4 feet in height. Excessively high risers may need some form of exterior access on top portion.
- Low flow orifice with trash rack device.

PRINCIPAL CONTROL STRUCTURE OUTLET BARREL

- Material (ASTM C-361 reinforced concrete pipe) with watertight joints. Prior approval required for all other pipe material (other RCP types, CMP, CPP, PVC, etc.).
- Support and bedding requirements for barrel - concrete cradles, etc. or as recommended by the Geotechnical Report.
- Pipe inverts, length, size, class and slope shown.
- Flared end section or endwall provided on barrel outlet.

SEEPAGE CONTROL

where

- Phreatic line shown (4:1 slope measured from the intersection of the embankment and the principal spillway design high water).

ANTI-SEEP COLLARS

- Anti-seep collar, concrete preferred.
- Size - 15 percent increase in length of saturation using outside pipe diameter.
- Spacing and location on barrel (located at least 2 feet from a pipe joint).

FILTER DIAPHRAGMS

Design based on latest NRCS design methods and certified by a professional engineer.

Yes No N/A

ELEVATION AND DIMENSIONAL DESIGN DATA

Top of facility - construction height and settled height (10 percent settlement).

Crest of principal control structure spillway at least one (1) foot below crest of emergency spillway, if provided.

Minimum freeboard of one (1) foot above the 100-year design high water elevation for facilities with an emergency spillway.

Minimum freeboard of two (2) feet above the 100-year design high water elevation for facilities without an emergency spillway or in accordance with the SCS National Engineering Handbook (prior approval required).

Basin Sediment Clean-Out elevation (permanent mode). Typically 10 to 25 percent of water quality volume.

NEED CO
ELEV
BMP #54
@ 750 Mope.

CROSS SECTION THROUGH FACILITY

Existing Ground.

Proposed grade.

Top of facility - constructed and settled.

Location of emergency spillway with side slopes labeled (emergency spillway in cut).

Bottom of core trench (4' minimum).

Location of each soil boring.

Barrel location.

Existing and proposed utility location/protection.

EMERGENCY SPILLWAY PROFILE

Existing ground.

Inlet, level (control) and outlet sections per SCS.

Spillway and crest elevations.

where?

PRETREATMENT DEVICES of adequate depth and properly designed using required pretreatment volumes for the selected County BMP facility type. Including, but not limited to: sediment forebays, sediment basins, sumps, grass channels, gravel diaphragms, plunge pools, chamber separators, manufactured systems or other acceptable methods.

Yes No N/A

CONSTRUCTION SPECIFICATIONS and NOTES

- Anticipated sequence of construction for BMP (consistent with erosion and sediment control plan).
- Provisions to control base stream or storm flow conditions encountered during construction.
- Site and subgrade preparation requirements.
- Embankment, fill and backfill material soil and placement (lift) thickness requirements.
- Compaction and soil moisture content requirements.
- Geosynthetics for drainage, filtration, moisture barrier, separation, and reinforcement purposes.
- Clay or synthetic (PVC or HDPE) pond liners.
- Storm drain, underdrain and pipe conduit requirements.
- Minimum depth of pipe cover for temporary (construction) and final cover conditions.
- Permanent shutoff valve and pond drain.
- Concrete requirements for structural components.
- Riprap and slope protection.
- Access or maintenance road surface, base, subbase.
- Temporary and permanent stabilization measures.
- Temporary or permanent safety fencing.
- BMP Landscaping (deep, shallow, fringe, perimeter, etc.)
- Dust and traffic control (if warranted).
- Construction monitoring and certification by professional.
- Other: _____
- Other: _____

with
DET

MAINTENANCE PROVISIONS

- Entity responsible for maintenance identified..
- Maintenance Plan which outlines the long-term schedule for inspection/maintenance of the facility and forebays
- Maintenance access from public right-of-way or publicly traveled road.
- Maintenance easement provided encompassing high water pool and buffer, principal and emergency spillways, outlet structures, forebays, embankment area and possible sediment-removal stockpile areas.
- Minimum 6 foot wide public safety shelf (landing) or alternative fencing.

**James City County, Virginia
Environmental Division
Stormwater Management Program**

**Stormwater Management Design Plan
Staff "Quick" Review**

Plan No. SP - 81 - 99 Date/Time: 04/05/01 2:00pm
 Project Name: Stonehouse Bent Tree, Section 5B, Phase 3 (35 Lots)
 Rough Location: 9000' NE OF INTX. I 64 & US 30
 ADC Map: Sheet 1 Grid: J - 2 First Review
 Flood Map / Zone: 510201- 00 10B Zone: A1X Review

Drainage Area: Description: A (SFHA) NO BFE's determined; X outside 500-YEAR.
 Onsite Only Offsite Only Combination of Both

Submitted: Y N

- Demolition Plan (if applicable) Sheets: _____
- Site, Geometric or Layout Plan Sheets: 2, 3, 4, 5, 6, 7, 8, 9
- Grading Plan Sheets: 13, 14, 15
- Storm Drainage Plan Sheets: 12, 13, 14, 15
- E&SC Plan Sheets: 13, 14, 15, 16
- Profiles (~~Storm~~ ROAD) Sheets: 10, 11
- Environmental Inventory Sheets: 16
- Note & Detail Sheets Sheets: 17, 18, 19, 20
- Drainage Map(s) 12
- Soils Map 16
- E&SC and SWM Design Plan Checklists.
- E&SC and/or Stormwater Management / Drainage Narratives.
- E&SC and/or Stormwater Management Design Report with Calculations (Attachment). DRY POND
- Geotechnical Report (Attachment).
- Waivers, Variances, or Exceptions (Attachments in Writing).
- VESCH CBP Ord (RPA, Steep Slope Policy) JCC BMP Manual
- Other (List): _____

JCC GIS Database: Zoning: PVO - R Tax Parcel/GPIN: (6-4)(1-1)
 Receiving Water: UT of Ware Creek Site Acreage: 35.07 acres / s.f.

Other Approvals (SUP, etc.): _____
 Site Plan Information: Owner: Stonehouse Development Company LLC.
 Zoning: PVO - R Description: Res Planned Unit Dev
 Site Area: 35.07 acres / s.f.
 Disturbed Area: 9.39 acres / s.f. (26.78 %)
 Disturbance > 5 acres, VPDES Notice of Intent required.
 Impervious Cover: ? acres / s.f. (. %)
 Less than or equal to 60 percent. Meets CBPO requirements.
 More than 60 percent. Does Not Meet CBPO requirements.
 Open / Green Space: ? acres / s.f. (. %)

Site Development Plan:
 Residential, Lots, etc. Commercial (B / O / R) Govern./Institutional Industrial
 Roadways or Entrances Parking or Loading Water Sanitary Sewer
 Landscaping SWM/BMP facilities Manmade Drainage Parks, Amenities
 Pump/Lift Station Dams (regulated) Other,
 Site Improvements: 35 LOTS; AVG SIZE 0.79AC; 1 LOT PER AC. DENSITY

Soils Information:
Soil Survey Sheet

Site: 11C, 14B, 15F, 17, 19B, 25B
 DA: SAME
 BMP: 15F
 Description of Soils at BMP: 15F

Hydric: Yes No 17
 HSG: _____
 Hydric: Yes No

BMP Control:
BMP Types:

None Onsite Offsite Previously Approved Manufactured BMP
 1- Name: DRY EXT DET (JCC BMP Type F - 2), Points 4
 2- Name: _____ (JCC BMP Type _____ - _____), Points _____
 3- Name: _____ (JCC BMP Type _____ - _____), Points _____

BMP 5.4

Onsite Drainage:

Reinforced Concrete Pipe Corrugated Metal Pipe Aluminum Type Pipe
 Corrugated Polyethylene Pipe PVC Type Pipe Open Channel Type
 Storm Drain Culverts Type: P6-2A, RCP
 Inlets Other (Specify): _____

1. VDOT Standards & Specifications Referenced for work **within** R/W: Yes No
 2. VDOT Standards & Specifications Referenced for work **outside** R/W: Yes No

Site Limitations:

RPA RMA Steep Slopes Delineated Wetlands
 Hydric Soils Critical Soils Vegetated Buffers: _____
 Defined Natural Drainage Features onsite Downstream Storm/Culv.
 Evidence of Downstream Channel Erosion (by Field Observation) _____
 Floodplain Problem Drainage Area Stormwater Hotspot
 Site Activities may warrant a General VPDES Permit for Discharge of Stormwater Associated with Industrial Activities (ie. process water, batch plants, etc.).
 Other (Specify): _____

Site Stormwater Management / BMP Control (Add sheets if necessary for Multiple Onsite Facilities):

SCS METHOD

<input type="checkbox"/> Yes <input type="checkbox"/> No	#			
	<u>BMP 5.4</u>			
Predev (Present)	DA = <u>12.19</u> ac.	C/CN = <u>72</u>	Tc = <u>37</u> min / hrs.	
2-year	<u>10.06</u>	cfs		<u>41,037 CF</u>
10-year	<u>27.10</u>	cfs		
100-year	<u>45.38</u>	cfs		
PostDev w/o Detention (Inflow)	DA = <u>11.05</u> ac.	C/CN = <u>75</u>	Tc = <u>20</u> min / hrs.	
1-year	<u>9.98</u>			
2-year	<u>16.19</u>	cfs		
10-year	<u>39.92</u>	cfs		
100-year	46.52 <u>64.49</u>	cfs		
PostDev with Detention (Routed)	DA = <u>11.05</u> ac.	C/CN = <u>75</u>	Tc = <u>20</u> min / hrs.	
2-year	<u>1.02</u>	cfs	at El. <u>42.07</u>	<u>52,217 CF</u>
10-year	<u>27.47</u>	cfs	at El. <u>43.68</u>	
100-year (DHW)	<u>59.86</u>	cfs	at El. <u>44.16</u>	

25-YR
31.95 cfs

25-YEAR
46.52 cfs

1-YR
0.90 cfs
@ EL 40.38

Downstream Tailwater Assumption for Pond Routing: 34.50 (4.1' Depth)
 Routed Peak Discharges (Outflows) from BMP meet Predevelopment Allowables: Yes No
 Appears to Meet VESCH / E&SC Ordinance / CBP Ordinance Requirements: Yes No

1-YR, 24 CONTROL Provided.

Pond / BMP Design Data (Add Sheet If Necessary for Multiple Onsite Facilities):

Check if None Provided: BMP # 5.4 Type: EXT DET DET

* See Below for Pertinent WQv / Stream CPv Design Information.

Y N

Top of Facility (Dam Crest) El. 46.0

Design High Water (100-year) El. 44.16

Emergency Spillway (ES) Crest El. 44.5 BW: _____ SS: _____

FreeBoard 1.84 1 ft. or > with Emerg. Spillway.

Acceptable Not Acceptable. 2 ft. or > w/o Emerg. Spillway.

Principal Spillway (Riser) Crest El. 43.0 Size/Type: _____

Principal Spillway Crest 1 ft. below Crest of Emergency Spillway. Yes No N/A

Stage-Storage Curve of Data

Outlet Rating Curve or Table (Composite Structure)

1-year design storm El. 40.6 or Volume 33,394 CF

1-year, 24 hour detention criteria for Stream Channel Protection. Yes No N/A

Extended Detention for WQ Provided (Min. 24 hours) Yes No N/A

Normal/Permanent Pool El. 40.0 N/A N/A

Orifice/Weir #1 (Highest El.) El. 44.5 Type: ES 6' WIDE, GRASS; 3H:1V

Orifice/Weir #2 El. 43.0 Type: TOP 60" RCP RISER

Orifice/Weir #3 El. 34.5 Type: 4" BMP ORIF.

Orifice/Weir #4 El. _____ Type: _____

Orifice/Weir #5 (Lowest El.) El. _____ Type: _____

Low Flow Orifice (ExDet, CPv) El. 34.5 Type: 4" BMP ORIF

Pond Drain w/ Valve (24 hr.) El. _____ Type: PVC GV PROVIDED, NOT RE'LD.

Pond Bottom (Positive Drain) El. 34.5 Riser Height: 11'

Steps or Access Provided (for over 4 ft. depth) N/A

Riser Base EXT WITH BASE Bottom El. 32 Type: 43-32

Core Trench N/A

Anti-Seep Collars or other Acceptable Seepage Control Method. N/A ROCK FILTER & ASC.

Principal Spillway-AntiVortex/Trash Rack Device Type: 72" CONC CAP.

Low Flow Orifice Trash Rack. EW- Type: EW-11 TYPE C, 4" ORIF

Outlet Barrel: Type/Class: III Size: 30"

Inv. U/S: 32.0 Inv D/S: 30.4

Slope: 2.00% Length: 80 (ft.)

Flared End Section/Wingwalls. Matches Outlet Barrel material type, over 48 inch with fence. EW-1

Outlet Protection.

Standard Riprap Outlet Protection (OP) Type: _____

Special Dissipator Structure (SDS) Type: STILLING BASIN (L & W?)

BMP Sediment Cleanout Elevation El. 35.5 or Depth 1'-0"

Adequate Channel Downstream of BMP: 1-year, 24-hour; or MS # 19 criteria.

Sketch or Notes, If Necessary:

TYPICAL RISER/BARREL CONFIG.

* WQv / Stream CPv Design Summary

Imperv. Area	?
WQTV (Per JCC Man)	<u>1.0 inch per imperv area</u>
WQ Vol. Required	?
WQ Vol. Provided	?
1-yr SCPv Required	<u>33,394 CF</u>
1-yr SCPv Provided	
Ext Det Orifice Size	<u>4-inch</u>

Sediment Trap & Basins

Temporary Sediment Trap # 1 _____ DA = _____ < 3 acres

Temporary Sediment Trap # 2 _____ DA = _____ < 3 acres

Temporary Sediment Basin # 1 _____ DA = _____ BMP # _____ convert.

Temporary Sediment Basin # 2 _____ DA = _____ BMP # _____ convert.

E&SC Plan Comments: _____

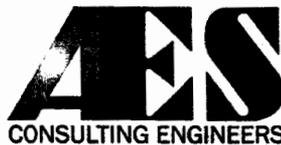
**STONEHOUSE
AREA 1, PHASE 1
BENT TREE, SECT. V-B
PHASE 3**

FOR
STONEHOUSE DEVELOPMENT COMPANY, LLC.

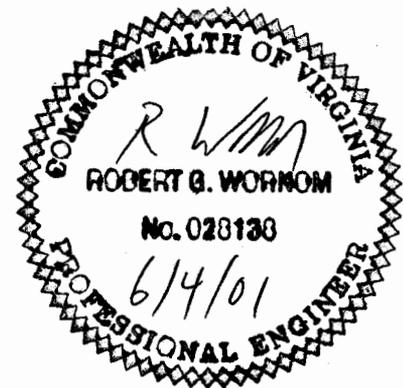
PROJECT NUMBER: 8878-00

STORMWATER MANAGEMENT/BMP #5.4

JUNE 4, 2001 (REVISED)



AES Consulting Engineers
5248 Olde Towne Road. Suite 1
Williamsburg, VA 23188
(757) 253-0040 Fax: (757) 220-8994
<http://www.aesva.com>



STREAM CHANNEL PROTECTION CALCULATIONS
for
STONEHOUSE Ph 1, Bent Tree (Sect. V-B) Ph3
AES Project No.: 8878-00

PROPOSED POND VOLUME

Eleva	Depth	Area (sq. ft.)	Incremental Volume (cu. ft.)	Sum Volume (cu. ft.)	Sum Volume (cu. yd.)	Volume Above NPE
34.5	0.0	0	0	0	0	
36.0	1.5	809	607	607	22	
38.0	2.0	2,568	3,377	3,984	148	
40.0	2.0	5,150	7,718	11,702	433	
42.0	2.0	8,390	13,540	25,242	935	
→ 43.0	1.0	10,281	9,336	34,577	1,281	
44.0	1.0	12,172	11,227	45,804	1,696	
44.5	0.5	12,915	6,272	52,076	1,929	
45.0	0.5	13,659	6,644	58,719	2,175	
46.0	1.0	15,146	14,403	73,122	2,708	

RELEASE RATE REQUIRED TO DETAINED VOLUME FOR 24 HOURS

Required Volume based upon 1-Year, 24-Hour Storm Hydrograph =

33,394 cubic feet

*SCS OR CRIT STORM?
SCV - SCS METHOD.*

Elevation of water surface associated with required volume =

43.0

Elevation of Low Flow Orifice =

34.5 ✓

Average Head, in feet =

4.3

Average Release Rate Calculation

$$\frac{33,394 \text{ cubic feet}}{(24 \text{ hours} \times 60 \text{ minutes/hour} \times 60 \text{ seconds/minute})} = 0.4 \text{ cfs}$$

LOW FLOW ORIFICE DIAMETER REQUIRED TO MAINTAIN AVERAGE RELEASE RATE

$$\text{Diameter of Low Flow Orifice} = 2 * (Q / ((64.32 * (h / 2)) ^ (1/2) * 0.6 * 3.14)) ^ (1/2)$$

where, Q equals average release rate (cfs), h equals average head (feet)

Diameter of Low Flow Orifice =

0.30 feet, or

4 inches

Hydrograph Summary Report

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Return period (yrs)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description	
1	SCS Runoff	7.0	2	736	37,219	2	—	—	—	Pre 2-yr	
2	SCS Runoff	22.4	2	736	104,210	10	—	—	—	Pre 10-yr	
3	SCS Runoff	39.6	2	736	180,441	100	—	—	—	Pre 100-yr	
5	SCS Runoff	7.7	2	732	33,545	1	—	—	—	Post 1-yr	
6	SCS Runoff	12.6	2	732	52,453	2	—	—	—	Post 2-yr	
7	SCS Runoff	31.3	2	730	125,405	10	—	—	—	Post 10-yr	
8	SCS Runoff	50.8	2	730	203,144	100	—	—	—	Post 100-yr	
10	Reservoir	1.0	2	804	33,545	1	5	40.30	13,705	1-yr Routed	
11	Reservoir	1.1	2	834	52,453	2	6	41.99	25,183	2-yr Routed	
12	Reservoir	21.9	2	744	125,405	10	7	43.67	42,103	10-yr Routed	
13	Reservoir	46.9	2	736	203,144	100	8	44.15 <i>0.11</i>	47,689	100-yr Routed	
Proj. file: 887854.gpw				IDF file: Jcc.IDF				Run date: 06-14-2001			

Hydrograph Plot

English

Hyd. No. 10

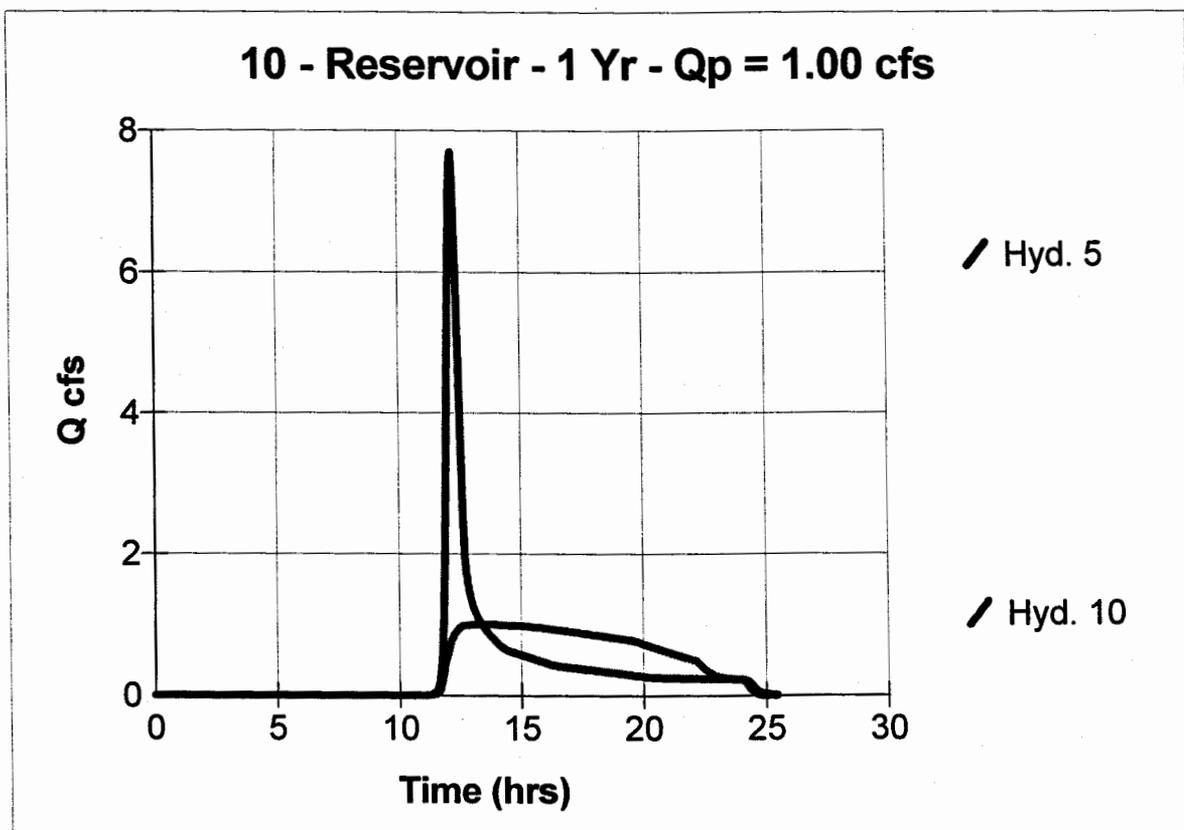
1-yr Routed

Hydrograph type = Reservoir
Storm frequency = 1 yrs
Inflow hyd. No. = 5
Max. Elevation = 40.30 ft

Peak discharge = 1.00 cfs
Time interval = 2 min
Reservoir name = BMP 5.4
Max. Storage = 13,705 cuft

Storage Indication method used.

Total Volume = 33,545 cuft



1-yr
Routed

Hydrograph Plot

English

Hyd. No. 11

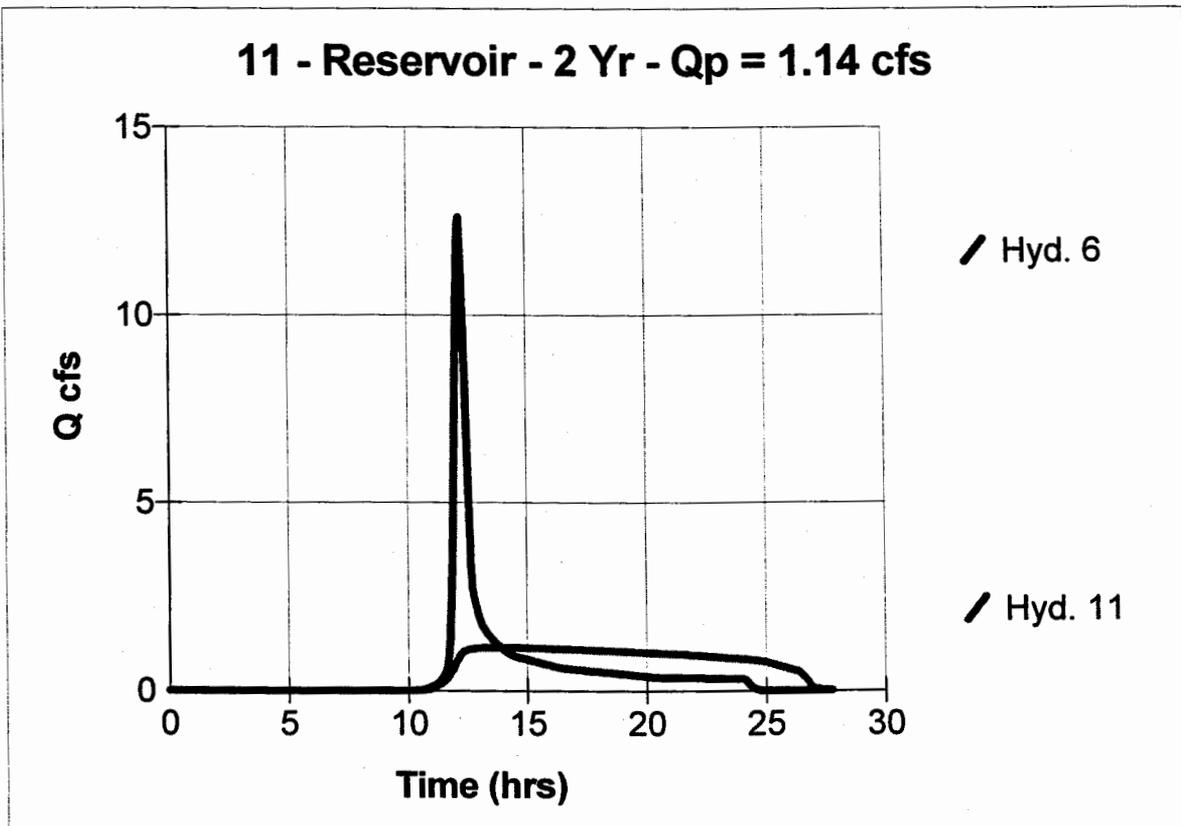
2-yr Routed

Hydrograph type = Reservoir
Storm frequency = 2 yrs
Inflow hyd. No. = 6
Max. Elevation = 41.99 ft

Peak discharge = 1.14 cfs
Time interval = 2 min
Reservoir name = BMP 5.4
Max. Storage = 25,183 cuft

Storage Indication method used.

Total Volume = 52,453 cuft



2-yr
Routed

Hydrograph Plot

English

Hyd. No. 12

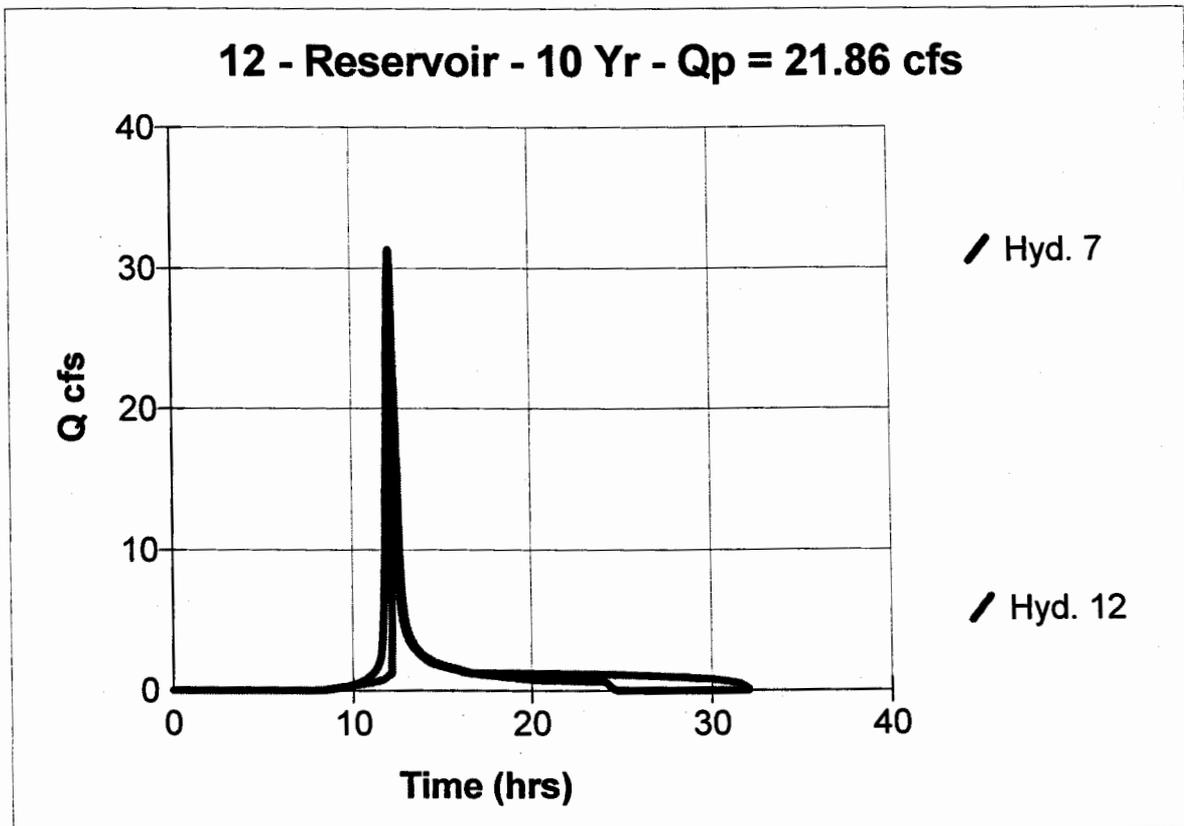
10-yr Routed

Hydrograph type = Reservoir
Storm frequency = 10 yrs
Inflow hyd. No. = 7
Max. Elevation = 43.67 ft

Peak discharge = 21.86 cfs
Time interval = 2 min
Reservoir name = BMP 5.4
Max. Storage = 42,103 cuft

Storage Indication method used.

Total Volume = 125,405 cuft



10-yr
Routed

Hydrograph Plot

English

Hyd. No. 13

100-yr Routed

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 8
Max. Elevation = 44.15 ft

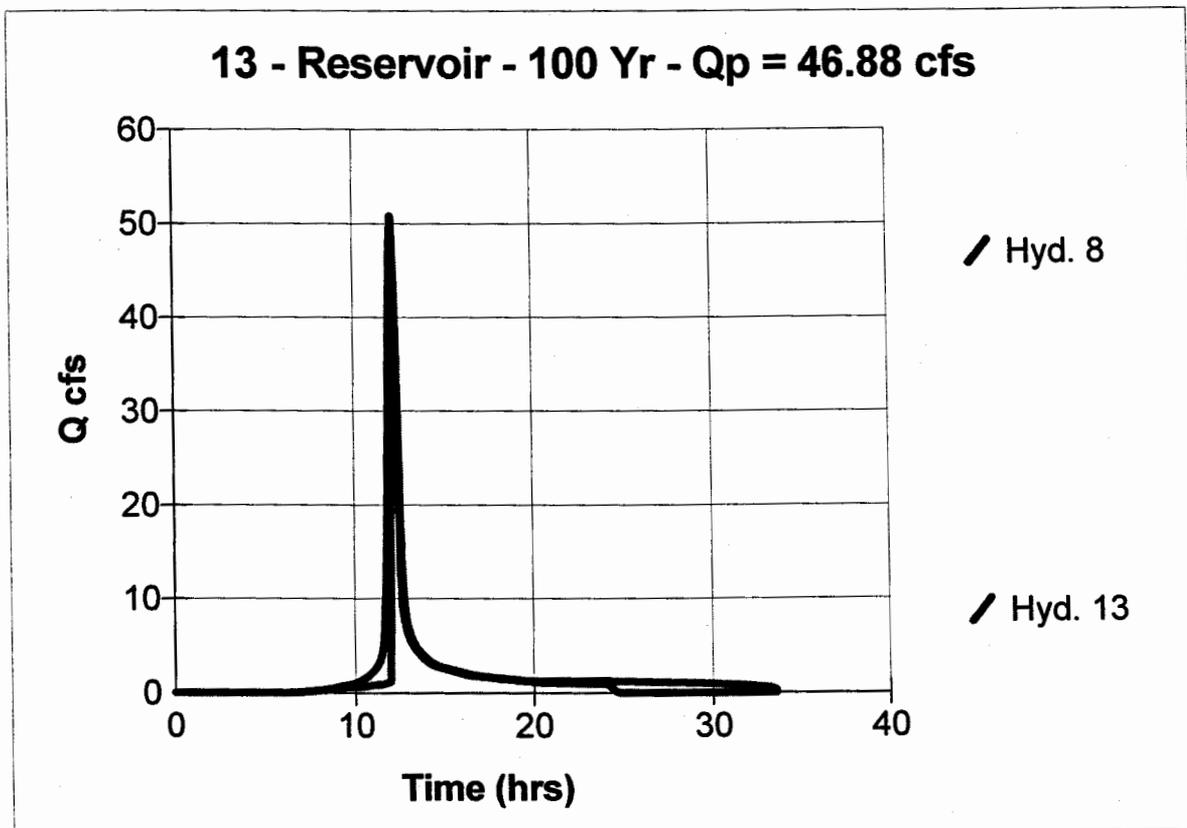
DHW

Peak discharge = 46.88 cfs
Time interval = 2 min
Reservoir name = BMP 5.4
Max. Storage = 47,689 cuft

DHW

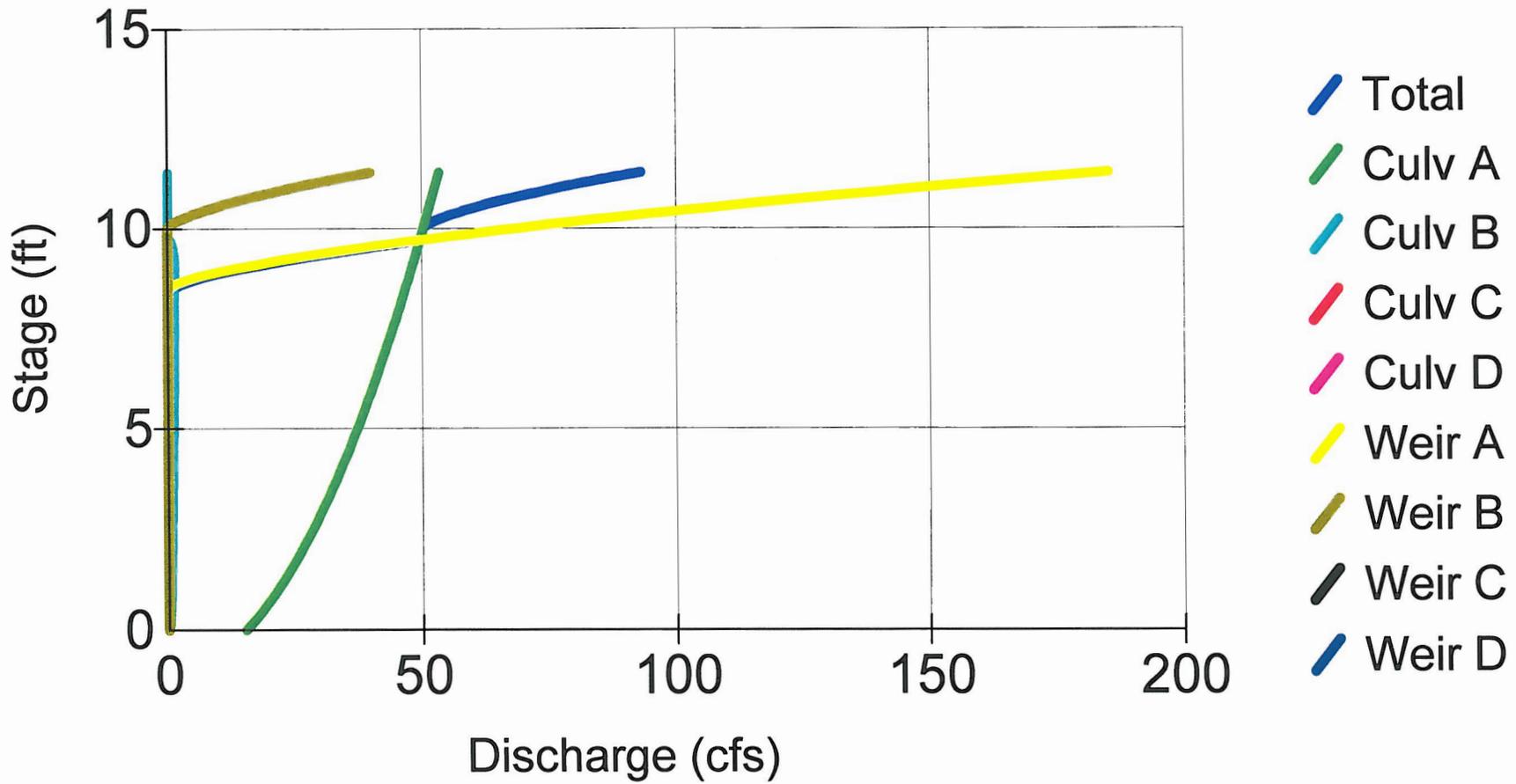
Storage Indication method used.

Total Volume = 203,144 cuft



*100-YEAR
ROUTED*

BMP 5.4



Reservoir Report

Reservoir No. 1 - BMP 5.4

Pond Data

Pond storage is based on known contour areas

Stage / Storage Table

Stage ft	Elevation ft	Contour area sqft	Incr. Storage cuft	Total storage cuft
0.00	34.50	00	0	0
1.50	36.00	809	607	607
3.50	38.00	2,568	3,377	3,984
5.50	40.00	5,150	7,718	11,702
7.50	42.00	8,390	13,540	25,242
8.50	43.00	10,281	9,336	34,578
9.50	44.00	12,172	11,227	45,805
10.00	44.50	12,915	6,272	52,077
10.50	45.00	13,659	6,644	58,721
11.50	46.00	15,146	14,403	73,124

Culvert / Orifice Structures

	[A]	[B]	[C]	[D]
Rise in	= 24.0 ✓	4.0 ✓	0.0	0.0
Span in	= 24.0 ✓	4.0 ✓	0.0	0.0
No. Barrels	= 1	1	0	0
Invert El. ft	= 32.50 ✓	34.50	0.00	0.00
Length ft	= 70.0 ✓	6.0 ✓	0.0	0.0
Slope %	= 3.00 ✓	5.00	0.00	0.00
N-Value	= .013	.013 ✓	.000	.000
Orif. Coeff.	= 0.60 ✓	0.60	0.00	0.00
Multi-Stage	= —	Yes	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len ft	= 12.5 ✓	8.0 ✓	0.0	0.0
Crest El. ft	= 43.00 ✓	44.50	0.00	0.00
Weir Coeff.	= 3.00 ✓	3.00	0.00	0.00
Eqn. Exp.	= 1.50	1.50	0.00	0.00
Multi-Stage	= Yes	No	No	No

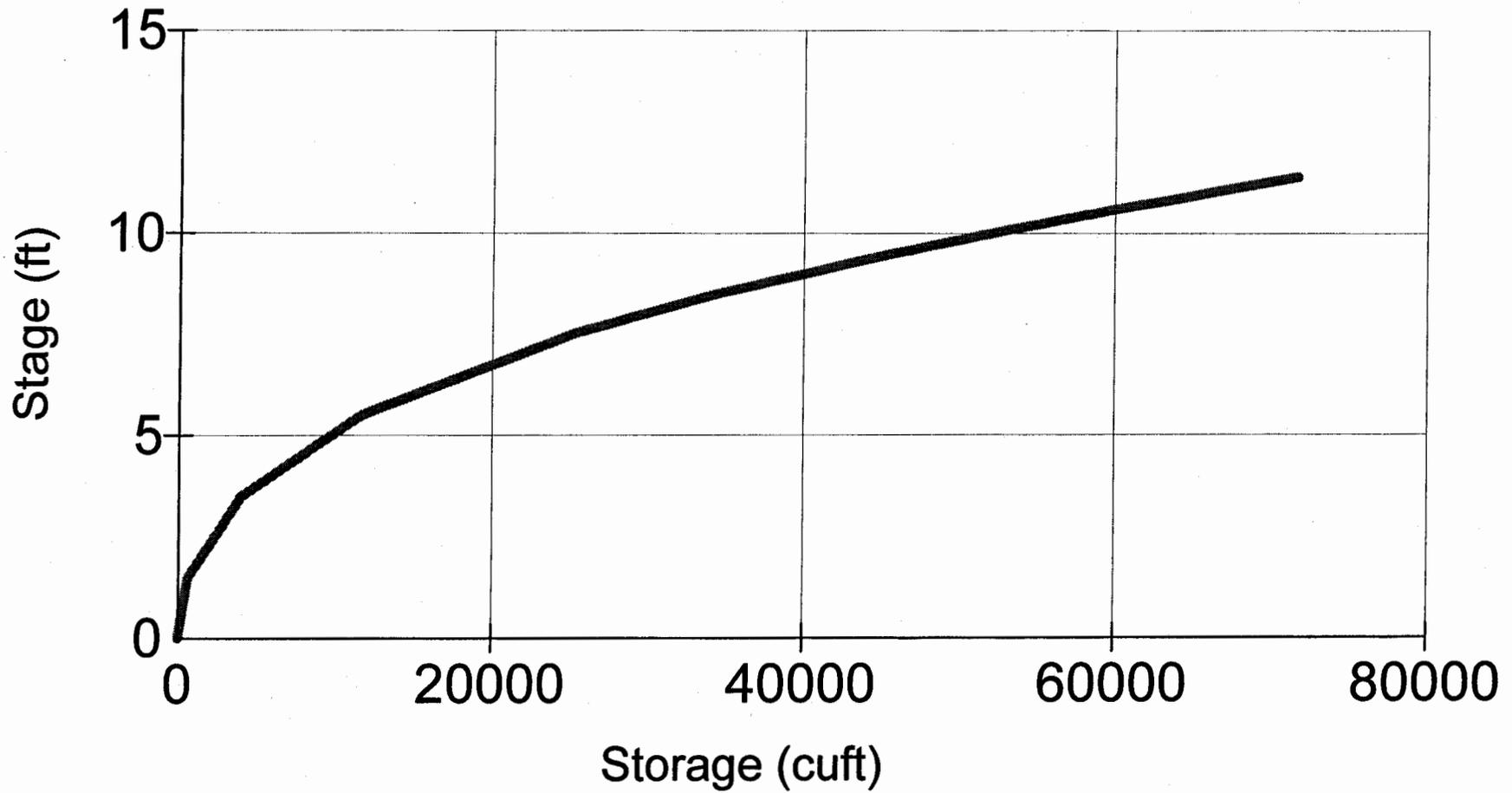
Tailwater Elevation = 32.00 ft (1.6')

Note: All outflows have been analyzed under inlet and outlet control.

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	Clv D cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Discharge cfs
0.00	0	34.50	15.12	0.00	—	—	0.00	0.00	—	—	0.00
1.50	607	36.00	23.91	0.49	—	—	0.00	0.00	—	—	0.49
3.50	3,984	38.00	32.08	0.77	—	—	0.00	0.00	—	—	0.77
5.50	11,702	40.00	38.56	0.97	—	—	0.00	0.00	—	—	0.97
7.50	25,242	42.00	44.10	1.14	—	—	0.00	0.00	—	—	1.14
8.50	34,578	43.00	46.62	1.21	—	—	0.00	0.00	—	—	1.21
9.50	45,805	44.00	49.01	1.00	—	—	37.50	0.00	—	—	38.50
10.00	52,077	44.50	50.16	0.00	—	—	68.89	0.00	—	—	50.16
10.50	58,721	45.00	51.29	0.00	—	—	106.07	8.49	—	—	59.78
11.50	73,124	46.00	53.47	0.00	—	—	194.86	44.09	—	—	97.57

BMP 5.4



SCS HYDROGRAPH GENERATION
for
STONEHOUSE Ph1, Bent Tree (Sect. V-B) Ph 3
AES Project No.: 8878-00
June 14, 2001

PRE-DEVELOPMENT CONDITIONS TO POINT OF CONCERN

A. Pre-Development Drainage Area to Point of Concern = 12.2 Acres

B. Pre-development Land Use, Soil Classification and Calculation of Composite Curve Number

	Soil Type	Hydrologic Group Appendix 4A*	Land Use	Area Acres	CN Table 4-6*	Adjusted CN
1)	10-B Craven Fine Sandy Loam	C	Wooded	3.6	70	253
2)	11-C Craven-Uchee	C	Wooded	3.1	70	214
3)	14-B Emporia Fine Sandy Loam	C	Wooded	0.8	70	54
3)	15-F Emporia Complex	C	Wooded	2.6	70	185
4)	19-B Kempsville-Emporia Fine Sandy Loam	B	Wooded	2.1	55	116
5)						
Totals =				12.2		822
Composite CN =						67

C. Pre-Development Time of Concentration Calculations

1)	Overland Flow	Segment C-D				
	Surface description					Woods - Light Underbrush
	Manning's roughness coefficient, n (Table 4-9a*)					0.40
	Length of overland flow, L					200 Feet
	2-year 24-hour rainfall, P2 (Appendix 4B*)					3.5 inches
	Average slope of overland flow, s					0.045 feet per foot
	Travel time, $T_t = (0.007 \cdot (n \cdot L)^{0.8}) / (P2^{0.5} \cdot s^{0.4})$					0.43 hours
2)	Shallow concentrated flow	Segment B-C				
	Surface description, paved or unpaved					unpaved
	Length of shallow concentrated flow, L					200 Feet
	Average slope of shallow concentrated flow, s					0.02 feet per foot
	Average velocity, v					1.0 feet per second
	Travel time, $T_t = L / (3600 \cdot v)$					0.06 hours
3)	Channel or Pipe Flow	Segment A-B				
	Length of channel flow, L					1180 Feet
	Average velocity of channel flow, v					2.5 feet per second
	Travel time, $T_t = L / (3600 \cdot v)$					0.13 hours
	Total Time of Concentration =					0.62 hours
					or	37 minutes

*Va. SWM Handbook (DCR, DSWC)

Hydrograph Plot

English

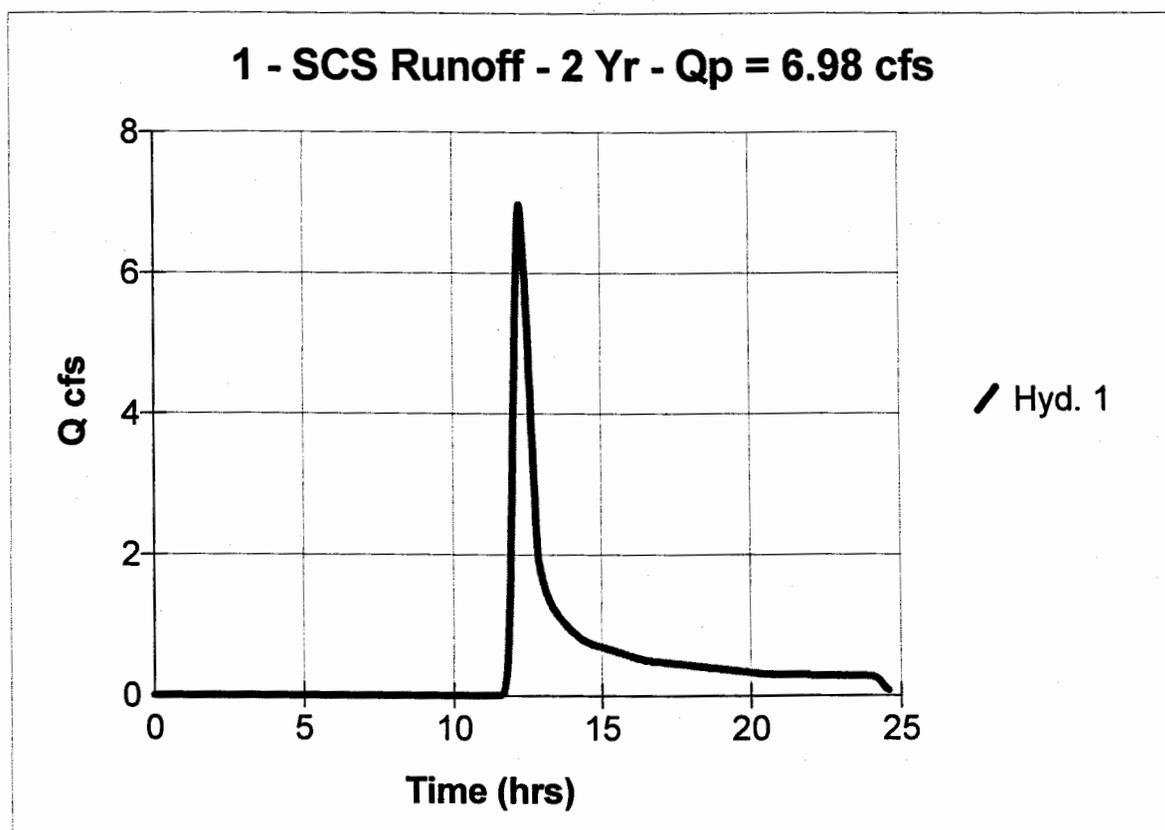
Hyd. No. 1

Pre-Development 2-yr

Hydrograph type = SCS Runoff
Storm frequency = 2 yrs
Drainage area = 12.20 ac
Basin Slope = 5.0 %
Tc method = USER
Total precip. = 3.50 in
Storm duration = 24 hrs

Peak discharge = 6.98 cfs
Time interval = 2 min
Curve number = 67
Hydraulic length = 1580 ft
Time of conc. (Tc) = 37 min
Distribution = Type II
Shape factor = 484

Total Volume = 37,219 cuft



Hydrograph Plot

English

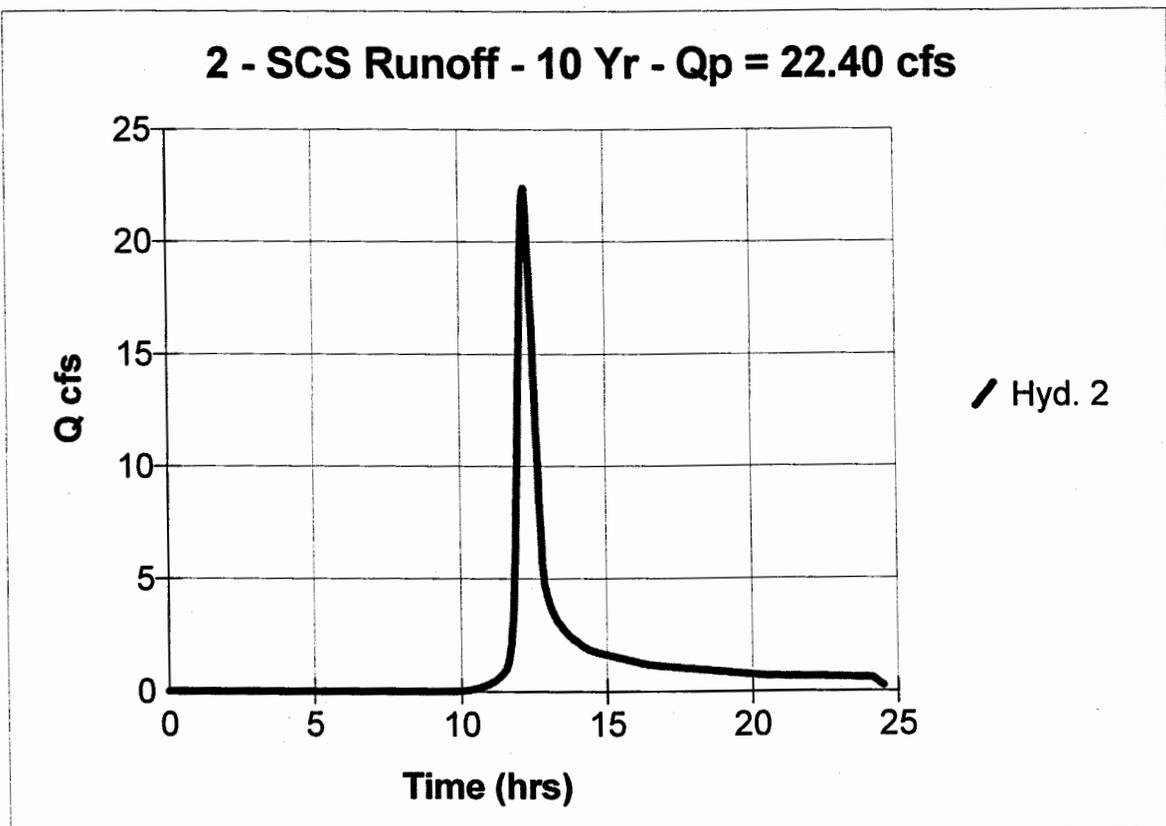
Hyd. No. 2

Pre-Development 10-yr

Hydrograph type = SCS Runoff
Storm frequency = 10 yrs
Drainage area = 12.20 ac
Basin Slope = 5.0 %
Tc method = USER
Total precip. = 5.80 in
Storm duration = 24 hrs

Peak discharge = 22.40 cfs
Time interval = 2 min
Curve number = 67
Hydraulic length = 1580 ft
Time of conc. (Tc) = 37 min
Distribution = Type II
Shape factor = 484

Total Volume = 104,210 cuft



Hydrograph Plot

English

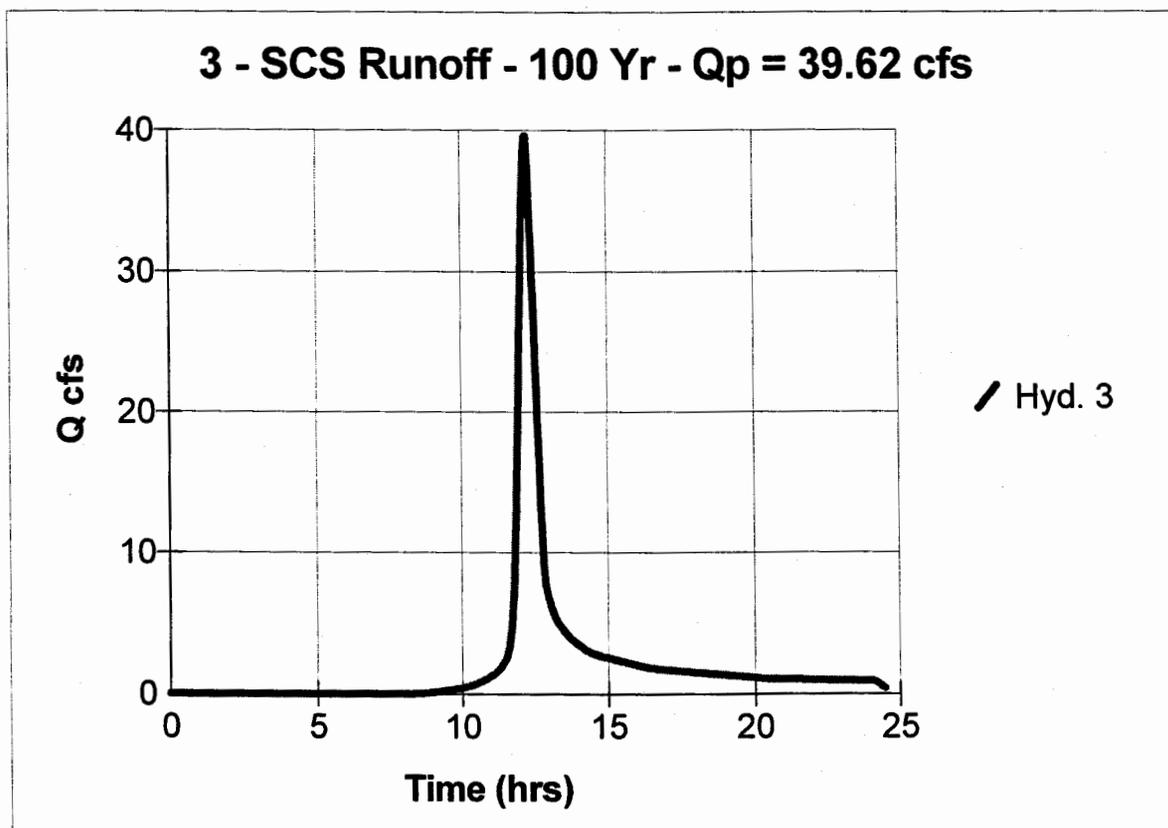
Hyd. No. 3

Pre-Development 100-yr

Hydrograph type = SCS Runoff
Storm frequency = 100 yrs
Drainage area = 12.20 ac
Basin Slope = 5.0 %
Tc method = USER
Total precip. = 8.00 in
Storm duration = 24 hrs

Peak discharge = 39.62 cfs
Time interval = 2 min
Curve number = 67
Hydraulic length = 1580 ft
Time of conc. (Tc) = 37 min
Distribution = Type II
Shape factor = 484

Total Volume = 180,440 cuft



SCS HYDROGRAPH GENERATION
for
STONEHOUSE Ph1, Bent Tree (Sect. V-B) Ph 3
AES Project No.: 8878-00
June 14, 2001

POST-DEVELOPMENT CONDITIONS TO POINT OF CONCERN (for total site)

- A. Post-Development Drainage Area to Point of Concern = 11.1 Acres
- B. Post-development Land Use, Soil Classification and Calculation of Composite Curve Number

	Soil Type	Hydrologic Group Appendix 4A*	Land Use	Area Acres	CN Table 4-6*	Adjusted CN
1)	10-B Craven Fine Sandy Loam	C	Residential - 1/2 acre lots	1.5	80	119
2)	10-B Craven Fine Sandy Loam	C	Open Space/Wooded	0.2	76	18
3)	10-B Craven Fine Sandy Loam	C	Right-of-Way	0.1	92	5
4)	11-C Craven-Uchee	C	Residential - 1/2 acre lots	2.8	80	223
5)	11-C Craven-Uchee	C	Right-of-Way	0.7	92	65
6)	14-B Emporia Fine Sandy Loam	C	Residential - 1/2 acre lots	0.5	80	39
7)	14-B Emporia Fine Sandy Loam	C	Right-of-Way	0.2	92	17
8)	15-F Emporia Complex	C	Residential - 1/2 acre lots	1.7	80	133
10)	15-F Emporia Complex	C	Open Space/Wooded	0.9	76	69
11)	15-F Emporia Complex	C	BMP Surface	0.4	100	36
12)	19-B Kempsville-Emporia Fine Sandy Loam	B	Residential - 1/2 acre lots	1.7	60	100
13)	19-B Kempsville-Emporia Fine Sandy Loam	B	Right-of-Way	0.5	89	45
Total Adjusted CN =				11.1		824
Composite CN =						75

C. Post-Development Time of Concentration Calculations

1) Overland Flow

Surface description	Dense Grass
Manning's roughness coefficient, n (Table 4-9a*)	0.24
Length of overland flow, L	200 Feet
2-year 24-hour rainfall, P2 (Appendix 4B*)	3.5 inches
Average slope of overland flow, s	0.030 feet per foot
Travel time, $T_t = (0.007 \cdot (n \cdot L)^{0.8}) / (P_2^{0.5} \cdot s^{0.4})$	0.34 hours

2) Shallow concentrated flow

Surface description, paved or unpaved	unpaved
Length of shallow concentrated flow, L	200 Feet
Average slope of shallow concentrated flow, s	0.02 feet per foot
Average velocity, v	1.00 feet per second
Travel time, $T_t = L / (3600 \cdot v)$	0.06 hours

3) Channel or Pipe Flow

Length of channel flow, L	655 Feet
Average velocity of channel flow, v	3 feet per second
Travel time, $T_t = L / (3600 \cdot v)$	0.06 hours

Total Time of Concentration = 0.45 hours
or 27 minutes

*Va. SWM Handbook (DCR, DSWC)

Hydrograph Plot

English

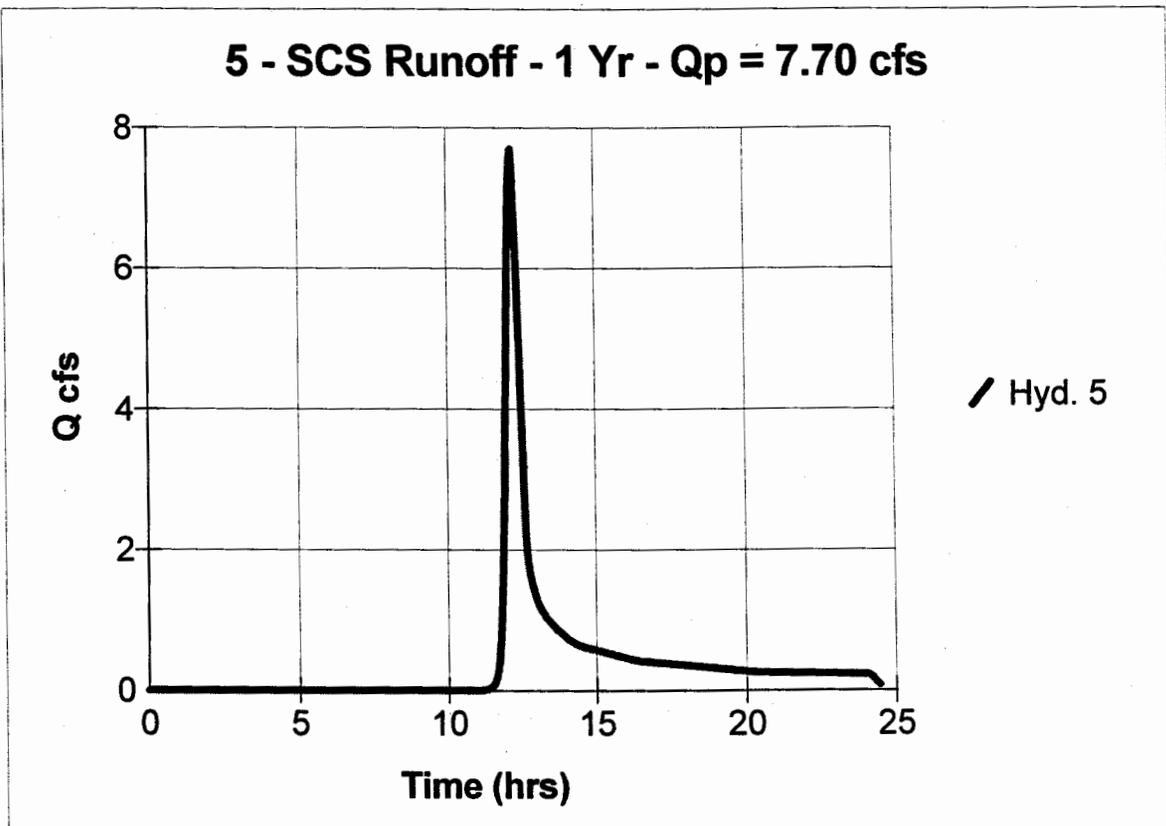
Hyd. No. 5

Post-Development 1-yr

Hydrograph type = SCS Runoff
Storm frequency = 1 yrs
Drainage area = 11.10 ac
Basin Slope = 6.0 %
Tc method = USER
Total precip. = 2.80 in
Storm duration = 24 hrs

Peak discharge = 7.70 cfs
Time interval = 2 min
Curve number = 75
Hydraulic length = 1055 ft
Time of conc. (Tc) = 27 min
Distribution = Type II
Shape factor = 484

Total Volume = 33,545 cuft ✓



Hydrograph Plot

English

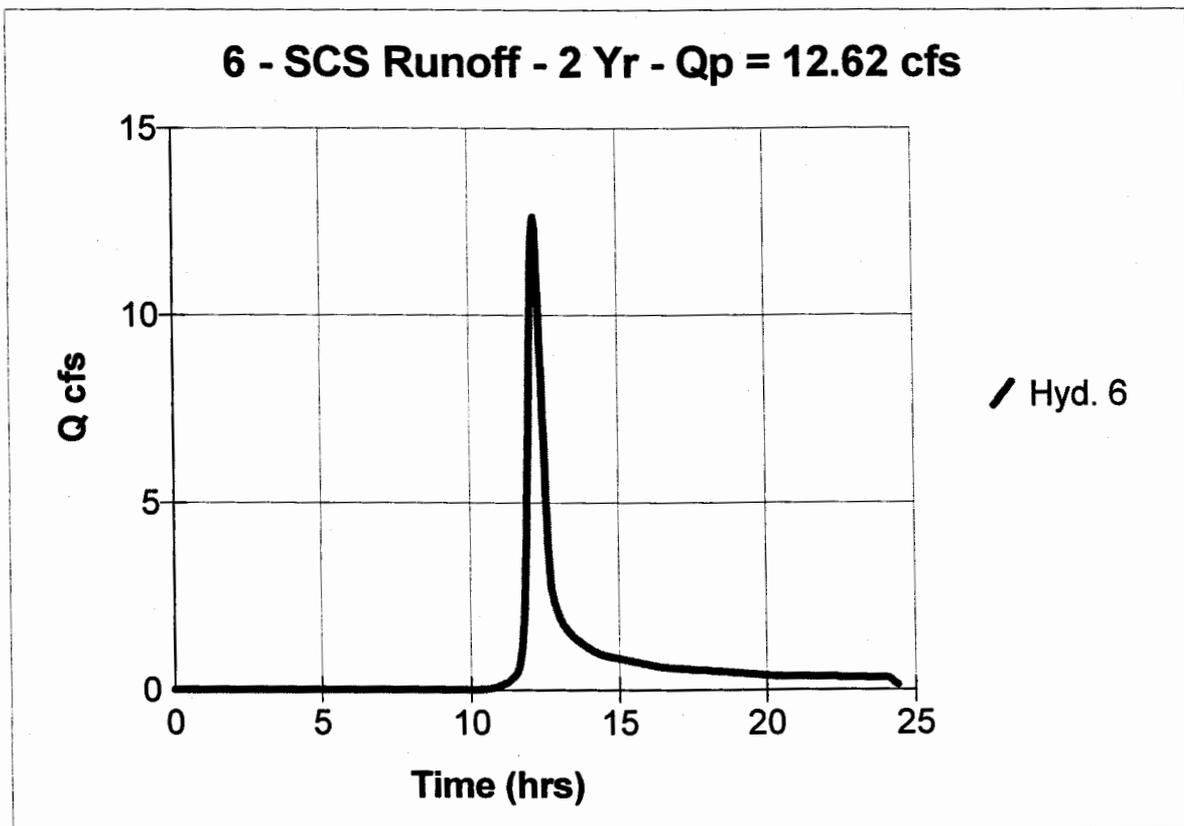
Hyd. No. 6

Post-Development 2-yr

Hydrograph type = SCS Runoff
Storm frequency = 2 yrs
Drainage area = 11.10 ac
Basin Slope = 6.0 %
Tc method = USER
Total precip. = 3.50 in
Storm duration = 24 hrs

Peak discharge = 12.62 cfs
Time interval = 2 min
Curve number = 75
Hydraulic length = 1055 ft
Time of conc. (Tc) = 27 min
Distribution = Type II
Shape factor = 484

Total Volume = 52,453 cuft



Hydrograph Plot

English

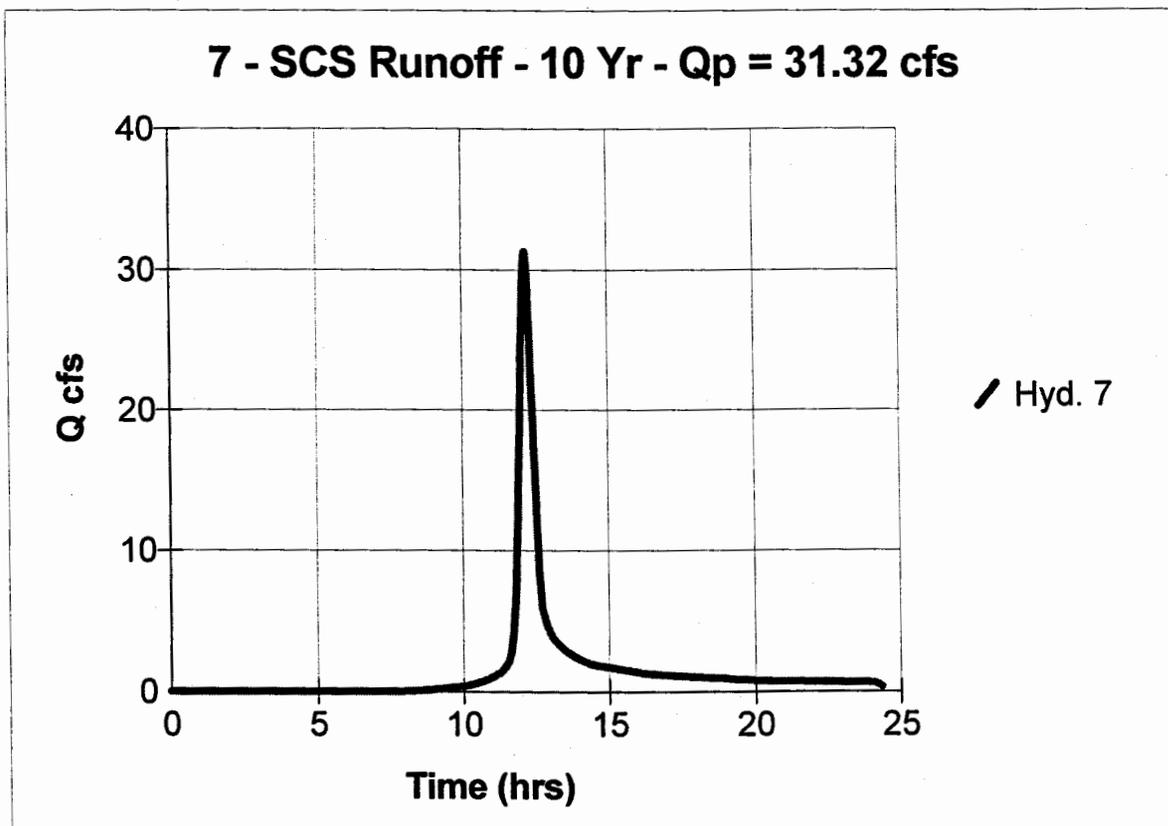
Hyd. No. 7

Post-Development 10-yr

Hydrograph type = SCS Runoff
Storm frequency = 10 yrs
Drainage area = 11.10 ac
Basin Slope = 6.0 %
Tc method = USER
Total precip. = 5.80 in
Storm duration = 24 hrs

Peak discharge = 31.32 cfs
Time interval = 2 min
Curve number = 75
Hydraulic length = 1055 ft
Time of conc. (Tc) = 27 min
Distribution = Type II
Shape factor = 484

Total Volume = 125,405 cuft



Hydrograph Plot

English

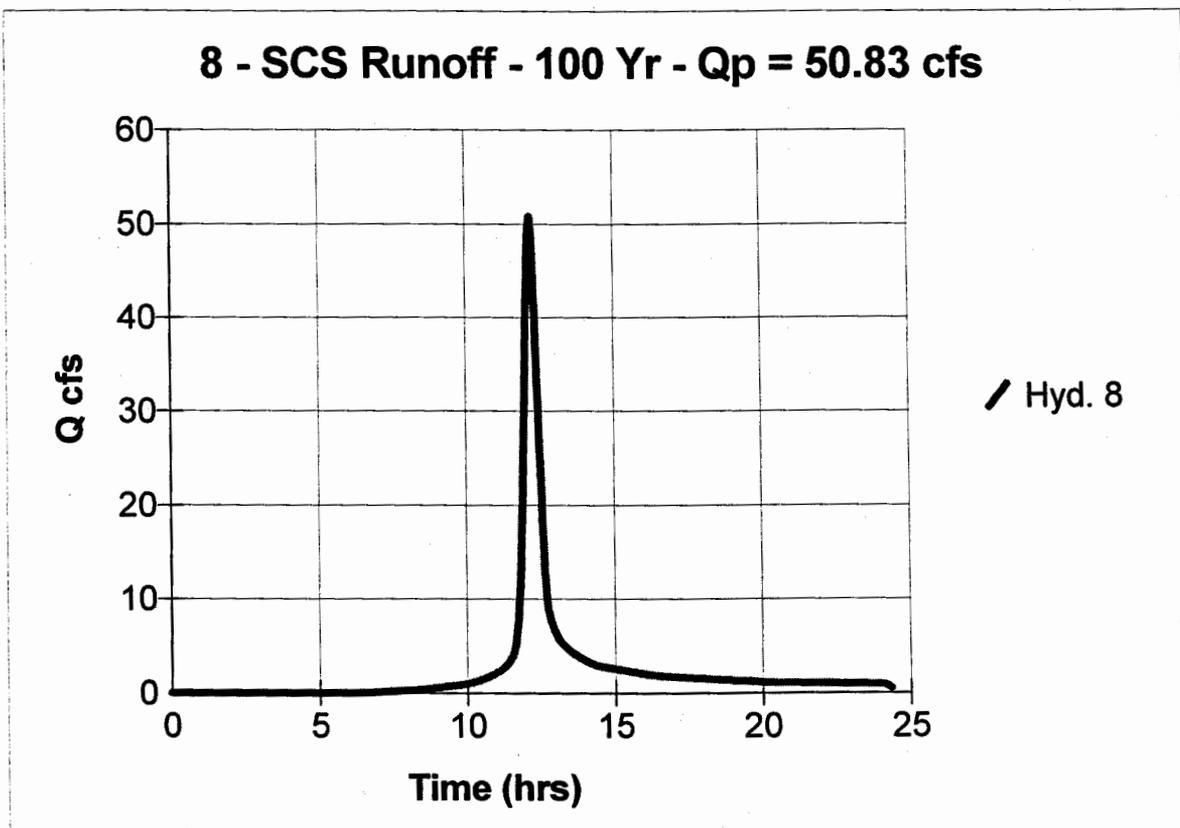
Hyd. No. 8

Post-Development 100-yr

Hydrograph type = SCS Runoff
Storm frequency = 100 yrs
Drainage area = 11.10 ac
Basin Slope = 6.0 %
Tc method = USER
Total precip. = 8.00 in
Storm duration = 24 hrs

Peak discharge = 50.83 cfs
Time interval = 2 min
Curve number = 75
Hydraulic length = 1055 ft
Time of conc. (Tc) = 27 min
Distribution = Type II
Shape factor = 484

Total Volume = 203,144 cuft



BMP Calcs-8878-00 Stonehouse Bent Tree Phase III

Impervious items	Totals		Acres
Houses	18 Ea	2000 SF	0.83
Driveways	20 Ea	600 SF	0.28
Roads:			
Sapling	438.2 LF	22 Width	0.22
Windy Branch	845.3 LF	18 Width	0.35
Sapling common driveway	166.6 LF	16 Width	0.06
Pond Access Rd	50 LF	12 Width	0.01
Sidewalks:			
At Windy Branch	317.64 LF	6 Width	0.04
Wet Pond Surface @ N.P.	135 LF	100 Width	<u>0.31</u>
Total Impervious Area (TIA)			2.10

~~Wet Pond's Required Volume = (1")(ft/12")(TIA Ac)(43560 sf/Ac) = 7,627 s.f. N/A~~

Dry Pond's Required Volume = (1")(ft/12")(TIA Ac)(43560 sf/Ac) = 7,627 s.f. ✓

Sediment Forebay's Required Volume = (0.1")(ft/12")(TIA Ac)(43560 sf/Ac) = 763 s.f.

BMP VOLUME CALCULATIONS
for
STONEHOUSE Ph 1, Bent Tree (Sect. V-B) Ph3
AES Project No.: 8878-00

PROPOSED POND VOLUME

Eleva	Depth	Area (sq. ft.)	Incremental Volume (cu. ft.)	Sum Volume (cu. ft.)	Sum Volume (cu. yd.)	Volume Above NPE
34.5	0.0	0	0	0	0	
36.0	1.5	809	607	607	22	
38.0	2.0	2,568	3,377	3,984	148	
40.0	2.0	5,150	7,718	11,702	433	
42.0	2.0	8,390	13,540	25,242	935	
43.0	1.0	10,240	9,315	34,557	1,280	
44.0	1.0	12,172	11,206	45,763	1,695	
46.0	2.0	15,416	27,588	73,351	2,717	
46.0	0.0	15,146	0	73,351	2,717	
46.0	0.0	15,146	0	73,351	2,717	

RELEASE RATE REQUIRED TO DETAINED VOLUME FOR 24 HOURS

Required BMP Volume (based upon Impervious Area) = 7,627 cubic feet

Elevation of water surface associated with required volume = 39.5

Elevation of Low Flow Orifice = 34.5

Average Head, in feet = 2.5

Average Release Rate Calculation = $\frac{7,627 \text{ cubic feet}}{(24 \text{ hours} \times 60 \text{ minutes/hour} \times 60 \text{ seconds/minute})}$ = 0.1 cfs

WBN

LOW FLOW ORIFICE DIAMETER REQUIRED TO MAINTAIN AVERAGE RELEASE RATE

$$\text{Diameter of Low Flow Orifice} = 2 * (Q / ((64.32 * (h / 2))^{(1/2)} * 0.6 * 3.14))^{(1/2)}$$

where, Q equals average release rate (cfs), h equals average head (feet)

Diameter of Low Flow Orifice = 0.10 feet, or 2 inches

4" used.

SEDIMENT FOREBAY
for
Stonehouse Ph1, Bent Tree (Sect. V-B) Ph3
AES Project No.: 8878-0

DRAINAGE AREA TO POINT OF CONCERN 11.10 Acres

IMPERVIOUS AREA TO POINT OF CONCERN 2.10 Acres

STORAGE REQUIRED

A. Volume = 0.1" per Impervious Area = 762 cf

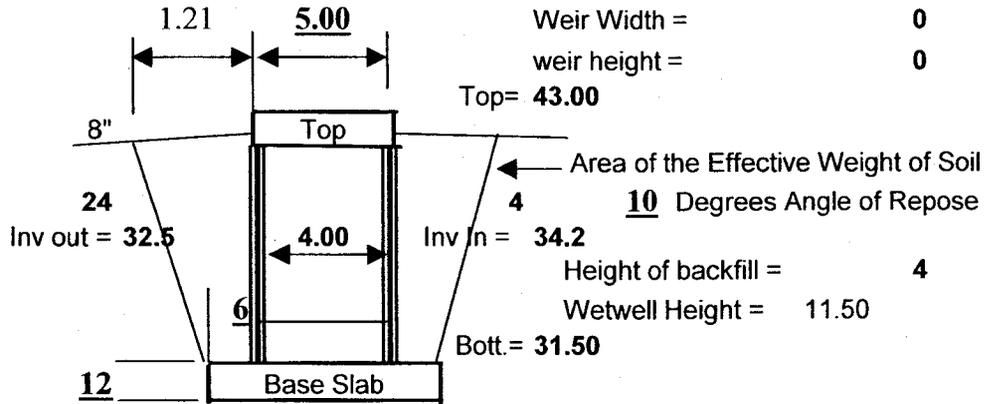
STORAGE PROVIDED

Eleva	Depth	Area (sq. ft.)	Incremental Volume (cu. ft.)	Wet Volume (cu. ft.)	Wet Volume (cu. yd.)
35.0	0.0	200	0	0	0
36.0	1.0	392	296	296	11
37.0	1.0	648	520	816	30

*Storage
BINS
pretreatment*

Buoyancy / Anti-Flotation Calculations

A. Sketch:



B. Buoyancy Calculations (Uplift)

Uplift = Wt. Water Displaced by the Wetwell

Vol. of the riser = $(O.D. / 2)^2 \times 3.14 \times \text{Height}$
 226 CF

Vol. of slab = $(\text{Dia. Slab} / 2)^2 \times 3.14 \times \text{Slab Thickness}$
 28 CF

Total Vol. of Displacement = 254 CF

Total Uplift 16354 LB ↑Up

Safety factor against uplift = 1.3

for any pond

Safety factor against uplift = 1.5

at normal pool elevation of wet ponds

Total Uplift with safety factor = 21260 LB ↑Up

C. Anti-Flotation Calculations

Down Force = Wt of riser + Wt. of Soil + Wt. of Anti-Vortex Cap

Wt. Riser = Wt. Walls + Wt. Slab + Wt. Grout - Openings - Weir

Wt. Walls =	$((O.D./2)^2 - (I.D./2)^2) \times 3.14 \times (\text{Height}) \times 150 \text{ LB/CF}$
Wt. of walls	12187 LB
Wt. Slab	Area Base Slab x Thickness x 150LB/CF
Wt. of slab	4239 LB
Wt. Grout	3485 LB
Wt. outlet opening	236 LB
Wt. of weir	0 LB
Wt. of Riser =	<u>19676</u> LB

Effective Wt. Of the Soil = Wt. Soil at the Angle of Repose - Wt. Water
 = (Vol. Above Base Slab - Vol. Riser) x (110LB - 64.4 LB)

Slab Area =	28.26 SF	
		Avg. Area =
Surface Area =	43.11 SF	35.69
Vol. above Base =	143 CF	
Vol. Riser =	64 CF	
Wt. Soil =	<u>2929</u> LB	

Wt. Anti-Vortex Cap **4270** LB

Total Down Force =	<u>26875</u> LB	↓	$(19676 + 2929 + 4270 = 26875\#)$
Total Uplift =	<u>21260</u> LB	↑	✓
Resultant Force =	<u>5615</u> LB	↓	

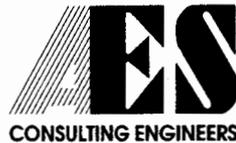
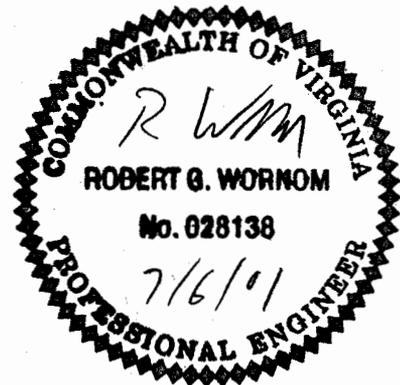
FS = 1.26

**STONEHOUSE
AREA 1, PHASE 1
BENT TREE, SECT. V-B
PHASE 3**

FOR
STONEHOUSE DEVELOPMENT COMPANY, LLC.

PROJECT NUMBER: 8878-00

DRAINAGE AND E&S CALCULATIONS



**AES CONSULTING ENGINEERS
5248 OLDE TOWNE ROAD, SUITE #1
WILLIAMSBURG, VIRGINIA 23188**

July 6, 2001

Hydraflow Storm Sewer Tabulation

Station		Len (ft)	Drng Area		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr (ac)	Total (ac)		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	
4	1	36.0	0.42	0.42	0.70	0.29	0.29	5.0	5.0	7.1	2.09	7.61	1.71	15	1.39	45.50	45.00	47.24	47.20	51.00	51.00	ss1 2-2A
3	2	36.0	0.76	0.76	0.76	0.58	0.58	5.0	5.0	7.1	4.12	7.61	3.36	15	1.39	65.00	64.50	66.24	66.10	70.00	70.00	ss1 3-4
2	1	160.0	0.42	1.18	0.83	0.35	0.93	5.0	5.2	7.1	6.55	22.54	5.71	15	12.19	64.50	45.00	65.52	47.20	70.00	51.00	ss1 2-3
1	End	128.0	0.26	1.86	0.70	0.18	1.40	5.0	5.7	6.9	9.73	17.12	11.06	15	7.03	45.00	36.00	46.18	36.69	51.00	37.25	ss1 1-2
Project File: ss1.stm								IDF File: JCCstormsewer.IDF						Total number of lines: 4				Run Date: 07-09-2001				
NOTES: Intensity = 143.72 / (Inlet time + 19.20) ^ 0.94; Return period = 10 Yrs. ; Initial tailwater elevation = 36.69 (ft)																						

Hydraflow Storm Sewer Tabulation

Station		Len (ft)	Drng Area		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr (ac)	Total (ac)		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	
1	End	100.0	3.16	3.16	0.66	2.09	2.09	5.0	5.0	7.1	14.86	24.27	16.20	15	14.13	77.63	63.50	78.87	64.22	83.63	63.25	ss2 2-1
Project File: ss2.stm									IDF File: JCCstormsewer.IDF							Total number of lines: 1			Run Date: 07-09-2001			
NOTES: Intensity = $143.72 / (\text{Inlet time} + 19.20)^{0.94}$; Return period = 10 Yrs. ; Initial tailwater elevation = 64.22 (ft)																						

Hydraflow Storm Sewer Tabulation

Station		Len (ft)	Drng Area		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr (ac)	Total (ac)		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	
2	1	34.0	0.27	0.27	0.75	0.20	0.20	5.0	5.0	7.1	1.44	7.00	2.66	15	1.18	73.30	72.90	73.78	73.61	77.70	77.80	ss3 2-3
1	End	144.0	0.09	0.36	0.80	0.07	0.27	5.0	5.5	7.0	1.92	30.87	8.76	15	22.85	72.90	40.00	73.45	40.21	77.80	43.25	ss3 1-2
Project File: ss3.stm						IDF File: JCCstormsewer.IDF						Total number of lines: 2				Run Date: 07-09-2001						
NOTES: Intensity = 143.72 / (Inlet time + 19.20) ^ 0.94; Return period = 10 Yrs. ; Initial tailwater elevation = 40.21 (ft)																						

Hydraflow Storm Sewer Tabulation

Station		Len (ft)	Drng Area		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr (ac)	Total (ac)		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	
2	1	36.0	0.20	0.20	0.82	0.16	0.16	5.0	5.0	7.1	1.17	6.81	1.50	15	1.11	56.00	55.60	56.62	56.63	60.59	61.10	ss4 2-3
1	End	169.0	0.70	0.90	0.69	0.48	0.65	5.0	5.6	7.0	4.50	26.10	10.23	15 ✓	16.33 ✓	55.60 ✓	28.00 ✓	56.45	28.36	61.10	33.25	ss4 1-2
Project File: ss4.stm									IDF File: JCCstormsewer.IDF						Total number of lines: 2				Run Date: 07-09-2001			

NOTES: Intensity = 143.72 / (Inlet time + 19.20) ^ 0.94; Return period = 10 Yrs. ; Initial tailwater elevation = 28.36 (ft)

SEDIMENT TRAP #1
for
STONEHOUSE, BENT TREE, Phase 3
AES Project No.: 8878-00

DRAINAGE AREA TO POINT OF CONCERN 1.34 Acres

STORAGE REQUIRED

- A. Wet Pond Volume = Drainage Area x 67 cy/ac = 89.78 cy
- B. Dry Pond Volume = Drainage Area x 67 cy/ac = 89.78 cy

STORAGE PROVIDED

Elev:	Depth	Area (sq. ft.)	Incremental Volume (cu. ft.)	Wet Volume (cu. ft.)	Wet Volume (cu. yd.)	Dry NPE=62.0 (cu. ft.)	Dry NPE=62.0 (cu. yd.)
38.0	0.0	850	0	0	0	0	0
40.0	2.0	1,541	2,391	2,391	89	0	0
42.0	2.0	2,524	4,065	6,456	239	4,065	151
43.5	1.5	3,506	4,523	10,979	407	8,588	318

SEDIMENT TRAP DATA

Type of Outlet (Aggregate & Rip Rap or Perforated CMP Riser):	Riser
Pond Bottom Elevation =	38.0 feet ✓
Base of Aggregate & Rip Rap (Begin Perforations) =	40.0 feet <i>40.5 ON PLAN</i>
Top of Aggregate & Rip Rap (Top of Riser Elevation) =	42.0 feet <i>42.5 ON PLAN</i>
Top of Diversion Dike =	43.5 feet <i>44.0 ON PLAN</i>
Length of Aggr. & Rip Rap (Diameter of Riser) = 6 x Drain. Area (6' min.) =	3.0 feet <i>8.04'</i>
Height of Aggregate & Rip Rap (Riser Top - Orifice Invert) =	2.0 feet
Diversion Dike Height = Top of D.D. - Base of Aggregate (Begin Perforatio	3.5 feet

SEDIMENT TRAP #2
Aggregate & Rip Rap Type Outlet
STONEHOUSE, BENT TREE, Phase 3
AES Project No.: 8878-00

DRAINAGE AREA TO POINT OF CONCERN 0.98 Acres

STORAGE REQUIRED

- A. Wet Pond Volume = Drainage Area x 67 cy/ac = 65.66 cy (not provided) *WHY?*
B. Dry Pond Volume = Drainage Area x 67 cy/ac = 65.66 cy

STORAGE PROVIDED

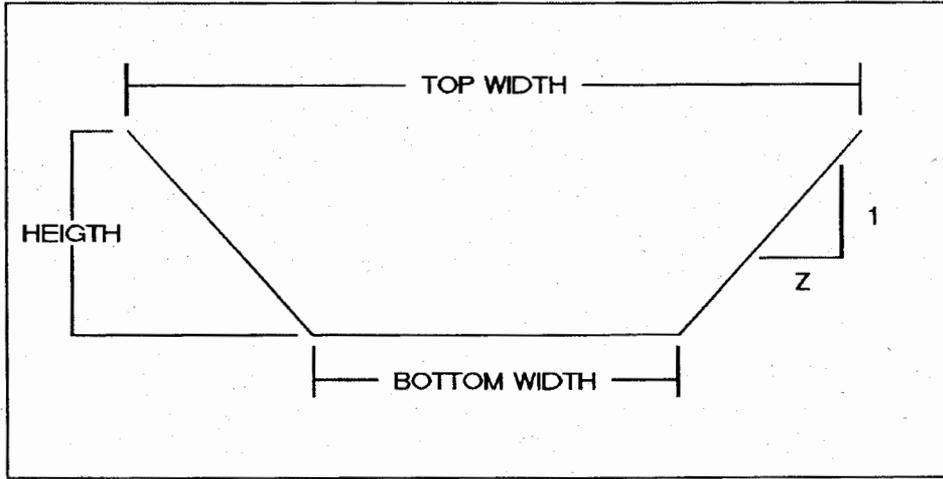
Eleva	Depth	Area (sq. ft.)	Incremental Volume (cu. ft.)	Wet Volume (cu. ft.)	Wet Volume (cu. yd.)	Dry NPE=51.6 (cu. ft.)	Dry NPE=51.6 (cu. yd.)
48.0	0.0	30	0	0	0	0	0
50.0	2.0	571	601	601	22	601	22
52.0	2.0	1,066	1,637	2,238	83	2,238	83

SEDIMENT TRAP DATA

- Pond Bottom Elevation = 48.0 feet ✓
Base of Aggregate & Rip Rap = 48.0 feet ✓
Top of Aggregate & Rip Rap = 52.0 feet *53.0*
Top of Diversion Dike = 53.0 feet ✓
Length of Aggr. & Rip Rap = 6 x Drain. Area = (6' min.) = 12.0 feet *6'*
Height of Aggregate & Rip Rap = 4.0 feet ✓
Top Width Aggregate & Rip Rap (Plate 3.13-1) = 4.5 feet ✓
Diversion Dike Height = Top of D.D. - Base of Aggregate = 5.0 feet ✓

Adequate Channel Analysis
 Stonehouse - Bent Tree Phase 3
 June 4, 2001
 Project No. 8878-0

CHANNEL GEOMETRY



BOTTOM WIDTH =	15 FT
HEIGHT =	5 FT
Z =	1.5 FT
SLOPE (S)	0.05 FT/FT
MANNING'S N	0.18

CALCULATION OF CHANNEL CAPACITY AND VELOCITY

MANNING'S EQUATION

$$V = 1.49 / N * R^{2/3} * S^{1/2}$$

WHERE:

- V = AVERAGE VELOCITY
- N = MANNING'S ROUGHNESS COEF.
- R = HYDRAULIC RADIUS = A / WP
- S = SLOPE OF CHANNEL
- A = AREA OF CROSS SECTION
- WP = WETTED PERIMETER

MANNING'S ROUGHNESS COEF.

$$N = (N1 + N2 + N3 + N4 + N5) * N6 + (N1 + N2 + N3 + N4 + N5)$$

WHERE:

N1 = CHANNEL IN EARTH	0.02
N2 = EROSION	0.01
N3 = SIZE/SHAPE OF CHANN	0.005
N4 = OBSTRUCTIONS	0.05
N5 = VEGETATION	0.075
N6 = MEANDER	0.15 <i>SE</i>

$$N = 0.18$$

SOIL TYPE

SANDY LOAM

MAX. PERMISSIBLE VELOCITY = 2.5 FT /SEC

2-YEAR STORM EVENT

TIME OF CONCENTRATION	5.6 MIN.	
RAINFALL INTENSITY =	1.8	
RUNOFF COEF. =	0.82	
DRAINAGE AREA =	<u>0.7 AC.</u>	<i>0.90 AC PER SSSCOMPS.</i>
PEAK FLOW RATE =	3.44 CFS	(SEE HYDROGRAPH)
PEAK VELOCITY =	0.76 CFS	(SEE FOLLOWING PAGE)

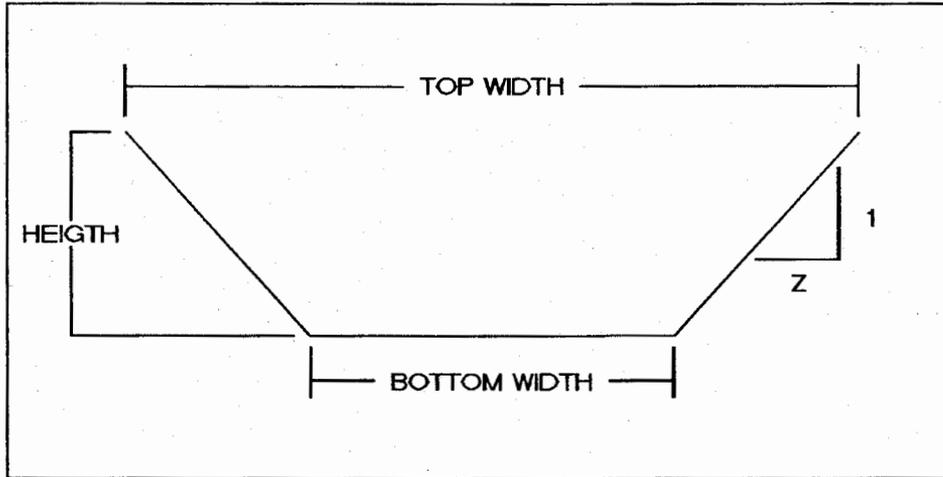
* **VELOCITY FOR POST DEVELOPMENT 2-YEAR STORM IS LESS THAN MAXIMUM PERMISSIBLE VELOCITY OF 2.37 CFS THEREFORE, CHANNEL IS ADEQUATE.**

<u>Incremental</u> <u>Depth</u> (FT)	<u>Area</u> (SQ FT)	<u>WP</u> (FT)	<u>Hydraulic</u> <u>Radius</u> (FT)	<u>Velocity</u> (FT/SEC)	<u>Flow</u> (CFS)
0.00	0.00	15.00	0.00	0.00	0.00
0.10	0.02	15.36	0.00	0.02	0.00
0.20	0.18	15.72	0.01	0.09	0.02
0.30	0.61	16.08	0.04	0.21	0.13
0.40	1.44	16.44	0.09	0.37	0.53
0.50	2.81	16.80	0.17	0.56	1.58
0.59	4.52	17.11	0.26	0.76	3.44
0.70	7.72	17.52	0.44	1.07	8.27

←-----

Adequate Channel Analysis
 Stonehouse - Bent Tree Phase 3
 June 4, 2001
 Project No. 8878-0

CHANNEL GEOMETRY



BOTTOM WIDTH =	5 FT
HEIGHT =	5 FT
Z =	1.8 FT
SLOPE (S)	0.1 FT/FT
MANNING'S N	0.18

CALCULATION OF CHANNEL CAPACITY AND VELOCITY

MANNING'S EQUATION

$$V = 1.49 / N * R^{2/3} * S^{1/2}$$

WHERE:

- V = AVERAGE VELOCITY
- N = MANNING'S ROUGHNESS COEF.
- R = HYDRAULIC RADIUS = A / WP
- S = SLOPE OF CHANNEL
- A = AREA OF CROSS SECTION
- WP = WETTED PERIMETER

MANNING'S ROUGHNESS COEF.

$$N = (N1 + N2 + N3 + N4 + N5) * N6 + (N1 + N2 + N3 + N4 + N5)$$

WHERE:

N1 = CHANNEL IN EARTH	0.02
N2 = EROSION	0.01
N3 = SIZE/SHAPE OF CHANN	0.005
N4 = OBSTRUCTIONS	0.05
N5 = VEGETATION	0.075
N6 = MEANDER	0.15 <i>msd.</i>

$$N = 0.18$$

SOIL TYPE

SANDY LOAM

MAX. PERMISSIBLE VELOCITY =

2.5 FT / SEC

2-YEAR STORM EVENT

TIME OF CONCENTRATION	5 MIN.
RAINFALL INTENSITY =	1.8
RUNOFF COEF. =	0.66 ✓
DRAINAGE AREA =	3.16 AC. ✓

PEAK FLOW RATE = 11.53 CFS (SEE HYDROGRAPH)

PEAK VELOCITY = 2.01 CFS (SEE FOLLOWING PAGE) ✓

*** VELOCITY FOR POST DEVELOPMENT 2-YEAR STORM IS LESS THAN MAXIMUM PERMISSIBLE VELOCITY OF 2.37 CFS THEREFORE, CHANNEL IS ADEQUATE.**

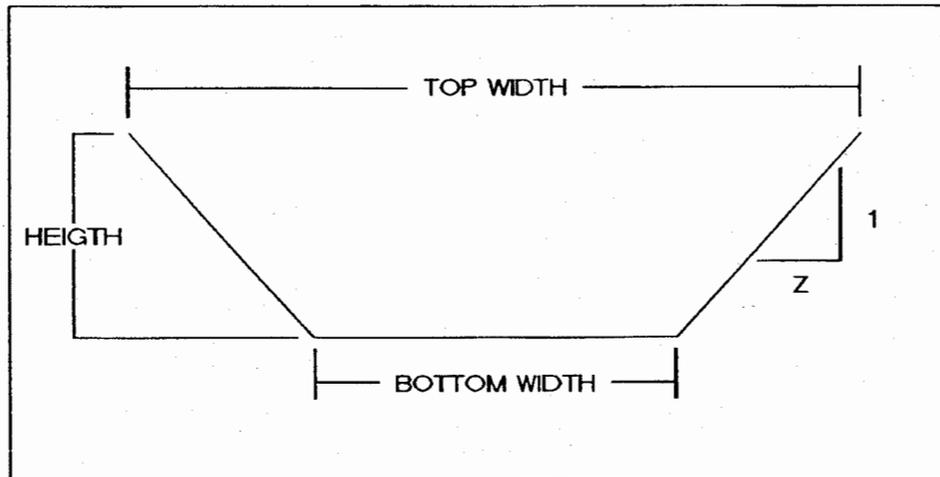
<u>Incremental Depth</u> (FT)	<u>Area</u> (SQ FT)	<u>WP</u> (FT)	<u>Hydraulic Radius</u> (FT)	<u>Velocity</u> (FT/SEC)	<u>Flow</u> (CFS)
0.00	0.00	5.00	0.00	0.00	0.00
0.10	0.01	5.41	0.00	0.04	0.00
0.20	0.07	5.82	0.01	0.14	0.01
0.30	0.24	6.24	0.04	0.30	0.07
0.40	0.58	6.65	0.09	0.51	0.30
0.50	1.13	7.06	0.16	0.77	0.87
0.60	1.94	7.47	0.26	1.07	2.07
0.70	3.09	7.88	0.39	1.40	4.33
0.80	4.61	8.29	0.56	1.77	8.15
0.86	5.74	8.55	0.67	2.01	11.53
1.00	9.00	9.12	0.99	2.59	23.35
1.10	11.98	9.53	1.26	3.05	36.52
1.20	15.55	9.94	1.56	3.53	54.86

←-----

Outfall of 30" culvert
by pump station on
Splitwood Rd. to
Downstream BMP

Adequate Channel Analysis
Stonehouse - Bent Tree Phase 3
June 4, 2001
Project No. 8878-0

CHANNEL GEOMETRY



BOTTOM WIDTH =	20 FT
HEIGHT =	8 FT
Z =	4.0 FT
SLOPE (S)	0.03 FT/FT
MANNING'S N	0.18

CALCULATION OF CHANNEL CAPACITY AND VELOCITY

MANNING'S EQUATION

$$V = 1.49 / N * R^{2/3} * S^{1/2}$$

WHERE:

- V = AVERAGE VELOCITY
- N = MANNING'S ROUGHNESS COEF.
- R = HYDRAULIC RADIUS = A / WP
- S = SLOPE OF CHANNEL
- A = AREA OF CROSS SECTION
- WP = WETTED PERIMETER

MANNING'S ROUGHNESS COEF.

$$N = (N1 + N2 + N3 + N4 + N5) * N6 + (N1 + N2 + N3 + N4 + N5)$$

WHERE:

N1 = CHANNEL IN EARTH	0.02	✓
N2 = EROSION	0.01	✓
N3 = SIZE/SHAPE OF CHANN	0.005	✓
N4 = OBSTRUCTIONS	0.05	✓
N5 = VEGETATION	0.075	
N6 = MEANDER	0.15	

$$N = 0.18$$

SOIL TYPE

SANDY LOAM

MAX. PERMISSIBLE VELOCITY =

2.5 FT / SEC

2-YEAR STORM EVENT

TIME OF CONCENTRATION	53 MIN.
RAINFALL INTENSITY =	1.8
RUNOFF COEF. =	0.37
DRAINAGE AREA =	15.57 AC.

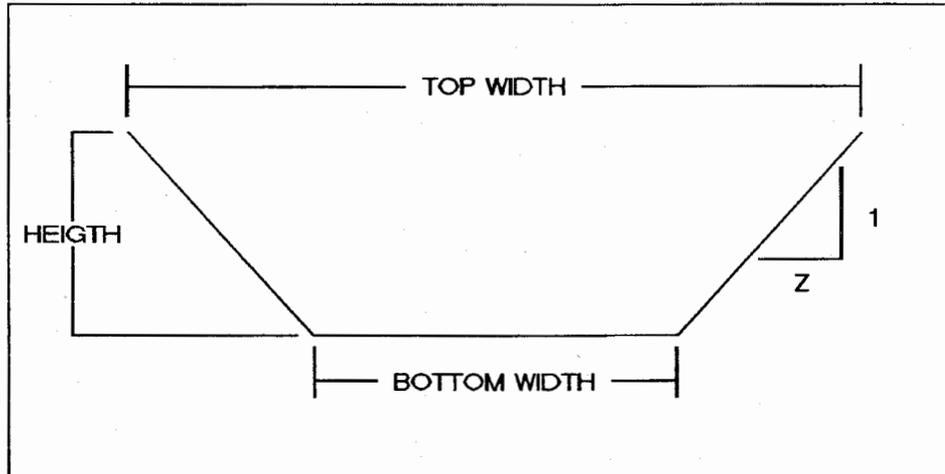
PEAK FLOW RATE =	8.04 CFS	(SEE HYDROGRAPH)
PEAK VELOCITY =	0.8 CFS	(SEE FOLLOWING PAGE)

* **VELOCITY FOR POST DEVELOPMENT 2-YEAR STORM IS LESS THAN MAXIMUM PERMISSIBLE VELOCITY OF 2.37 CFS THEREFORE, CHANNEL IS ADEQUATE.**

<u>Incremental</u> <u>Depth</u> (FT)	<u>Area</u> (SQ FT)	<u>WP</u> (FT)	<u>Hydraulic</u> <u>Radius</u> (FT)	<u>Velocity</u> (FT/SEC)	<u>Flow</u> (CFS)
0.00	0.00	20.00	0.00	0.00	0.00
0.10	0.08	20.82	0.00	0.04	0.00
0.20	0.64	21.65	0.03	0.14	0.09
0.30	2.16	22.47	0.10	0.30	0.65
0.40	5.12	23.30	0.22	0.52	2.67
0.50	10.00	24.12	0.41	0.80	7.97
0.50	10.05	24.13	0.42	0.80	8.04
0.70	27.44	25.77	1.06	1.49	41.02
0.80	40.96	26.60	1.54	1.91	78.32
0.86	51.04	27.10	1.88	2.19	111.60
1.00	80.00	28.25	2.83	2.87	229.61
1.10	106.48	29.07	3.66	3.41	362.76
1.20	138.24	29.90	4.62	3.98	550.12

Adequate Channel Analysis
Stonehouse - Bent Tree Phase 3
June 4, 2001
Project No. 8878-0

CHANNEL GEOMETRY



BOTTOM WIDTH =	25 FT
HEIGHT =	6 FT
Z =	5.0 FT
SLOPE (S)	0.036 FT/FT
MANNING'S N	0.18

CALCULATION OF CHANNEL CAPACITY AND VELOCITY

MANNING'S EQUATION

$$V = 1.49 / N * R^{2/3} * S^{1/2}$$

WHERE:

- V = AVERAGE VELOCITY
- N = MANNING'S ROUGHNESS COEF.
- R = HYDRAULIC RADIUS = A / WP
- S = SLOPE OF CHANNEL
- A = AREA OF CROSS SECTION
- WP = WETTED PERIMETER

MANNING'S ROUGHNESS COEF.

$$N = (N1 + N2 + N3 + N4 + N5) * N6 + (N1 + N2 + N3 + N4 + N5)$$

WHERE:

N1 = CHANNEL IN EARTH	0.02
N2 = EROSION	0.01
N3 = SIZE/SHAPE OF CHANN	0.005
N4 = OBSTRUCTIONS	0.05
N5 = VEGETATION	0.075
N6 = MEANDER	0.15

$$N = 0.18$$

SOIL TYPE

SANDY LOAM

MAX. PERMISSIBLE VELOCITY = 2.5 FT / SEC

2-YEAR STORM EVENT

TIME OF CONCENTRATION	53 MIN.
RAINFALL INTENSITY =	1.8
RUNOFF COEF. =	0.37
DRAINAGE AREA =	15.57 AC.

PEAK FLOW RATE = 13.9 CFS (SEE HYDROGRAPH)
PEAK VELOCITY = 0.96 CFS (SEE FOLLOWING PAGE)

*** VELOCITY FOR POST DEVELOPMENT 2-YEAR STORM IS LESS THAN MAXIMUM PERMISSIBLE VELOCITY OF 2.37 CFS THEREFORE, CHANNEL IS ADEQUATE.**

<u>Incremental</u> <u>Depth</u> (FT)	<u>Area</u> (SQ FT)	<u>WP</u> (FT)	<u>Hydraulic</u> <u>Radius</u> (FT)	<u>Velocity</u> (FT/SEC)	<u>Flow</u> (CFS)
0.00	0.00	25.00	0.00	0.00	0.00
0.10	0.13	26.02	0.00	0.04	0.01
0.20	1.00	27.04	0.04	0.17	0.17
0.30	3.38	28.06	0.12	0.38	1.29
0.40	8.00	29.08	0.28	0.66	5.31
0.49	14.41	29.96	0.48	0.96	13.90 ←
0.50	15.71	30.11	0.52	1.02	15.99
0.70	42.88	32.14	1.33	1.90	81.61
0.80	64.00	33.16	1.93	2.43	155.82
0.86	79.75	33.78	2.36	2.78	222.06
1.00	125.00	35.20	3.55	3.66	456.99
1.10	166.38	36.22	4.59	4.34	722.10
1.20	216.00	37.24	5.80	5.07	1095.22

Outfall
For: SS #5-1

$Q_{10} = 10.77 \text{ cfs}$
 $D = 18''$

BENT TREE III
8878
5/29/01

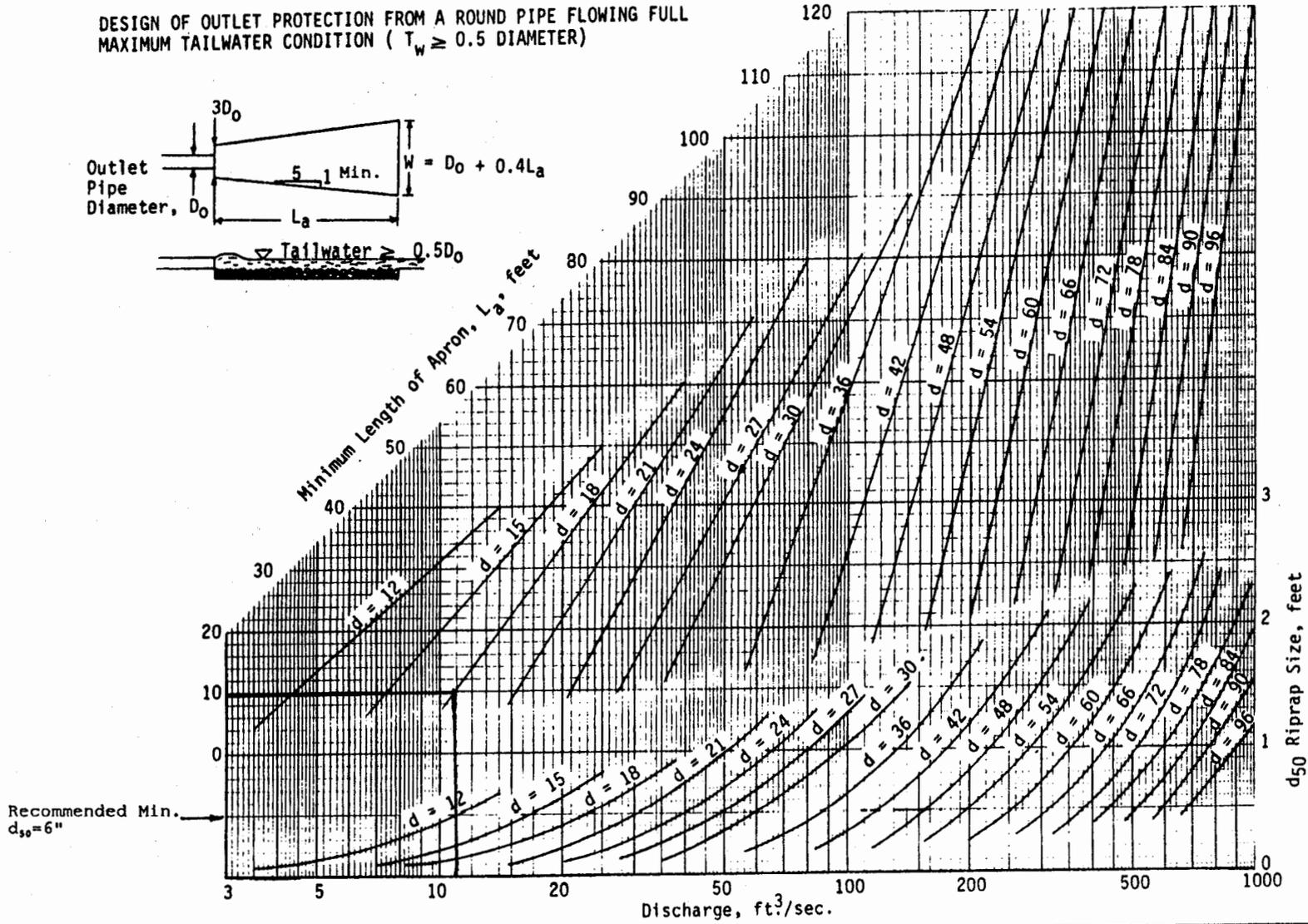
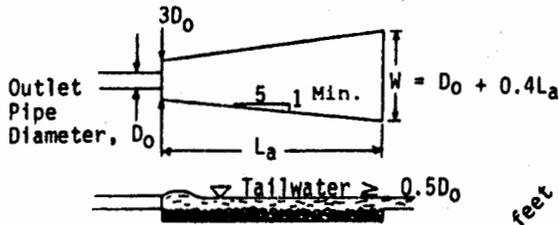
10' x 10'

Source: USDA-SCS

III - 165

Plate 3.18-4

DESIGN OF OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL
MAXIMUM TAILWATER CONDITION ($T_w \geq 0.5 \text{ DIAMETER}$)



1992

3.18

FOR SS#2-1

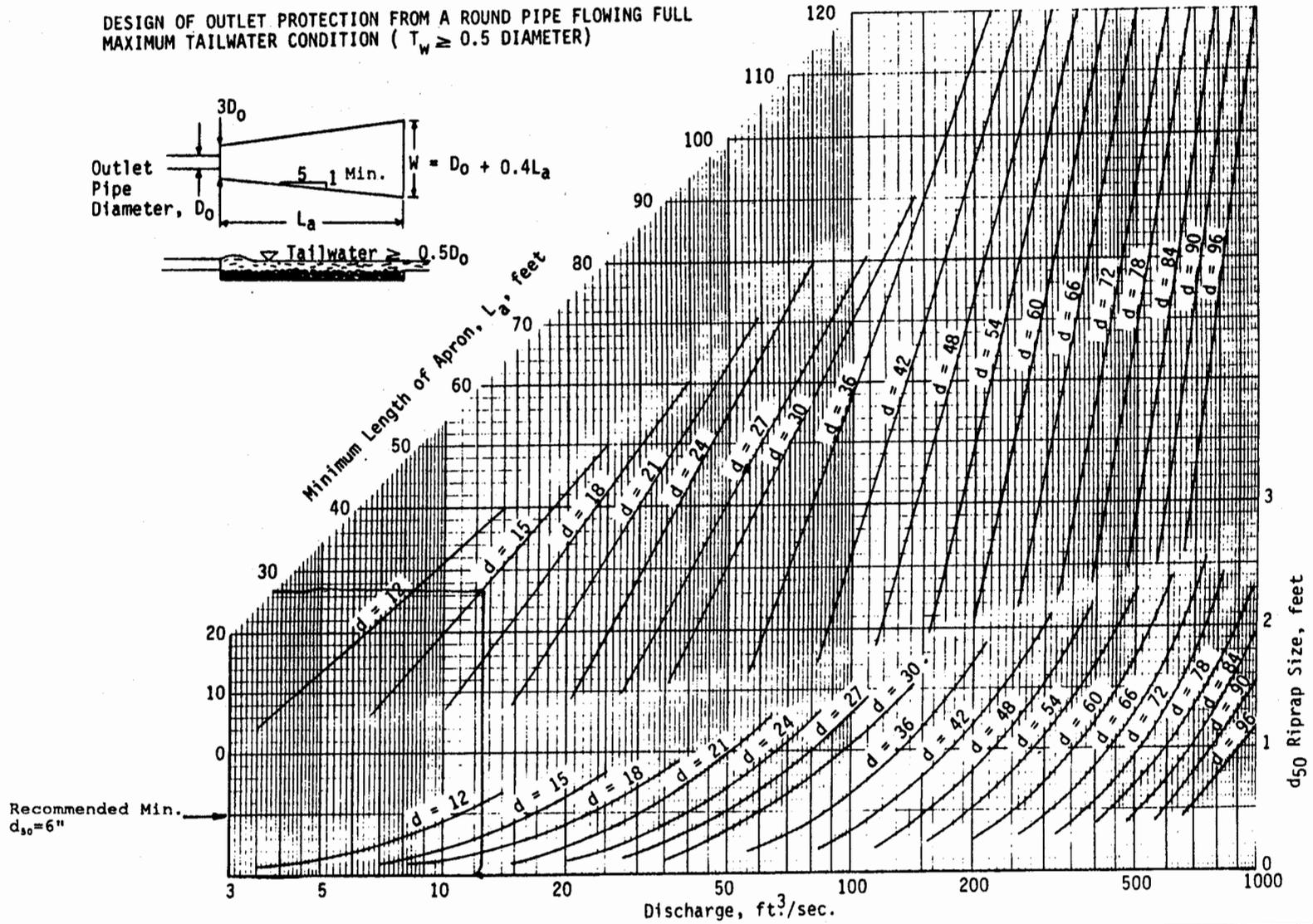
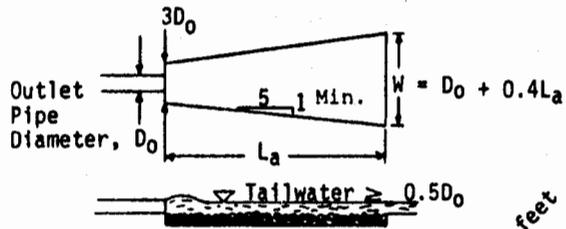
$Q_0 = 14.86 \text{ cfs}$
 $D = 15''$

BENT TREE III
8878
5/29/01

$L_a = 27'$ $W = 12'$

Source: USDA-SCS

DESIGN OF OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL
MAXIMUM TAILWATER CONDITION ($T_w \geq 0.5$ DIAMETER)



III - 165

Plate 3.18-4

1992

3.18

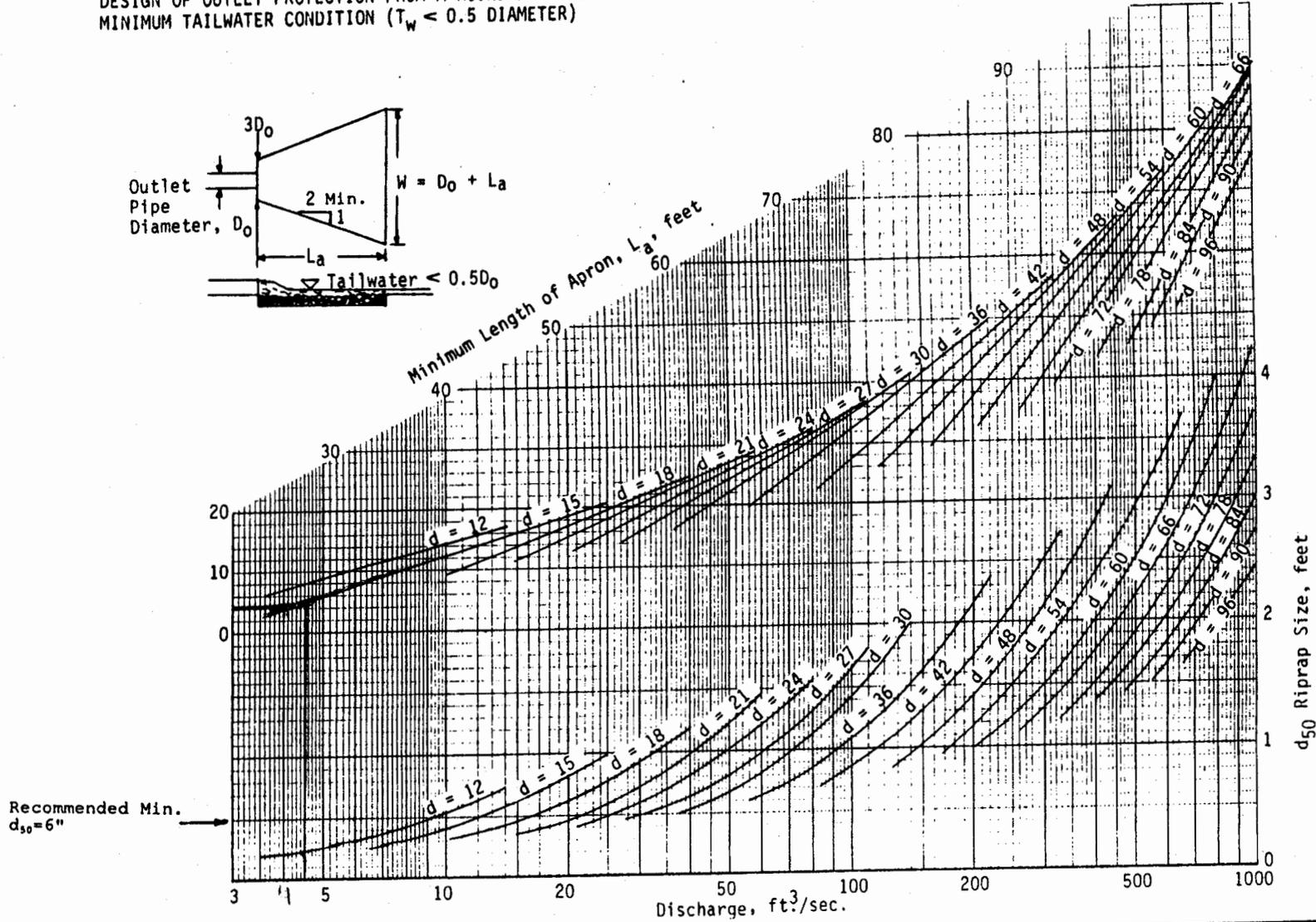
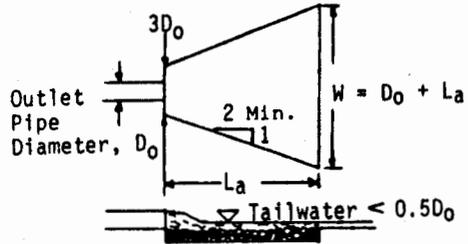
SS# 4-1

$Q_{10} = 4,500 \text{ cfs}$
 $D = 15''$

10' x 10'

Source: USDA-SCS

DESIGN OF OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL
MINIMUM TAILWATER CONDITION ($T_w < 0.5 \text{ DIAMETER}$)

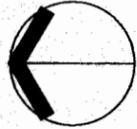
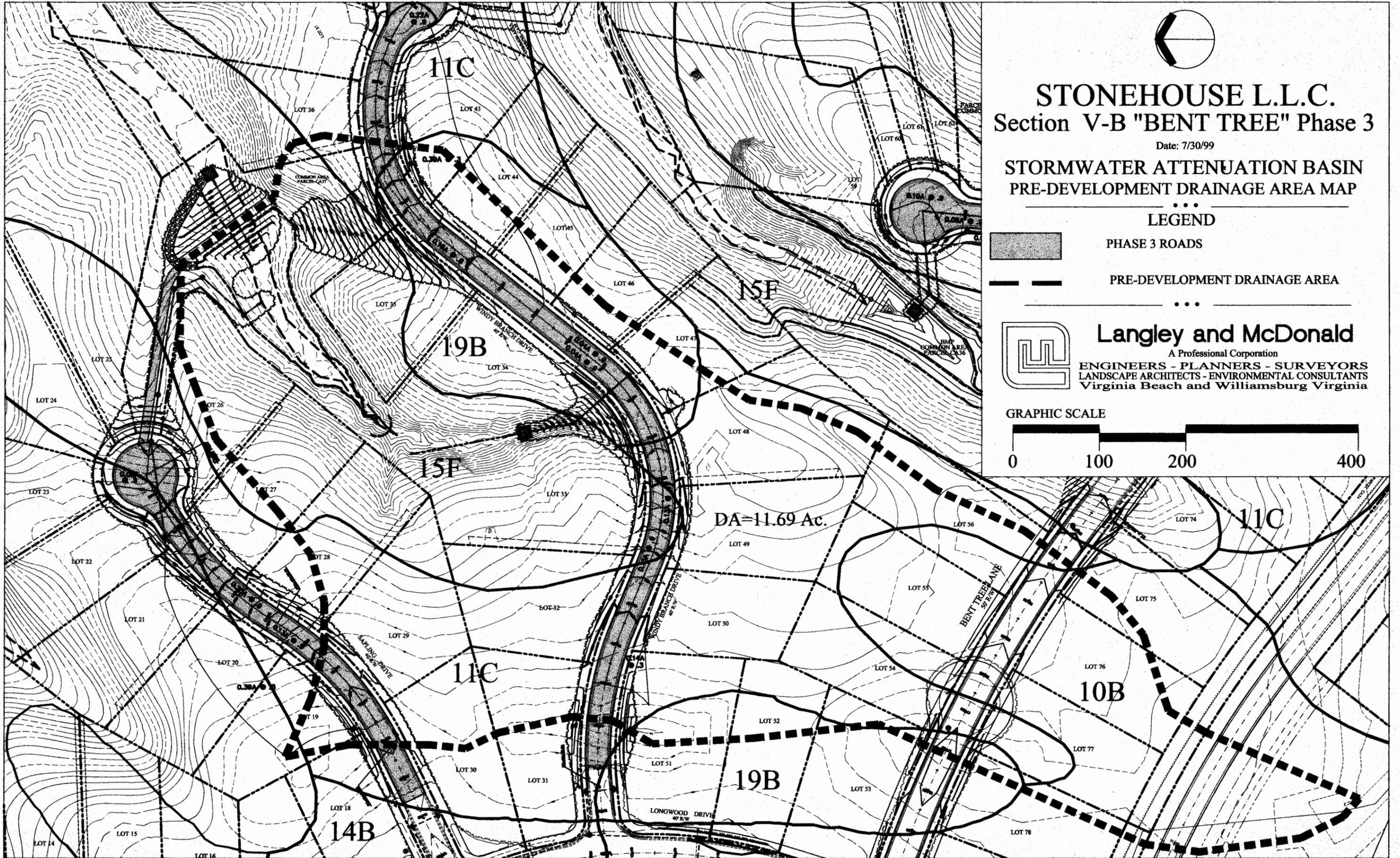


III - 164

Plate 3.18-3

1992

3.18



STONEHOUSE L.L.C.
Section V-B "BENT TREE" Phase 3

Date: 7/30/99

**STORMWATER ATTENUATION BASIN
 PRE-DEVELOPMENT DRAINAGE AREA MAP**

LEGEND

-  PHASE 3 ROADS
-  PRE-DEVELOPMENT DRAINAGE AREA



Langley and McDonald

A Professional Corporation
 ENGINEERS - PLANNERS - SURVEYORS
 LANDSCAPE ARCHITECTS - ENVIRONMENTAL CONSULTANTS
 Virginia Beach and Williamsburg Virginia

GRAPHIC SCALE



**DRAINAGE, STORMWATER MANAGEMENT,
EROSION CONTROL AND PAVEMENT DESIGN CALCULATIONS
AND
ENVIRONMENTAL INVENTORY**

STONEHOUSE L.L.C.

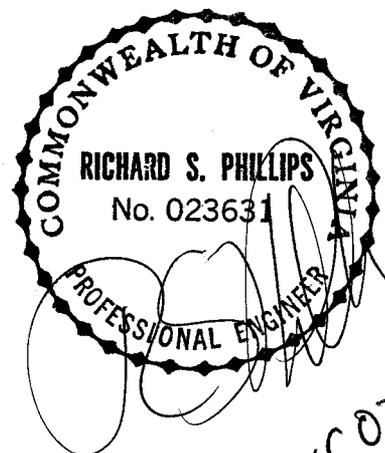
**DEVELOPMENT AREA ONE, PHASE I
SECTION VB**

“BENT TREE” – PHASE 3

Revised February 21, 2000
July 30, 1999

LMDG No. 1960038-111.73

**LANDMARK
DESIGN GROUP**



WC072
BMP 5.4

Engineers ♦ Planners ♦ Surveyors ♦ Landscape Architects ♦ Environmental Consultants
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- **BMP 5-4**
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 - SEEPAGE COLLAR CALCULATION
 - OUTFALL PROTECTION CHART

- **STORM SEWER**
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 - TEMPORARY SEDIMENT BASIN/TRAP CALCULATIONS
 - SEWER DESIGN CALCULATIONS
 - HYDRAULIC GRADELINE CALCULATIONS
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- **TRAFFIC SKETCH AND PAVEMENT CALCULATION**

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STORMWATER DESIGN PARAMETERS
STONEHOUSE DEVELOPMENT
JAMES CITY COUNTY

U.S.D.A.	S.C.S	24 HOUR RAINFALL
1 YR.		2.80 INCHES
2 YR.		3.36 INCHES
10 YR.		5.04 INCHES
100 YR.		7.68 INCHES

ROADWAY INLETS BASED ON V.D.O.T.
INTENSITY 4 INCHES PER HOUR

CHANNEL PROTECTION VOLUME CALCULATION

Project Name : Stonehouse, Section V-B, BMP 5.4

Project # : 1980036-111.73

One Year Precipitation : P= 2.8 Inches

PRE-DEVELOPMENT CONDITIONS :

Drainage Area : DA_{PRE} = 11.69 Acres
 SCS Curve Number : CN_{PRE} = 70 Unitless
 Time of Concentration : T_{CPRE} = 0.25 Hours

I _a /P	C ₀	C ₁	C ₂
0.10	2.55323	-0.61512	-0.16403
0.30	2.46532	-0.62257	-0.11657
0.35	2.41896	-0.61594	-0.08820
0.40	2.36409	-0.59857	-0.05621
0.45	2.29238	-0.57005	-0.02281
0.50	2.20282	-0.51599	-0.01259

Initial abstraction ; $I_a = 0.2 \times (1000 / CN - 10) = 0.857$ Inches
 $I_a / P = 0.31$

Accumulated direct runoff : $Q_U = (P - I_a)^2 / (P + 4 \times I_a) = 0.61$ Inches

Unit Peak Discharge : $q_u = 628$ cfs/sq.mile/in.
 $\log(q_u) = C_0 + C_1 \log(T_c) + C_2 [\log(T)]^2$
 C₀, C₁, C₂ Coefficients from TABLE F1 above

Pre-development peak discharge : $q_p = q_u \times DA \times Q_U / 640 = 6.95$ c.f.s.

POST DEVELOPMENT CONDITIONS :

Drainage Area : DA_{POST} = 11.57 Acres
 SCS Curve Number : CN_{POST} = 77 Unitless
 Time of Concentration : T_{CPOST} = 0.2 Hours

Initial abstraction ; $I_a = 0.597$ Inches
 $I_a / P = 0.21$

Accumulated direct runoff : $Q_U = 0.93$ Inches

Unit Peak Discharge : $q_u = 800$ cfs/sq.mile/in.

Post development peak discharge rate : $q_i = q_p = 13.52$ c.f.s.

Ration of outflow to inflow : * $q_o / q_i = 11.98 \times q_u^{0.937} = 0.0228$
 * Direct calculation using equation for T=24hr. developed by Stewart Comstock, P.E., MDE

Peak outflow discharge : $q_o = 0.3085$ c.f.s.

Ratio of storage volume to runoff volume : $V_s / V_r = 0.65$
 $V_s / V_r = 0.683 - 1.43(qq_i) + 1.64(q_o / q_i)^2 - 8.04(q_o / q_i)^3 =$

Required Storage Volume : $V_s = V_s / V_r \times Q_u \times A / 12 \times 43560 = 25568$ cubic feet ✓

ESTIMATED POND FULL DRAWDOWN

H_{TRIAL} = 6
 A_o = 0.026183
 d_o = 2.191011

BMP POND 5.4

DORIFICE = 2 inches

W.S.E. (feet)	AREA s.f.	INC. VOL c.f.	STORAGE c.f.	H _{AVG} ft.	Q _{AVG} cfs	dT hours
44.00	16056	28362	58915	8.00		
42.00	12306	17814	30553	6.00		
41.60	10946	13164	25903	5.80	0.2512	14.6
40.00	5508	8541	12739	4.00	0.2079	11.4
38.00	3033	4198	4198	1.50	0.1250	9.3
36.00	1165	691	691	0.50	0.0678	2.8
35.00	217	0	0	0.00		

DRAW DOWN TIME = 35.3

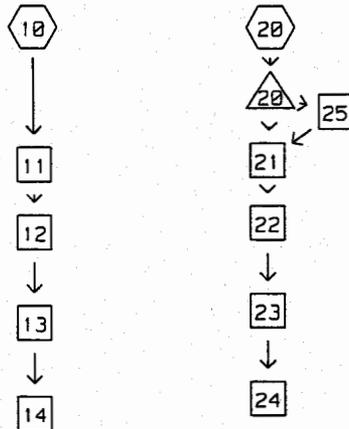
TYPE II 24-HOUR RAINFALL= 2.80 IN

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WATERSHED ROUTING =====



SUBCATCHMENT 10	= PREDEVELOPMENT DRAINAGE AREA BMP 5.4	-> REACH 11
SUBCATCHMENT 20	= POST DEVELOPMENT / PHASE 3 BMP5.4	-> POND 20
REACH 11	= WOODLAND RAVINE SECTION #1	-> REACH 12
REACH 12	= WOODLAND RAVINE SECTION #2	-> REACH 13
REACH 13	= WOODLAND RAVINE SECTION #3	-> REACH 14
REACH 14	= WOODLAND RAVINE SECTION #4	->
REACH 21	= WOODLAND RAVINE SECTION #1	-> REACH 22
REACH 22	= WOODLAND RAVINE SECTION #2	-> REACH 23
REACH 23	= WOODLAND RAVINE SECTION #3	-> REACH 24
REACH 24	= WOODLAND RAVINE SECTION #4	->
REACH 25	= EMERGENCY SPILLWAY	-> REACH 21
POND 20	= STORMWATER MANAGEMENT POND 5.4	-> REACH 21
POND 20 secondary	= STORMWATER MANAGEMENT POND 5.4	-> REACH 25

TYPE II 24-HOUR RAINFALL= 2.80 IN

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SUBCATCHMENT 10

PREDEVELOPMENT DRAINAGE AREA BMP 5.4

PEAK= 6.38 CFS @ 12.11 HRS, VOLUME= .59 AF

<u>ACRES</u>	<u>CN</u>	
11.69	70	WOODS

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 2.80 IN
 SPAN= 6-66 HRS, dt=.12 HRS

<u>Method</u>	<u>Comment</u>	<u>Tc (min)</u>
DIRECT ENTRY	PRE DEVELOPMENT WOODLAND SWALE	20.0

SUBCATCHMENT 20

POST DEVELOPMENT / PHASE 3 BMP5.4

PEAK= 12.85 CFS @ 12.02 HRS, VOLUME= .90 AF

<u>ACRES</u>	<u>CN</u>	
11.57	77	SUBDIVISION

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 2.80 IN
 SPAN= 6-66 HRS, dt=.12 HRS

<u>Method</u>	<u>Comment</u>	<u>Tc (min)</u>
DIRECT ENTRY	DEVELOPED SITE	15.0

TYPE II 24-HOUR RAINFALL= 2.80 IN

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REACH 11

WOODLAND RAVINE SECTION #1

Qin = 6.38 CFS @ 12.11 HRS, VOLUME= .59 AF
 Qout= 6.28 CFS @ 12.13 HRS, VOLUME= .59 AF, ATTEN= 2%, LAG= 1.0 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
27.80	0.0	0.00		PEAK ELEV.= 28.08 FT
28.00	.4	4.00	n= .1	PEAK VELOCITY= 2.7 FPS
30.00	50.0	46.44	LENGTH= 100 FT	TRAVEL TIME = .6 MIN
32.00	154.0	58.65	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 871.1 CFS	

REACH 12

WOODLAND RAVINE SECTION #2

Qin = 6.28 CFS @ 12.13 HRS, VOLUME= .59 AF
 Qout= 6.08 CFS @ 12.15 HRS, VOLUME= .59 AF, ATTEN= 3%, LAG= 1.4 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
24.00	0.0	0.00		PEAK ELEV.= 24.12 FT
26.00	46.0	43.20	n= .1	PEAK VELOCITY= 2.2 FPS
28.00	145.0	56.60	LENGTH= 100 FT	TRAVEL TIME = .8 MIN
30.00	227.0	72.50	SLOPE= .02 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1021 CFS	

REACH 13

WOODLAND RAVINE SECTION #3

Qin = 6.08 CFS @ 12.15 HRS, VOLUME= .59 AF
 Qout= 5.82 CFS @ 12.18 HRS, VOLUME= .59 AF, ATTEN= 4%, LAG= 1.5 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
21.80	0.0	0.00		PEAK ELEV.= 22.01 FT
22.00	5.0	47.00	n= .1	PEAK VELOCITY= 1.1 FPS
24.00	130.0	78.46	LENGTH= 100 FT	TRAVEL TIME = 1.5 MIN
26.00	298.0	90.67	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1957.8 CFS	

REACH 14

WOODLAND RAVINE SECTION #4

Qin = 5.82 CFS @ 12.18 HRS, VOLUME= .59 AF
 Qout= 5.61 CFS @ 12.22 HRS, VOLUME= .59 AF, ATTEN= 4%, LAG= 2.5 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
20.00	0.0	0.00		PEAK ELEV.= 20.07 FT
22.00	54.0	54.20	n= .1	PEAK VELOCITY= 3.0 FPS
24.00	177.0	69.58	LENGTH= 100 FT	TRAVEL TIME = .6 MIN
26.00	328.0	82.69	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 2442.7 CFS	

TYPE II 24-HOUR RAINFALL= 2.80 IN

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REACH 21 WOODLAND RAVINE SECTION #1

Q_{in} = .29 CFS @ 19.86 HRS, VOLUME= .90 AF
 Q_{out}= .29 CFS @ 19.91 HRS, VOLUME= .90 AF, ATTEN= 0%, LAG= 2.9 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
27.80	0.0	0.00		PEAK ELEV.= 28.00 FT
28.00	.4	4.00	n= .1	PEAK VELOCITY= .7 FPS
30.00	50.0	46.44	LENGTH= 100 FT	TRAVEL TIME = 2.3 MIN
32.00	154.0	58.65	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 871.1 CFS	

REACH 22 WOODLAND RAVINE SECTION #2

Q_{in} = .29 CFS @ 19.91 HRS, VOLUME= .90 AF
 Q_{out}= .29 CFS @ 19.94 HRS, VOLUME= .90 AF, ATTEN= 0%, LAG= 1.5 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
24.00	0.0	0.00		PEAK ELEV.= 24.01 FT
26.00	46.0	43.20	n= .1	PEAK VELOCITY= 2.2 FPS
28.00	145.0	56.60	LENGTH= 100 FT	TRAVEL TIME = .8 MIN
30.00	227.0	72.50	SLOPE= .02 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1021 CFS	

REACH 23 WOODLAND RAVINE SECTION #3

Q_{in} = .29 CFS @ 19.94 HRS, VOLUME= .90 AF
 Q_{out}= .29 CFS @ 20.02 HRS, VOLUME= .90 AF, ATTEN= 0%, LAG= 5.0 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
21.80	0.0	0.00		PEAK ELEV.= 21.82 FT
22.00	5.0	47.00	n= .1	PEAK VELOCITY= .7 FPS
24.00	130.0	78.46	LENGTH= 100 FT	TRAVEL TIME = 2.5 MIN
26.00	298.0	90.67	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1957.8 CFS	

REACH 24 WOODLAND RAVINE SECTION #4

Q_{in} = .29 CFS @ 20.02 HRS, VOLUME= .90 AF
 Q_{out}= .29 CFS @ 20.04 HRS, VOLUME= .90 AF, ATTEN= 0%, LAG= 1.1 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
20.00	0.0	0.00		PEAK ELEV.= 20.00 FT
22.00	54.0	54.20	n= .1	PEAK VELOCITY= 3.0 FPS
24.00	177.0	69.58	LENGTH= 100 FT	TRAVEL TIME = .6 MIN
26.00	328.0	82.69	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 2442.7 CFS	

TYPE II 24-HOUR RAINFALL= 2.80 IN

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REACH 25

EMERGENCY SPILLWAY

Qin = 0.00 CFS @ 0.00 HRS, VOLUME= 0.00 AF
Qout= 0.00 CFS @ 0.00 HRS, VOLUME= 0.00 AF, ATTEN= 0%, LAG= 0.0 MIN

DEPTH (FT)	END AREA (SQ-FT)	DISCH (CFS)	8' x 1' CHANNEL SIDE SLOPE= 3 '/' n= .03 LENGTH= 70 FT SLOPE= .1667 FT/FT	STOR-IND+TRANS METHOD PEAK DEPTH= 0.00 FT PEAK VELOCITY= 0.0 FPS TRAVEL TIME = 0.0 MIN SPAN= 6-66 HRS, dt=.12 HRS
0.00	0.00	0.00		
.10	.80	3.45		
.20	1.61	10.84		
.30	2.43	21.11		
.43	3.50	38.01		
.60	4.92	65.25		
.80	6.61	103.70		
1.00	8.33	148.18		

TYPE II 24-HOUR RAINFALL= 2.80 IN

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POND 20

STORMWATER MANAGEMENT POND 5.4

$Q_{in} = 12.85$ CFS @ 12.02 HRS, VOLUME= .90 AF
 $Q_{out} = .29$ CFS @ 19.86 HRS, VOLUME= .90 AF, ATTEN= 98%, LAG= 470.4 MIN
 $Q_{pri} = .29$ CFS @ 19.86 HRS, VOLUME= .90 AF
 $Q_{sec} = 0.00$ CFS @ 0.00 HRS, VOLUME= 0.00 AF

ELEVATION (FT)	AREA (SF)	INC.STOR (CF)	CUM.STOR (CF)	STOR-IND METHOD
34.0	0	0	0	PEAK STORAGE = 26874 CF
36.0	1165	1165	1165	PEAK ELEVATION= 41.8 FT
38.0	3033	4198	5363	FLOOD ELEVATION= 46.0 FT
40.0	5508	8541	13904	START ELEVATION= 34.0 FT
42.0	8715	14223	28127	SPAN= 6-66 HRS, dt=.12 HRS
44.0	12306	21021	49148	Tdet= 1037.1 MIN (.9 AF)
46.0	16056	28362	77510	

#	ROUTE	INVERT	OUTLET DEVICES
1	3	34.0'	2" ORIFICE/GRATE $Q = .6 \pi r^2 \text{SQR}(2g) \text{SQR}(H-r)$ (Use H/2 if H<d)
2	3	42.3'	48" HORIZONTAL ORIFICE/GRATE $Q = .6 \text{Area} \text{SQR}(2gH)$ (Limited to weir flow @ low head)
3	P	31.0'	18" CULVERT $n = .013$ L=100' S=.078'/' Ke=.6 Cc=.9 Cd=.56
4	S	44.0'	6' BROAD-CRESTED RECTANGULAR WEIR X 1.81 $Q = C L H^{1.5}$ C=1.4, 1.45, 1.5, 0, 0, 0, 0, 0

Primary Discharge

└─3=Culvert
 ├─1=Orifice/Grate
 └─2=Orifice/Grate

Secondary Discharge

└─4=Broad-Crested Rectangular Weir

TYPE II 24-HOUR RAINFALL= 3.36 IN

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SUBCATCHMENT 10

PREDEVELOPMENT DRAINAGE AREA BMP 5.4

PEAK= 10.45 CFS @ 12.10 HRS, VOLUME= .90 AF

ACRES	CN	
11.69	70	WOODS

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 3.36 IN
 SPAN= 6-66 HRS, dt=.12 HRS

Method	Comment	Tc (min)
DIRECT ENTRY	PRE DEVELOPMENT WOODLAND SWALE	20.0

SUBCATCHMENT 20

POST DEVELOPMENT / PHASE 3 BMP5.4

PEAK= 18.68 CFS @ 12.02 HRS, VOLUME= 1.28 AF

ACRES	CN	
11.57	77	SUBDIVISION

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 3.36 IN
 SPAN= 6-66 HRS, dt=.12 HRS

Method	Comment	Tc (min)
DIRECT ENTRY	DEVELOPED SITE	15.0

TYPE II 24-HOUR RAINFALL= 3.36 IN

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REACH 11

WOODLAND RAVINE SECTION #1

Qin = 10.45 CFS @ 12.10 HRS, VOLUME= .90 AF
 Qout= 10.35 CFS @ 12.12 HRS, VOLUME= .90 AF, ATTEN= 1%, LAG= 1.1 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
27.80	0.0	0.00		PEAK ELEV.= 28.13 FT
28.00	.4	4.00	n= .1	PEAK VELOCITY= 2.9 FPS
30.00	50.0	46.44	LENGTH= 100 FT	TRAVEL TIME = .6 MIN
32.00	154.0	58.65	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 871.1 CFS	

REACH 12

WOODLAND RAVINE SECTION #2

Qin = 10.35 CFS @ 12.12 HRS, VOLUME= .90 AF
 Qout= 10.06 CFS @ 12.14 HRS, VOLUME= .90 AF, ATTEN= 3%, LAG= 1.3 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
24.00	0.0	0.00		PEAK ELEV.= 24.20 FT
26.00	46.0	43.20	n= .1	PEAK VELOCITY= 2.2 FPS
28.00	145.0	56.60	LENGTH= 100 FT	TRAVEL TIME = .8 MIN
30.00	227.0	72.50	SLOPE= .02 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1021 CFS	

REACH 13

WOODLAND RAVINE SECTION #3

Qin = 10.06 CFS @ 12.14 HRS, VOLUME= .90 AF
 Qout= 9.84 CFS @ 12.16 HRS, VOLUME= .90 AF, ATTEN= 2%, LAG= 1.0 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
21.80	0.0	0.00		PEAK ELEV.= 22.03 FT
22.00	5.0	47.00	n= .1	PEAK VELOCITY= 1.5 FPS
24.00	130.0	78.46	LENGTH= 100 FT	TRAVEL TIME = 1.1 MIN
26.00	298.0	90.67	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1957.8 CFS	

REACH 14

WOODLAND RAVINE SECTION #4

Qin = 9.84 CFS @ 12.16 HRS, VOLUME= .90 AF
 Qout= 9.33 CFS @ 12.18 HRS, VOLUME= .90 AF, ATTEN= 5%, LAG= 1.4 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
20.00	0.0	0.00		PEAK ELEV.= 20.12 FT
22.00	54.0	54.20	n= .1	PEAK VELOCITY= 3.0 FPS
24.00	177.0	69.58	LENGTH= 100 FT	TRAVEL TIME = .6 MIN
26.00	328.0	82.69	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 2442.7 CFS	

TYPE II 24-HOUR RAINFALL= 3.36 IN

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REACH 21

WOODLAND RAVINE SECTION #1

Qin = 1.23 CFS @ 13.64 HRS, VOLUME= 1.28 AF
 Qout= 1.23 CFS @ 13.67 HRS, VOLUME= 1.28 AF, ATTEN= 0%, LAG= 1.5 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
27.80	0.0	0.00		PEAK ELEV.= 28.01 FT
28.00	.4	4.00	n= .1	PEAK VELOCITY= 1.7 FPS
30.00	50.0	46.44	LENGTH= 100 FT	TRAVEL TIME = 1.0 MIN
32.00	154.0	58.65	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 871.1 CFS	

REACH 22

WOODLAND RAVINE SECTION #2

Qin = 1.23 CFS @ 13.67 HRS, VOLUME= 1.28 AF
 Qout= 1.23 CFS @ 13.70 HRS, VOLUME= 1.28 AF, ATTEN= 0%, LAG= 1.8 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
24.00	0.0	0.00		PEAK ELEV.= 24.02 FT
26.00	46.0	43.20	n= .1	PEAK VELOCITY= 2.2 FPS
28.00	145.0	56.60	LENGTH= 100 FT	TRAVEL TIME = .8 MIN
30.00	227.0	72.50	SLOPE= .02 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1021 CFS	

REACH 23

WOODLAND RAVINE SECTION #3

Qin = 1.23 CFS @ 13.70 HRS, VOLUME= 1.28 AF
 Qout= 1.23 CFS @ 13.79 HRS, VOLUME= 1.28 AF, ATTEN= 0%, LAG= 5.6 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
21.80	0.0	0.00		PEAK ELEV.= 21.87 FT
22.00	5.0	47.00	n= .1	PEAK VELOCITY= .7 FPS
24.00	130.0	78.46	LENGTH= 100 FT	TRAVEL TIME = 2.5 MIN
26.00	298.0	90.67	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1957.8 CFS	

REACH 24

WOODLAND RAVINE SECTION #4

Qin = 1.23 CFS @ 13.79 HRS, VOLUME= 1.28 AF
 Qout= 1.23 CFS @ 13.81 HRS, VOLUME= 1.28 AF, ATTEN= 0%, LAG= 1.2 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
20.00	0.0	0.00		PEAK ELEV.= 20.02 FT
22.00	54.0	54.20	n= .1	PEAK VELOCITY= 3.0 FPS
24.00	177.0	69.58	LENGTH= 100 FT	TRAVEL TIME = .6 MIN
26.00	328.0	82.69	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 2442.7 CFS	

TYPE II 24-HOUR RAINFALL= 3.36 IN

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REACH 25

EMERGENCY SPILLWAY

Qin = 0.00 CFS @ 0.00 HRS, VOLUME= 0.00 AF

Qout= 0.00 CFS @ 0.00 HRS, VOLUME= 0.00 AF, ATTEN= 0%, LAG= 0.0 MIN

DEPTH (FT)	END AREA (SQ-FT)	DISCH (CFS)
0.00	0.00	0.00
.10	.80	3.45
.20	1.61	10.84
.30	2.43	21.11
.43	3.50	38.01
.60	4.92	65.25
.80	6.61	103.70
1.00	8.33	148.18

8' x 1' CHANNEL

SIDE SLOPE= 3 '/'

n= .03

LENGTH= 70 FT

SLOPE= .1667 FT/FT

STOR-IND+TRANS METHOD

PEAK DEPTH= 0.00 FT

PEAK VELOCITY= 0.0 FPS

TRAVEL TIME = 0.0 MIN

SPAN= 6-66 HRS, dt=.12 HRS

TYPE II 24-HOUR RAINFALL= 3.36 IN

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POND 20

STORMWATER MANAGEMENT POND 5.4

Qin = 18.68 CFS @ 12.02 HRS, VOLUME= 1.28 AF
 Qout= 1.23 CFS @ 13.64 HRS, VOLUME= 1.28 AF, ATTEN= 93%, LAG= 97.6 MIN
 Qpri= 1.23 CFS @ 13.64 HRS, VOLUME= 1.28 AF
 Qsec= 0.00 CFS @ 0.00 HRS, VOLUME= 0.00 AF

ELEVATION (FT)	AREA (SF)	INC.STOR (CF)	CUM.STOR (CF)	STOR-IND METHOD
34.0	0	0	0	PEAK STORAGE = 31722 CF
36.0	1165	1165	1165	PEAK ELEVATION= 42.3 FT
38.0	3033	4198	5363	FLOOD ELEVATION= 46.0 FT
40.0	5508	8541	13904	START ELEVATION= 34.0 FT
42.0	8715	14223	28127	SPAN= 6-66 HRS, dt=.12 HRS
44.0	12306	21021	49148	Tdet= 912.9 MIN (1.28 AF)
46.0	16056	28362	77510	

#	ROUTE	INVERT	OUTLET DEVICES
1	3	34.0'	2" ORIFICE/GRATE Q=.6 PI r ² SQR(2g) SQR(H-r) (Use H/2 if H<d)
2	3	42.3'	48" HORIZONTAL ORIFICE/GRATE Q=.6 Area SQR(2gH) (Limited to weir flow @ low head)
3	P	31.0'	18" CULVERT n=.013 L=100' S=.078'/' Ke=.6 Cc=.9 Cd=.56
4	S	44.0'	6' BROAD-CRESTED RECTANGULAR WEIR X 1.81 Q=C L H ^{1.5} C=1.4, 1.45, 1.5, 0, 0, 0, 0

Primary Discharge

- └─3=Culvert
- ├─1=Orifice/Grate
- └─2=Orifice/Grate

Secondary Discharge

- └─4=Broad-Crested Rectangular Weir

TYPE II 24-HOUR RAINFALL= 5.04 IN

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SUBCATCHMENT 10

PREDEVELOPMENT DRAINAGE AREA BMP 5.4

PEAK= 25.06 CFS @ 12.09 HRS, VOLUME= 2.01 AF

ACRES	CN	
11.69	70	WOODS

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 5.04 IN
 SPAN= 6-66 HRS, dt=.12 HRS

Method	Comment	Tc (min)
DIRECT ENTRY	PRE DEVELOPMENT WOODLAND SWALE	20.0

SUBCATCHMENT 20

POST DEVELOPMENT / PHASE 3 BMP5.4

PEAK= 38.08 CFS @ 12.01 HRS, VOLUME= 2.56 AF

ACRES	CN	
11.57	77	SUBDIVISION

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 5.04 IN
 SPAN= 6-66 HRS, dt=.12 HRS

Method	Comment	Tc (min)
DIRECT ENTRY	DEVELOPED SITE	15.0

TYPE II 24-HOUR RAINFALL= 5.04 IN

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REACH 11 WOODLAND RAVINE SECTION #1

Qin = 25.06 CFS @ 12.09 HRS, VOLUME= 2.01 AF
 Qout= 24.88 CFS @ 12.11 HRS, VOLUME= 2.01 AF, ATTEN= 1%, LAG= 1.2 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
27.80	0.0	0.00		PEAK ELEV.= 28.32 FT
28.00	.4	4.00	n= .1	PEAK VELOCITY= 3.0 FPS
30.00	50.0	46.44	LENGTH= 100 FT	TRAVEL TIME = .6 MIN
32.00	154.0	58.65	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 871.1 CFS	

REACH 12 WOODLAND RAVINE SECTION #2

Qin = 24.88 CFS @ 12.11 HRS, VOLUME= 2.01 AF
 Qout= 24.34 CFS @ 12.13 HRS, VOLUME= 2.01 AF, ATTEN= 2%, LAG= 1.4 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
24.00	0.0	0.00		PEAK ELEV.= 24.49 FT
26.00	46.0	43.20	n= .1	PEAK VELOCITY= 2.2 FPS
28.00	145.0	56.60	LENGTH= 100 FT	TRAVEL TIME = .8 MIN
30.00	227.0	72.50	SLOPE= .02 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1021 CFS	

REACH 13 WOODLAND RAVINE SECTION #3

Qin = 24.34 CFS @ 12.13 HRS, VOLUME= 2.01 AF
 Qout= 23.82 CFS @ 12.14 HRS, VOLUME= 2.01 AF, ATTEN= 2%, LAG= .9 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
21.80	0.0	0.00		PEAK ELEV.= 22.08 FT
22.00	5.0	47.00	n= .1	PEAK VELOCITY= 2.5 FPS
24.00	130.0	78.46	LENGTH= 100 FT	TRAVEL TIME = .7 MIN
26.00	298.0	90.67	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1957.8 CFS	

REACH 14 WOODLAND RAVINE SECTION #4

Qin = 23.82 CFS @ 12.14 HRS, VOLUME= 2.01 AF
 Qout= 23.21 CFS @ 12.16 HRS, VOLUME= 2.01 AF, ATTEN= 3%, LAG= 1.2 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
20.00	0.0	0.00		PEAK ELEV.= 20.29 FT
22.00	54.0	54.20	n= .1	PEAK VELOCITY= 3.0 FPS
24.00	177.0	69.58	LENGTH= 100 FT	TRAVEL TIME = .6 MIN
26.00	328.0	82.69	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 2442.7 CFS	

TYPE II 24-HOUR RAINFALL= 5.04 IN

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REACH 21

WOODLAND RAVINE SECTION #1

Qin = 26.09 CFS @ 12.17 HRS, VOLUME= 2.56 AF
 Qout= 23.89 CFS @ 12.21 HRS, VOLUME= 2.56 AF, ATTEN= 8%, LAG= 2.7 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
27.80	0.0	0.00		PEAK ELEV.= 28.30 FT
28.00	.4	4.00	n= .1	PEAK VELOCITY= 3.0 FPS
30.00	50.0	46.44	LENGTH= 100 FT	TRAVEL TIME = .6 MIN
32.00	154.0	58.65	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 871.1 CFS	

REACH 22

WOODLAND RAVINE SECTION #2

Qin = 23.89 CFS @ 12.21 HRS, VOLUME= 2.56 AF
 Qout= 24.00 CFS @ 12.24 HRS, VOLUME= 2.56 AF, ATTEN= 0%, LAG= 1.7 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
24.00	0.0	0.00		PEAK ELEV.= 24.49 FT
26.00	46.0	43.20	n= .1	PEAK VELOCITY= 2.2 FPS
28.00	145.0	56.60	LENGTH= 100 FT	TRAVEL TIME = .8 MIN
30.00	227.0	72:50	SLOPE= .02 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1021 CFS	

REACH 23

WOODLAND RAVINE SECTION #3

Qin = 24.00 CFS @ 12.24 HRS, VOLUME= 2.56 AF
 Qout= 24.30 CFS @ 12.25 HRS, VOLUME= 2.56 AF, ATTEN= 0%, LAG= .8 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
21.80	0.0	0.00		PEAK ELEV.= 22.08 FT
22.00	5.0	47.00	n= .1	PEAK VELOCITY= 2.5 FPS
24.00	130.0	78.46	LENGTH= 100 FT	TRAVEL TIME = .7 MIN
26.00	298.0	90.67	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1957.8 CFS	

REACH 24

WOODLAND RAVINE SECTION #4

Qin = 24.30 CFS @ 12.25 HRS, VOLUME= 2.56 AF
 Qout= 22.77 CFS @ 12.27 HRS, VOLUME= 2.56 AF, ATTEN= 6%, LAG= 1.0 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
20.00	0.0	0.00		PEAK ELEV.= 20.29 FT
22.00	54.0	54.20	n= .1	PEAK VELOCITY= 3.0 FPS
24.00	177.0	69.58	LENGTH= 100 FT	TRAVEL TIME = .6 MIN
26.00	328.0	82.69	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 2442.7 CFS	

TYPE II 24-HOUR RAINFALL= 5.04 IN

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REACH 25

EMERGENCY SPILLWAY

Qin = 0.00 CFS @ 0.00 HRS, VOLUME= 0.00 AF

Qout= 0.00 CFS @ 0.00 HRS, VOLUME= 0.00 AF, ATTEN= 0%, LAG= 0.0 MIN

DEPTH (FT)	END AREA (SQ-FT)	DISCH (CFS)	8' x 1' CHANNEL SIDE SLOPE= 3 '/' n= .03 LENGTH= 70 FT SLOPE= .1667 FT/FT	STOR-IND+TRANS METHOD PEAK DEPTH= 0.00 FT PEAK VELOCITY= 0.0 FPS TRAVEL TIME = 0.0 MIN SPAN= 6-66 HRS, dt=.12 HRS
0.00	0.00	0.00		
.10	.80	3.45		
.20	1.61	10.84		
.30	2.43	21.11		
.43	3.50	38.01		
.60	4.92	65.25		
.80	6.61	103.70		
1.00	8.33	148.18		

TYPE II 24-HOUR RAINFALL= 5.04 IN

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POND 20

STORMWATER MANAGEMENT POND 5.4

Qin = 38.08 CFS @ 12.01 HRS, VOLUME= 2.56 AF
 Qout= 26.09 CFS @ 12.17 HRS, VOLUME= 2.56 AF, ATTEN= 31%, LAG= 9.3 MIN
 Qpri= 26.09 CFS @ 12.17 HRS, VOLUME= 2.56 AF
 Qsec= 0.00 CFS @ 0.00 HRS, VOLUME= 0.00 AF

ELEVATION (FT)	AREA (SF)	INC.STOR (CF)	CUM.STOR (CF)	STOR-IND METHOD
34.0	0	0	0	PEAK STORAGE = 38529 CF
36.0	1165	1165	1165	PEAK ELEVATION= 43.0 FT
38.0	3033	4198	5363	FLOOD ELEVATION= 46.0 FT
40.0	5508	8541	13904	START ELEVATION= 34.0 FT
42.0	8715	14223	28127	SPAN= 6-66 HRS, dt=.12 HRS
44.0	12306	21021	49148	Tdet= 469.6 MIN (2.56 AF)
46.0	16056	28362	77510	

#	ROUTE	INVERT	OUTLET DEVICES
1	3	34.0'	2" ORIFICE/GRATE $Q = .6 \text{ PI } r^2 \text{ SQR}(2g) \text{ SQR}(H-r)$ (Use H/2 if H<d)
2	3	42.3'	48" HORIZONTAL ORIFICE/GRATE $Q = .6 \text{ Area } \text{SQR}(2gH)$ (Limited to weir flow @ low head)
3	P	31.0'	18" CULVERT $n = .013 \quad L = 100' \quad S = .078'/' \quad K_e = .6 \quad C_c = .9 \quad C_d = .56$
4	S	44.0'	6' BROAD-CRESTED RECTANGULAR WEIR X 1.81 $Q = C L H^{1.5} \quad C = 1.4, 1.45, 1.5, 0, 0, 0, 0, 0$

Primary Discharge

- └─3=Culvert
- └─1=Orifice/Grate
- └─2=Orifice/Grate

Secondary Discharge

- └─4=Broad-Crested Rectangular Weir

TYPE II 24-HOUR RAINFALL= 7.68 IN

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SUBCATCHMENT 10

PREDEVELOPMENT DRAINAGE AREA BMP 5.4

PEAK= 51.60 CFS @ 12.08 HRS, VOLUME= 4.08 AF

ACRES	CN	
11.69	70	WOODS

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 7.68 IN
 SPAN= 6-66 HRS, dt=.12 HRS

Method	Comment	Tc (min)
DIRECT ENTRY	PRE DEVELOPMENT WOODLAND SWALE	20.0

SUBCATCHMENT 20

POST DEVELOPMENT / PHASE 3 BMP5.4

PEAK= 70.87 CFS @ 12.01 HRS, VOLUME= 4.80 AF

ACRES	CN	
11.57	77	SUBDIVISION

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 7.68 IN
 SPAN= 6-66 HRS, dt=.12 HRS

Method	Comment	Tc (min)
DIRECT ENTRY	DEVELOPED SITE	15.0

TYPE II 24-HOUR RAINFALL= 7.68 IN

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REACH 11 WOODLAND RAVINE SECTION #1

Qin = 51.60 CFS @ 12.08 HRS, VOLUME= 4.08 AF
 Qout= 51.27 CFS @ 12.10 HRS, VOLUME= 4.08 AF, ATTEN= 1%, LAG= 1.3 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
27.80	0.0	0.00		PEAK ELEV.= 28.65 FT
28.00	.4	4.00	n= .1	PEAK VELOCITY= 3.1 FPS
30.00	50.0	46.44	LENGTH= 100 FT	TRAVEL TIME = .5 MIN
32.00	154.0	58.65	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 871.1 CFS	

REACH 12 WOODLAND RAVINE SECTION #2

Qin = 51.27 CFS @ 12.10 HRS, VOLUME= 4.08 AF
 Qout= 50.30 CFS @ 12.12 HRS, VOLUME= 4.08 AF, ATTEN= 2%, LAG= 1.4 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
24.00	0.0	0.00		PEAK ELEV.= 25.02 FT
26.00	46.0	43.20	n= .1	PEAK VELOCITY= 2.2 FPS
28.00	145.0	56.60	LENGTH= 100 FT	TRAVEL TIME = .8 MIN
30.00	227.0	72.50	SLOPE= .02 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1021 CFS	

REACH 13 WOODLAND RAVINE SECTION #3

Qin = 50.30 CFS @ 12.12 HRS, VOLUME= 4.08 AF
 Qout= 49.46 CFS @ 12.13 HRS, VOLUME= 4.08 AF, ATTEN= 2%, LAG= .8 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
21.80	0.0	0.00		PEAK ELEV.= 22.17 FT
22.00	5.0	47.00	n= .1	PEAK VELOCITY= 3.2 FPS
24.00	130.0	78.46	LENGTH= 100 FT	TRAVEL TIME = .5 MIN
26.00	298.0	90.67	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 1957.8 CFS	

REACH 14 WOODLAND RAVINE SECTION #4

Qin = 49.46 CFS @ 12.13 HRS, VOLUME= 4.08 AF
 Qout= 48.42 CFS @ 12.15 HRS, VOLUME= 4.08 AF, ATTEN= 2%, LAG= 1.0 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)	SPECIAL 100' CHANNEL	STOR-IND+TRANS METHOD
20.00	0.0	0.00		PEAK ELEV.= 20.61 FT
22.00	54.0	54.20	n= .1	PEAK VELOCITY= 3.0 FPS
24.00	177.0	69.58	LENGTH= 100 FT	TRAVEL TIME = .6 MIN
26.00	328.0	82.69	SLOPE= .04 FT/FT	SPAN= 6-66 HRS, dt=.12 HRS
			CAPACITY= 2442.7 CFS	

TYPE II 24-HOUR RAINFALL= 7.68 IN

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REACH 21

WOODLAND RAVINE SECTION #1

Qin = 43.72 CFS @ 12.17 HRS, VOLUME= 4.80 AF
 Qout= 42.95 CFS @ 12.20 HRS, VOLUME= 4.80 AF, ATTEN= 2%, LAG= 2.3 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)
27.80	0.0	0.00
28.00	.4	4.00
30.00	50.0	46.44
32.00	154.0	58.65

SPECIAL 100' CHANNEL
 n= .1
 LENGTH= 100 FT
 SLOPE= .04 FT/FT
 CAPACITY= 871.1 CFS

STOR-IND+TRANS METHOD
 PEAK ELEV.= 28.54 FT
 PEAK VELOCITY= 3.1 FPS
 TRAVEL TIME = .5 MIN
 SPAN= 6-66 HRS, dt=.12 HRS

REACH 22

WOODLAND RAVINE SECTION #2

Qin = 42.95 CFS @ 12.20 HRS, VOLUME= 4.80 AF
 Qout= 42.48 CFS @ 12.23 HRS, VOLUME= 4.80 AF, ATTEN= 1%, LAG= 1.4 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)
24.00	0.0	0.00
26.00	46.0	43.20
28.00	145.0	56.60
30.00	227.0	72.50

SPECIAL 100' CHANNEL
 n= .1
 LENGTH= 100 FT
 SLOPE= .02 FT/FT
 CAPACITY= 1021 CFS

STOR-IND+TRANS METHOD
 PEAK ELEV.= 24.85 FT
 PEAK VELOCITY= 2.2 FPS
 TRAVEL TIME = .8 MIN
 SPAN= 6-66 HRS, dt=.12 HRS

REACH 23

WOODLAND RAVINE SECTION #3

Qin = 42.48 CFS @ 12.23 HRS, VOLUME= 4.80 AF
 Qout= 42.64 CFS @ 12.24 HRS, VOLUME= 4.80 AF, ATTEN= 0%, LAG= .8 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)
21.80	0.0	0.00
22.00	5.0	47.00
24.00	130.0	78.46
26.00	298.0	90.67

SPECIAL 100' CHANNEL
 n= .1
 LENGTH= 100 FT
 SLOPE= .04 FT/FT
 CAPACITY= 1957.8 CFS

STOR-IND+TRANS METHOD
 PEAK ELEV.= 22.15 FT
 PEAK VELOCITY= 3.0 FPS
 TRAVEL TIME = .6 MIN
 SPAN= 6-66 HRS, dt=.12 HRS

REACH 24

WOODLAND RAVINE SECTION #4

Qin = 42.64 CFS @ 12.24 HRS, VOLUME= 4.80 AF
 Qout= 41.28 CFS @ 12.26 HRS, VOLUME= 4.80 AF, ATTEN= 3%, LAG= 1.0 MIN

ELEV (FT)	END AREA (SQ-FT)	PERIM (FT)
20.00	0.0	0.00
22.00	54.0	54.20
24.00	177.0	69.58
26.00	328.0	82.69

SPECIAL 100' CHANNEL
 n= .1
 LENGTH= 100 FT
 SLOPE= .04 FT/FT
 CAPACITY= 2442.7 CFS

STOR-IND+TRANS METHOD
 PEAK ELEV.= 20.52 FT
 PEAK VELOCITY= 3.0 FPS
 TRAVEL TIME = .6 MIN
 SPAN= 6-66 HRS, dt=.12 HRS

TYPE II 24-HOUR RAINFALL= 7.68 IN

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REACH 25

EMERGENCY SPILLWAY

Qin = 15.28 CFS @ 12.16 HRS, VOLUME= .31 AF

Qout= 14.82 CFS @ 12.17 HRS, VOLUME= .31 AF, ATTEN= 3%, LAG= .4 MIN

DEPTH (FT)	END AREA (SQ-FT)	DISCH (CFS)	8' x 1' CHANNEL SIDE SLOPE= 3 '/' n= .03 LENGTH= 70 FT SLOPE= .1667 FT/FT	STOR-IND+TRANS METHOD PEAK DEPTH= .23 FT PEAK VELOCITY= 7.5 FPS TRAVEL TIME = .2 MIN SPAN= 6-66 HRS, dt=.12 HRS
0.00	0.00	0.00		
.10	.80	3.45		
.20	1.61	10.84		
.30	2.43	21.11		
.43	3.50	38.01		
.60	4.92	65.25		
.80	6.61	103.70		
1.00	8.33	148.18		

TYPE II 24-HOUR RAINFALL= 7.68 IN

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POND 20

STORMWATER MANAGEMENT POND 5.4

Qin = 70.87 CFS @ 12.01 HRS, VOLUME= 4.80 AF
 Qout= 44.18 CFS @ 12.16 HRS, VOLUME= 4.80 AF, ATTEN= 38%, LAG= 9.2 MIN
 Qpri= 28.90 CFS @ 12.16 HRS, VOLUME= 4.50 AF
 Qsec= 15.28 CFS @ 12.16 HRS, VOLUME= .31 AF

ELEVATION (FT)	AREA (SF)	INC.STOR (CF)	CUM.STOR (CF)	STOR-IND METHOD
34.0	0	0	0	PEAK STORAGE = 62533 CF
36.0	1165	1165	1165	PEAK ELEVATION= 44.9 FT
38.0	3033	4198	5363	FLOOD ELEVATION= 46.0 FT
40.0	5508	8541	13904	START ELEVATION= 34.0 FT
42.0	8715	14223	28127	SPAN= 6-66 HRS, dt=.12 HRS
44.0	12306	21021	49148	Tdet= 262.9 MIN (4.79 AF)
46.0	16056	28362	77510	

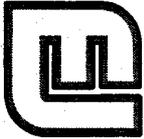
#	ROUTE	INVERT	OUTLET DEVICES
1	3	34.0'	2" ORIFICE/GRATE $Q=.6 \text{ PI } r^2 \text{ SQR}(2g) \text{ SQR}(H-r)$ (Use H/2 if H<d)
2	3	42.3'	48" HORIZONTAL ORIFICE/GRATE $Q=.6 \text{ Area } \text{SQR}(2gH)$ (Limited to weir flow @ low head)
3	P	31.0'	18" CULVERT $n=.013 \text{ L}=100' \text{ S}=.078'/' \text{ Ke}=.6 \text{ Cc}=.9 \text{ Cd}=.56$
4	S	44.0'	6' BROAD-CRESTED RECTANGULAR WEIR X 1.81 $Q=C \text{ L } H^{1.5} \text{ C}=1.4, 1.45, 1.5, 0, 0, 0, 0, 0$

Primary Discharge

- └─3=Culvert
 - └─1=Orifice/Grate
 - └─2=Orifice/Grate

Secondary Discharge

- └─4=Broad-Crested Rectangular Weir



Langley and McDonald, P.C.

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Subject STONEHOUSE

VB Phase 3

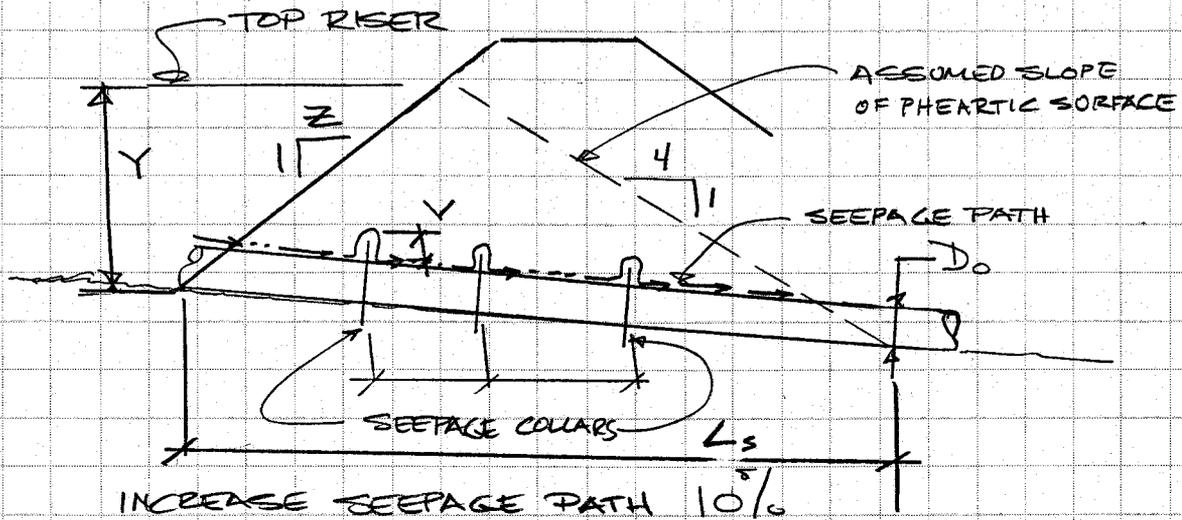
Computed By RSP Checked by _____

Project No. 1960033-11.73

Client Stonehouse L.L.C.

Date _____ Sheet No. _____

BMP 5.4 SEEPAGE COLLAR DESIGN



L_s : LENGTH IN SATURATED ZONE S : SLOPE OF PIPE ft/ft.

$$L_s = Y(z+4)\left(1 + \frac{S}{2z-S}\right)$$

$$Y = 423 - 2S = 7.3$$

$$S = .02$$

4x4 COLLARS $V = 4 - \frac{1.7}{2} = 1.15$

$$\therefore L_s = 7.3 \times 7 \times \left(1 + \frac{.02}{.22}\right) = 55.54 \text{ ft.}$$

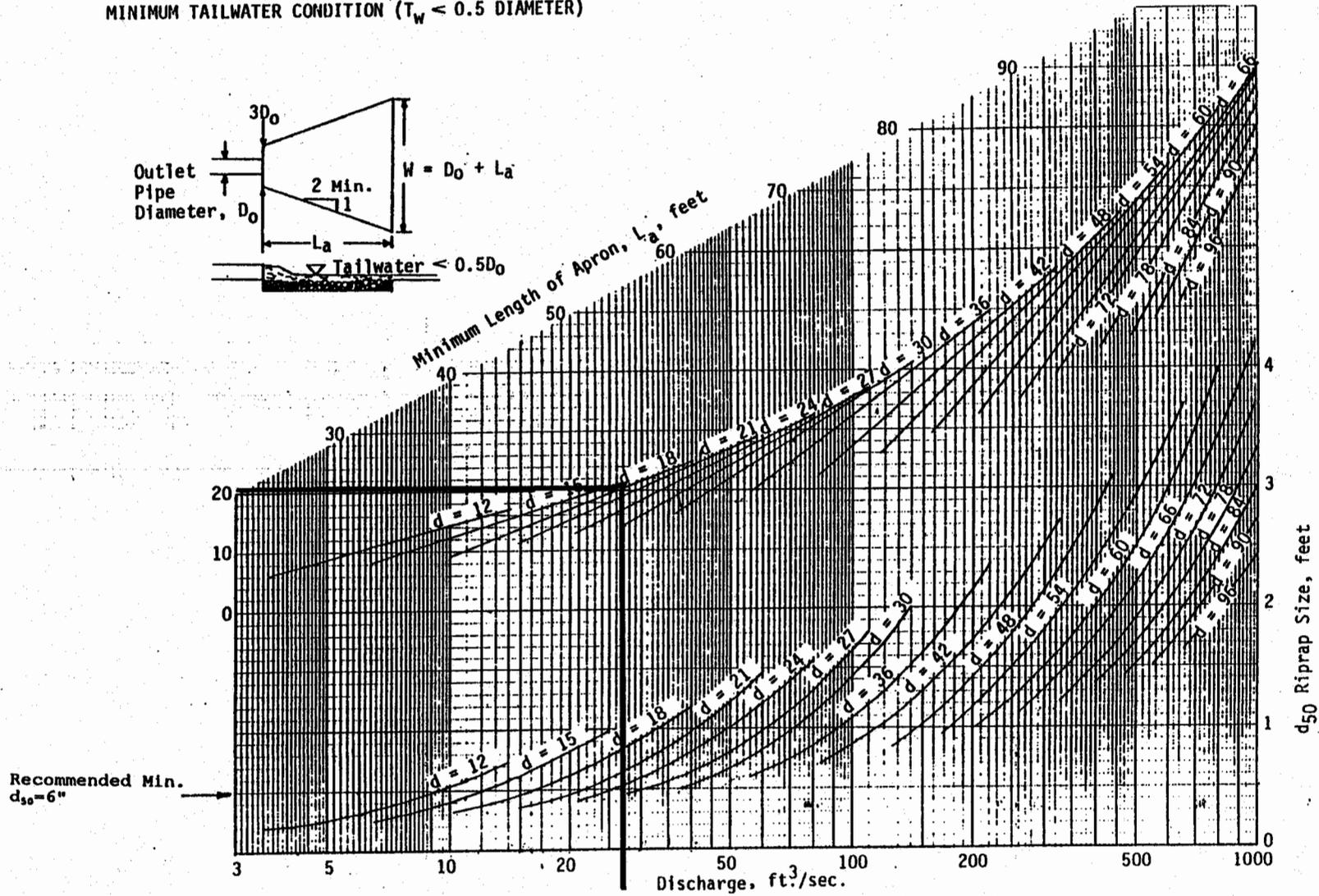
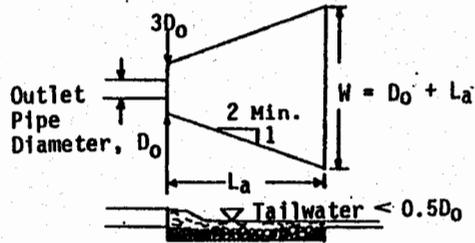
$$L_s + 10\% = 61 \text{ ft.}$$

REQD. SEEPAGE PATH: $L_{\text{REQD}} = L_s \times 1.1$

$$L_{\text{REQD}} = L_{s1} + 2 \times V \times N = 55.5 + 2 \times 1.15 \times N = 61$$

$$N = \frac{61 - 55.5}{2.3} = \frac{5.5}{2.3} = 2.41 \xrightarrow{\text{USE}} 3$$

DESIGN OF OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL
 MINIMUM TAILWATER CONDITION ($T_w < 0.5$ DIAMETER)



OUTLET BMP 5.4 $Q_{10} = 26.09$ cfs
 $d_o = 18''$ $Q_{1.05} = 28.9$ cfs
 use $L_a = 20$ ft.

=====

INLET NUMBER E-5 LENGTH 8.0 STATION 15+50L

DRAINAGE AREA = 0.130 ACRES C VALUE = .900 CA = 0.117
DRAINAGE AREA = 0.390 ACRES C VALUE = .300 CA = 0.117
SUM CA= 0.234 INT= 4.00 CFS= 0.936 CO= 0.000 GUTTER FLOW= 0.936

GUTTER SLOPE = 0.0267 FT/FT PAVEMENT CROSS SLOPE = 0.0208 FT/FT

SPREAD	W	W/T	SW	SW/SX	Eo	a	S'W	SE
3.31	2.0	0.60	0.0833	4.0	0.98	3.5	0.146	0.164

XXXXXXXXXX CURB INLET ON A CONTINUOUS GRADE XXXXXXXXXXXX
REQUIRED LENGTH (ft) = 7.2 EFFICIENCY= 1.00
CFS INTERCEPTED= 0.94 CFS CARRYOVER= 0.00

=====

INLET NUMBER E-4 LENGTH 8.0 STATION 16+60 END

DRAINAGE AREA = 0.080 ACRES C VALUE = .900 CA = 0.072
DRAINAGE AREA = 0.250 ACRES C VALUE = .900 CA = 0.225

FOR THE FIRST SIDE
SUM CA= 0.072 INT= 4.00 CFS= 0.288 CO= 0.000 GUTTER FLOW= 0.288
FOR THE OTHER SIDE
SUM CA= 0.225 INT= 4.00 CFS= 0.900 CO= 0.000 GUTTER FLOW= 0.900
AT THE INLET

SUM CA= 0.297 INT= 4.00 CFS= 1.188 CO= 0.000 GUTTER FLOW= 1.188

GUTTER SLOPE = 0.0010 FT/FT PAVEMENT CROSS SLOPE = 0.0208 FT/FT

SPREAD AT A SLOPE OF .001 (ft./ft.) AND 0.90 (cfs) IS 9.07 (ft.)

XXXXXXXXXX CURB INLET IN A SUMP XXXXXXXXXXXX
P EFFEC. LENGTH (ft) = 11.60 H (ft) = 0.458
DEPTH OF WATER (ft) = 0.13 SPREAD (ft) = 6.03

=====

INLET NUMBER F-3	LENGTH	8.0	STATION	15+75 R
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DRAINAGE AREA = 0.130 ACRES	C VALUE = .900	CA = 0.117
DRAINAGE AREA = 0.140 ACRES	C VALUE = .300	CA = 0.042
DRAINAGE AREA = 0.040 ACRES	C VALUE = .900	CA = 0.036

FOR THE FIRST SIDE

SUM CA= 0.159 INT= 4.00 CFS= 0.636 CO= 0.000 GUTTER FLOW= 0.636

FOR THE OTHER SIDE

SUM CA= 0.036 INT= 4.00 CFS= 0.144 CO= 0.000 GUTTER FLOW= 0.144

AT THE INLET

SUM CA= 0.195 INT= 4.00 CFS= 0.780 CO= 0.000 GUTTER FLOW= 0.780

GUTTER SLOPE = 0.0010 FT/FT PAVEMENT CROSS SLOPE = 0.0208 FT/FT

SPREAD AT A SLOPE OF .001 (ft./ft.) AND 0.64 (cfs) IS 7.66 (ft.)

XXXXXXXXXXXX CURB INLET IN A SUMP XXXXXXXXXXXX
P EFFEC. LENGTH (ft) = 11.60 H (ft) = 0.458
DEPTH OF WATER (ft) = 0.09 SPREAD (ft) = 4.56

=====

INLET NUMBER F-2	LENGTH	6.0	STATION	15+75 L
------------------	--------	-----	---------	---------

DRAINAGE AREA = 0.130 ACRES	C VALUE = .900	CA = 0.117
DRAINAGE AREA = 0.040 ACRES	C VALUE = .900	CA = 0.036

FOR THE FIRST SIDE

SUM CA= 0.117 INT= 4.00 CFS= 0.468 CO= 0.000 GUTTER FLOW= 0.468

FOR THE OTHER SIDE

SUM CA= 0.036 INT= 4.00 CFS= 0.144 CO= 0.000 GUTTER FLOW= 0.144

AT THE INLET

SUM CA= 0.153 INT= 4.00 CFS= 0.612 CO= 0.000 GUTTER FLOW= 0.612

GUTTER SLOPE = 0.0010 FT/FT PAVEMENT CROSS SLOPE = 0.0208 FT/FT

SPREAD AT A SLOPE OF .001 (ft./ft.) AND 0.47 (cfs) IS 6.50 (ft.)

XXXXXXXXXXXX CURB INLET IN A SUMP XXXXXXXXXXXX
P EFFEC. LENGTH (ft) = 9.60 H (ft) = 0.458
DEPTH OF WATER (ft) = 0.09 SPREAD (ft) = 4.40

PROJECT 1960038-111.73
HEC12 Version: V2.91

Run Date: 07-28-1999

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INLET NUMBER G-4	LENGTH 10.0	STATION 21+63L
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DRAINAGE AREA = 0.220 ACRES	C VALUE = .900	CA = 0.198
DRAINAGE AREA = 0.180 ACRES	C VALUE = .300	CA = 0.054
DRAINAGE AREA = 0.210 ACRES	C VALUE = .300	CA = 0.063
DRAINAGE AREA = 0.190 ACRES	C VALUE = .900	CA = 0.171

FOR THE FIRST SIDE
SUM CA= 0.252 INT= 4.00 CFS= 1.008 CO= 0.000 GUTTER FLOW= 1.008
FOR THE OTHER SIDE
SUM CA= 0.234 INT= 4.00 CFS= 0.936 CO= 0.000 GUTTER FLOW= 0.936
AT THE INLET

SUM CA= 0.486 INT= 4.00 CFS= 1.944 CO= 0.000 GUTTER FLOW= 1.944

GUTTER SLOPE = 0.0010 FT/FT PAVEMENT CROSS SLOPE = 0.0208 FT/FT

SPREAD AT A SLOPE OF .001 (ft./ft.) AND 1.01 (cfs) IS 8.95 (ft.)

XXXXXXXXXX CURB INLET IN A SUMP XXXXXXXXXXXX
P EFFEC. LENGTH (ft) = 13.60 H (ft) = 0.458
DEPTH OF WATER (ft) = 0.16 SPREAD (ft) = 7.54

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=====
INLET NUMBER H-4                LENGTH  2.5                STATION  15+25 L
DRAINAGE AREA =  0.040 ACRES      C VALUE = .900          CA =  0.036
DRAINAGE AREA =  0.100 ACRES      C VALUE = .300          CA =  0.030
DRAINAGE AREA =  0.010 ACRES      C VALUE = .900          CA =  0.009
DRAINAGE AREA =  0.030 ACRES      C VALUE = .300          CA =  0.009

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FOR THE FIRST SIDE
SUM CA=  0.066 INT=  4.00 CFS=  0.264 CO=  0.000 GUTTER FLOW=  0.264
FOR THE OTHER SIDE
SUM CA=  0.018 INT=  4.00 CFS=  0.072 CO=  0.000 GUTTER FLOW=  0.072
AT THE INLET

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SUM CA=  0.084 INT=  4.00 CFS=  0.336 CO=  0.000 GUTTER FLOW=  0.336
GUTTER SLOPE = 0.0010 FT/FT      PAVEMENT CROSS SLOPE = 0.0208 FT/FT

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SPREAD AT A SLOPE OF .001 (ft./ft.) AND 0.26 (cfs) IS 4.53 (ft.)

```

XXXXXXXXXXXX CURB INLET IN A SUMP XXXXXXXXXXXXX
P EFFEC. LENGTH (ft) = 6.10                H (ft) = 0.458
DEPTH OF WATER (ft) = 0.08                SPREAD (ft) = 3.99

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=====
INLET NUMBER H-3a                LENGTH  6.0                STATION  17+35 END
DRAINAGE AREA =  0.080 ACRES      C VALUE = .900          CA =  0.072
DRAINAGE AREA =  0.030 ACRES      C VALUE = .300          CA =  0.009
DRAINAGE AREA =  0.080 ACRES      C VALUE = .900          CA =  0.072

```

```

FOR THE FIRST SIDE
SUM CA=  0.081 INT=  4.00 CFS=  0.324 CO=  0.000 GUTTER FLOW=  0.324
FOR THE OTHER SIDE
SUM CA=  0.072 INT=  4.00 CFS=  0.288 CO=  0.000 GUTTER FLOW=  0.288
AT THE INLET

```

```

SUM CA=  0.153 INT=  4.00 CFS=  0.612 CO=  0.000 GUTTER FLOW=  0.612
GUTTER SLOPE = 0.0010 FT/FT      PAVEMENT CROSS SLOPE = 0.0208 FT/FT

```

SPREAD AT A SLOPE OF .001 (ft./ft.) AND 0.32 (cfs) IS 5.22 (ft.)

```

XXXXXXXXXXXX CURB INLET IN A SUMP XXXXXXXXXXXXX
P EFFEC. LENGTH (ft) = 9.60                H (ft) = 0.458
DEPTH OF WATER (ft) = 0.09                SPREAD (ft) = 4.40

```

=====

INLET NUMBER H-5 LENGTH 2.5 STATION 15+25 R

DRAINAGE AREA = 0.040 ACRES C VALUE = .900 CA = 0.036

DRAINAGE AREA = 0.010 ACRES C VALUE = .900 CA = 0.009

FOR THE FIRST SIDE

SUM CA= 0.036 INT= 4.00 CFS= 0.144 CO= 0.000 GUTTER FLOW= 0.144

FOR THE OTHER SIDE

SUM CA= 0.009 INT= 4.00 CFS= 0.036 CO= 0.000 GUTTER FLOW= 0.036

AT THE INLET

SUM CA= 0.045 INT= 4.00 CFS= 0.180 CO= 0.000 GUTTER FLOW= 0.180

GUTTER SLOPE = 0.0010 FT/FT PAVEMENT CROSS SLOPE = 0.0208 FT/FT

SPREAD AT A SLOPE OF .001 (ft./ft.) AND 0.14 (cfs) IS 2.59 (ft.)

XXXXXXXXXX CURB INLET IN A SUMP XXXXXXXXXXXX

P EFFEC. LENGTH (ft) = 6.10 H (ft) = 0.458

DEPTH OF WATER (ft) = 0.05 SPREAD (ft) = 2.63

=====

INLET NUMBER I-3	LENGTH	0.0	STATION	17+00 L
DRAINAGE AREA = 1.340 ACRES	C VALUE = .300		CA = 0.402	
DRAINAGE AREA = 0.170 ACRES	C VALUE = .900		CA = 0.153	
DRAINAGE AREA = 0.270 ACRES	C VALUE = .300		CA = 0.081	
DRAINAGE AREA = 0.190 ACRES	C VALUE = .900		CA = 0.171	
TOTAL AREA = 1.97	COMPOSITE C = .41		CUM. CA = .81	
FOR THE FIRST SIDE				
SUM CA= 0.555 INT= 4.00 CFS= 2.220 CO= 0.000 GUTTER FLOW= 2.220				
FOR THE OTHER SIDE				
SUM CA= 0.252 INT= 4.00 CFS= 1.008 CO= 0.000 GUTTER FLOW= 1.008				
AT THE INLET				
SUM CA= 0.807 INT= 4.00 CFS= 3.228 CO= 0.000 GUTTER FLOW= 3.228				
GUTTER SLOPE = 0.0290 FT/FT	PAVEMENT CROSS SLOPE =	0.0233 FT/FT		

SPREAD AT A SLOPE OF .029 (ft./ft.) AND 2.22 (cfs) IS 16.06 (ft.)

XXXXXXXXXX GRATE INLET IN A SUMP XXXXXXXXXXXX
DEPTH OF WATER (ft) = 0.19 SPREAD (ft) = 8.24
Grate operates as A WEIR

STORM SEWER DESIGN / RATIONAL METHOD 10 YEAR RETURN PERIOD

STONEHOUSE SECTION VB, PHASE 3

Concrete Pipe, "n" = 0.013 Capacity @ 80% Full Depth

VDOT L&D 229		Area Drained	Run-off Coeff.	"C x A		Inlet Time	Time of Conc.	Rainfall Intensity	RUNOFF	INVERT ELEVATIONS		LENGTH	SLOPE	DIAM	CAPACITY	VELOCITY	TRAVEL "t"	REMARKS
FROM PT.	TO PT.	"Acres"	"C"	INCR.	ACCUM	"t"	"tc"	"I"	"QRational"	UPPER END	LOWER END	ft.	ft/ft	Inch	cfs	fps	min.	
(1)	(2)	(3)	(4)	(5)	(6)	*	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	
SYSTEM "E" SAPLING DRIVE																		
PAVEMENT	E-5	0.13	0.90	0.12	0.12	1.26	5.00	7.2	0.84									
ROADSIDE AREA	E-5	0.39	0.30	0.12	0.23	7.90	7.90	6.4	1.50									
DI-3B @ E-5	E-4								1.50	77.00	70.40	110	0.0600	15	15.47	14.70	0.12	E-4 TOP = 82.19
PAVEMENT	E-4	0.08	0.90	0.07	0.31	2.54	8.02	6.4	1.96									
PAVEMENT	E-4	0.25	0.90	0.23	0.53	1.05	8.02	6.4	3.40									
DI-3C @ E-4	E-3								3.40	65.20	55.85	77	0.1214	15	22.00	20.91	0.06	E-4 TOP = 75.56
MH-1 @ E-3	E-2								3.40	55.75	45.10	103	0.1034	15	20.30	19.29	0.09	E-3 RIM = 65.50
LOT AREA	E-2	1.38	0.42	0.58	1.11	1.71	8.17	6.4	7.06									
MH-1 @ E-2	E-1								7.06	45.00	43.90	56	0.0196	15	8.85	8.41	0.11	E-2 RIM = 50.50
MH-1 @ E-1	E-0								7.06	41.00	39.70	65	0.0200	15	8.93	8.48	0.13	E-1 RIM = 48.50
MH-1 @ E-0	E-00	2.23							7.06	39.54	39.00	27	0.0200	15	8.93	8.48	0.05	E-0@46.5/ E-00 WSE@43.0
SYSTEM "F" WINDY BRANCH																		
WOODS AND LOT	F-4	3.02	0.30	0.91	0.91	24.40	24.40	4.0	3.65									
DI-1/DI-7 @ F-4	F-3								3.65	81.00	76.60	110	0.0400	15	12.63	12.00	0.15	F-4 TOP 86.00
PAVEMENT	F-3	0.13	0.90	0.12	0.12	2.21	24.55	4.0	0.47									
SHOULDER	F-3	0.14	0.30	0.04	0.16	0.84	24.55	4.0	0.64									
PAVEMENT	F-3	0.04	0.90	0.04	0.20	1.24	24.55	4.0	0.78									
DI-3C @ F-3	F-2								0.78	80.30	80.00	30	0.0100	15	6.31	6.00	0.08	F-3 TOP = 86.28
PAVEMENT	F-2	0.13	0.90	0.12	0.31	2.89	24.64	4.0	1.25									
PAVEMENT	F-2	0.04	0.90	0.04	0.35	1.24	24.64	4.0	1.40									
DI-3C @ F-2	F-1								5.05	76.28	66.00	54	0.1904	15	27.55	26.18	0.03	F-2 TOP = 86.28
DROP MH-1 @ F-1	F-0	3.50							5.05	58.00	56.00	50	0.0400	15	12.63	12.00	0.07	F-1 RIM = 71.00
SYSTEM "G" WINDY BRANCH																		
PAVEMENT 17+00 - 21+50 L	G-4	0.22	0.90	0.20	0.20	3.48	5.00	7.2	1.43									
LOT / SHOULDER	G-4	0.18	0.30	0.05	0.25	5.64	5.64	7.0	1.77									
LOT / SHOULDER	G-4	0.21	0.30	0.06	0.32	3.65	5.64	7.0	2.21									
PAVEMENT 17+00 - 21+50 L	G-4	0.19	0.90	0.17	0.49	3.48	5.64	7.0	3.41									
DI - 3C @ G-4	G-3								3.41	64.00	59.00	100	0.0500	15	14.12	13.42	0.12	G-4 TOP = 68.04
DROP MH-1 @ G-3	G-2								3.41	55.00	40.00	100	0.1500	15	24.45	23.24	0.07	G-3 RIM = 69.00
DROP MH-1 @ G-2	G-1	0.80							3.41	36.50	36.00	50	0.0100	15	6.31	6.00	0.14	G-2 RM = 44.00
SYSTEM "H" WINTER WOOD																		
PAVEMENT	H-5	0.04	0.90	0.04	0.04	1.48	5.00	7.2	0.26									
PAVEMENT	H-5	0.01	0.90	0.01	0.05	0.72	5.00	7.2	0.32									
DI-3B @ H-5	H-4								0.32	91.00	90.70	30	0.0100	15	6.31	6.00	0.08	H-5 TOP = 96.93
PAVEMENT	H-4	0.04	0.90	0.04	0.08	0.25	5.00	7.2	0.58									
LOT / SHOULDER	H-4	0.10	0.30	0.03	0.11	0.38	5.00	7.2	0.80									
PAVEMENT	H-4	0.01	0.90	0.01	0.12	0.72	5.00	7.2	0.86									
SHOULDER	H-4	0.03	0.30	0.01	0.13	0.55	5.00	7.2	0.93									
DI-3C @ H-4	H-3								0.93	90.60	88.30	120	0.0192	15	8.74	8.31	0.24	H-4 TOP = 96.93
MH-1 @ H-3	H-2								0.93	83.00	82.00	50	0.0200	15	8.93	8.48	0.10	H-3 RIM = 95.50
PAVEMENT	H-2	0.06	0.90	0.05	0.18	2.72	5.00	7.2	1.32									
SHOULDER	H-2	0.03	0.30	0.01	0.19	2.72	5.00	7.2	1.38									
PAVEMENT	H-2	0.10	0.90	0.09	0.28	0.86	5.00	7.2	2.03									
DI-3C @ H-2	H-1								2.03	81.00	66.00	75	0.2000	15	28.24	26.83	0.05	H-2 TOP = 93.56
MH-1 @ H-1	H-0	0.42							2.03	62.50	62.00	19	0.0263	15	10.24	9.73	0.03	H-1 RIM = 81
SYSTEM "I" SPLIT WOOD ROAD																		
LOT & PAVING	I-3	1.97	0.41	0.81	0.81	2.62	5.00	7.2	5.82									
DI - 3B/DI-7 @ I-3	I-2								5.82	73.00	72.60	40	0.0100	15	6.31	6.00	0.11	TEMP. DI-7 TOP
DMH-1 @ I-2	I-1								5.82	72.50	70.52	125	0.0158	15	7.95	7.55	0.28	
MH-1 @ I-1	A-1								5.82	70.42	66.22	84	0.0500	15	14.12	13.42	0.10	EXIST. TEMP. SB RISER
MH-1@S.B. RISER	ES-1								19.69	62.00	59.80	66	0.0333	24	40.37	14.98	0.07	EXISTING SB OUTFALL

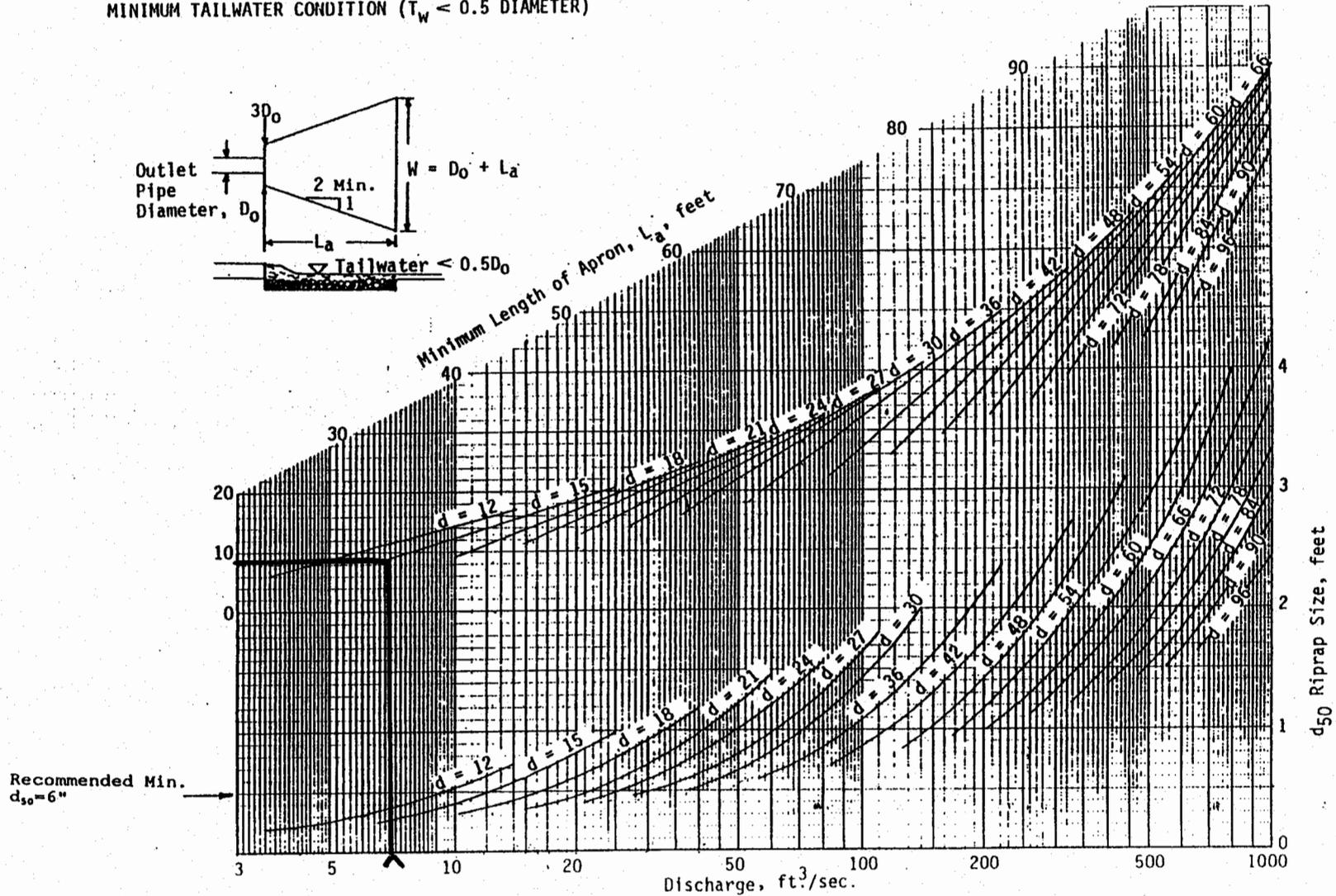
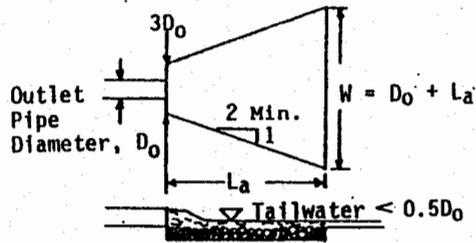
VDOT L&D 229		INVERT ELEVATI		LENGTH	SLOPE	DIAM	RUNOFF	Y _n	V _n	REMARKS
FROM PT. (1)	TO PT. (2)	UPPER (10)	LOWER (11)	ft. (12)	ft/ft (13)	inch (14)	"QRational" (9)	ft.	fps	
SYSTEM "I"		SPLIT WOOD ROAD								
MH-1@S.B. RISER	ES-1	62.00	59.80	66	0.0333	24	19.69	0.47	9.51	A-1 MH RIM = 70.00
MH-1 @ I-1	A-1	70.42	66.22	84	0.0500	15	5.82	0.55	11.13	I-1 MH RIM = 79.17
DMH-I @ I-2	I-1	72.50	70.52	125	0.0158	15	5.82	0.78	7.20	I-2 RIM = 77.22
DI - 3B/DI-7 @ I-3	I-2	73.00	72.60	40	0.0100	15	5.82	0.93	5.96	I-3 TEMP. DI-7 TOP = 77
SYSTEM "H"		WINTER WOOD								
MH-1 @ H-1	H-0	62.50	62.00	19	0.0263	15	2.03	0.37	6.61	H-1 RIM = 73.50
DI-3C @ H-2	H-1	81.00	66.00	75	0.2000	15	2.03	0.22	13.57	H-2 TOP = 93.56
MH-1 @ H-3	H-2	83.00	82.00	50	0.0200	15	0.93	0.32	3.74	H-3 RIM = 95.50
DI-3C @ H-4	H-3	90.60	88.30	120	0.0192	15	0.93	0.32	3.74	H-4 TOP = 96.93
DI-3B @ H-5	H-4	91.00	90.70	30	0.0100	15	0.32	0.19	2.74	H-5 TOP = 96.93
SYSTEM "G"		WINDY BRANCH								
DROP MH-1 @ G-2	G-1	36.50	36.00	50	0.0100	15	3.41	0.65	5.33	G-2 RM = 44.00
DROP MH-1 @ G-3	G-2	55.00	40.00	100	0.1500	15	3.41	0.31	14.27	G-3 RIM = 69.00
DI - 3C @ G-4	G-3	64.00	59.00	100	0.0500	15	3.41	0.41	9.63	G-4 TOP = 68.04
SYSTEM "F"		WINDY BRANCH								
DROP MH-I @ F-1	F-0	58.00	56.00	50	0.0400	15	5.05	0.27	7.17	F-1 RIM = 71.00
DI-3C @ F-2	F-1	76.28	66.00	54	0.1904	15	5.05	0.19	12.32	F-2 TOP = 86.28
DI-3C @ F-3	F-2	80.30	80.00	30	0.0100	15	0.78	0.15	2.50	F-3 TOP = 86.28
DI-1/DI-7 @ F-4	F-2	81.00	76.60	110	0.0400	15	3.65	0.23	6.49	F-4 TOP 86.00
SYSTEM "E"		SAPLING DRIVE								E-00 10YR WSE @ 43.00
MH-1 @ E-0	E-00	39.54	39.00	27	0.0200	15	7.06	0.36	6.25	E-0 RIM= 46.50
MH-1 @ E-1	E-0	41.00	39.70	65	0.0200	15	7.06	0.36	6.25	E-1 RIM = 48.50
MH-I @ E-2	E-1	45.00	43.90	56	0.0196	15	7.06	0.37	6.20	E-2 RIM = 50.50
MH-1 @ E-3	E-2	55.75	45.10	103	0.1034	15	3.40	0.18	8.83	E-3 RIM = 65.50
DI-3C @ E-4	E-3	65.20	57.50	55	0.1400	15	3.40	0.32	13.90	E-4 TOP = 75.56
DI-3B @ E-5	E-4	77.00	70.40	110	0.0600	15	1.50	0.26	8.12	E-4 TOP = 82.19

HYDRAULIC GRADELINE CALCULATION

STONEHOUSE SECTION VB, PHASE 3

INLET STATION	Outlet Water Surface	FRICTION LOSS IN PIPE							JUNCTION LOSS										H Adjusted	Inlet Water Surface Elevation	Rim Elevation	
		D _o	Q _o	L _o	n _o	S _{to} / S _o	H _r	V _o	H _o	Q _i	V _i	Q _i x V _i	V ² / 2g	H _i	Δ	H _{delta}	H _t	.3 x H _t				0.5 x H _t
1	2	3	4	5	5A	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22
SYSTEM "I"	SPLIT WOOD ROAD																					
DMH-1 @ RISER FROM SYS. "A"	60.80	24	19.89	66	0.013	0.0076	0.500	6.27	0.15	5.82	11.13	64.78	0.49	0.17	69	0.27	0.80	0.18	-0.30	0.98	61.78	A-1 MH RIM = 70.00
DMH-1 @ I-1	61.78	15	5.82	84	0.013	0.0081	0.682	4.74	0.09	5.82	7.2	41.90	0.80	0.28	28	0.18	0.55	0.16	-0.27	1.12	62.90	I-1 MH RIM = 79.17
DMH-1 @ I-2	62.90	15	5.82	125	0.013	0.0081	1.015	4.74	0.09	5.82	5.96	34.69	0.55	0.19	90	0.39	0.67	0.20	-0.33	1.55	64.44	I-2 RIM = 77.22
DI-3B/DI-7 @ I-3	64.44	15	5.82	40	0.013	0.0081	0.325	4.74	0.09			0.00	0.00	0.00	0	0.00	0.09	0.03	-0.04	0.39	64.84	TEMP. DI-7 TOP = 77
SYSTEM "H"	WINTER WOOD																					
MH-1 @ H-1	63.00	15	2.03	19	0.013	0.0010	0.019	1.65	0.01	2.03	13.57	27.55	2.86	1.00	43	1.09	2.10	0.63	-1.05	1.70	64.70	H-1 RIM = 73.50
DI-3C @ H-2	64.70	15	2.03	75	0.013	0.0010	0.074	1.65	0.01	0.93	3.74	3.48	0.22	0.08	77	0.00	0.09	0.03	-0.04	0.14	64.84	H-2 TOP = 93.56
MH-1 @ H-3	64.84	15	0.93	50	0.013	0.0002	0.010	0.76	0.00	0.93	3.74	3.48	0.22	0.08	14	0.00	0.08	0.02	-0.04	0.07	64.91	H-3 RIM = 95.50
DI-3C @ H-4	64.91	15	0.93	119	0.013	0.0002	0.025	0.76	0.00	0.32	2.74	0.88	0.12	0.04	90	0.08	0.12	0.04	-0.06	0.12	65.04	H-4 TOP = 96.93
DI-3B @ H-5	65.04	15	0.32	25	0.013	0.0000	0.001	0.26	0.00			0.00	0.00	0.00	0	0.00	0.00	0.00	-0.00	0.00	65.04	H-5 TOP = 96.93
SYSTEM "G"	WINDY BRANCH																					
DROP MH-1 @ G-2	37.00	15	3.41	50	0.013	0.0028	0.139	2.78	0.03	3.41	14.27	48.66	3.16	1.11	71	0.00	1.14	0.34	-0.57	1.05	38.05	G-2 RM = 44.00
DROP MH-1 @ G-3	38.05	15	3.41	100	0.013	0.0028	0.279	2.78	0.03	3.41	9.63	32.84	1.44	0.50	23	0.23	0.76	0.23	-0.38	0.89	38.94	G-3 RIM = 69.00
DI-3C @ G-4	38.94	15	3.41	100	0.013	0.0028	0.279	2.78	0.03			0.00	0.00	0.00	0	0.00	0.03	0.01	-0.01	0.30	39.24	G-4 TOP = 68.04
SYSTEM "F"	WINDY BRANCH																					
DROP MH-1 @ F-1	57.00	15	5.05	50	0.013	0.0061	0.306	4.12	0.07	5.05	12.32	62.22	2.36	0.82	32	0.66	1.55	0.47	-0.78	1.55	58.55	F-1 RIM = 71.00
DI-3C @ F-2	58.55	15	5.05	64	0.013	0.0061	0.330	4.12	0.07	0.78	2.5	1.95	0.10	0.03	0	0.00	0.10	0.03	-0.05	0.41	58.96	F-2 TOP = 86.28
DI-3C @ F-3	58.96	15	0.78	30	0.013	0.0001	0.004	0.64	0.00	3.65	6.49	23.69	0.65	0.23	80	0.43	0.66	0.20	-0.33	0.53	59.49	F-3 TOP = 86.28
DI-1/DI-7 @ F-4	59.49	15	3.65	60	0.013	0.0032	0.192	2.97	0.03			0.00	0.00	0.00	0	0.00	0.03	0.01	-0.02	0.22	59.71	F-4 TOP 86.00
SYSTEM "E"	SAPLING DRIVE																					
MH-1 @ E-0	43.00	15	7.06	30	0.013	0.0119	0.358	5.75	0.13	7.06	6.25	44.13	0.61	0.21	80	0.40	0.74	0.22	-0.37	0.95	43.95	E-00 10YR WSE @ 43.00 E-0 RIM= 46.50
MH-1 @ E-1	43.95	15	7.06	65	0.013	0.0119	0.776	5.75	0.13	7.06	6.2	43.77	0.60	0.21	65	0.33	0.67	0.20	-0.33	1.31	45.26	E-1 RIM = 48.50
MH-1 @ E-2	45.26	15	7.06	35	0.013	0.0119	0.418	5.75	0.13	3.4	8.83	30.02	1.21	0.42	60	0.67	1.22	0.37	-0.61	1.39	46.65	E-2 RIM = 50.50
MH-1 @ E-3	46.65	15	3.4	125	0.013	0.0028	0.346	2.77	0.03	3.4	13.9	47.26	3.00	1.05	0	0.00	1.08	0.32	-0.54	1.21	47.86	E-3 RIM = 65.50
DI-3C @ E-4	47.86	15	3.4	65	0.013	0.0028	0.152	2.77	0.03	1.5	8.12	12.18	1.02	0.36	18	0.10	0.49	0.15	-0.25	0.54	48.41	E-4 TOP = 75.56
DI-3B @ E-5	48.41	15	1.5	110	0.013	0.0005	0.059	1.22	0.01			0.00	0.00	0.00	0	0.00	0.01	0.00	-0.00	0.06	48.47	E-4 TOP = 82.19

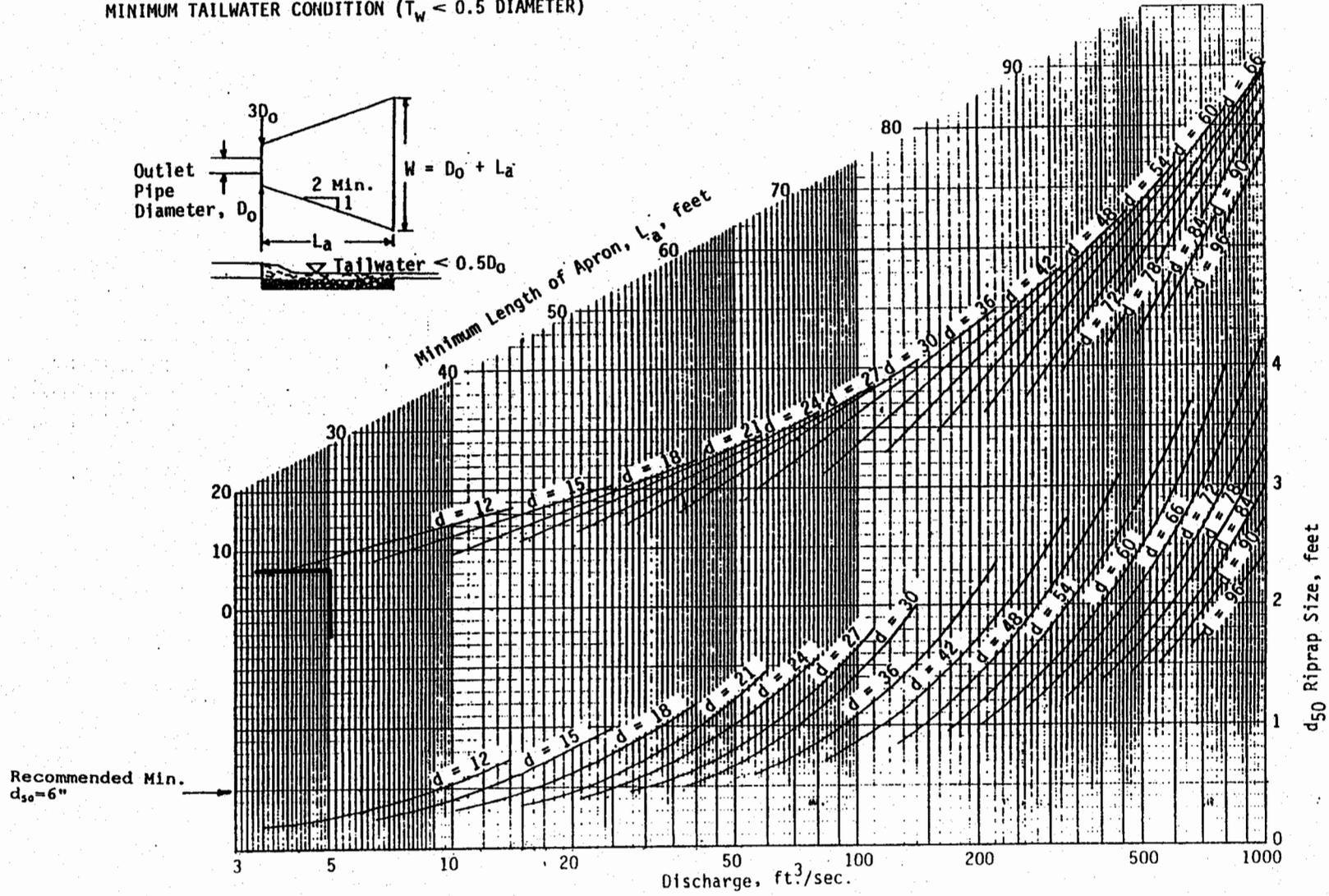
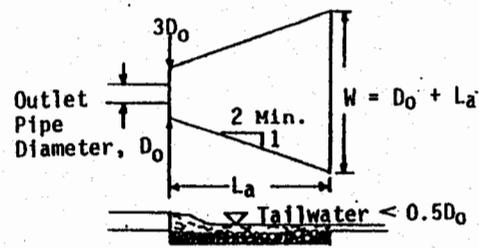
DESIGN OF OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL
 MINIMUM TAILWATER CONDITION ($T_w < 0.5$ DIAMETER)



SYS. "E"
 $D_0 = 15''$
 $Q_{10} = 7.06$
 USE $L_a = 10'$

Source: USDA-SCS

DESIGN OF OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL
MINIMUM TAILWATER CONDITION ($T_w < 0.5$ DIAMETER)

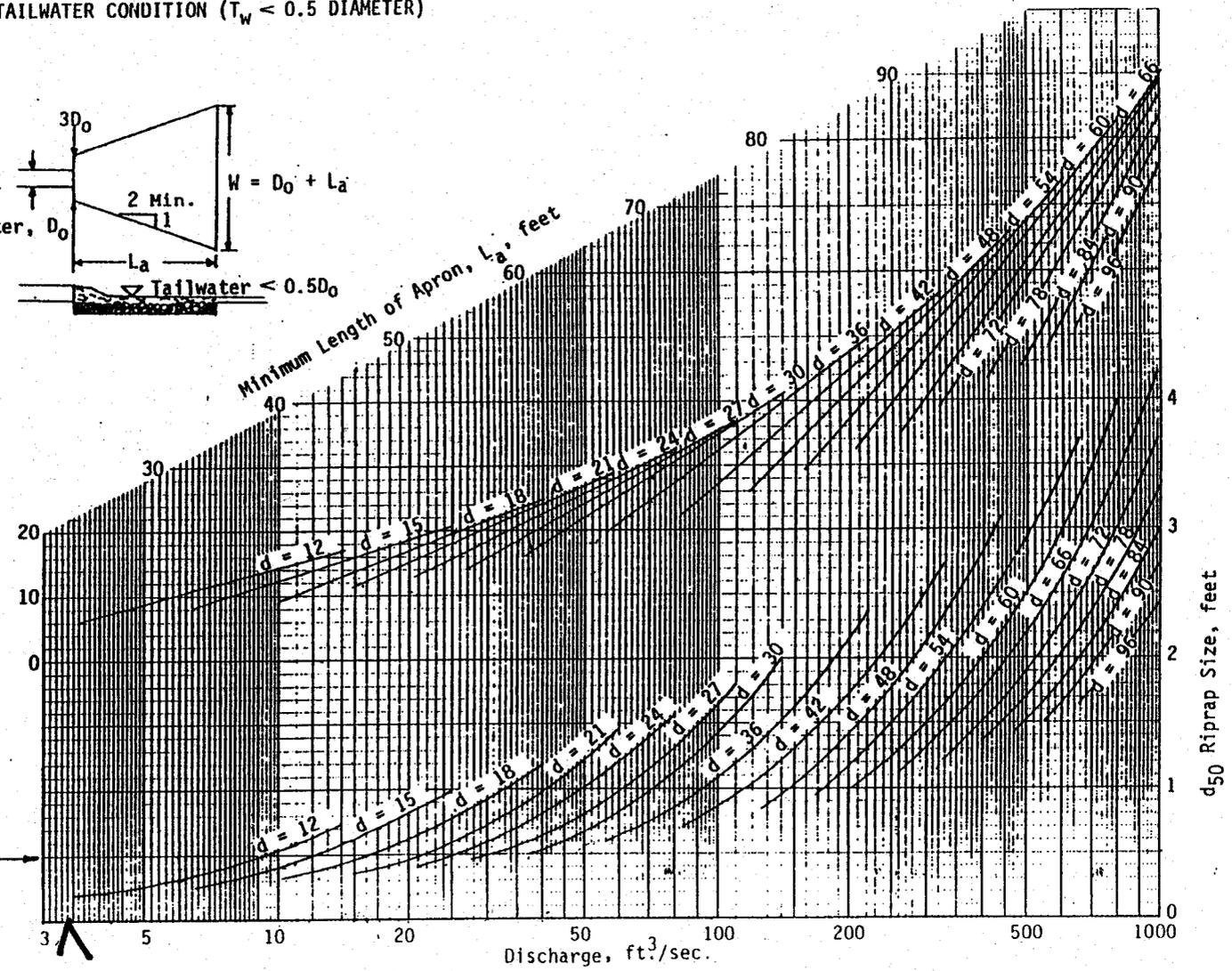
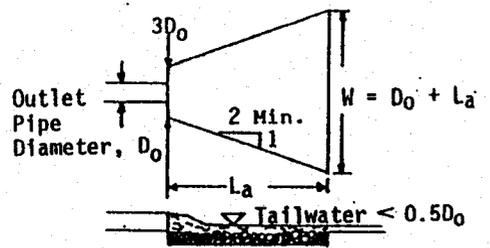


III - 164

Plate 3.18-3

SYS "F" $Q_{10} = 5.05$ $D_0 = 15$
 USE $L_a = 10'$

DESIGN OF OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL
 MINIMUM TAILWATER CONDITION ($T_w < 0.5$ DIAMETER)



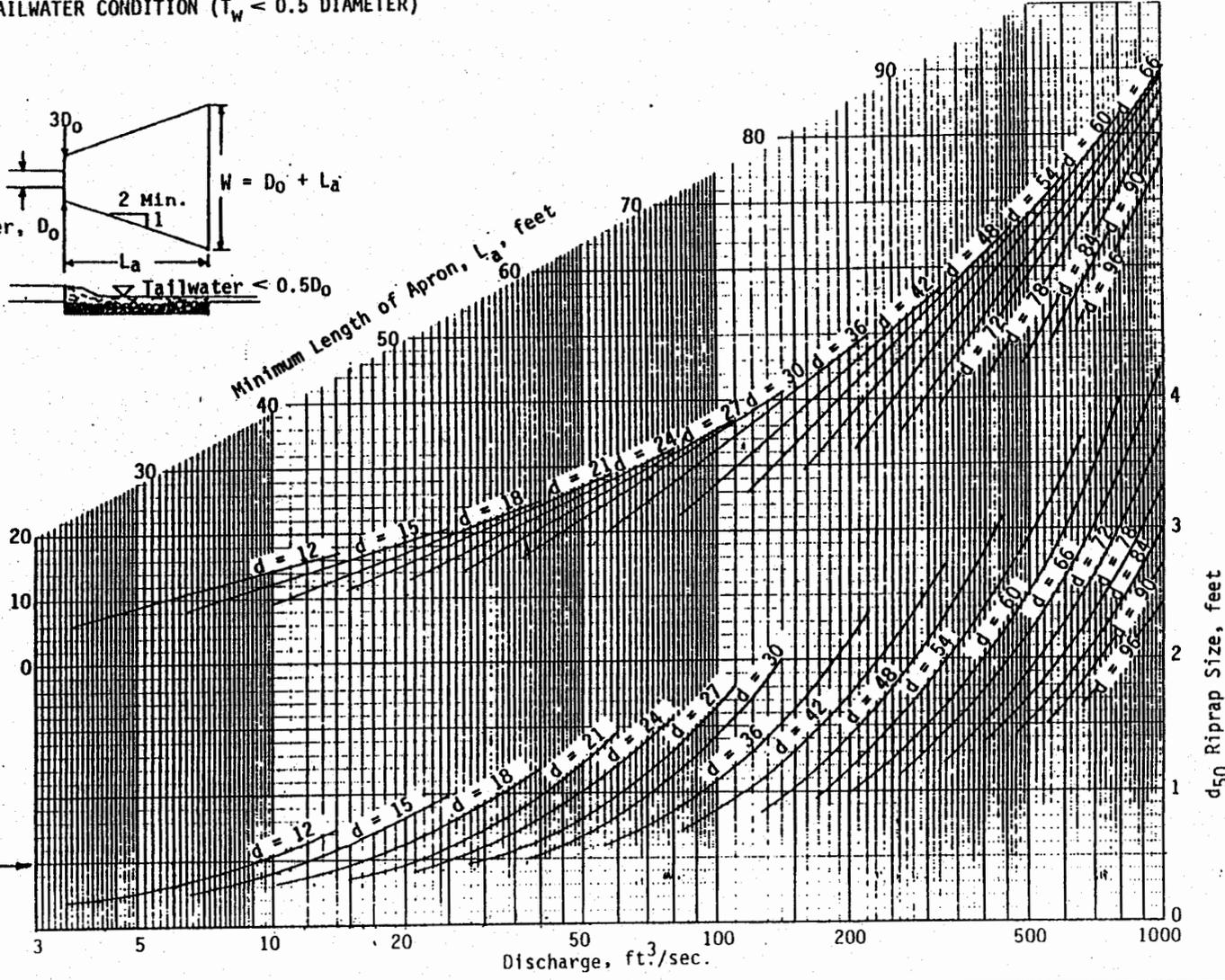
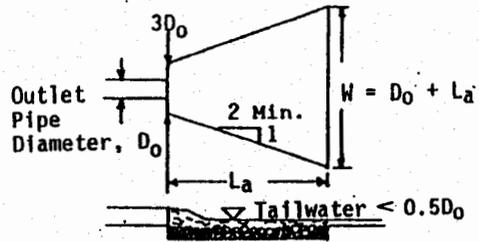
III - 164

Plate 3.18-3

3.18

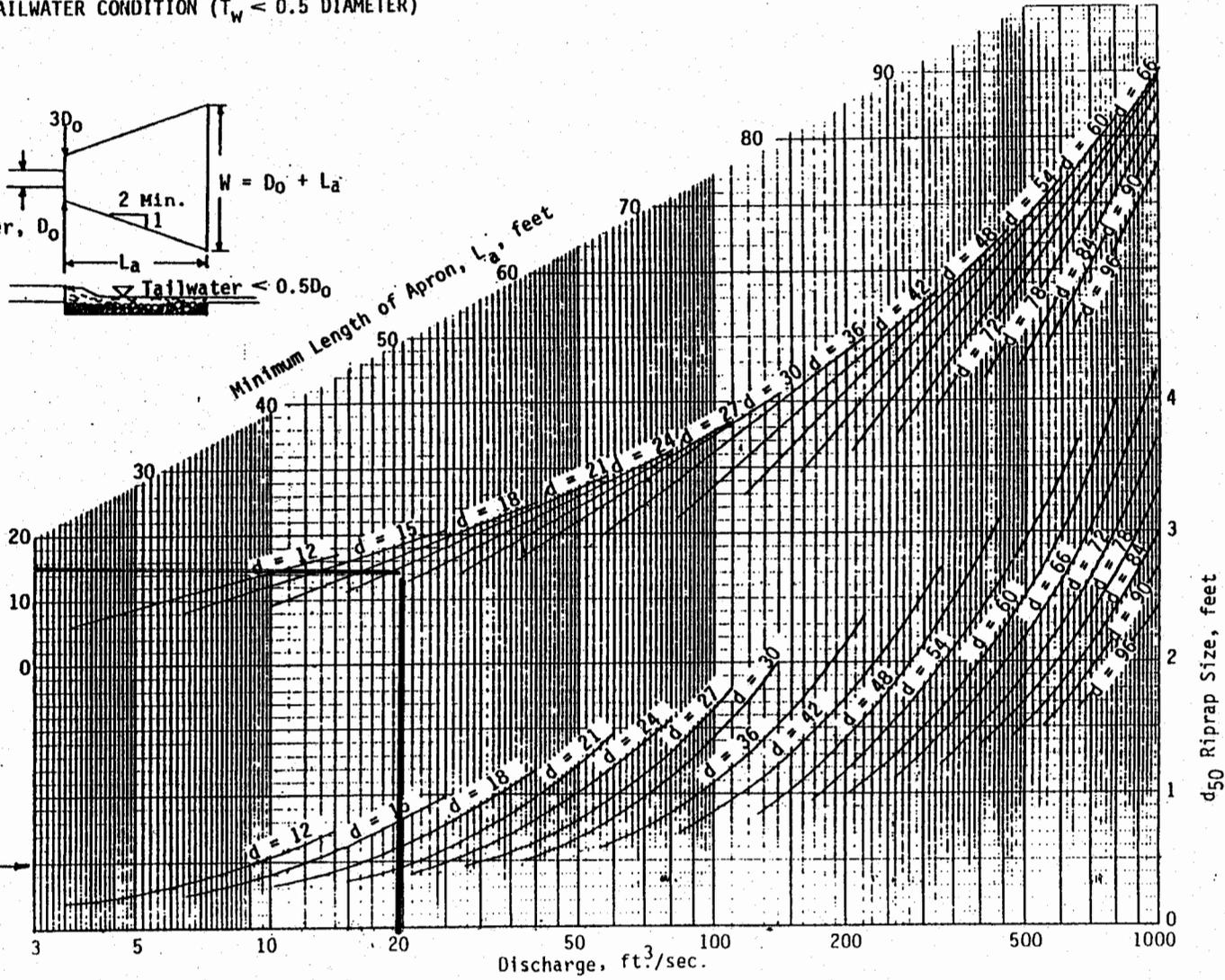
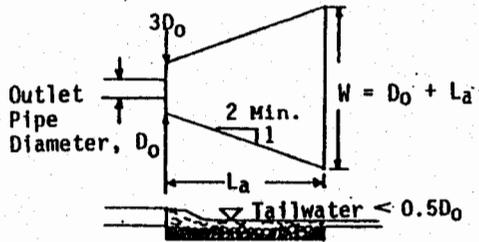
SYS. "G" $Q_{10} = 3.41$ $D_o = 15"$
 Use $L_a = 10'$

DESIGN OF OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL
 MINIMUM TAILWATER CONDITION ($T_w < 0.5$ DIAMETER)



SYS "H" $Q_{10} = 2.03$ $D_o = 15"$
 USE $L_a = 10'$

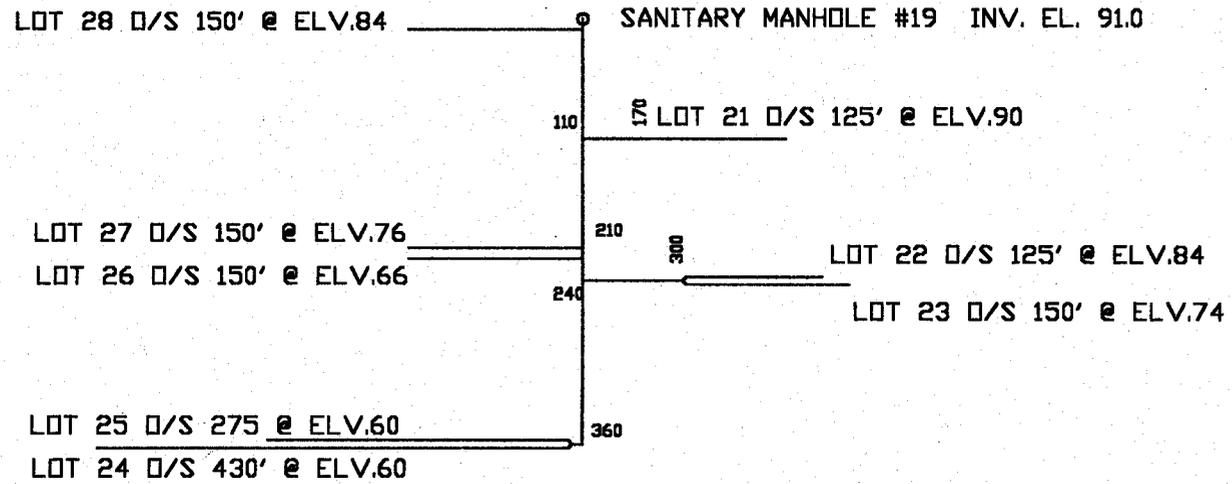
DESIGN OF OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL
 MINIMUM TAILWATER CONDITION ($T_w < 0.5$ DIAMETER)



SYS "I"
 $Q_{10} = 19.69$ $D_o = 24$
 USE $L_a = 20'$

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LOW PRESSURE FORCE MAIN SCHEMATIC
SAPLING DRIVE, Stonehouse, L. L. C.
JAMES CITY COUNTY



SEWAGE PUMPING STATION DESIGN CALCULATIONS:

PROJECT:
STONEHOUSE, L. L. C.
SECTION VB, Phase 3
SAPLING DRIVE
JAMES CITY COUNTY, VA

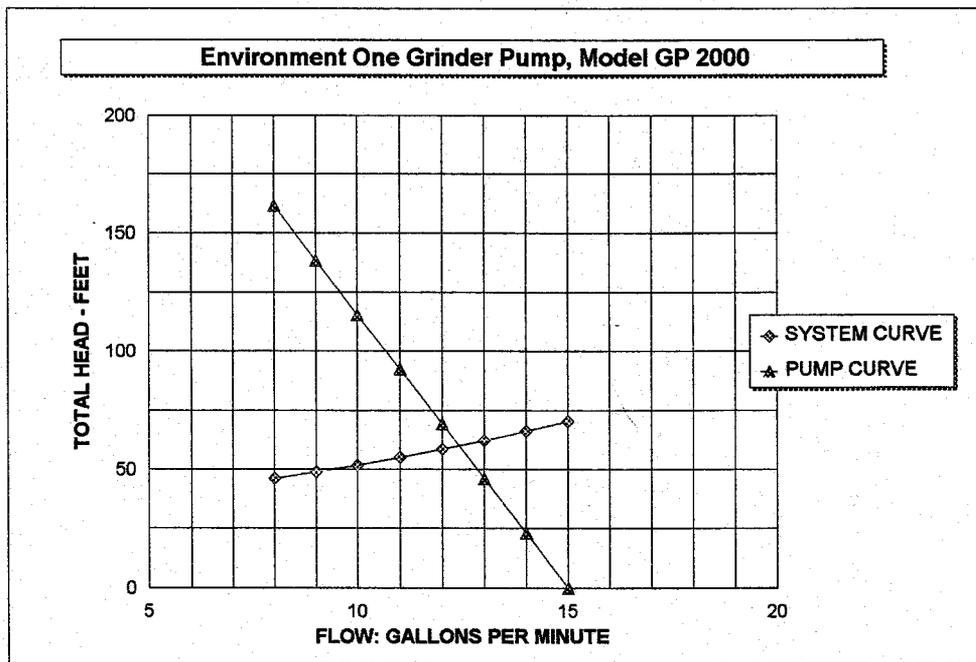
DATE: 07/26/99
Prepared by: RS PHILLIPS
FILE NO.: 1960038-111.73

LOT 24 PUMP / NO OTHER PUMPS RUNNING

PUMP TOTAL DYNAMIC HEAD CALCULATION:

PUMP ON LIQUID ELEV.:	56	FEET						
PUMP OFF LIQUID ELEV.:	55.67	FEET						
HIGH POINT ELEVATION :	91	FEET						
CONNECTION ELEVATION :	91	FEET						
PRESSURE HEAD AT CONNECTION:	0	FEET						
STATIC HEAD :	35.33	FEET						
			SEG.#1	SEG.#2	SEG.#3			
NUMBER OF PUMPS SIMULTANEOUSLY :	1		1	1	1			
LENGTH OF FORCE MAIN :	430		120	240		FEET		
EQUIVALENT LENGTH OF FITTINGS :	29		12	12		FEET		
PIPE DIAMETER :	1.25		1.5	1.5		INCHES		
HAZEN-WILLIAMS CONSTANT :	140		140	140				
DESIGN DISCHARGE FLOW RATE :	10		10	10		GALLONS PER MINUTE		
FLOW VELOCITY =	2.61		1.82	1.82		FEET PER SECOND		
PIPE FRICTION HEAD =	11.47		1.32	2.64		FEET		
TOTAL DYNAMIC HEAD =	50.75	FEET						

FLOW G.P.M. at PUMP	T.D.H. FEET at PUMP	Environment One Grinder Pump, Model GP 2000
8	46.22	162
9	48.88	139
10	51.79	116
11	54.96	92
12	58.39	69
13	62.07	46
14	66.00	23
15	70.18	0



OPERATING FLOW : 12.41 G.P.M @ PUMP
OPERATING HEAD : 58.32 FEET +/-
1 1/4" FORCE MAIN VELOCITY : 3.24 F.P.S.
1 1/2" FORCE MAIN VELOCITY : 2.25 F.P.S.

SEWAGE PUMPING STATION DESIGN CALCULATIONS:
PROJECT:

STONEHOUSE, L. L. C.
 SECTION VB, Phase 3
 SAPLING DRIVE
 JAMES CITY COUNTY, VA

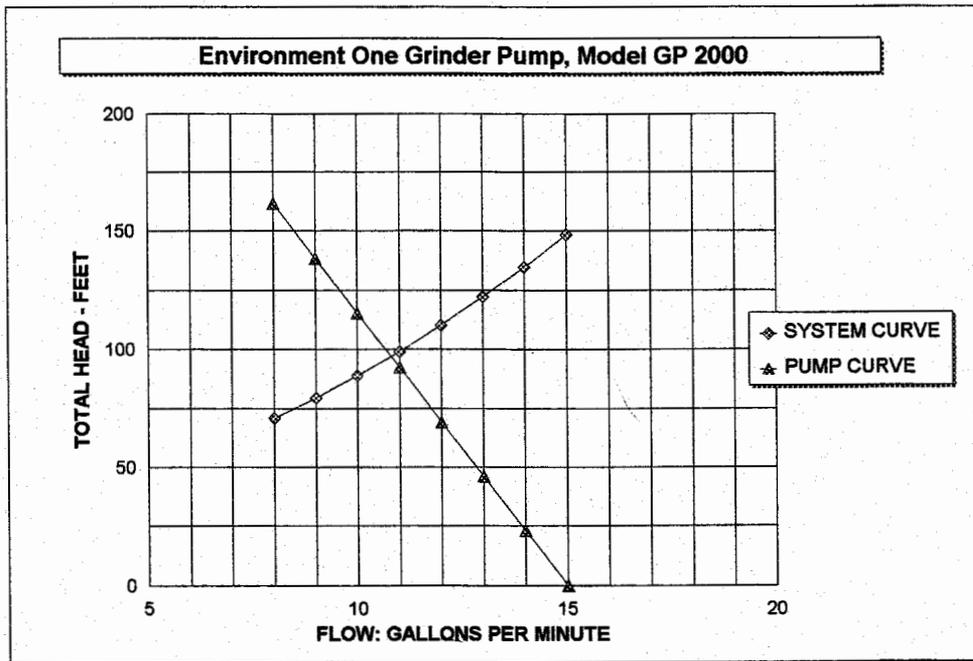
DATE: 07/26/99
 Prepared by: RS PHILLIPS
 FILE NO.: 1960038-111.73

LOT 24 PUMP / PUMPS RUNNING : LOTS 25, 22 & 23

PUMP TOTAL DYNAMIC HEAD CALCULATION:

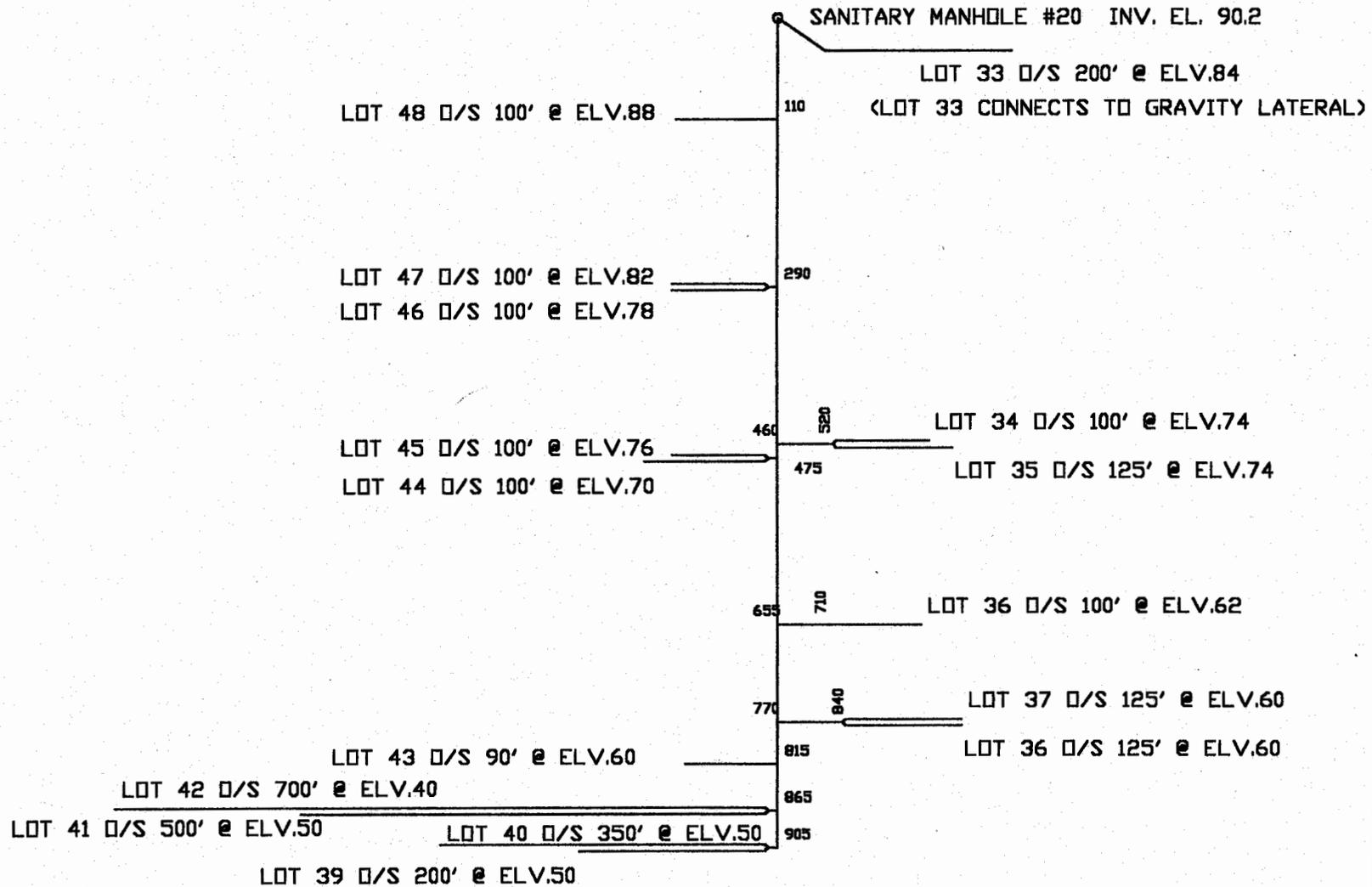
PUMP ON LIQUID ELEV.:	56	FEET			
PUMP OFF LIQUID ELEV.:	55.67	FEET			
HIGH POINT ELEVATION :	91	FEET			
CONNECTION ELEVATION :	91	FEET			
PRESSURE HEAD AT CONNECTION:	0	FEET			
STATIC HEAD :	35.33	FEET			
	SEG.#1	SEG.#2	SEG.#3		
NUMBER OF PUMPS SIMULTANEOUSLY :	1	2	4		
LENGTH OF FORCE MAIN :	430	120	240	FEET	
EQUIVALENT LENGTH OF FITTINGS :	29	12	12	FEET	
PIPE DIAMETER :	1.25	1.5	1.5	INCHES	
HAZEN-WILLIAMS CONSTANT :	140	140	140		
DESIGN DISCHARGE FLOW RATE :	10	20	40	GALLONS PER MINUTE	
FLOW VELOCITY =	2.61	3.63	7.26	FEET PER SECOND	
PIPE FRICTION HEAD =	11.47	4.75	34.26	FEET	
TOTAL DYNAMIC HEAD =	85.82			FEET	

FLOW G.P.M. at PUMP	T.D.H. FEET at PUMP	Environment One Grinder Pump, Model GP 2000
8	70.67	162
9	79.28	139
10	88.74	116
11	99.03	92
12	110.16	69
13	122.10	46
14	134.85	23
15	148.40	0



OPERATING FLOW : 10.80 G.P.M @ PUMP
 OPERATING HEAD : 93.55 FEET +/-
 1 1/4" FORCE MAIN VELOCITY : 2.82 F.P.S.
 1 1/2" FORCE MAIN VELOCITY : 7.84 F.P.S.

**LOW PRESSURE FORCE MAIN SCHEMATIC
 WINDY BRANCH DRIVE, Stonehouse, L. L. C.
 JAMES CITY COUNTY**



SEWAGE PUMPING STATION DESIGN CALCULATIONS:
PROJECT:

STONEHOUSE, L. L. C.
 SECTION VB, Phase 3
 WINDY BRANCH DRIVE
 JAMES CITY COUNTY, VA

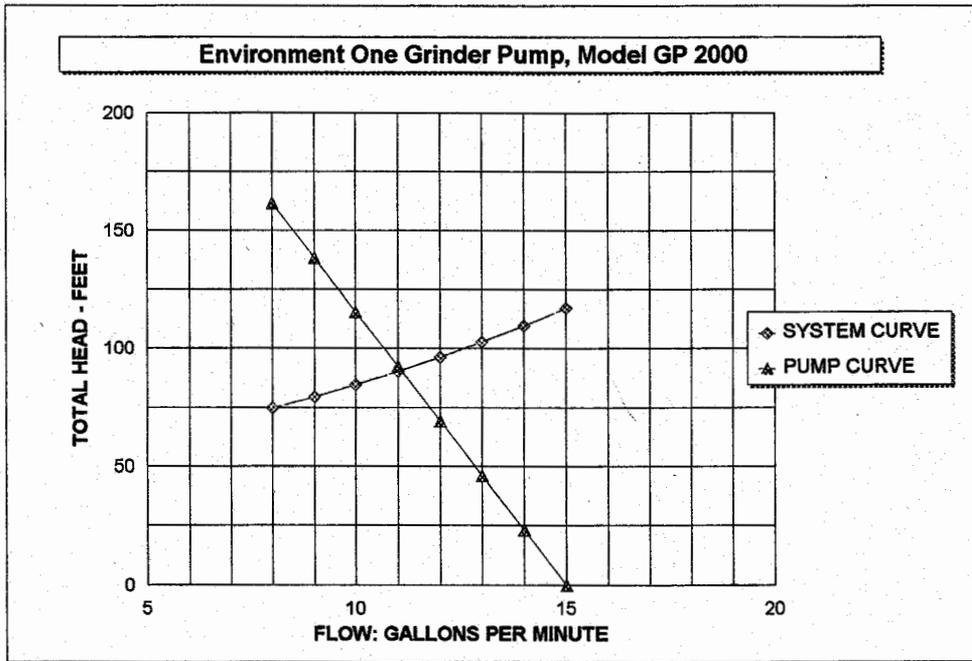
DATE: 07/26/99
Prepared by: RS PHILLIPS
FILE NO.: 1960038-111.73

LOT 42/ NO OTHER PUMPS RUNNING

PUMP TOTAL DYNAMIC HEAD CALCULATION:

PUMP ON LIQUID ELEV.:	36	FEET						
PUMP OFF LIQUID ELEV.:	35.67	FEET						
HIGH POINT ELEVATION :	91	FEET						
CONNECTION ELEVATION :	91	FEET						
PRESSURE HEAD AT CONNECTION.:	0	FEET						
STATIC HEAD :	55.33	FEET						
	SEG.#1	SEG.#2	SEG.#3					
NUMBER OF PUMPS SIMULTANEOUSLY :	1	1	1					
LENGTH OF FORCE MAIN :	700	405	460	FEET				
EQUIVALENT LENGTH OF FITTINGS :	29	12	12	FEET				
PIPE DIAMETER :	1.25	1.5	1.5	INCHES				
HAZEN-WILLIAMS CONSTANT :	140	140	140					
DESIGN DISCHARGE FLOW RATE :	10	10	10	GALLONS PER MINUTE				
FLOW VELOCITY =	2.61	1.82	1.82	FEET PER SECOND				
PIPE FRICTION HEAD =	18.67	4.45	5.05	FEET				
TOTAL DYNAMIC HEAD =	83.5			FEET				

FLOW G.P.M. at PUMP	T.D.H. FEET at PUMP	<i>Environment One Grinder Pump, Model GP 2000</i>
8	74.66	162
9	79.37	139
10	84.54	116
11	90.17	92
12	96.26	69
13	102.79	46
14	109.76	23
15	117.17	0



OPERATING FLOW : 11.08 G.P.M @ PUMP
OPERATING HEAD : 89.37 FEET +/-
1 1/4" FORCE MAIN VELOCITY : 2.90 F.P.S.
1 1/2" FORCE MAIN VELOCITY : 2.01 F.P.S.

SEWAGE PUMPING STATION DESIGN CALCULATIONS:
PROJECT:

STONEHOUSE, L. L. C.
SECTION VB, Phase 3
WINDY BRANCH DRIVE
JAMES CITY COUNTY, VA

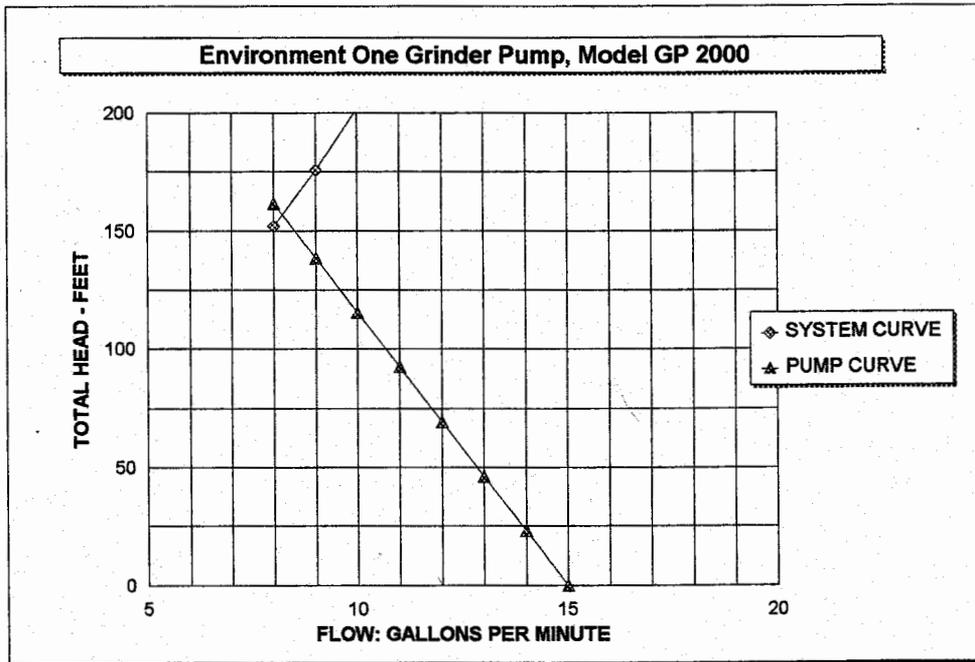
DATE: 07/26/99
Prepared by: RS PHILLIPS
FILE NO.: 1960038-111.73

LOT 42/ PUMPS RUNNING: 39, 40, & 41

PUMP TOTAL DYNAMIC HEAD CALCULATION:

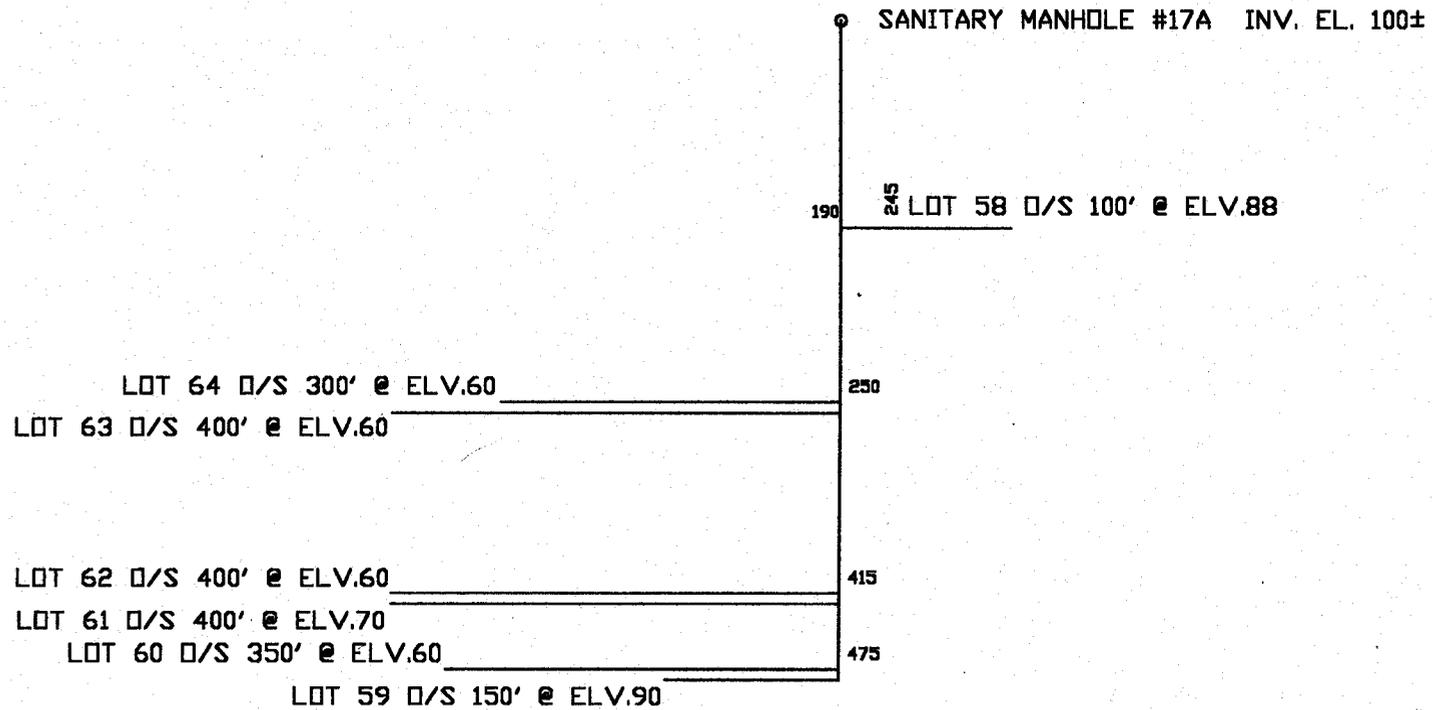
PUMP ON LIQUID ELEV.:	36	FEET					
PUMP OFF LIQUID ELEV.:	35.67	FEET					
HIGH POINT ELEVATION :	91	FEET					
CONNECTION ELEVATION :	91	FEET					
PRESSURE HEAD AT CONNECTION:	0	FEET					
STATIC HEAD :	55.33	FEET					
	SEG.#1	SEG.#2	SEG.#3				
NUMBER OF PUMPS SIMULTANEOUSLY :	1	4	4				
LENGTH OF FORCE MAIN :	700	405	460	FEET			
EQUIVALENT LENGTH OF FITTINGS :	29	12	12	FEET			
PIPE DIAMETER :	1.25	1.5	1.5	INCHES			
HAZEN-WILLIAMS CONSTANT :	140	140	140				
DESIGN DISCHARGE FLOW RATE :	10	40	40	GALLONS PER MINUTE			
FLOW VELOCITY =	2.61	7.26	7.26	FEET PER SECOND			
PIPE FRICTION HEAD =	18.67	57.82	65.67	FEET			
TOTAL DYNAMIC HEAD =	197.5 FEET						

FLOW G.P.M. at PUMP	T.D.H. FEET at PUMP	<i>Environment One Grinder Pump, Model GP 2000</i>
8	152.15	162
9	175.72	139
10	201.63	116
11	229.84	92
12	260.31	69
13	293.03	46
14	327.96	23
15	365.07	0



OPERATING FLOW : 8.20 G.P.M @ PUMP
OPERATING HEAD : 153.91 FEET +/-
1 1/4" FORCE MAIN VELOCITY : 2.15 F.P.S.
1 1/2" FORCE MAIN VELOCITY : 5.96 F.P.S.

**LOW PRESSURE FORCE MAIN SCHEMATIC
WINTER WOOD LANE, Stonehouse, L. L. C.
JAMES CITY COUNTY**



SEWAGE PUMPING STATION DESIGN CALCULATIONS:
PROJECT:

STONEHOUSE, L. L. C.
SECTION VB, Phase 3
WINTER WOOD DRIVE
JAMES CITY COUNTY, VA

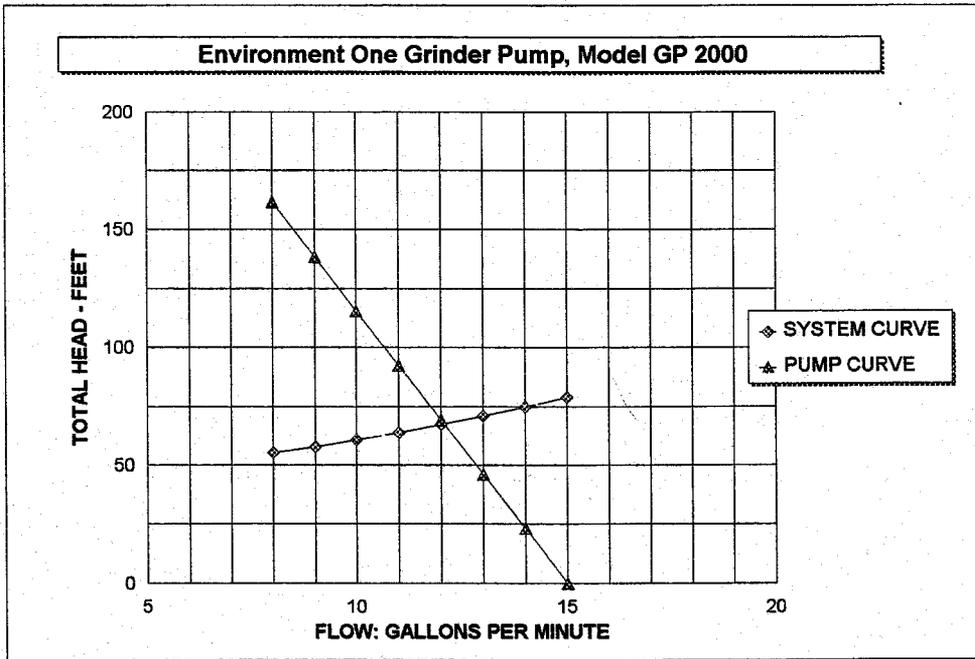
DATE: 07/26/99
Prepared by: RS PHILLIPS
FILE NO.: 1960038-111.73

LOT 62 / NO OTHER PUMPS RUNNING

PUMP TOTAL DYNAMIC HEAD CALCULATION:

PUMP ON LIQUID ELEV.:	56	FEET					
PUMP OFF LIQUID ELEV.:	55.67	FEET					
HIGH POINT ELEVATION :	100	FEET					
CONNECTION ELEVATION :	100	FEET					
PRESSURE HEAD AT CONNECTION:	0	FEET					
STATIC HEAD :	44.33	FEET					
	SEG.#1	SEG.#2	SEG.#3				
NUMBER OF PUMPS SIMULTANEOUSLY :	1	1	1				
LENGTH OF FORCE MAIN :	400	165	250	FEET			
EQUIVALENT LENGTH OF FITTINGS :	29	12	12	FEET			
PIPE DIAMETER :	1.25	1.5	1.5	INCHES			
HAZEN-WILLIAMS CONSTANT :	140	140	140				
DESIGN DISCHARGE FLOW RATE :	10	10	10	GALLONS PER MINUTE			
FLOW VELOCITY =	2.61	1.82	1.82	FEET PER SECOND			
PIPE FRICTION HEAD =	10.67	1.81	2.75	FEET			
TOTAL DYNAMIC HEAD =	59.56	FEET					

FLOW G.P.M. at PUMP	T.D.H. FEET at PUMP	<i>Environment One Grinder Pump, Model GP 2000</i>
8	55.09	162
9	57.71	139
10	60.59	116
11	63.73	92
12	67.12	69
13	70.76	46
14	74.64	23
15	78.77	0



OPERATING FLOW : 12.08 G.P.M @ PUMP
OPERATING HEAD : 65.94 FEET +/-
1 1/4" FORCE MAIN VELOCITY : 3.16 F.P.S.
1 1/2" FORCE MAIN VELOCITY : 2.19 F.P.S.

SEWAGE PUMPING STATION DESIGN CALCULATIONS:
PROJECT:

STONEHOUSE, L. L. C.
SECTION VB, Phase 3
WINTER WOOD DRIVE
JAMES CITY COUNTY, VA

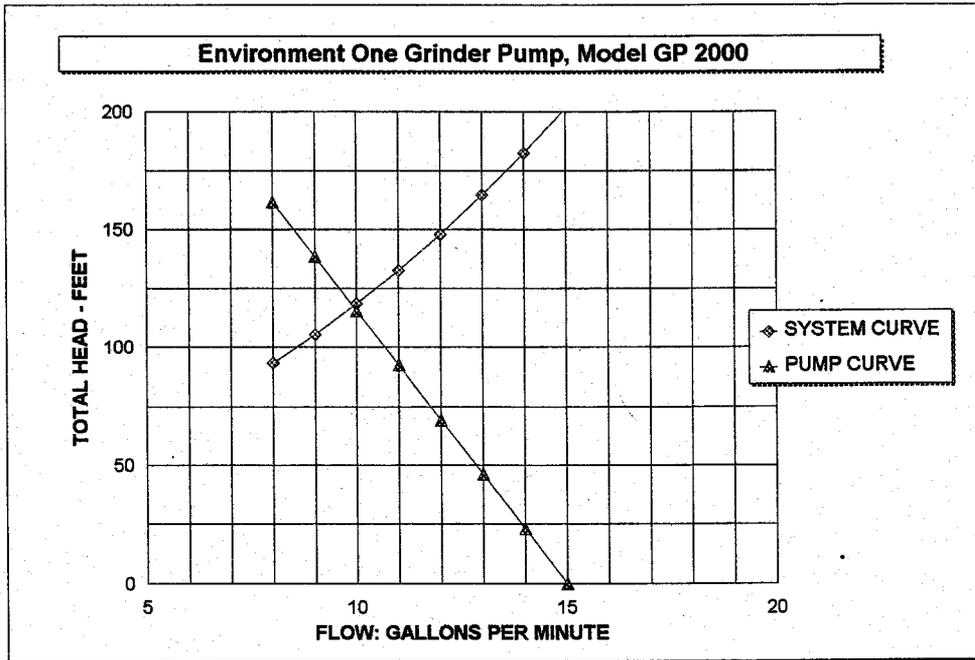
DATE: 07/26/99
Prepared by: RS PHILLIPS
FILE NO.: 1960038-111.73

LOT 62 / PUMPS RUNNING: LOTS 59, 60 & 61

PUMP TOTAL DYNAMIC HEAD CALCULATION:

PUMP ON LIQUID ELEV.:	56	FEET						
PUMP OFF LIQUID ELEV.:	55.67	FEET						
HIGH POINT ELEVATION :	100	FEET						
CONNECTION ELEVATION :	100	FEET						
PRESSURE HEAD AT CONNECTION.:	0	FEET						
STATIC HEAD :	44.33	FEET						
	SEG.#1	SEG.#2	SEG.#3					
NUMBER OF PUMPS SIMULTANEOUSLY :	1	4	4					
LENGTH OF FORCE MAIN :	400	165	250	FEET				
EQUIVALENT LENGTH OF FITTINGS :	29	12	12	FEET				
PIPE DIAMETER :	1.25	1.5	1.5	INCHES				
HAZEN-WILLIAMS CONSTANT :	140	140	140					
DESIGN DISCHARGE FLOW RATE :	10	40	40	GALLONS PER MINUTE				
FLOW VELOCITY =	2.61	7.26	7.26	FEET PER SECOND				
PIPE FRICTION HEAD =	10.67	23.56	35.69	FEET				
TOTAL DYNAMIC HEAD =	114.2	FEET						

FLOW G.P.M. at PUMP	T.D.H. FEET at PUMP	<i>Environment One Grinder Pump, Model GP 2000</i>
8	93.34	162
9	105.27	139
10	118.38	116
11	132.66	92
12	148.09	69
13	164.65	46
14	182.32	23
15	201.11	0



OPERATING FLOW : 9.92 G.P.M @ PUMP
OPERATING HEAD : 113.22 FEET +/-
1 1/4" FORCE MAIN VELOCITY : 2.59 F.P.S.
1 1/2" FORCE MAIN VELOCITY : 7.20 F.P.S.



Langley and McDonald, P.C.

ENGINEERS • SURVEYORS • PLANNERS
LANDSCAPE ARCHITECTS • ENVIRONMENTAL CONSULTANTS

VIRGINIA BEACH • WILLIAMSBURG, VIRGINIA

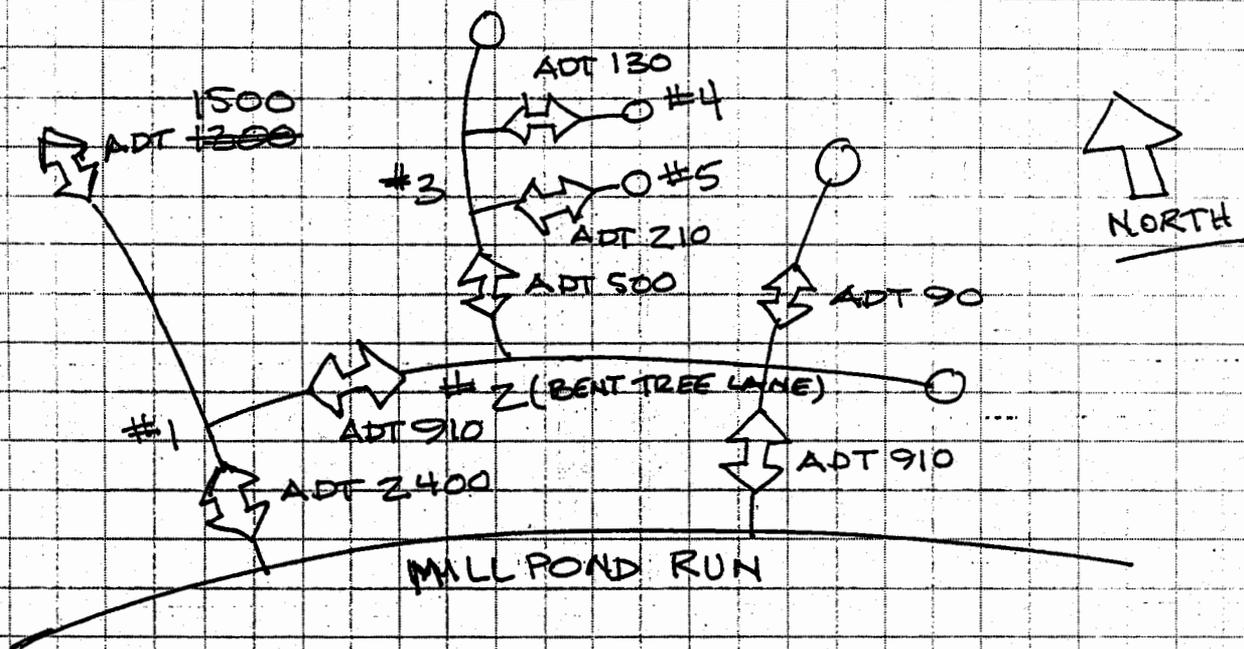
Subject SECTION VB
TRAFFIC SKETCH

Computed By _____ Checked by _____

Project No. _____

Client _____

Date _____ Sheet No. _____



ADT

ROAD #1 9 LOTS + 150 FUTURE \rightarrow 2400

ROAD #2 9 LOTS \rightarrow 910 ADT

ROAD #3 50 LOTS \rightarrow 500 ADT

USE 400 ADT MIN.

Q.SSNV = 20

V.I.D.O.T.
APPENDIX II

ROAD #1 ADT 2400 \rightarrow $D_R = 15.2$

$2 \times 25 + 9.0$

ROAD #2 ADT 910 \rightarrow $D_R = 12.8$

$2 \times 2.5 + 6.0$

ROAD #3 ADT 500 \rightarrow $D_R = 10.2$

$2 \times 2 + 6.0$

ADT 400 \rightarrow $D_R = 9.6$

Appendix IV

Flexible Pavement Design Worksheet for New Subdivision Streets

This sheet is intended for use in conjunction with VDOT's Subdivision Street Requirements

County	JAMES CITY COUNTY	Date:	JAN 7, 1999
Subdivision	SECTION VB "BENT TREE"		
Street Name	SPLIT WOOD STA + to 17+50		
Developer	STONEHOUSE L.L.C.	Phone:	234-5100

- ADT Projected traffic for the street segment considered, as defined in the Subdivision Street Requirements.
- CBR_D Design CBR = Average of CBR_T x 2/3 and modified only as discussed in the Pavement Design Guide.
- CBR_T CBR value of the subgrade sample, taken and tested as specified in the Pavement Design Guide
- DME VDOT District Materials Engineer
- EPT Equivalent projected traffic
- HCV Number of Heavy Commercial Vehicles (e.g. trucks, buses, etc., with 2 or more axles and 6 or more tires).
- %HCV Percentage of the total traffic volume composed of Heavy Commercial Vehicles.
- RF Resiliency Factor = Relative value of the subgrade soil's ability to withstand repeated loading.
- SSV Soil support value of subgrade (SSV = CBR_D x RF)
- D_P Thickness index of proposed pavement design computed by the Conventional Pavement Design Method
- D_R Thickness index required, based on Design ADT and SSV, determined by Appendix II.

Step 1: Determine Design ADT	
ADT	1500
%HCV = 100 x HCV ÷ ADT	5%
EPT = 0.20(%HCV x ADT) or 20 x HCV	
Note: For %HCV ≤ 5%, use ADT	Note: For %HCV > 5%, EPT > ADT
Design ADT = greater of ADT or EPT	1500

Step 2: Determine Design Values CBR, RF and SSV			
Sample #	CBR _T	Resiliency Factor (RF)	Value
# 1		Source	
# 2		Table I	
# 3	6	Appendix I	3.0
#		DME approved RF	
#		For preliminary designs, use the lowest RF value in the equation	
#			
CBR _D x RF =			SSV
(6.67) x (3) =			20

Step 3: Pavement Design (Check appropriate box and show proposed pavement design below.)			
<input type="checkbox"/>	(A) Limited to Design ADT ≤ 400 - Show pavement material notations and thickness from Appendix IV Tables A and B.		
<input type="checkbox"/>	(B) Show pavement section as developed in the Pavement Design Guide. (See Appendix III for material notations and thickness equivalency values (a)).		D _R = 14.0 from Appendix II
Description of Proposed Pavement Section			
	Material Notation	Thickness, h	a (a x h)
Surface	SM-2A	2	2.25 4.50
Base	IM-1A	2.5	2.25 5.625
Subbase	TYPE 21B AGG BASE MATERIAL	3.0	0.6 4.8
D _P must equal or exceed the value of D _R .		D _P = Σ(a x h) = 14.93	

D_R 14.93 > D_R 14.0

Appendix IV

Flexible Pavement Design Worksheet for New Subdivision Streets

This sheet is intended for use in conjunction with VDOT's Subdivision Street Requirements

County	JAMES CITY COUNTY	Date:	JAN. 7, 1999
Subdivision	SECTION VB "BENT TREE"		
Street Name	ROAD #2 WINTER WOOD LANE 10+50 to 12+50		
Developer	STONEHOUSE, L.L.C.	Phone:	234-5100

- ADT Projected traffic for the street segment considered, as defined in the Subdivision Street Requirements.
- CBR_D Design CBR = Average of CBR_T x 2/3 and modified only as discussed in the Pavement Design Guide.
- CBR_T CBR value of the subgrade sample, taken and tested as specified in the Pavement Design Guide
- DME VDOT District Materials Engineer
- EPT Equivalent projected traffic
- HCV Number of Heavy Commercial Vehicles (e.g. trucks, buses, etc., with 2 or more axles and 6 or more tires).
- %HCV Percentage of the total traffic volume composed of Heavy Commercial Vehicles.
- RF Resiliency Factor = Relative value of the subgrade soil's ability to withstand repeated loading.
- SSV Soil support value of subgrade (SSV = CBR_D x RF)
- D_p Thickness index of proposed pavement design computed by the Conventional Pavement Design Method
- D_R Thickness index required, based on Design ADT and SSV, determined by Appendix II.

Step 1: Determine Design ADT	
ADT	
%HCV = 100 x HCV ÷ ADT	910
EPT = 0.20(%HCV x ADT) or 20 x HCV	
Note: For %HCV ≤ 5%, use ADT	Note: For %HCV > 5%, EPT > ADT
Design ADT = greater of ADT or EPT	910

Step 2: Determine Design Values CBR, RF and SSV			
Sample #	CBR _T	Resiliency Factor (RF)	Value
# 1		Source	
# 2		Table 1	
# 3	6	Appendix I	3.0
#		DME approved RF	
#		For preliminary designs, use the lowest RF value in the equation	
CBR _D x RF =			SSV
(6.67) x (3) =			20

Step 3: Pavement Design (Check appropriate box and show proposed pavement design below.)			
<input type="checkbox"/>	(A) Limited to Design ADT ≤ 400 - Show pavement material notations and thickness from Appendix IV Tables A and B.		
<input type="checkbox"/>	(B) Show pavement section as developed in the Pavement Design Guide. (See Appendix III for material notations and thickness equivalency values (a)).		D _R = 12.8 from Appendix II
Description of Proposed Pavement Section			
	Material Notation	Thickness, h	a (a x h)
Surface	SM-2A	2.0	2.25 4.5
Base	IM-1A	2.5	2.25 5.625
Subbase	TYPE 2IB AGG. BASE	0	.6 3.6
D _p must equal or exceed the value of D _R .		D _p = Σ(a x h) = 13.7	

13.7 > 12.8 ok

Appendix IV

Flexible Pavement Design Worksheet for New Subdivision Streets

This sheet is intended for use in conjunction with VDOT's Subdivision Street Requirements

County	JAMES CITY COUNTY	Date:	JAN. 7, 1999
Subdivision	SECTION VB "BENT TREE"		
Street Name	ROADS # 3, 4 & 5 SAPPING DRIVE WINDY BRANCH DRIVE WINTER WOOD DRIVE		
Developer	STONEHOUSE, L.L.C.	Phone:	234-5100

- ADT Projected traffic for the street segment considered, as defined in the Subdivision Street Requirements.
- CBR_D Design CBR = Average of CBR_T x 2/3 and modified only as discussed in the Pavement Design Guide.
- CBR_T CBR value of the subgrade sample, taken and tested as specified in the Pavement Design Guide
- DME VDOT District Materials Engineer
- EPT Equivalent projected traffic
- HCV Number of Heavy Commercial Vehicles (e.g. trucks, buses, etc., with 2 or more axles and 6 or more tires).
- %HCV Percentage of the total traffic volume composed of Heavy Commercial Vehicles.
- RF Resiliency Factor = Relative value of the subgrade soil's ability to withstand repeated loading.
- SSV Soil support value of subgrade (SSV = CBR_D x RF)
- D_p Thickness index of proposed pavement design computed by the Conventional Pavement Design Method
- D_R Thickness index required, based on Design ADT and SSV, determined by Appendix II.

Step 1: Determine Design ADT	
ADT	500
%HCV = 100 x HCV ÷ ADT	
EPT = 0.20(%HCV x ADT) or 20 x HCV	
Note: For %HCV ≤ 5%, use ADT	Note: For %HCV > 5%, EPT > ADT
Design ADT = greater of ADT or EPT	500

Step 2: Determine Design Values CBR, RF and SSV			
Sample #	CBR _T	Resiliency Factor (RF)	Value
# 1		Source	
# 2		Table 1	
# 3	6	Appendix I	3.0
#		DME approved RF	
#		For preliminary designs, use the lowest RF value in the equation	
#			
CBR _D x RF =			SSV
(6.67) x (3.0) =			20

Step 3: Pavement Design (Check appropriate box and show proposed pavement design below.)				
<input type="checkbox"/> (A) Limited to Design ADT ≤ 400 - Show pavement material notations and thickness from Appendix IV Tables A and B.				
<input type="checkbox"/> (B) Show pavement section as developed in the Pavement Design Guide. (See Appendix III for material notations and thickness equivalency values (a)).				D _R = 10.2 from Appendix II
Description of Proposed Pavement Section				
	Material Notation	Thickness, h	a	(a x h)
Surface	SM-2A	2	1.67	3.34
Base	EM-1A	2	1.67	3.34
Subbase	TYPE 2 1/2 AGG. BASE	6	0.6	3.6
D _p must equal or exceed the value of D _R .		D _p = Σ(a x h) = 10.28		

10.28 > 10.2 ✓

Environmental Inventory Section V

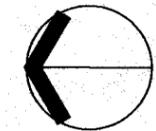
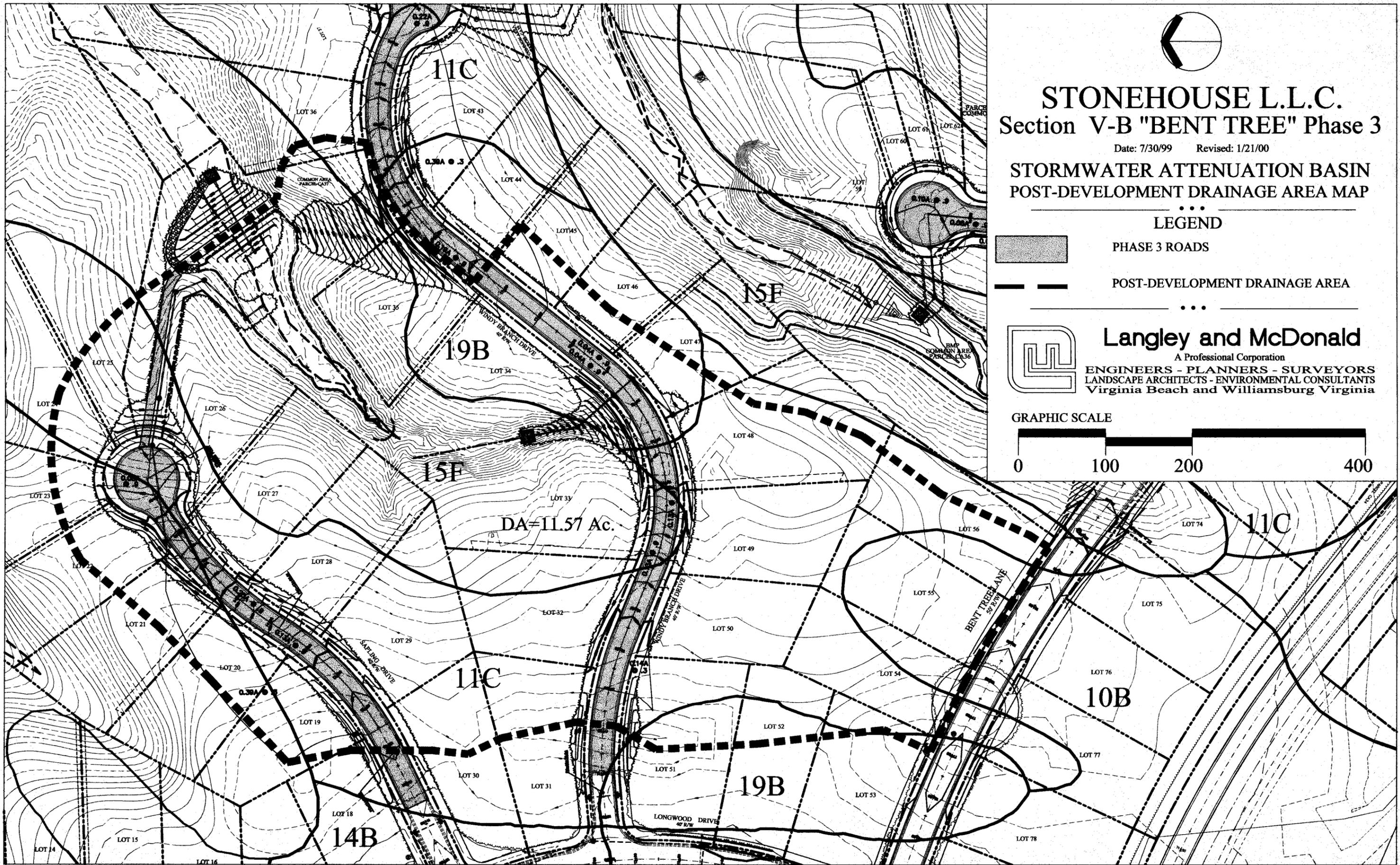
Development Section V is divided into Section VA and VB. Section VA is bordered by Section VIC, Ware Creek, and Coates Pond to the east and north east, Ware Creek to the North, Section VB to the west and Golf Hole 13 to the south.

Section VB is bordered by Section VA to the west, Ware Creek to the north, Mill Pond Run Sections II and III and Section VI to the south, and Section VII to the east.

The canopy vegetation of Section VB is comprised of beech (*Fagus grandifolia*) white oak, (*Quercus alba*), sweet gum (*Liquidambar styraciflua*), loblolly pine (*Pinus taeda*) and red maple (*Acer rubrum*). Section VA canopy vegetation is predominantly pine. The sappling/shrub stratum is comprised of very dense mountain laurel, (*Kalmia latifolia*) holly (*Ilex opaca*), and flowering dogwood (*Cornus florida*); and the herbaceous layer includes wild ginger (*Hexistylis* sp.), strawberry bush (*Euonymus americanus*), pine, beech, white oak and red maple seedlings.

The habitat along Ware Creek is considered scrub-shrub and emergent wetlands. The canopy is comprised of alders (*Alnus serrulata*) and black willow (*Salix nigra*) with lizards tail (*Saururus cernuus*), golden ragwort (*Senecio aureus*), pickerel weed (*Pontedaria cordata*) and saw grass (*Cladium jamaicense*) in the herbaceous layer. There were a few floating aquatic plants present in ponded areas comprised of duckweed (*Lemna minor* and *Spirodela* sp.)

The wildlife usage of the area would include species typical of mature woods including mammals such as white tailed deer, raccoons, gray squirrel, beaver, Virginia opossum, red fox and birds including robins, cardinals, sparrows, black birds, blue jays, doves, meadowlarks and turkey vultures. Reptiles and amphibians usage would include toads, bull frogs, black snake, copperhead, cottonmouth water moccasin, and eastern garter snake



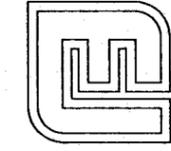
STONEHOUSE L.L.C.
Section V-B "BENT TREE" Phase 3

Date: 7/30/99 Revised: 1/21/00

**STORMWATER ATTENUATION BASIN
 POST-DEVELOPMENT DRAINAGE AREA MAP**

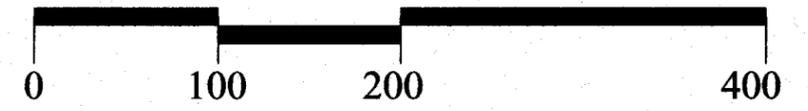
LEGEND

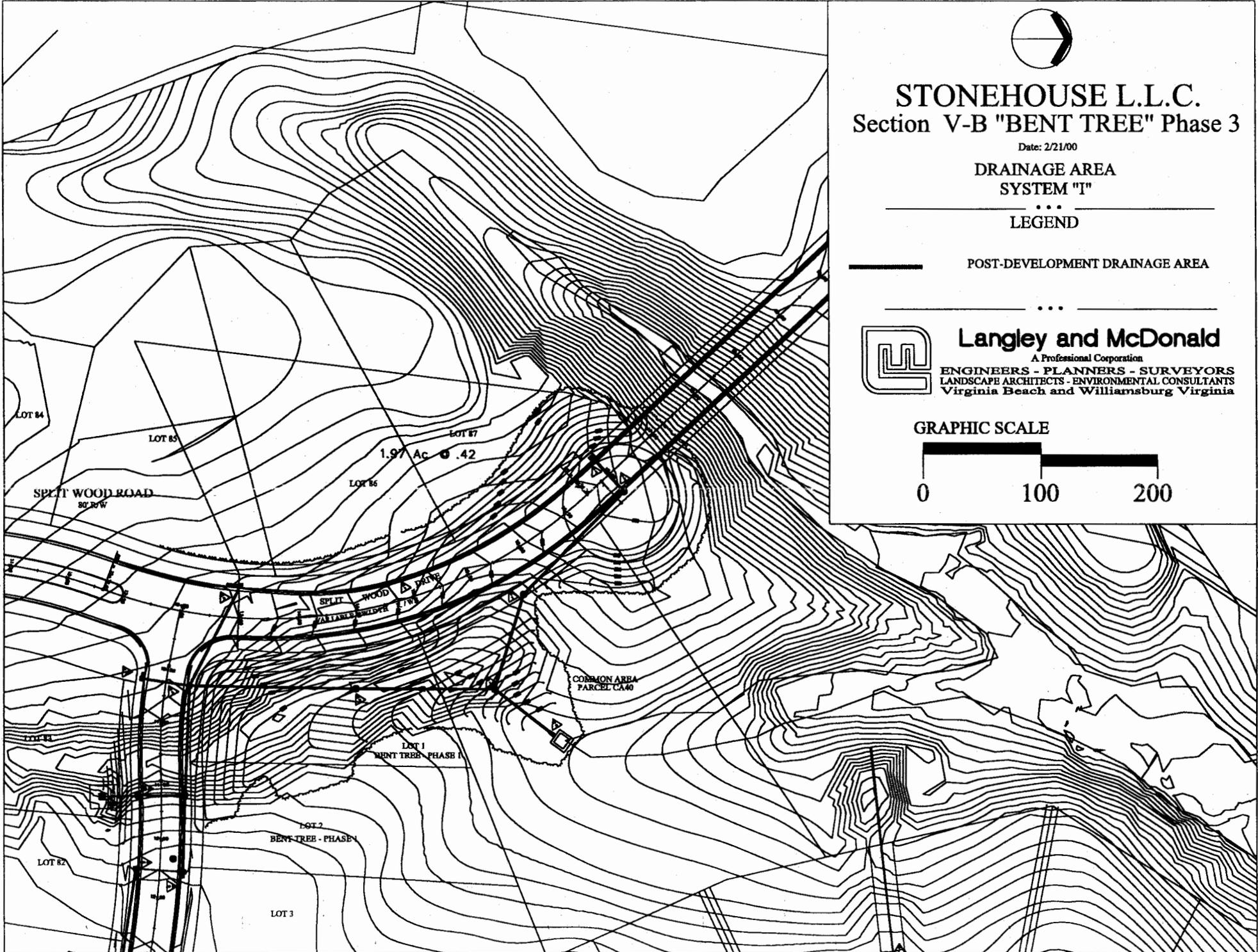
-  PHASE 3 ROADS
-  POST-DEVELOPMENT DRAINAGE AREA



Langley and McDonald
 A Professional Corporation
 ENGINEERS - PLANNERS - SURVEYORS
 LANDSCAPE ARCHITECTS - ENVIRONMENTAL CONSULTANTS
 Virginia Beach and Williamsburg Virginia

GRAPHIC SCALE






STONEHOUSE L.L.C.
Section V-B "BENT TREE" Phase 3

Date: 2/21/00

**DRAINAGE AREA
 SYSTEM "T"**

...
LEGEND


POST-DEVELOPMENT DRAINAGE AREA



Langley and McDonald

A Professional Corporation
ENGINEERS - PLANNERS - SURVEYORS
LANDSCAPE ARCHITECTS - ENVIRONMENTAL CONSULTANTS
 Virginia Beach and Williamsburg Virginia

GRAPHIC SCALE



Scott Thomas

From: Bains, Victoria A. [vbains@aesva.com]
Sent: Tuesday, May 23, 2006 4:30 PM
To: Scott Thomas
Cc: ggoder@kaufcanconsulting.com
Subject: Stonehouse - BMP Inspection List

Scott,

Here is the list of BMP's that need to be inspected.

Bent Tree:

AES No.	JCC No.	
5-3-99 BMP 5.1	WC071	✓ REINSPECT 5/30/06. OK. WALL CLEAN LFO.
5-42-99 BMP 5.4	WC072	✓ REINSPECT 5/30/06. OK. " "
5-42-99 BMP 5.2	WC073	✓ REINSPECT 5/30/06. OK. " "
5-91-99 BMP 5.3	WC074	✓ REINSPECT 5/30/06. OK. " " + more DAM.

Richardson's Mill:

AES No.	JCC No.	
BMP 7.3	WC075	✓ REINSPECT 5/30/06. OK. NO PROBLEMS. Deep Valley. PP
BMP 7.4	WC076	✓ REINSPECT 5/30/06. OK. NO " "
BMP 7.2	WC077	✓ REINSPECT 5/30/06. OK. " " "
BMP 7.1	WC078	Reinspect 5/30/06. BMP OK, Inflow pipe undercut. Process Letter.

Let me know if you cannot find any of the certifications or calculations and I can have copies sent to you before we meet. See you at the Sales Center next Tuesday May 30 at 1:00pm.

Thank you,

Tory

Victoria (Tory) A. Bains
 Project Engineer

AES Consulting Engineers

Williamsburg | Richmond | Gloucester
 (757) 253-0040
 www.aesva.com

AES Consulting Engineers Confidentiality Note: This e-mail and any attachments are confidential and may be protected by legal privilege. If you are not the intended recipient, be aware that any disclosure, copying, distribution or use of this e-mail or any attachment is prohibited. If you have received this e-mail in error, please notify us immediately by returning it to the sender and deleting this copy from your system. Thank you for your cooperation.



**James City County Environmental Division
Stormwater Management / BMP Inspection Report
Detention and Retention Pond Facilities**

Reinspect 5/30/06. Items OK.

County BMP ID Code (if known): WC 072
 Name of Facility: Honchove Bentree BMP-5-4 BMP No.: _____ of _____ Date: 1/13/05
 Location: Sapling
 Name of Owner: _____
 Name of Inspector: SJ Thomas, Tari Bains AES
 Type of Facility: Dry Pond
 Weather Conditions: _____ Type: Final Inspection County BMP Inspection Program Owner Inspection

If an inspection item is not applicable, mark NA, otherwise mark the appropriate column.

- O.K. - The item checked is in adequate condition and the maintenance program is currently satisfactory. No action required.
- Routine - The item checked requires attention, but does not present an immediate threat to the function/integrity of the BMP.
- Urgent - The item checked requires immediate attention to keep the BMP operational and to prevent damage to the facility.

Provide an explanation and details in the comment column, if routine or urgent are marked.



Facility Item	O.K.	Routine	Urgent	Comments
Embankments and Side Slopes: <i>Earth 10' wide; 3H:1V SS; Dam 15-20' High</i>				
Grass Height	✓			<i>OK.</i>
Vegetation Condition	✓			
Tree Growth	✓			<i>None. Some bayberries on 5' high</i>
Erosion	✓			<i>o/s toe & around riser. Will allow if maintained.</i>
Trash & Debris	✓			
Seepage	✓			<i>No signs.</i>
Fencing or Benches				<i>(About 20 bayberries)</i>
Interior Landscaping/Planted Areas: <input type="checkbox"/> None <input type="checkbox"/> Constructed Wetland/Shallow Marsh <input checked="" type="checkbox"/> Naturally Established Vegetation				
Vegetated Conditions	✓			<i>Natural ravine.</i>
Trash & Debris	✓			
Floating Material	✓			<i>Some dead wood.</i>
Erosion	✓			
Sediment		✓		<i>Outfall pipe from subdiv.</i>
Dead Plant	✓			<i>Sediment.</i>
Aesthetics	✓			
Other				
Notes:	<i>Service SF & Roads</i>			

Quality Item	O.K.	Routine	Urgent	Comments
Water Pools: <input type="checkbox"/> Permanent Pool (Retention Basin) <input type="checkbox"/> Shallow Marsh (Detention Basin) <input checked="" type="checkbox"/> None, Dry (Detention Basin)				
Shoreline Erosion	✓			None
Algae	✓			
Trash & Debris	✓			
Sediment		✓		
Aesthetics				
Other				sed. @ inflow pipe outfall 2' deep.
Inflows (Describe Types/Locations): 15-18" RCP FROM WEST, WITHIN 50' OF RISER.				
Condition of Structure	✓			
Erosion	✓			
Trash and Debris	✓			
Sediment		✓		Sediment 1-2' deep, clean
Outlet Protection		✓		10'x10' CLASS I
Other				
Principal Flow Control Structure - Riser, Intake, etc. (Describe Type): 48" RCP RISER w/ CAP				
Condition of Structure	✓			LOW FLOW RIF w/ SCREEN
Corrosion	✓			HIGHER 6" PVC TURN DOWN
Trash and Debris	✓			
Sediment	✓			INSIDE RISER IS A BACKUP
Vegetation	✓			4-6" ORFIC w/ PE VALVE (CLOSED)
Other	✓			WHY?
Principal Outlet Structure - Barrel, Conduit, etc.: 24" RCP w/ ENDWALL, LARGE OP STILL BASIN				
Condition of Structure	✓			CLASS I RR 30'x30'
Settlement	✓			CLASS I RR ALONG TOE OF DAM
Trash & Debris	✓			
Erosion/Sediment	✓			Sediment in RR. MINOR
Outlet Protection	✓			
Other				
Emergency Spillway (Overflow): 10' W GRASS ES; TRAP. 2-2.5' DEEP.				
Vegetation	✓			
Lining	✓			GRASS
Erosion	✓			
Trash & Debris	✓			
Other				
Notes:	✓ plan active SF discharging sediment into BMP.			

Priority Item	O.K.	Routine	Urgent	Comments
Discharge Type Conditions:				
Mosquito Breeding	✓			
Animal Burrows	✓			
Graffiti	✓			
Other	✓			
Surrounding Perimeter Conditions: <i>N, W - SF; East/South Woods (ravine)</i>				
Land Uses	✓			
Vegetation	✓			
Trash & Debris	✓			
Aesthetics	✓			<i>Sediment from SF Construction</i>
Access /Maintenance Roads or Paths				<i>easy off sapling</i>
Other				

Remarks: *BMP great condition, except for sediments from SF.*

- ▷ clean screen on LF out mesh screen
- ▷ clean sediment from inflow pipe.

Overall Environmental Division Internal Rating: 3

Signature: *[Handwritten Signature]*
 Title: *Senior Engineer ENV DIV*

Date: 1/13/05

Date Record Created:

WS_BMPNO:

WC072

Print Form

Created By:

WATERSHED WC

BMP ID NO 072

PLAN NO S-81-99

TAX PARCEL

PIN NO

CONSTRUCTION DATE 10/1/2002

PROJECT NAME Stonehouse Bent Tree Sec 5B PH 3

FACILITY LOCATION North of Windy Branch Drive

CITY-STATE Toano, Va. 23168

CURRENT OWNER Stonehouse LLC

OWNER ADDRESS P.O. Box 759

OWNER ADDRESS 2

CITY-STATE-ZIP CODE Toano, VA 23168

OWNER PHONE 7572345000

MAINT AGREEMENT Yes

EMERG ACTION PLAN No

**PRINTED ON:
Friday, March 12, 2010
1:25:53 PM**

MAINTENANCE PLAN

Yes

SITE AREA acre

35.07

LAND USE

Planned Unit Dev

old BMP TYP

Dry Pond

JCC BMP CODE

F2 Dry ED with forebay

POINT VALUE

0

SVC DRAIN AREA acres

11.1

SERVICE AREA DESCRI

SF Lots & Roadways

IMPERV AREA acres

2.10

RECV STREAM

UT of Ware Creek RMP

EXT DET-WQ-CTRL

Yes

WTR QUAL VOL acre-ft

0.175

CHAN PROT CTRL

Yes

CHAN PROT VOL acre-ft

0.76

SW/FLOOD CONTROL

Yes

GEOTECH REPORT

No

CTRL STRUC DESC

RCP Riser

CTRL STRUC SIZE Inches

48

OTLT BARRL DESC

RCP Barrel

OTLT BARRL SIZE inch

24

EMERG SPILLWAY

Yes

DESIGN HW ELEV

44.15

PERM POOL ELEV

n/a

2-YR OUTFLOW cfs

1.14

10-YR OUTFLOW cfs

21.86

REC DRAWING

Yes

CONSTR CERTIF

Yes

LAST INSP DATE 5/30/2006

Inspected by:

INTERNAL RATING 3

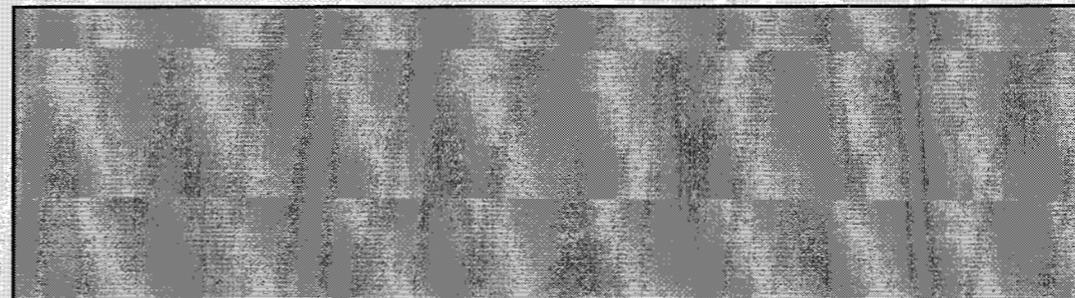
MISC/COMMENTS

BMP # 5.4, amend S-68-0. Not a WQ BMP, attenuation only.

Get Last BMP No

Return to Menu

Additional Comments:



ENVIRONMENTAL DIVISION REVIEW COMMENTS
STONEHOUSE BENT TREE, SECTION 5, PHASE 3
COUNTY PLAN NO. S - 81 - 99
April 10, 2001

MDW/SJT

General Comments:

1. A Land Disturbing Permit and Siltation Agreement, with surety, are required for this project.
2. A Subdivision Agreement, with surety, shall be executed with the County prior to recordation of lots.
3. Water and sewer inspection fees must be paid prior to the issuance of a Land Disturbing Permit.
4. An Inspection/Maintenance Agreement shall be executed with the County for the BMP facility for this project.
5. As-built drawings must be provided for the detention basin upon completion.
6. Wetlands. Provide evidence that any necessary wetlands permits have been obtained or have not expired for this portion of the project.
7. Offsite Work. In accordance with the Step 10 of the construction sequence as provided on Sheet 16, provide evidence of permission to occupy or disturb the offsite adjacent tract from the parcel owner (Fernandez Tract).
8. Streetlights. A streetlight rental fee for 5 lights must be paid prior to the recordation of the subdivision plat. Add one additional streetlight between Lots 34 and 35.
9. VPDES. It appears land disturbance for the project will exceed five (5) acres. Therefore, it is the owners responsibility to register for a General Virginia Pollutant Discharge Elimination System (VPDES) Permit for Discharges of Stormwater from Construction Activities, in accordance with current requirements of the Virginia Department of Environmental Quality and 9 VAC 25-180-10 et seq. Contact the Tidewater Regional Office of the DEQ at (757) 518-2000 or the Central Office at (804) 698-4000 for further information.
10. Professional seal and signature is required on final and complete approved stormwater management plans, drawings, technical reports and specifications.

Floodplain:

11. FEMA Data. Based on FEMA FIRM data, it appears Special Flood Hazard Area, Zone A is present along the northeast portion of the site. Designate SFHA Zone A on the note provided on the cover sheet and correctly label the floodplain as Zone A on all applicable plan sheets, especially the Environmental Inventory.

Chesapeake Bay Preservation:

12. Waiver Request. Waiver request to disturb approximately 1.86 acres of 25 percent slopes dated March 9th 2001 is acknowledged.

Erosion & Sediment Control Plan:

13. Temporary Stockpile Areas. Show any temporary soil stockpile, staging and equipment storage areas (with required erosion and sediment controls) or indicate on the plans that none are anticipated for this portion of the project.

14. Offsite Land Disturbing Areas. Profile sheets 10 & 11 indicate a large amount of areas to be cut to meet proposed road grades. Identify any offsite land disturbing areas including waste or disposal sites (with required erosion and sediment controls) or indicate on the plans that none are anticipated for this project.
15. Grading Plan. Label intended cut/fill slopes on plan Sheets 13, 14 and 15 to the greatest extent possible (3H:1V, 2H:1V, etc.). Use standard VESCH Chapter 3 symbols to indicate areas where matting is required.
16. Limits of Clearing. Check and adjust clearing limits as necessary on the plan to account for any extremely deep utility installations, some of which are well in excess of 15 ft. depth (ie. sanitary sewer).
17. Temporary Sediment Basins. Submit Sediment Basin Design Data Sheets and associated computations to ensure Temporary Sediment Basins # 1 and # 2 are in compliance with Minimum Standard 3.14 of the VESCH. Include hydrology computations, hydraulic and basin routings as necessary. Sheet 16 should reflect use of sediment basins, not traps for Phase 1 temporary basins # 1 and # 2. Step 15 of the construction sequence on Sheet 16 indicates that BMP # 5.4 is to be cleaned of sediment. If this facility is to be utilized as a sediment trapping facility during construction, show the cleanout elevation for BMP # 5.4 during the construction phase and include any special provisions that are required to be provided to this facility (ie. riser/orifice modifications) during the construction phase.
18. Sediment Trapping Facilities. Transpose the locations of Sediment Basins # 1 and # 2 on the 1"=50' grading and drainage plans.
19. Site Stabilization. Include provisions in the sequence of construction, Step 9 or 10, to perform early stabilization (seed & mulch) of disturbed areas associated with road grading, storm drainage systems and installation of BMP # 5.4. In order to minimize erosion, stabilization of certain areas which are at finished grade, especially road cut/fill slopes, outfall areas and the BMP, do not need to wait until remaining sitework such as road ditch grading, road stabilization (with stone) and other incidental utility installations are complete.
20. Culvert Inlet Protection. It appears the culvert inlet protection at the inlet to the 24-inch RCP culvert at Splitwood Road Sta. 18+00 will require a sediment-trap type (CIP) device per VESCH Minimum Standard 3.08, since drainage area to this measure appears to exceed 1 acre. Ensure this is properly specified on the plans and adequate details are provided.
21. Channel Adequacy. Submit adequacy analyses for all receiving natural drainage facilities. Adequacy computations are required to verify that natural channels are adequate for velocity and capacity using the 2-year design storm event. In specific, provide computations for the following four (4) areas: downstream of SS # 2-1 (System 2) prior to BMP # 5.4; downstream of SS # 4-1 (System 4); downstream of the 24-inch culvert at Splitwood Sta. 18+00 before existing BMP # 5.1; and at outfall SS # 5-2 near the Splitwood Pump Sta.(System 5).
22. Rock Check Dams. Add rock check dam structures for secondary control at the following proposed stilling basin locations: at the outfall of the 24-inch RCP culvert at Splitwood Road Sta. 18+00; at the outfall of the 15-inch RCP culvert across Windy Branch Sta. 15+50; and downstream of the 30-inch outlet barrel for BMP # 5.4. These measures will help provide control during first clearing and grading activities until associated storm drainage structures are in place. Stone from the check dams can then be utilized in the stilling basins once tributary site areas are substantially stabilized.

23. Stilling Basins. No dimensions were found on Sheets 13 & 14 for stilling basins proposed at SS # 1-1, SS # 2-1, SS # 3-1, SS # 4-1 and at BMP # 5.4. Also, some side walls of the basins are shown at 1H:1V (ie. slope down areas). The detail on Sheet 19 should reflect slopes for the basins at 2H:1V maximum per Minimum Standard 3.18 of the VESCH. Also indicate slope required (3H:1V, etc.) above the upper limit of riprap, if additional cut is required to tie/meet original ground.

Stormwater Management / Drainage:

24. BMP/Water Quality Points. Provide a County standard Worksheet for BMP Point System to ensure the stormwater management plan for this portion of the project attains at least 10 BMP points or is consistent with the overall stormwater management master plan for the project.
25. BMP Water Quality. Computations were provided in the design report to show 24-hour detention of the 1-year, 24-hour storm to meet County stream channel protection criteria. Provide similar computations as necessary to show water quality treatment volume and detention time through the 4-inch low flow orifice. Design shall be consistent with a County type F-2 facility design (extended dry detention) for a treatment volume of 1.0 inch per impervious acre.
26. Stream Channel Protection. In the design report, the elevation of the release inlet (El. 36.0) does not match the elevation of the 4-inch low-flow orifice on the construction plan (El. 34.5). Determine if this difference will have any impact on the orifice size provided for extended detention for water quality and/or stream channel protection.
27. Hydrology. Provide the basis for the CN selection of 74 as used in the predevelopment conditions analyses for HSG C, wooded subareas associated with subareas tributary to BMP 5.4. Normally "good" hydrologic conditions are used in predevelopment analyses, which in this case would reflect a CN value of around 70. These subareas make up for approximately 82 percent of area tributary to the pond.
28. BMP Design. Explain the purpose of the 4-inch PVC gate valve at the end of the low-flow orifice if basin design is intended as dry extended detention. If the valve is necessary, indicate "normally open" on the detail on Sheet 17.
29. BMP Tailwater. Provide the basis for the 4.1 ft. tailwater depth assumption (El. 34.5) as used in the basin routings for BMP # 5.4. This is the water surface elevation in the natural channel below the pond outlet barrel.
30. Emergency Spillway. Minimum bottom widths for token emergency spillways are 8 feet.
31. Concrete Riser. Specify if the riser barrel is to meet the requirements of ASTM C361 for reinforced concrete pipe or ASTM C 478 for precast reinforced concrete manholes.
32. Flotation Computations. Provide flotation (buoyancy) computations for the riser and base structure.
33. BMP Pretreatment. No provisions were shown on the plan to address BMP pretreatment requirements per the JCC BMP manual.
34. BMP Labels. Properly label BMP # 5.4 on plan Sheets 3, 12, 13, 14, and 16.
35. Pond Buffer. Sheet 3 shows a 15 ft. maintenance easement to be provided from the 100-year floodplain. In addition to the maintenance easement, a pond buffer/setback is required 25 feet outward (landward) from the design high water surface elevation of the pond (currently at El. 44.16). The preferred arrangement is for the design high water plus the 25 ft. buffer to be located in common area rather than having a maintenance easement or buffer/setback situated on proposed lots.

36. Storm Drain System 3. The storm drain computation (table) in the design report for System 3 is missing design drainage area, time of concentration, intensity, flow/capacity and velocity data.
37. Roadside Channels. Based on the roadside channel computations in the design report, Windy Branch Drive, right side, Sta. 14+50 to 15+50 requires a deeper paved channel section due to a 7-inch 10-year design storm channel depth. The construction plan does not reflect transition from a 6-inch paved channel to a deeper paved channel section at this location.
38. Stormwater Conveyance. Describe whether an onsite designed stormwater conveyance channel is necessary just downstream of outfall SS # 5-2 to convey drainage to the natural downstream channel once the site is stabilized and the temporary sediment trap is removed.