

CERTIFICATE OF AUTHENTICITY

THIS IS TO CERTIFY THAT THE FOLLOWING ELECTRONIC RECORDS ARE
TRUE AND ACCURATE REPRODUCTIONS OF THE ORIGINAL RECORDS OF
JAMES CITY COUNTY GENERAL SERVICES DEPARTMENT- STORMWATER
DIVISION; WERE SCANNED IN THE REGULAR COURSE OF BUSINESS
PURSUANT TO GUIDELINES ESTABLISHED BY THE LIBRARY OF VIRGINIA AND
ARCHIVES; AND HAVE BEEN VERIFIED IN THE CUSTODY OF THE INDIVIDUAL
LISTED BELOW.

BMP NUMBER:

CC-018

DATE VERIFIED:

March 15, 2012

QUALITY ASSURANCE TECHNICIAN:

Leah Hardenbergh

Ceah Hardenbugh

LOCATION: WILLIAMSBURG, VIRGINIA



Stormwater Division

MEMORANDUM

DATE:

March 11, 2010

TO:

Michael J. Gillis, Virginia Correctional Enterprises Document Management Services

FROM:

Jo Anna Ripley, Stormwater

PO:

270712

RE:

Files Approved for Scanning

General File ID or BMP ID:

CC018

PIN: 5020900013

Subdivision, Tract, Business or Owner

Name (if known):

Busch Corporate Center

Property Description:

Site 13

Site Address:

348 Mclaws Circle

(For internal use only)

Box 12

Drawer: 7

Agreements: (in file as of scan date)

N

Book or Doc#:

Page:

Comments

As of 3/11/2010 the owner of the property is Goodfarb Family Virginia Land LLC

CC018

Contents for Stormwater Management Facilities As-built Files

Each file is to contain:

- As-built plan
- 2. Completed construction certification
- 3. Construction Plan
- Design Calculations
- (5) Watershed Map
- 6. Maintenance Agreement
- 7. Correspondence with owners
- 8. Inspection Records
- 9. Enforcement Actions

FIFTH AMENDMENT TO CONTRACT BETWEEN BUSCH PROPERTIES, INC.

AND

LOUIS C. GOODFARD

for the purchase of Site 13

THIS AMENDMENT entered into by and between BUSCH PROPERTIES, INC., a Delaware Corporation (Seller) and LOUIS C. GOODFARB, Trading as VIRBY REALTY COMPANY, a sole partnership (Buyer).

WHEREAS, Seller and Buyer have heretofore entered into a contract dated July 13, 1979 and amended on July 22, 1980, July 14, 1981 and July 22, 1982, which provided that Buyer shall purchase from Seller certain property located within the Busch Corporate Center - Williamsburg, and identified as Site 13 (11.24 acres) on that certain plat entitled, "Busch Corporate Center - Williamsburg, Plat of Site 13, and 18, to be Conveyed to Louis C. Goodfarb, Trading as Virby Realty Company, from Busch Properties, Inc., James City County, Virginia", dated June 1, 1979, revised June 21, 1979, revised June 22, 1979, prepared by Langley and McDonald, Consulting Engineers, Virginia Beach, Virginia, and recorded in the Circuit Court for the City of Williamsburg and County of James City in Plat Book 35 on Page 86, and; WHEREAS, Buyer and Seller mutually agree to alter certain terms of the aforesaid contract;

NOW, THEREFORE in consideration of and reliance upon the premises set forth above and the undertakings hereinafter set forth, the parties hereto agree as follows:

- 1. Plat. The aforesaid plat dated June 1, 1979, revised June 21, 1979 and June 22, 1979, shall be extinguished by Seller and a new plat entitled "Busch Corporate Center Williamsburg, Plat of Phase IV, to be conveyed to Louis C. Goodfarb, Trading as Virby Realty Company, from Busch Properties, Inc.", dated August 4, 1982, prepared by Langley and McDonald, Consulting Engineers, Virginia Beach, Virginia incorporated herewith as Exhibit "D", and to be recorded by Seller.
- 2. Property. The "Property" to be purchased by Buyer is hereby reduced to 5.41 acres, to include 3.03 acres hereafter referred to as Site 13 plus the 2.38 acre storm water retention pond between Site 13 and Buyer's Phase I, II and III property, to be conveyed to Buyer at no cost as per the provisions of paragraph 19 of the Contract, and shown on Exhibit "D".

Contract

18. ROAD AND UTILITY IMPROVEMENTS. This Agreement is contingent upon Seller completing construction of an extension of McLaws Circle Road shown on Exhibit "A" from its present terminus at the eastern property line of Site 13 to the western property line of Site 12 by November 30, 1979, but only if Closing shall take place on or before August 15, 1979; however, if Closing shall not take place until after August 15, 1979, then construction of the road will be completed by July 15, 1980.

19. CONVEYANCE OF DRAINAGE POND. Seller agrees to convey at no cost to Buyer and Buyer agrees to accept title to that area between Phase IV and Phases I, II and III, purchased by buyer under a contract of sale with Seller dated April 13, 1977, currently used as a storm water retention pond so that the southeasterly property line of Phase IV will be coterminous with that of Phase III. Seller agrees to have his representatives on the Williamsburg Corporate Center Association Board of Trustee support a resolution for the Williamsburg Corporate Center Association to accept responsibility for the maintenance of this storm water retention pond. Buyer agrees that he will support similar resolutions regarding all other storm water retention ponds constructed or to be constructed within the area shown on Exhibit "A".

These provisions shall survive Closing.

IN WITNESS WHEREOF, the parties have executed this Agreement as of the day and year hereinbelow written. The latter of the dates appearing below shall be the effective date of this Agreement.

SELLER:

BUSCH PROPERTIES, INC.

By W. Fan 202/ Bakan

Date: 4/27/79

BUYER:

VIRBY REALTY COMPANY

Ry My Morofout

7/13/19

AMENDMENT

THIS AMENDMENT, entered into by and between BUSCH PROPERTIES, INC., a
Delaware Corporation (Seller), and LOUIS C. GOODFARB, Trading as VIRBY REALTY
COMPANY, a sole proprietorship (Buyer),

WHEREAS, Seller and Buyer have entered into a contract of sale dated July 13, 1979 which provides that Buyer shall purchase certain real estate from Seller located within the Busch Corporate Center-Williamsburg identified in said contract as "Phase IV (Contract)," and further identified as Site 13 on a plat dated June 20, 1979 by Langley and McDonald Engineers of property to be conveyed to Buyer; and

WHEREAS, Seller and Buyer desire to modify and amend the Contract as hereinafter set forth, and

WHEREAS, it will be necessary for Seller to construct a sanitary sewer line across Site 13 at a future date generally from the right of way of McLaws Circle on the east and north of Site 13 to a 30' sanitary sewer easement retained by Seller on the west and south of Site 13 to serve Buyer's property and that of others, and

WHEREAS, the location of the sanitary sewer line easement has been deferred by Seller to allow it to be located to better serve the buildings Buyer is to construct on Site 13,

NOW, THEREFORE, in consideration of and reliance upon the premises set forth above and the undertakings hereinafter set forth, the parties hereto agree as follows:

1. Buyer hereby agrees that there shall be a 20' or 30' wide sanitary sewer easement crossing Site 13 from McLaws Circle on the north or east and the 30' wide sanitary sewer easement on the south or west of Site 13.

- 2. The location of said easement is to be subsequently determined by Langley and McDonald Consulting Engineers in consultation with Buyer, Seller and requisite public officials.
- 3. Buyer hereby agrees to convey said sanitary sewer easement to Seller or James City County, as appropriate, at no cost, in a timely manner when its location has been determined. Buyer further agrees to allow Seller and its contractors, engineers, surveyors, or public officials and their equipment and material to enter onto Site 13 to survey, design and construct the sanitary sewer line.
- 4. The provisions of this Amendment shall survive delivery of the Deed at closing.

WITNESS the following signatures and seals:

SELLER:	
BUSCH PROPERTIES, INC. By Colors	Date 9/27/82
BUYER:	
VIRBY REALTY COMPANY	
NA By Mis Chings	Date 9/8/82



DEVELOPMENT MANAGEMENT

101-E Mounts Bay Road, P.O. Box 8784, Williamsburg, Virginia 23187-8784 (757) 253-6671 Fax: (757) 253-6850 E-mail: devtman@james-city.va.us

COUNTY ENGINEER

CODE COMPLIANCE (757) 253-6626 codecomp@james-city.va.us

Environmental Division (757) 253-6670 environ@james-city.va.us

Planning (757) 253-6685 planning@james-city.va.us (757) 253-6678 Integrated Pest Management (757) 253-2620

April 22, 1998

Mr. Paul Cathcart Printpack, Inc. 400 Packets Court Williamsburg, VA 23185

RE: Printpack Expansion and BMP Maintenance

Dear Mr. Cathcart:

Attached are documents from the Busch Corporate Center Association that address the long-term maintenance of the Best Management Practice (BMP), or detention pond adjacent to the Printpack property. The information presents that the BMP's maintenance is the responsibility of the Association. This information satisfies the concerns the Environmental Division raised during the review of the Printpack expansion site plan allowing approval of the plan by the Division.

Please contact me at 253-6673 if you have any further questions.

Sincerely,

Darryl E. Cook, P.E.

Environmental Director

Warryl & Cok





April 15, 1998

Mr. Darryl Cook Civil Engineer, Environmental Services James City County P.O. Box 8784 Williamsburg, Virginia 23187

RE: Retention Pond - Busch Corporate Center

Dear Mr. Cook:

Please find attached property transfer documents identifying the responsibility of drainage maintenance and repair for the retention pond located in the Busch Corporate Center as the responsibility of the Busch Corporate Center Association.

Should the County, during the course of inspections, find the need to repair or address maintenance issues relative to the drainage system within the Busch Corporate Center please contact the Association office at 253-3950.

If we may be of further assistance please contact us.

Sincerely

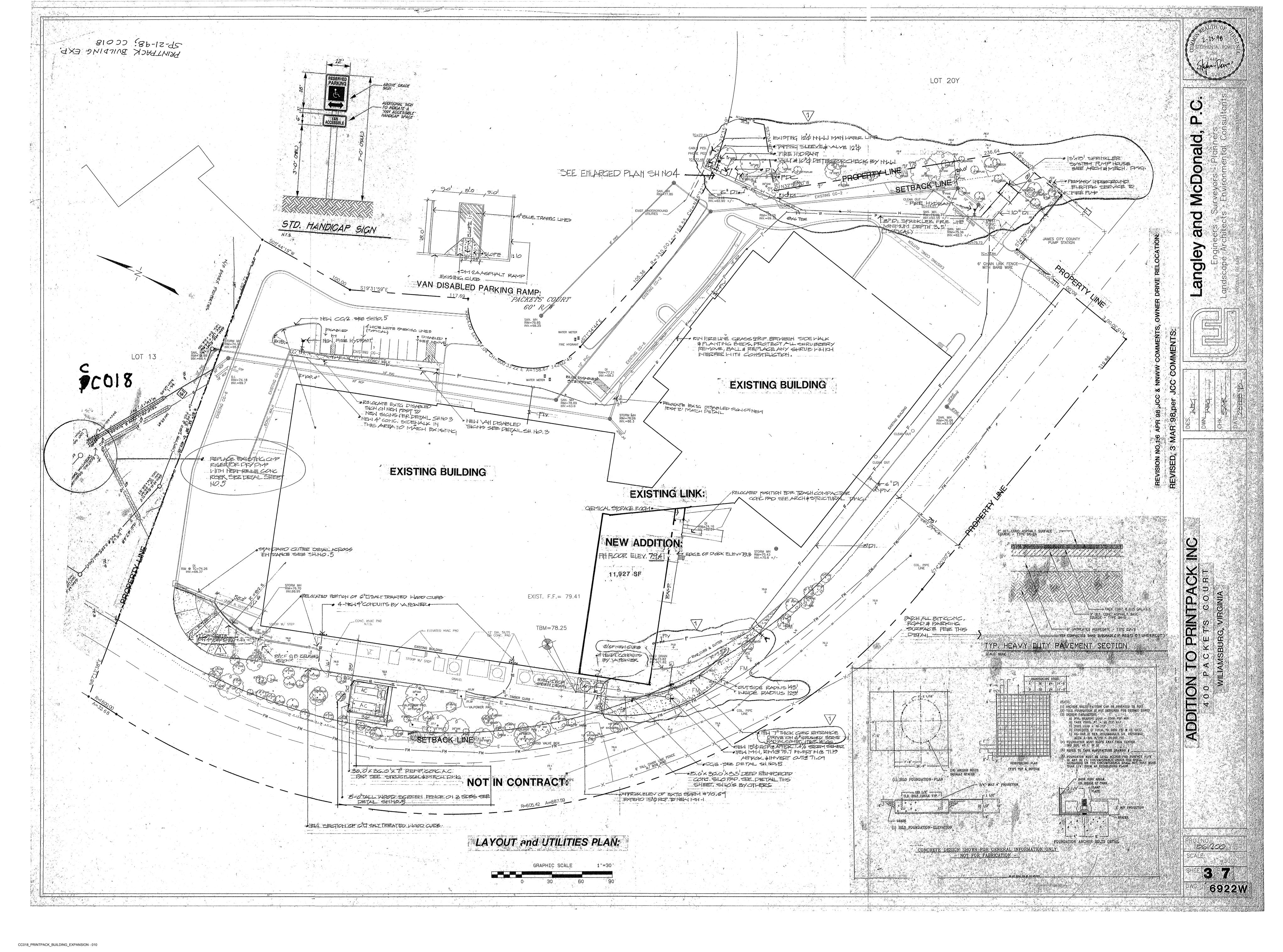
William B. Voliva,

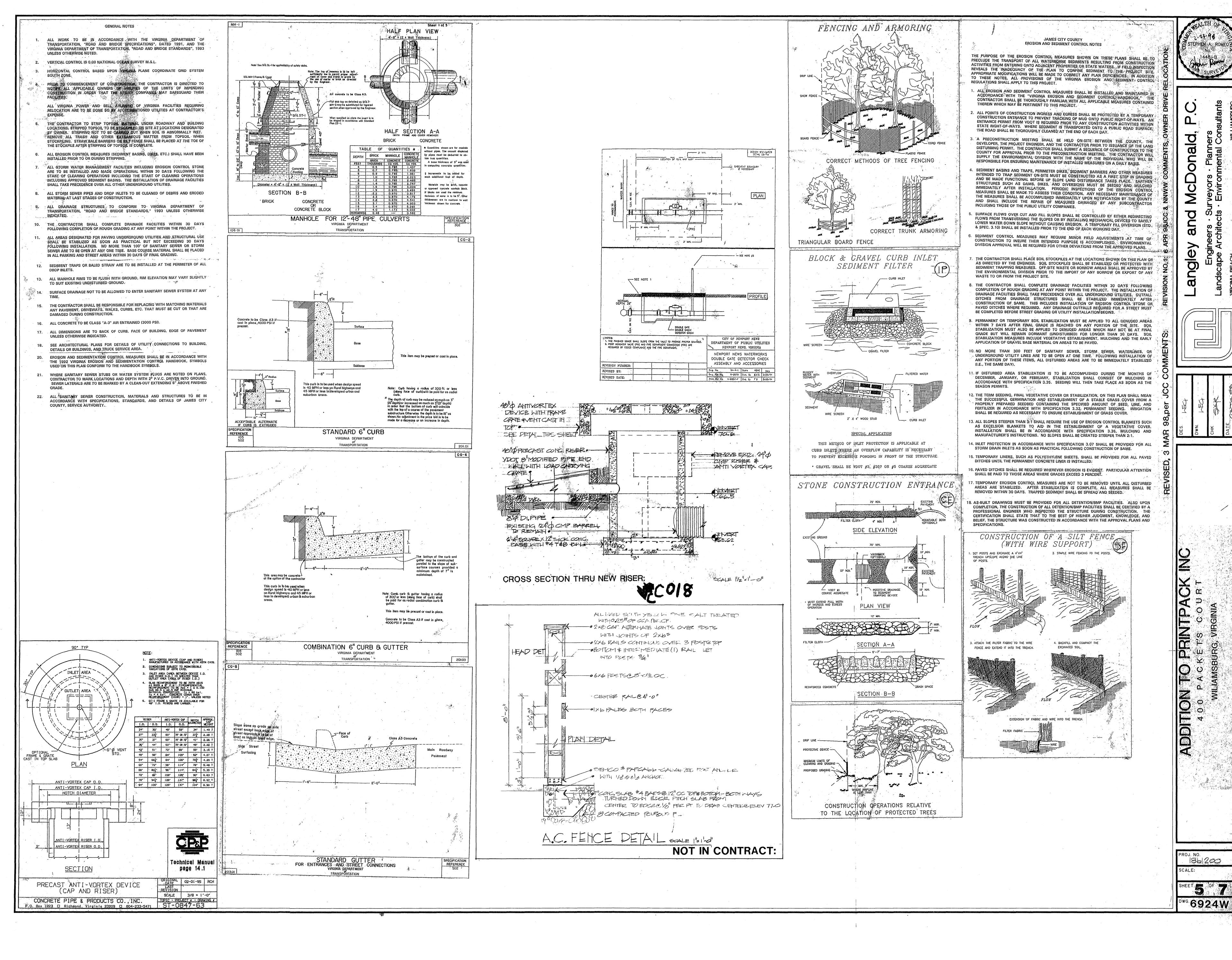
President

Busch Corporate Center Association

cc: Mr. William F. Brown

Attachments





CC018_PRINTPACK_BUILDING_EXPANSION - 011

Langley and McDonald, P.C.

Engineers Surveyors **Planners** Landscape Architects **Environmental Consultants**

Main Office: 5544 Greenwich Road, Virginia Beach, VA 23462 (757) 473-2000 FAX#: (757) 497-7933 Williamsburg Office: 201 Packets Court, Wmbg, VA 23185 (757) 253-2975 FAX#: (757) 229-0049 e-mail address: langley @norfolk.infi.net

WEG FILE COM

CC-018

To:

Darryl Cook, James City County

From:

Diana Browne, L&M

Date:

January 29, 1998

Subject: Printpack Expansion

L&M 86120-103

As requested, enclosed please find additional calculations regarding the 100-year storm for the referenced project. The results indicate that the existing 100-year flood elevation for the detention pond is 73.23 feet, which overtops the dam crest (dam crest elevation is 73.1). Under the proposed conditions, the 100-year flood elevation is 73.4 feet.

Please call us if you have any questions or comments.

Printpack Plant Expansion Stormwater Management

L&M Job 86120-103 January 16, 1998

Printpack is located at 400 Packets Court in the Busch Corporate Center in James City County. The Printpack property is approximately 9.7 acres in area, and consists of two buildings, paved parking and sidewalks, and open areas. Printpack is proposing to expand their plant by constructing a 70' x 160' addition to one of the existing buildings, along with a new gravel road for fire truck access. Since the building expansion will be located over an existing paved area, there will be no increase in impervious area with the proposed expansion.

The Printpack site currently drains to an off-site dry detention pond that is owned by Busch. The drainage area to the pond is 18.7 acres, which includes the Printpack site, as well as Eastern International and the adjacent parking lot. No increase in peak flowrates to the pond from the contributing watershed are anticipated with the proposed plant expansion.

Under the County's Chesapeake Bay Preservation Regulations, the proposed expansion is considered redevelopment, and a 10% reduction in pollutant loads from the project is required. Since the site currently drains to a stormwater management pond, James City County has indicated that no additional treatment is necessary as long as the pond is in good operating condition. Based upon field observations, the existing outfall structure is a 24" CMP riser with 1" diameter holes around its perimeter, and a 24" CMP barrel. The riser structure needs to be upgraded for the pond to be considered in good operating condition.

A 48" RCP riser is proposed to replace the existing 24" CMP riser. The riser crest elevation will increase from the existing elevation of 67.43 to 70.6 to allow for additional water quality drawdown volume. The volume of water at Elev. 70.6 (41,347 c.f.) is equivalent to 0.6 inches of runoff over the 18.7-acre drainage area. An 8" diameter orifice at the bottom of the riser is proposed to allow gradual drawdown for water quality enhancement. No changes to the barrel or dam are anticipated. The modeling results for existing and proposed conditions are as follows:

GEORGE E. LANGLEY

Consultant
T. JOSEPH McDONALD

1906-1982



Langley and McDonald, P.C.

Engineers Surveyors Planners Landscape Architects Environmental Consultants

January 19, 1998

Mr. Darryl E. Cook Environmental Director James City County P.O. Box 8784 Williamsburg, VA 23187-8784

Re: Retrofit of BMP at Packets Court for Printpack Inc.

Dear Darryl:

Thank you for your prompt reply to our request for a meeting with Diana Brown and myself yesterday. Both Diana and I were pleased with the meeting and have worked to meet the modified criteria you spoke of.

The results of this are provided at enclosure, Printpack Plant Expansion Stormwater Management, Langley and McDonald Job Number 86120-103, January 16, 1998.

As this project is a County expedited review process, we request your comments as soon as possible so that we can make any necessary changes and/or adjustments.

Respectfully yours,

LANGLEY AND McDONALD, P.C.

Willard E. Gwilliam, F.A.I.A.

Senior Project Manager

WEG/tmp Enclosure

cc: Mr. Paul Holt, w/ enclosure

Mr. Paul Cathcart, w/enclosure

MAIN OFFICE 5544 Greenwich Road Virginia Beach, VA 23462 (757) 473-2000 FAX: (757) 497-7933

201 Packets Court Williamsburg, VA 23185 (757) 253-2975 FAX: (757) 229-0049

100 year storm?

PRINTPACK PLANT EXPANSION STORMWATER MANAGEMENT

L&M JOB 86120-103 JANUARY 16, 1998

Printpack Plant Expansion Stormwater Management

L&M Job 86120-103 January 16, 1998

Printpack is located at 400 Packets Court in the Busch Corporate Center in James City County. The Printpack property is approximately 9.7 acres in area, and consists of two buildings, paved parking and sidewalks, and open areas. Printpack is proposing to expand their plant by constructing a 70' x 160' addition to one of the existing buildings, along with a new gravel road for fire truck access. Since the building expansion will be located over an existing paved area, there will be no increase in impervious area with the proposed expansion.

The Printpack site currently drains to an off-site dry detention pond that is owned by Busch. The drainage area to the pond is 18.7 acres, which includes the Printpack site, as well as Eastern International and the adjacent parking lot. No increase in peak flowrates to the pond from the contributing watershed are anticipated with the proposed plant expansion.

Under the County's Chesapeake Bay Preservation Regulations, the proposed expansion is considered redevelopment, and a 10% reduction in pollutant loads from the project is required. Since the site currently drains to a stormwater management pond, James City County has indicated that no additional treatment is necessary as long as the pond is in good operating condition. Based upon field observations, the existing outfall structure is a 24" CMP riser with 1" diameter holes around its perimeter, and a 24" CMP barrel. The riser structure needs to be upgraded for the pond to be considered in good operating condition.

A 48" RCP riser is proposed to replace the existing 24" CMP riser. The riser crest elevation will increase from the existing elevation of 67.43 to 70.6 to allow for additional water quality drawdown volume. The volume of water at Elev. 70.6 (41,347 c.f.) is equivalent to 0.6 inches of runoff over the 18.7-acre drainage area. An 8" diameter orifice at the bottom of the riser is proposed to allow gradual drawdown for water quality enhancement. No changes to the barrel or dam are anticipated. The modeling results for existing and proposed conditions are as follows:

PrintPack Plant Expansion Stormwater Management Page 2

Existing Conditions

Storm Event	Peak .	Peak	Peak :
Total Control of the	Inflow	Outflow	Elevation
2-year	54 cfs	26 cfs	70.16
10-year	91 cfs	32 cfs	71.69

Drawdown time from Elev 70.6 = 3.7 hours

67.43 - riser

Proposed Conditions

Storm Event	Peak . Peak	Peak	Peak 1
	Inflow	Outflow	Elevation
2-year	54 cfs	24 cfs	71.20
10-year	91 cfs	47 cfs	72.10

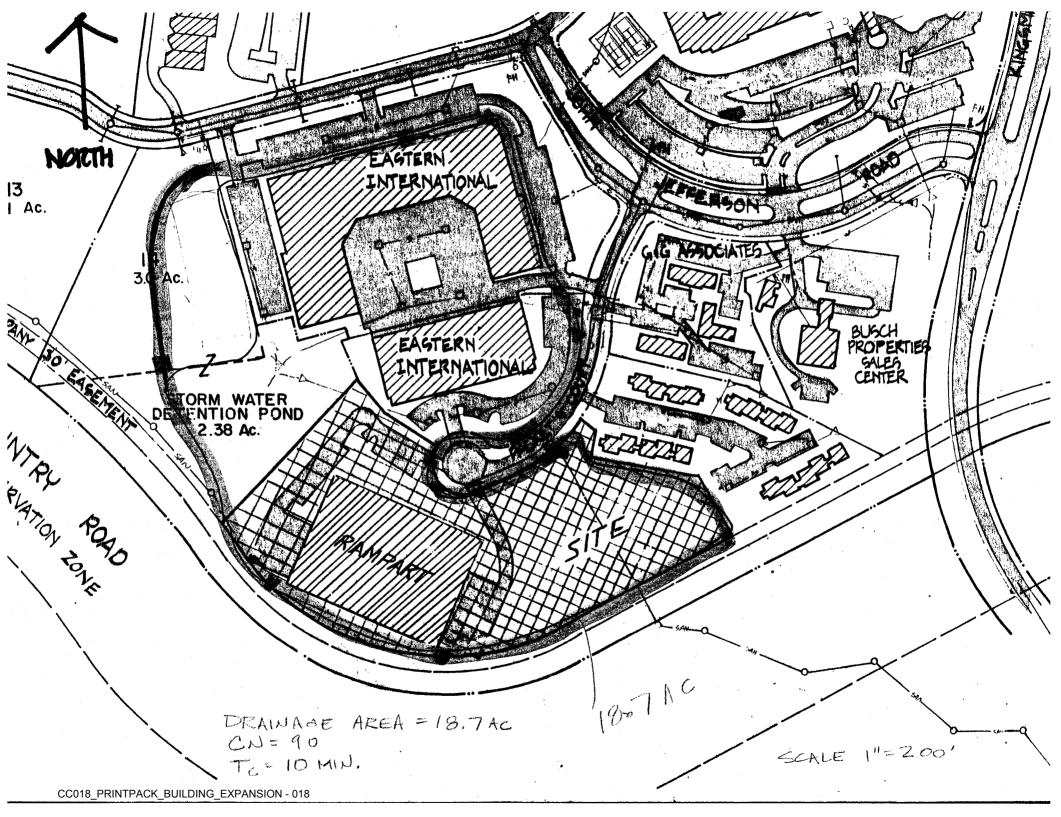
Drawdown time from Elev 70.6 = 5.1 hours

70.6- (15er

Under proposed conditions,

- there is a reduction in the 2-year peak flowrate from 26 cfs to 24 cfs.
- the drawdown time for water quality enhancement is increased.
- the 10-year peak elevation increases by 0.4 feet; however, 1 foot of freeboard is maintained (top of dam elev. = 73.1).

With the proposed changes in outlet structure, the pond should continue to provide stormwater management for the entire 18.7-acre drainage area.



EXISTING CONDITIONS

Page 1
Return Frequency: 2 years

TR-55 TABULAR HYDROGRAPH METHOD Type II. Distribution (24 hr. Duration Storm)

Executed: 01-16-1998 11:11:39

Watershed file: --> C:\86120-~1\WSHED .MOP Hydrograph file: --> C:\86120-~1\SITE2YR.HYD

PrintPack 86120-103

Hydrographs for drainage area to existing BMP No changes in hydrographs for Print Pack project

>>>> Input Parameters Used to Compute Hydrograph <<<<

Subarea Description	AREA (acres)	CN	Tc (hrs)	* Tt (hrs)	Precip. (in)	Runoff (in)	Ia, input,	/p /used
area to BMP	18.70	90.0	0.20	0.00	3.36	2.32	I.07	.10

^{*} Travel time from subarea outfall to composite watershed outfall point.

Total area = 18.70 acres or 0.02922 sq.mi
Peak discharge = 54 cfs

>>>> Computer Modifications of Input Parameters <<<<

Subarea Description	Input Tc (hr)	Values * Tt (hr)	Rounded Tc (hr)		Ia/p Interpolated (Yes/No)	l Ia/p Messages
area to BMP	0.17	0.00	0.20	0.00	No	Computed Ia/p < .1

^{*} Travel time from subarea outfall to composite watershed outfall point.

I -- Subarea where user specified interpolation between Ia/p tables.

Return Frequency: 2 years

TR-55 TABULAR HYDROGRAPH METHOD Type II. Distribution (24 hr. Duration Storm)

Executed: 01-16-1998 11:11:39

Watershed file: --> C:\86120-~1\WSHED .MOF Hydrograph file: --> C:\86120-~1\SITE2YR.HYD

PrintPack 86120-103

Hydrographs for drainage area to existing BMP No changes in hydrographs for Print Pack project

>>>> Summary of Subarea Times to Peak <<<<

	Peak Discharge at Composite Outfall	Time to Peak at Composite Outfall
Subarea	(cfs)	(hrs)
area to BMP	54	12.2
Composite Watershed	54	12.2

Return Frequency: 2 years

TR-55 TABULAR HYDROGRAPH METHOD Type II. Distribution (24 hr. Duration Storm)

Executed: 01-16-1998 11:11:39

Watershed file: --> C:\86120-~1\WSHED .MOP Hydrograph file: --> C:\86120-~1\SITE2YR.HYD

> PrintPack 86120-103

Hydrographs for drainage area to existing BMP No changes in hydrographs for Print Pack project

	(Composi	te Hydro	ograph s	Summary	(cfs)			
Subarea Description	11.0 hr	11.3 hr	11.6 hr	11.9 hr	12.0 hr	12.1 hr	12.2 hr	12.3 hr	12.4 hr
area to BMP	2	2	3	14	27	50	54	33	17
Total (cfs)	2	2	3	14	27	50	54	33	17
Subarea Description	12.5 hr	12.6 hr	12.7 hr	12.8 hr	13.0 hr	13.2 hr	13.4 hr	13.6 hr	13.8 hr
area to BMP	11	9	7	6	5	4	4	3	3
Total (cfs)	11	9	7	6	5	4	4	3	3
Subarea Description	14.0 hr	14.3 hr	14.6 hr	15.0 hr	15.5 hr	16.0 hr	16.5 hr	17.0 hr	17.5 hr
area to BMP	3	2	2	2	2	2	1	1	1
Total (cfs)	3	2	2	2	2	2	1	1	1
Subarea Description	18.0 hr	19.0 hr	20.0 hr	22.0 hr	26.0 hr				
area to BMP	1	1	1	1	0				
Total (cfs)	1	1	1.	1	0				

Return Frequency: 10 years

TR-55 TABULAR HYDROGRAPH METHOD Type II. Distribution (24 hr. Duration Storm)

Executed: 01-16-1998 11:11:39
Watershed file: --> C:\86120-~1\WSHED .MOP
Hydrograph file: --> C:\86120-~1\SITE10YR.HYD

PrintPack 86120-103

Hydrographs for drainage area to existing BMP No changes in hydrographs for Print Pack project

>>>> Input Parameters Used to Compute Hydrograph <<<<

Subarea Description	AREA (acres)	CN	Tc (hrs)	* Tt (hrs)	Precip. (in)		Runoff (in)	Ia input	· -
area to BMP	18.70	90.0	0.20	0.00	5.04		3.91	I.04	.10

^{*} Travel time from subarea outfall to composite watershed outfall point.

Total area = 18.70 acres or 0.02922 sq.mi
Peak discharge = 91 cfs

>>>> Computer Modifications of Input Parameters <<<<

Subarea Description	Input Tc (hr)	Values * Tt (hr)	Rounded Tc (hr)	Values * Tt (hr)	Ia/p Interpolated (Yes/No)	l Ia/p Messages
area to BMP	0.17	0.00	0.20	0.00	No	Computed Ia/p < .1

^{*} Travel time from subarea outfall to composite watershed outfall point.

I -- Subarea where user specified interpolation between Ia/p tables.

Return Frequency: 10 years

TR-55 TABULAR HYDROGRAPH METHOD Type II. Distribution (24 hr. Duration Storm)

Executed: 01-16-1998 11:11:39

Watershed file: --> C:\86120-~1\WSHED .MOP Hydrograph file: --> C:\86120-~1\SITE10YR.HYD

PrintPack 86120-103

Hydrographs for drainage area to existing BMP No changes in hydrographs for Print Pack project

>>>> Summary of Subarea Times to Peak <<<<

	Peak Discharge at Composite Outfall	Time to Peak at Composite Outfall
Subarea	(cfs)	(hrs)
area to BMP	91	12.2
Composite Watershed	91	12.2

Return Frequency: 10 years

TR-55 TABULAR HYDROGRAPH METHOD Type II. Distribution

(24 hr. Duration Storm)

Executed: 01-16-1998 11:11:39

Watershed file: --> C:\86120-~1\WSHED .MOP Hydrograph file: --> C:\86120-~1\SITE10YR.HYD

> **PrintPack** 86120-103

Hydrographs for drainage area to existing BMP No changes in hydrographs for Print Pack project

Composite Hydrograph Summary (cfs) Subarea 11.0 11.3 11.6 11.9 12.0 12.1 12.2 12.3 12.4 Description hr ______ area to BMP 3 4 5 24 46 84 91 55 29 Total (cfs) 3 4 5 24 46 84 91 55 29 Subarea 12.5 12.6 12.7 12.8 13.0 13.2 13.4 13.6 13.8 Description hr area to BMP 19 15 12 10 8 7 6 6 5 ------Total (cfs) 19 15 12 10 8 7 6 6 5 Subarea 14.0 14.3 14.6 15.0 15.5 16.0 16.5 17.0 17.5 Description hr hr hr hr hr hr hr hr ______ area to BMP 5 4 4 3 3 3 2 2 2 2 Total (cfs) 5 4 4 3 3 3 2 2 2 Subarea 18.0 19.0 20.0 22.0 26.0 Description hr hr hr hr hr hr area to BMP 2 2 1 1 0 _____ Total (cfs) 2 2 1 1 0

POND-2 Version: 5.20

S/N:

Print Pack 86120-103 existing volume from 87 calculations

CALCULATED 01-16-1998 11:12:41 DISK FILE: c:\86120-~1\EXIST .VOL

Planimeter scale: 1 inch = 1 ft.

				*	•	
Elevation (ft)	Planimeter (sq.in.)	Area (sq.ft)	A1+A2+sqr(A1*A2) (sq.ft)		Volume ubic-ft)	Volume Sum (cubic-ft)
66.50 67.00 67.30 67.40 68.00 69.00 69.40 69.90 70.00 70.30	0.00 1,980.00 *I* *I* 5,850.00 12,690.00 *I* *I*	1,980 2,926 3,282 5,850 12,690 15,090 18,383 19,080 20,728	0 1,980 7,313 7,812 11,233 27,156 41,618 46,346 47,330 59,695	731 1,042 5,549 3,904 5,970	0 330 3,744 9,052	0 330 1,061 1,372 4,074 13,126 18,676 27,030 28,903 34,873
70.60 71.00 72.00 73.00	*I* 24,840.00 31,140.00 37,440.00	22,445 24,840 31,140 37,440	•	.2,444	21,897 27,931 34,242	41,347 50,800 78,731 112,972

I ---> Interpolated area from closest two planimeter readings.

$$IA = (sq.rt(Area1) + ((Ei-E1)/(E2-E1))*(sq.rt(Area2)-sq.rt(Area1)))$$

IA = Interpolated area for Ei

* Incremental volume computed by the Conic Method for Reservoir Volumes.

Volume =
$$(1/3)$$
 * $(EL2-EL1)$ * $(Areal + Area2 + sq.rt.(Area1*Area2))$

where: EL1, EL2 = Lower and upper elevations of the increment Area1, Area2 = Areas computed for EL1, EL2, respectively Volume = Incremental volume between EL1 and EL2

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103 existing pond

**** COMPOSITE OUTFLOW SUMMARY ****

Elevation (ft)	Q (cfs)	Contributing Structures
66.50	0.0	1 +7
67.00	0.2	1 +7
67.50	0.8	3 + 2 + 6 + 1 + 7
68.00	9.4	3 +2 +6 +1 +7
68.50	16.3	3 +2 +6 +1 +7
69.00	19.7	3 +2 +6 +1 +7
69.50	22.5	3 + 2 + 6 + 1 + 7
70.00	25.1	3 + 2 + 6 + 1 + 7
70.50	27.4	3 +2 +6 +1 +7
71.00	29.6	3 +2 +6 +1 +7
71.50	31.6	3 +2 +6 +1 +7
72.00	33.4	3 +2 +6 +1 +7
72.50	35.2	3 +2 +6 +1 +7
73.00	36.9	3 +2 +6 +1 +7
		2'riser 1"\$? 1"\$?

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103 existing pond

Outlet Structure File: c:\86120-~1\EXIST .STR Planimeter Input File: c:\86120-~1\EXIST .VOL Rating Table Output File: c:\86120-~1\EXIST .PND

Min. Elev.(ft) = 66.5 Max. Elev.(ft) = 73 Incr.(ft) = .5

No.	Q	Table	Q	Table
			_	
- 3			->	3
4	?	3	->	5
2			->	2
6			->	6
. 1			->	1
7			->	7
	3	3 4 ?	3 4 ? 3	3 -> 4 ? 3 -> 2 -> 6 -> 1 ->

Outflow rating table summary was stored in file: c:\86120-~1\EXIST .PND

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103 existing pond

>>>>> Structure No. 3 <<<<< (Input Data)

STAND PIPE Stand Pipe with weir or orifice flow

E1 elev.(ft)? 67.43
E2 elev.(ft)? 73.001
Crest elev.(ft)? 67.43
Diameter (ft)? 2
Weir coefficient? 3.3
Orifice coefficient? 0.6
Start transition elev.(ft) @ ?
Transition height (ft)?

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103 existing pond

>>>>> Structure No. 4 <<<<< (Input Data)

CULVERT-CR Circular Culvert (With Inlet Control)

E1 elev.(ft)?	67.43
E2 elev.(ft)?	73.001
Diam. (ft)?	2
<pre>Inv. el.(ft)?</pre>	63.62
Slope (ft/ft)?	.02
T1 ratio?	
T2 ratio?	
K Coeff.?	.0078
M Coeff.?	2.0
c Coeff.?	.0379
Y Coeff.?	.69
Form 1 or 2?	1
Slope factor?	-0.5

POND-2 Version: 5.20

Date Executed:

S/N:

Time Executed:

Print Pack 86120~103 existing pond

>>>>> Structure No. 2 <<<<< (Input Data)

ORIFICE-VC Orifice - Vertical Circular

E1 elev.(ft)?	67.31
E2 elev.(ft)?	73.001
Orifice coeff.?	0.6
<pre>Invert elev.(ft)?</pre>	67.23
Datum elev.(ft)?	67.27
Diameter (ft)?	.083
	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1
	1"6

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103 existing pond

>>>>> Structure No. 6 <<<<< (Input Data)

TABLE

Constant (ft) added to each elevation was:

Elev. (ft)	Q (cfs)
66.5	0
67	0
68	.18
69	.28
70	.35
71	.41
72	.46
73	. 5

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103 existing pond

>>>>> Structure No. 1 <<<<< (Input Data)

ORIFICE-VC Orifice - Vertical Circular

E1 elev.(ft)?	66.2
E2 elev.(ft)?	73.001
Orifice coeff.?	0.6
<pre>Invert elev.(ft)?</pre>	66.12
Datum elev.(ft)?	66.16
Diameter (ft)?	.083

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

existing pond

>>>>> Structure No. 7 <<<<< (Input Data)

TABLE

Input your own rating table.

E1 (ft) =66.2 E2 (ft) = 73.001

Constant (ft) added to each elevation was:

Elev. (ft)	Q (cfs)
66.5	0
67	.19
68	.28
69	.35
70	.41
71	.46
72	.51
73	.55

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103 existing pond

Outflow Rating Table for Structure #3
STAND PIPE Stand Pipe with weir or orifice flow

***** INLET CONTROL ASSUMED *****

Elevation (ft)	Q (cfs)	Computation Messages
66.50	0.0	E < Inv.El.= 67.43
67.00	0.0	E < E1 = 67.43
67.50	0.4	Weir: $H = .07$
68.00	8.9	Weir: $H = .570$
68.50	15.6	Orifice: H =1.07
69.00	19.0	Orifice: H =1.57
69.50	21.8	Orifice: $H = 2.07$
70.00	24.2	Orifice: $H = 2.57$
70.50	26.5	Orifice: $H = 3.07$
71.00	28.6	Orifice: H =3.57
71.50	30.5	Orifice: $H = 4.07$
72.00	32.3	Orifice: $H = 4.57$
72.50	34.1	Orifice: H =5.07
73.00	35.7	Orifice: H =5.57

Weir Cw = 3.3 Weir length = 6.283186 ft
Orifice Co = .6 Orifice area = 3.141593 sq.ft.
Q (cfs) = (Cw * L * H**1.5) or (Co * A * sqr(2*g*H))
No transition used, transition height = 0.0
Weir equation = Orifice equation @ elev. = 68.15955 ft

POND-2 Version: 5.20

Date Executed:

S/N:

Time Executed:

***** Print Pack 86120-103

existing pond

Outflow Rating Table for Structure #4 CULVERT-CR Circular Culvert (With Inlet Control)

***** INLET CONTROL ASSUMED *****

Elevation (ft)	Q (cfs)	Computation Messages
66.50	0.0	E < E1=67.43
67.00	0.0	E < E1=67.43
67.50	25.7	Submerged: HW =3.88
68.00	28.0	Submerged: HW =4.38
68.50	30.3	Submerged: HW =4.88
69.00	32.3	Submerged: HW =5.38
69.50	34.3	Submerged: HW =5.88
70.00	36.1	Submerged: HW =6.38
70.50	37.9	Submerged: HW =6.88
71.00	39.6	Submerged: HW =7.38
71.50	41.2	Submerged: HW =7.880
72.00	42.8	Submerged: HW =8.38
72.50	44.3	Submerged: HW =8.88
73.00	45.7	Submerged: HW =9.38

Used Unsubmerged Equ. Form (1) for elev. less than 65.87 ft Used Submerged Equation for elevations greater than 66.189 ft HW=Headwater (ft) dc=Critical depth (ft) Ac=Area (sq.ft) at dc

Transition flows interpolated from the following values: E1=65.87 ft; Q1=15.55 cfs; Dc=1.42 ft; E2=66.189 ft; Q2=17.77 cfs

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103 existing pond

Outflow Rating Table for Structure #2
ORIFICE-VC Orifice - Vertical Circular

Elevation (ft)	Q (cfs)	Computation Messages
66.50 67.00 67.50 68.00 68.50 69.00 69.50 70.00 71.00 71.50	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	E < E1=67.31 E < E1=67.31 H = .23 H = .73 H =1.23 H =1.73 H =2.23 H =2.73 H =3.23 H =3.73 H =3.73 H =4.23
72.00 72.50 73.00	0.1 0.1 0.1	H =4.73 H =5.23 H =5.73

C = .6 A = 5.410608E-03 sq.ft.

H (ft) = Table elev. - Datum elev. (67.27 ft) Q (cfs) = C * A * sqr(2g * H)

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103 existing pond

Outflow Rating Table for Structure #6
TABLE Input your own rating table.

Elevation (ft)	Q (cfs)	Computation Messages
66.50	0.0	E < E1=67.31
67.00	0.0	E < E1=67.31
67.50	0.1	Interpolated from input table
68.00 68.50	0.2	Intermelated from input table
69.00	0.2 0.3	Interpolated from input table
69.50	0.3	Interpolated from input table
70.00	0.3	
70.50 71.00	0.4	Interpolated from input table
71.50	0.4	Interpolated from input table
72.00	0.5	
72.50	0.5	Interpolated from input table
73.00	0.5	

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103 existing pond

Outflow Rating Table for Structure #1 ORIFICE-VC Orifice - Vertical Circular

Elevation (ft)	Q (cfs)	Computation	Messages
66.50	0.0	H = .34	
67.00	0.0	H = .84	
67.50	0.0	H = 1.34	
68.00	0.0	H = 1.84	
68.50	0.0	H = 2.34	
69.00	0.0	H = 2.84	
69.50	0.0	H = 3.34	
70.00	0.1	H = 3.84	
70.50	0.1	H = 4.34	
71.00	0.1	H = 4.84	
71.50	0.1	H = 5.34	
72.00	0.1	H = 5.84	
72.50	0.1	H = 6.34	
73.00	0.1	H = 6.84	

C = .6 A = 5.410608E-03 sq.ft.

H (ft) = Table elev. - Datum elev. (66.16 ft) Q (cfs) = C * A * sqr(2g * H)

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack
86120-103
existing pond

Outflow Rating Table for Structure #7
TABLE Input your own rating table.

Elevation (ft)	Q (cfs)	Computation Messages
66.50	0.0	
67.00	0.2	
67.50	0.2	Interpolated from input table
68.00	0.3	
68.50	0.3	Interpolated from input table
69.00	0.3	
69.50	0.4	Interpolated from input table
70.00	0.4	
70.50	0.4	Interpolated from input table
71.00	0.5	
71.50	0.5	Interpolated from input table
72.00	0.5	
72.50	0.5	Interpolated from input table
73.00	0.6	

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103 existing pond

Outflow Rating Table 5
Table 5 = 3 ? 4

Elevation (ft)	Q (cfs)	Contributing	Structures
66.50	0.0	-	
67.00	0.0	- .	
67.50	0.4	3	
68.00	8.9	3	
68.50	15.6	3	
69.00			

EXECUTED: 01-16-1998 11:13:45 Return Freq: 2 years

Inflow Hydrograph: c:\86120-~1\SITE2YR .HYD
Rating Table file: c:\86120-~1\EXIST .PND

----INITIAL CONDITIONS---Elevation = 66.50 ft
Outflow = 0.00 cfs
Storage = 0 cu-ft

GIVEN POND DATA

INTERMEDIATE ROUTING COMPUTATIONS

2S/t + 0 (cfs)
0.0
8 2.0
5 10.3
6 32.0
0 59.3
9 92.6
3 134.8
6 185.7
4 244.8
2 311.8
4 387.0
4 470.8
1 563.3
6 664.5

Time increment (t) = 6.0 min.

EXECUTED: 01-16-1998 11:13:45 Return Freq: 2 years

********* SUMMARY OF ROUTING COMPUTATIONS ***********

Pond File: c:\86120-~1\EXIST .PND Inflow Hydrograph: c:\86120-~1\SITE2YR .HYD Outflow Hydrograph: c:\86120-~1\OUT-2 .HYD

Starting Pond W.S. Elevation = 66.50 ft

***** Summary of Peak Outflow and Peak Elevation *****

Peak Inflow = 54.00 cfs Peak Outflow = 25.83 cfs Peak Elevation = 70.16 ft

**** Summary of Approximate Peak Storage ****

Initial Storage = 0 cu-ft
Peak Storage From Storm = 32,150 cu-ft
Total Storage in Pond = 32,150 cu-ft

Warning: Inflow hydrograph truncated on left side.

EXECUTED: 01-16-1998 11:13:46 Return Freq: 10 years

Inflow Hydrograph: c:\86120-~1\SITE10YR.HYD
Rating Table file: c:\86120-~1\EXIST .PND

----INITIAL CONDITIONS---Elevation = 66.50 ft
Outflow = 0.00 cfs
Storage = 0 cu-ft

GIVEN POND DATA

INTERMEDIATE ROUTING COMPUTATIONS

ELEVATION (ft)	OUTFLOW (cfs)	STORAGE (cu-ft)	2S/t (cfs)	2S/t + 0 (cfs)
66.50 67.00 67.50 68.00 68.50 69.00 69.50 70.00 71.00 71.50 72.00 72.50 73.00	0.0 0.2 0.8 9.4 16.3 19.7 22.5 25.1 27.4 29.6 31.6 33.4 35.2 36.9	0 330 1,718 4,075 7,745 13,126 20,216 28,903 39,132 50,800 63,978 78,731 95,064 112,972	0.0 1.8 9.5 22.6 43.0 72.9 112.3 160.6 217.4 282.2 355.4 437.4 528.1 627.6	0.0 2.0 10.3 32.0 59.3 92.6 134.8 185.7 244.8 311.8 387.0 470.8 563.3 664.5

Time increment (t) = 6.0 min.

POND-2 Version: 5.20 S/N: Page 6
EXECUTED: 01-16-1998 11:13:46 Return Freq: 10 years

********** SUMMARY OF ROUTING COMPUTATIONS ************

Pond File: c:\86120-~1\EXIST .PND Inflow Hydrograph: c:\86120-~1\SITE10YR.HYD Outflow Hydrograph: c:\86120-~1\OUT-10 .HYD

Starting Pond W.S. Elevation = 66.50 ft

**** Summary of Peak Outflow and Peak Elevation ****

Peak Inflow = 91.00 cfs Peak Outflow = 32.28 cfs Peak Elevation = 71.69 ft

**** Summary of Approximate Peak Storage *****

Initial Storage =

PROPOSED CONDITIONS

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

**** COMPOSITE OUTFLOW SUMMARY ****

Elevation (ft)	Q (cfs)	Contributing	Structures
66.50 67.00 67.18 67.50 68.00 68.50 69.00 69.50 70.00 70.50 71.00 71.50 72.00 72.50 73.00	0.0 0.8 1.0 1.4 1.8 2.2 2.5 2.8 3.0 3.3 14.0 39.1 46.6 48.3 49.9	1 - 8" orifice 2 2 2 2 2 2 2 2 4 / Ø riser 3 + 2 3 + 2 4 + 2 4 + 2 4 + 2	
		p posses	

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

Outlet Structure File: c:\86120-~1\MODEXST3.STR Planimeter Input File: c:\86120-~1\EXIST .VOL Rating Table Output File: c:\86120-~1\MODEXST3.PND

Min. Elev. (ft) = 66.5 Max. Elev. (ft) = 73 Incr. (ft) = .5

Structure	No.	Q	Table	e Q	Tabl	е
						-
STAND PIPE	3			->	3	
CULVERT-CR	4	?	3	->	5	
ORIFICE-VC	2			->	2	
TABLE	1			->	1	

Outflow rating table summary was stored in file: c:\86120-~1\MODEXST3.PND

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

>>>>> Structure No. 3 <<<<< (Input Data)

STAND PIPE Stand Pipe with weir or orifice flow

E1 elev.(ft)? 70.6
E2 elev.(ft)? 73.001
Crest elev.(ft)? 70.6
Diameter (ft)? 4
Weir coefficient? 3.3
Orifice coefficient? 0.6
Start transition elev.(ft) @ ?
Transition height (ft)?

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

>>>>> Structure No. 4 <<<<< (Input Data)

CULVERT-CR

Circular Culvert (With Inlet Control)

E1 elev.(ft)?	70.6
E2 elev.(ft)?	73.001
Diam. (ft)?	2
Inv. el.(ft)?	63.62
Slope (ft/ft)?	.02
T1 ratio?	
T2 ratio?	
K Coeff.?	.0078
M Coeff.?	2.0
c Coeff.?	.0379
Y Coeff.?	.69
Form 1 or 2?	1
Slope factor?	-0.5

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

>>>>> Structure No. 2 <<<<< (Input Data)

ORIFICE-VC Orifice - Vertical Circular

E1 elev.(ft)?	67.17
E2 elev.(ft)?	73.001
Orifice coeff.?	0.6
Invert elev.(ft)?	66.5
Datum elev.(ft)?	66.83
Diameter (ft)?	0.67

POND-2 Version: 5.20

Date Executed:

S/N:

Time Executed:

Print Pack 86120-103

change riser structure

>>>>> Structure No. 1 <<<<< (Input Data)

TABLE

Input your own rating table.

E1 (ft) =66.5 E2 (ft) =67.16

Constant (ft) added to each elevation was:

Elev. (ft)	Q (cfs)
66.5	0
66.83	.5
67.16	1

POND-2 Version: 5.20

s/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

Outflow Rating Table for Structure #3 STAND PIPE Stand Pipe with weir or orifice flow

***** INLET CONTROL ASSUMED *****

Elevation (ft)	Q (cfs)	Computation Messages
66.50	0.0	E < Inv.El.= 70.6
67.00	0.0	E < E1 = 70.6
67.18	0.0	E < E1 = 70.6
67.50	0.0	E < E1 = 70.6
68.00	0.0	E < E1=70.6
68.50	0.0	E < E1=70.6
69.00	0.0	E < E1=70.6
69.50	0.0	E < E1 = 70.6
70.00	0.0	E < E1=70.6
70.50	0.0	E < E1=70.6
71.00	10.5	Weir: $H = .4$
71.50	35.4	Weir: $H = .9$
72.00	68.7	Weir: $H = 1.4$
72.50	83.4	Orifice: H =1.9
73.00	93.7	Orifice: H =2.4

Weir Cw = 3.3 Weir length = 12.56637 ft
Orifice Co = .6 Orifice area = 12.56637 sq.ft.
Q (cfs) = (Cw * L * H**1.5) or (Co * A * sqr(2*g*H))
No transition used, transition height = 0.0
Weir equation = Orifice equation @ elev.= 72.05908 ft

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

Outflow Rating Table for Structure #4
CULVERT-CR Circular Culvert (With Inlet Control)

***** INLET CONTROL ASSUMED *****

Elevation (ft)	Q (cfs)	Computation Messages
66.50	0.0	E < E1=70.6
67.00	0.0	E < E1=70.6
67.18	0.0	E < E1=70.6
67.50	0.0	E < E1=70.6
68.00	0.0	E < E1=70.6
69.00 69.50 70.00 70.50 71.00 71.50	0.0 0.0 0.0 39.6 41.2 42.8	E < E1=70.6 E < E1=70.6 E < E1=70.6 E < E1=70.6 Submerged: HW =7.38 Submerged: HW =7.880 Submerged: HW =8.38
72.50	44.3	Submerged: HW =8.88
73.00	45.7	Submerged: HW =9.38

Used Unsubmerged Equ. Form (1) for elev. less than 65.87 ft Used Submerged Equation for elevations greater than 66.189 ft HW=Headwater (ft) dc=Critical depth (ft) Ac=Area (sq.ft) at dc

Transition flows interpolated from the following values: E1=65.87 ft; Q1=15.55 cfs; Dc=1.42 ft; E2=66.189 ft; Q2=17.77 cfs

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

Outflow Rating Table for Structure #2 ORIFICE-VC Orifice - Vertical Circular

Elevation (ft)	Q (cfs)	Computation Messages
66.50	0.0	E < E1=67.17
67.00	0.0	E < E1=67.17
67.18	1.0	H = .35
67.50	1.4	H = .67
68.00	1.8	H =1.17
68.50	2.2	H =1.67
69.00	2.5	H =2.17
69.50	2.8	H =2.67
70.00	3.0	H =3.17
70.50	3.3	H =3.67
71.00	3.5	H =4.17
71.50	3.7	H =4.67
72.00	3.9	H =5.17
72.50	4.0	H =5.67
73.00	4.2	H =6.17

C = .6 A = .3525653 sq.ft. H (ft) = Table elev. - Datum elev. (66.83 ft)

Q (cfs) = C * A * sqr(2g * H)

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

Outflow Rating Table for Structure #1 TABLE Input your own rating table.

Elevation (ft)	Q (cfs)	Computation Messages
66.50	0.0	
	0.0	
67.00	0.8	Interpolated from input table
67.18	0.0	E = or > E2 = 67.16
67.50	0.0	E = or > E2 = 67.16
68.00	0.0	E = or > E2=67.16
68.50	0.0	E = or > E2 = 67.16
69.00	0.0	E = or > E2 = 67.16
69.50	0.0	E = or > E2 = 67.16
70.00	0.0	E = or > E2 = 67.16
70.50	0.0	E = or > E2 = 67.16
71.00	0.0	E = or > E2 = 67.16
71.50	0.0	E = or > E2 = 67.16
72.00	0.0	E = or > E2 = 67.16
72.50	0.0	E = or > E2 = 67.16
73.00	0.0	E = or > E2=67.16

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

Outflow Rating Table 5 Table 5 = 3 ? 4

Elevation (ft)	Q (cfs)	Contributing	Structures
66.50	0.0		
67.00	0.0	· -	
67.18	0.0	-	
67.50	0.0	-	
68.00	0.0	-	
68.50	0.0	-	
69.00	0.0	· <u>-</u>	
69.50	0.0	_ '	
70.00	0.0		
70.50	0.0	-	
71.00	10.5	3	
71.50	35.4	3	
72.00	42.8	4	
72.50	44.3	4	
73.00	45.7	4	

EXECUTED: 01-16-1998 11:14:56 Return Freq: 2 years

Inflow Hydrograph: c:\86120-~1\SITE2YR .HYD
Rating Table file: c:\86120-~1\MODEXST3.PND

----INITIAL CONDITIONS---Elevation = 66.50 ft
Outflow = 0.00 cfs
Storage = 0 cu-ft

GIVEN POND DATA

INTERMEDIATE ROUTING COMPUTATIONS

ELEVATION		STORAGE		2S/t	2S/t + 0
(ft)	(cfs)	(cu-ft)		(cfs)	(cfs)
66.50	0.0	0		0.0	0.0
67.00	0.8	330		1.8	2.6
67.18	1.0	734	·	4.1	5.1
67.50	1.4	1,718		9.5	10.9
68.00	1.8	4,075		22.6	24.4
68.50	2.2	7,745		43.0	45.2
69.00	2.5	13,126		72.9	75.4
69.50	2.8	20,216		112.3	115.1
70.00	3.0	28,903		160.6	163.6
70.50	3.3	39,132		217.4	220.7
71.00	14.0	50,800		282.2	296.2
71.50	39.1	63,978		355.4	394.5
72.00	46.6	78,731		437.4	484.0
72.50	48.3	95,064		528.1	576.4
73.00	49.9	112,972	,	627.6	677.5

Time increment (t) = 6.0 min.

EXECUTED: 01-16-1998 11:14:56 Return Freq: 2 years

*********** SUMMARY OF ROUTING COMPUTATIONS ************

Pond File: c:\86120-~1\MODEXST3.PND Inflow Hydrograph: c:\86120-~1\SITE2YR .HYD Outflow Hydrograph: c:\86120-~1\MOD2 .HYD

Starting Pond W.S. Elevation = 66.50 ft

***** Summary of Peak Outflow and Peak Elevation *****

Peak Inflow = 54.00 cfs Peak Outflow = 23.90 cfs Peak Elevation = 71.20 ft

***** Summary of Approximat

EXECUTED: 01-16-1998 11:14:57 Return Freq: 10 years

Inflow Hydrograph: c:\86120-~1\SITE10YR.HYD
Rating Table file: c:\86120-~1\MODEXST3.PND

----INITIAL CONDITIONS---Elevation = 66.50 ft
Outflow = 0.00 cfs
Storage = 0 cu-ft

GIVEN POND DATA

INTERMEDIATE ROUTING COMPUTATIONS

ELEVATION (ft)	OUTFLOW (cfs)	STORAGE (cu-ft)		2S/t (cfs)	2S/t + 0 (cfs)
66.50 67.00 67.18 67.50 68.00 68.50 69.00 69.50 70.00 71.50 71.50 72.00	0.0 0.8 1.0 1.4 1.8 2.2 2.5 2.8 3.0 3.3 14.0 39.1 46.6	0 330 734 1,718 4,075 7,745 13,126 20,216 28,903 39,132 50,800 63,978 78,731		0.0 1.8 4.1 9.5 22.6 43.0 72.9 112.3 160.6 217.4 282.2 355.4 437.4	0.0 2.6 5.1 10.9 24.4 45.2 75.4 115.1 163.6 220.7 296.2 394.5 484.0
72.50 73.00	48.3 49.9	95,064 112,972	in the second se	528.1 627.6	576.4 677.5

Time increment (t) = 6.0 min.

POND-2 Version: 5.20 S/N: Page 6
EXECUTED: 01-16-1998 11:14:57 Return Freq: 10 years

*********** SUMMARY OF ROUTING COMPUTATIONS ***********

Pond File: c:\86120-~1\MODEXST3.PND Inflow Hydrograph: c:\86120-~1\SITE10YR.HYD Outflow Hydrograph: c:\86120-~1\MOD10 .HYD

Starting Pond W.S. Elevation = 66.50 ft

**** Summary of Peak Outflow and Peak Elevation *****

Peak Inflow = 91.00 cfs Peak Outflow = 46.94 cfs Peak Elevation = 72.10 ft

***** Summary of Approximat

DRAWDOWN CALCULATIONS

Page 1 EXECUTED: 01-16-1998 11:22:27 drawdown Return Freq: 1 years

> ******** Drawdown calculations * Existing conditions

> *******

Inflow Hydrograph: c:\86120-~1\DRAWDOWN.HYD Rating Table file: c:\86120-~1\EXIST

----INITIAL CONDITIONS----Elevation = 70.60 ft Outflow = 27.84 cfs 41,465 cu-ft Storage =

GIVEN POND DATA

INTERMEDIATE ROUTING COMPUTATIONS

ELEVATION (ft)	OUTFLOW (cfs)	STORAGE (cu-ft)	2S/t (cfs)	2S/t + 0 (cfs)
66.50 67.00 67.50 68.00 68.50 69.00 69.50 70.00 71.50 71.00	0.0 0.2 0.8 9.4 16.3 19.7 22.5 25.1 27.4 29.6 31.6 33.4	0 330 1,718 4,075 7,745 13,126 20,216 28,903 39,132 50,800 63,978 78,731	0.0 1.8 9.5 22.6 43.0 72.9 112.3 160.6 217.4 282.2 355.4 437.4	0.0 2.0 10.3 32.0 59.3 92.6 134.8 185.7 244.8 311.8 387.0 470.8
72.50	35.2 36.9	95,064 112,972	528.1 627.6	563.3 664.5

Time increment (t) = 6.0 min.

EXISTING DRAWDOWN TIME = 882 -660 = 222 MIN 02 3.7 HR

EXECUTED: 01-16-1998 11:23:32 drawdown

Return Freq: 1 years

******** Drawdown calculations Change riser structure *********

Inflow Hydrograph: c:\86120-~1\DRAWDOWN.HYD Rating Table file: c:\86120-~1\MODEXST3.PND

----INITIAL CONDITIONS----Elevation = 70.60 ft Outflow = 5.44 cfs Storage = 41,465 cu-ft

GIVEN POND DATA

INTERMEDIATE ROUTING COMPUTATIONS

ELEVATION (ft)	OUTFLOW (cfs)	STORAGE (cu-ft)	2S/t (cfs)	2S/t + 0 (cfs)
66.50	0.0	o	0.0	0.0
67.00	0.8	330	1.8	2.6
67.18	1.0	734	4.1	5.1
67.50	1.4	1,718	9.5	10.9
68.00	1.8	4,075	22.6	24.4
68.50	2.2	7,745	43.0	45.2
69.00	2.5	13,126	72.9	75.4
69.50	2.8	20,216	112.3	115.1
70.00	3.0	28,903	160.6	163.6
70.50	3.3	39,132	217.4	220.7
71.00	14.0	50,800	282.2	296.2
71.50	39.1	63,978	355.4	394.5
72.00	46.6	78,731	437.4	484.0
72.50	48.3	95,064	528.1	576.4
73.00	49.9	112,972	627.6	677.5

Time increment (t) = 6.0 min.

PROPOSED DRAWDOWN TIME = 966-660= 306 MIN 02 5.1 HR

EXECUTED: 01-16-1998 11:23:32 drawdown Return Freq: 1 years

Pond File: c:\86120-~1\MODEXST3.PND Inflow Hydrograph: c:\86120-~1\DRAWDOWN.HYD Outflow Hydrograph: c:\86120-~1\OUT .HYD

INFLOW HYDROGRAPH

ROUTING COMPUTATIONS

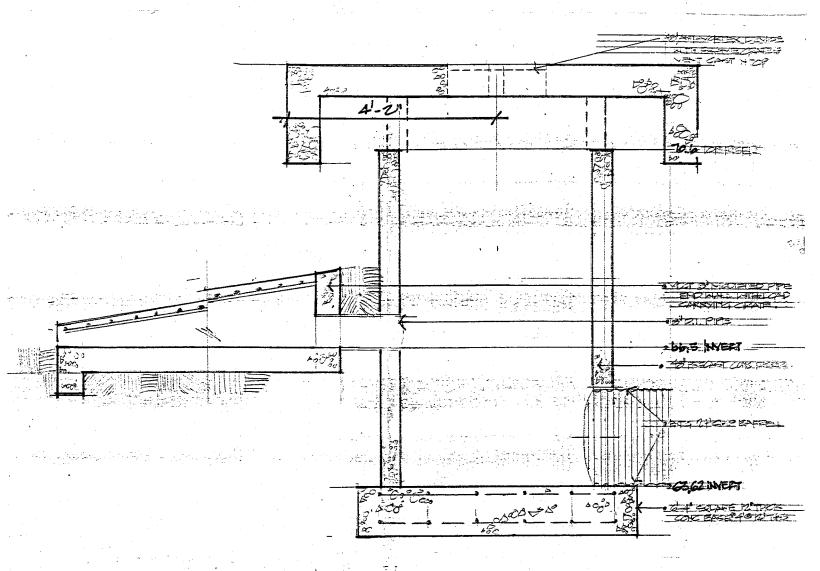
TIME (min)	INFLOW (cfs)	I1+I2 (cfs)	2S/t - 0 (cfs)	2S/t + 0 (cfs)	OUTFLOW (cfs)	ELEVATION (ft)
660.0 666.0 672.0 678.0	0.00 0.00 0.00 0.00	0.0	224.9 217.1 210.6 204.1	235.8 224.9 217.1 210.6	5.44 3.90 3.28 3.25	70.60 70.53 70.47 70.41
684.0 690.0 696.0 702.0 708.0	0.00 0.00 0.00 0.00	0.0 0.0 0.0 0.0	197.6 191.3 185.0 178.8 172.6	204.1 197.6 191.3 185.0 178.8	3.21 3.18 3.15 3.11 3.08	70.35 70.30 70.24 70.19 70.13
714.0 720.0 726.0 732.0	0.00 0.00 0.00 0.00	0.0 0.0 0.0	166.5 160.5 154.5 148.6	172.6 166.5 160.5 154.5	3.05 3.02 2.99 2.96	70.08 70.03 69.97 69.91
738.0 744.0 750.0 756.0 762.0	0.00 0.00 0.00 0.00 0.00	0.0 0.0 0.0 0.0	142.7 136.9 131.1 125.4 119.7	148.6 142.7 136.9 131.1 125.4	2.94 2.91 2.89 2.87 2.84	69.85 69.78 69.72 69.66 69.61
768.0 774.0 780.0 786.0 792.0	0.00 0.00 0.00 0.00	0.0 0.0 0.0 0.0	114.0 108.5 103.0 97.5 92.2	119.7 114.0 108.5 103.0 97.5	2.82 2.79 2.75 2.71 2.67	69.55 69.49 69.42 69.35 69.28
798.0 804.0 810.0 816.0	0.00 0.00 0.00 0.00	0.0 0.0 0.0 0.0	87.0 81.8 76.7 71.7	92.2 87.0 81.8 76.7	2.63 2.59 2.55 2.51	69.21 69.15 69.08 69.02
822.0 828.0 834.0 840.0 846.0	0.00 0.00 0.00 0.00	0.0 0.0 0.0 0.0	66.7 61.9 57.2 52.5 48.0	71.7 66.7 61.9 57.2 52.5	2.46 2.41 2.37 2.32 2.27	68.94 68.86 68.78 68.70 68.62
852.0 858.0 864.0 870.0	0.00 0.00 0.00 0.00	0.0	43.5 39.2 35.0 31.0	48.0 43.5 39.2 35.0	2.23 2.17 2.08 2.00	68.55 68.46 68.36 68.26
876.0 882.0 888.0 894.0	0.00 0.00 0.00 0.00	0.0 0.0 0.0	27.2 23.5 19.9 16.6	31.0 27.2 23.5 19.9	1.93 1.85 1.77 1.67	68.16 68.07 67.96 67.83
900.0 906.0 912.0 918.0 924.0	0.00 0.00 0.00 0.00	0.0 0.0 0.0 0.0	13.5 10.5 7.8 5.4 3.4	16.6 13.5 10.5 7.8 5.4	1.57 1.47 1.37 1.18 1.02	67.71 67.59 67.48 67.33 67.20

EXECUTED: 01-16-1998 11:23:32 drawdown Return Freq: 1 years

Pond File: c:\86120-~1\MODEXST3.PND Inflow Hydrograph: c:\86120-~1\DRAWDOWN.HYD Outflow Hydrograph: c:\86120-~1\OUT .HYD

INFLOW HYDROGRAPH ROUTING COMPUTATIONS

TIME	INFLOW	I1+I2	2S/t - 0	2S/t + 0	OUTFLOW	ELEVATION
(min)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(ft)
930.0	0.00	0.0	1.6	3.4	0.86	67.05
936.0	0.00	0.0	0.6	1.6	0.50	66.81
942.0	0.00	0.0	0.3	0.6	0.20	66.62
948.0	0.00	0.0	0.1	0.3	0.08	66.55
954.0	0.00	0.0	0.0	0.1	0.03	66.52
960.0	0.00	0.0	0.0	0.0	0.01	66.51
966.0	0.00	0.0	0.0	0.0	0.00	66.50
972.0	0.00	0.0	0.0	0.0	0.00	66.50
978.0	0.00	0.0	0.0	0.0	0.00	66.50
984.0	0.00	0.0	0.0	0.0	0.00	66.50
990.0	0.00	0.0	0.0	0.0	0.00	66.50
996.0	0.00	0.0	0.0	0.0	0.00	66.50
1002.0	0.00	0.0	0.0	0.0	0.00	66.50
1008.0	0.00	0.0	0.0	0.0	0.00	66.50
1014.0	0.00	0.0	0.0	0.0	0.00	66.50
1020.0	0.00	0.0	0.0	0.0	0.00	66.50
1026.0	0.00	0.0	0.0	0.0	0.00	66.50
1032.0	0.00	0.0	0.0	0.0	0.00	66.50
1038.0	0.00	0.0	0.0	0.0	0.00	66.50
1044.0	0.00	0.0	0.0	0.0	0.00	66.50
1050.0	0.00	0.0	0.0	0.0	0.00	66.50
1056.0	0.00	0.0	0.0	0.0	0.00	66.50
1062.0	0.00	0.0	0.0	0.0	0.00	66.50
1068.0	0.00	0.0	0.0	0.0	0.00	66.50
1074.0	0.00	0.0	0.0	0.0	0.00	66.50
1080.0	0.00	0.0	0.0	0.0	0.00	66.50
1086.0	0.00	0.0	0.0	0.0	0.00	66.50
1092.0	0.00	0.0	0.0	0.0	0.00	66.50
1098.0	0.00	0.0	0.0	0.0	0.00	66.50
1104.0	0.00	0.0	0.0	0.0	0.00	66.50
1110.0	0.00	0.0	0.0	0.0	0.00	66.50
1116.0	0.00	0.0	0.0	0.0	0.00	66.50
1122.0	0.00	0.0	0.0	0.0	0.00	66.50
1128.0	0.00	0.0	0.0	0.0	0.00	66.50
1134.0	0.00	0.0	0.0	0.0	0.00	66.50
1140.0	0.00	0.0	0.0	0.0	0.00	66.50
1146.0	0.00	0.0	0.0	0.0	0.00	66.50
1152.0	0.00	0.0	0.0	0.0	0.00	66.50
1158.0	0.00	0.0	0.0	0.0	0.00	66.50
1164.0	0.00	0.0	0.0	0.0	0.00	66.50
1170.0	0.00	0.0	0.0	0.0	0.00	66.50
1176.0	0.00	0.0	0.0	0.0	0.00	66.50
1182.0	0.00	0.0	0.0	0.0	0.00	66.50
1188.0	0.00	0.0	0.0	0.0	0.00	66.50
1194.0	0.00	0.0	0.0	0.0	0.00	66.50
1200.0	0.00	0.0	0.0	0.0	0.00	66.50



proposed RISER REPLACEMENT FOR PRINTPACT INC.

Page 1
Return Frequency: 100 years

TR-55 TABULAR HYDROGRAPH METHOD Type II. Distribution (24 hr. Duration Storm)

Executed: 01-29-1998 12:53:58
Watershed file: --> C:\86120-~1\WSHED .MOP
Hydrograph file: --> C:\86120-~1\SITE100.HYD

PrintPack 86120-103

Hydrographs for drainage area to existing BMP No changes in hydrographs for Print Pack project

>>>> Input Parameters Used to Compute Hydrograph <<<<

Subarea Description	AREA (acres)	CN	Tc (hrs)	* Tt (hrs)	Precip.		Ia/p input/used
area to BMP	18.70	90.0	0.20	0.00	7.68	6.49	I.03 .10

^{*} Travel time from subarea outfall to composite watershed outfall point.

Total area = 18.70 acres or 0.02922 sq.mi Peak discharge = 152 cfs

>>>> Computer Modifications of Input Parameters <<<<

Subarea Description	Input Tc (hr)	Values * Tt (hr)	Rounded Tc (hr)	Values * Tt (hr)	Ia/p Interpolated (Yes/No)	l Ia/p Messages
area to BMP	0.17	0.00	0.20	0.00	No	Computed Ia/p < .1

^{*} Travel time from subarea outfall to composite watershed outfall point.

I -- Subarea where user specified interpolation between Ia/p tables.

Page 2
Return Frequency: 100 years

TR-55 TABULAR HYDROGRAPH METHOD
Type II. Distribution
(24 hr. Duration Storm)

Executed: 01-29-1998 12:53:58
Watershed file: --> C:\86120-~1\WSHED .MOP

Hydrograph file: --> C:\86120-~1\SITE100.HYD

PrintPack 86120-103

Hydrographs for drainage area to existing BMP No changes in hydrographs for Print Pack project

>>>> Summary of Subarea Times to Peak <<<<

	Peak Discharge at Composite Outfall	Time to Peak at Composite Outfall
Subarea	(cfs)	(hrs)
area to BMP	152	12.2
Composite Watershed	152	12.2

Page 3
Return Frequency: 100 years

TR-55 TABULAR HYDROGRAPH METHOD Type II. Distribution (24 hr. Duration Storm)

Executed: 01-29-1998 12:53:58

Watershed file: --> C:\86120-~1\WSHED .MOP Hydrograph file: --> C:\86120-~1\SITE100.HYD

PrintPack 86120-103

Hydrographs for drainage area to existing BMP No changes in hydrographs for Print Pack project

	(Composi	te Hydro	ograph :	Summary	(cfs)			
Subarea Description	11.0 hr	11.3 hr	11.6 hr	11.9 hr	12.0 hr	12.1 hr	12.2 hr	12.3 hr	12.4 hr
area to BMP	4	6	9	40	76	140	152	91	47
Total (cfs)	4	6	9	40	76	140	152	91	47
Subarea Description	12.5 hr	12.6 hr	12.7 hr	12.8 hr	13.0 hr	13.2 hr	13.4 hr	13.6 hr	13.8 hr
area to BMP	31	24	19	16	13	12	10	9	8
Total (cfs)	31	24	19	16	13	12	10	9	8
Subarea Description	14.0 hr	14.3 hr	14.6 hr	15.0 hr	15.5 hr	16.0 hr	16.5 hr	17.0 hr	17.5 hr
area to BMP	8	7	6	6	5	5	4	4	4
Total (cfs)	8	7	6	6	5	5	4	4	4
Subarea Description	18.0 hr	19.0 hr	20.0 hr	22.0 hr	26.0 hr				
area to BMP	3	3	2	2	0				
Total (cfs)	3	3	2	2	0				

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

**** COMPOSITE OUTFLOW SUMMARY ****

Elevation (ft)	Q (cfs)	Contributing	Structures
66.50	0.0	1	
67.00	0.8	1	
67.18	1.0	2	
67.50	1.4	2	
68.00	1.8	2	
68.50	2.2	2	
69.00	2.5	2	
69.50	2.8	2	
70.00	3.0	2	
70.50	3.3	2	
71.00	14.0	3 +2	
71.50	39.1	3 +2	
72.00	46.6	4 +2	
72.50	48.3	4 +2	
73.00	49.9	4 +2	
73.50	127.4	4 +2 +8	
74.00	309.1	4 +2 +8	

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

Outlet Structure File: C:\86120-~1\MODEXST3.STR Planimeter Input File: C:\86120-~1\EXIST .VOL Rating Table Output File: C:\86120-~1\MODEXST3.PND

Min. Elev. (ft) = 66.5 Max. Elev. (ft) = 74 Incr. (ft) = .5

> Structure No. Q Table Q Table --------STAND PIPE 3
> CULVERT-CR 4 ? 3
> ORIFICE-VC 2 -> 3 -> 5 2 -> TABLE 1 1 -> -> 8 WEIR-VR 8

Outflow rating table summary was stored in file: C:\86120-~1\MODEXST3.PND

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

>>>>> Structure No. 3 <<<<< (Input Data)

STAND PIPE Stand Pipe with weir or orifice flow

E1 elev.(ft)? 70.6
E2 elev.(ft)? 74.001
Crest elev.(ft)? 70.6
Diameter (ft)? 4
Weir coefficient? 3.3
Orifice coefficient? 0.6
Start transition elev.(ft) @ ?
Transition height (ft)?

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

>>>>> Structure No. 4 <<<<< (Input Data)

CULVERT-CR

Circular Culvert (With Inlet Control)

E1 elev.(ft)?	70.6
E2 elev.(ft)?	74.001
Diam. (ft)?	2
<pre>Inv. el.(ft)?</pre>	63.62
Slope (ft/ft)?	.02
T1 ratio?	
T2 ratio?	
K Coeff.?	.0078
M Coeff.?	2.0
c Coeff.?	.0379
Y Coeff.?	.69
Form 1 or 2?	1
Slope factor?	-0.5

POND-2 Version: 5.20 S/N:

Date Executed: Time Executed:

Print Pack 86120-103 change riser structure

>>>>> Structure No. 2 <<<<< (Input Data)

ORIFICE-VC Orifice - Vertical Circular

E1 elev.(ft)?	67.17
E2 elev.(ft)?	74.001
Orifice coeff.?	0.6
<pre>Invert elev.(ft)?</pre>	66.5
Datum elev.(ft)?	66.83
Diameter (ft)?	0.67

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

>>>>> Structure No. 1 <<<<< (Input Data)

TABLE

Constant (ft) added to each elevation was:

Elev. (ft)	Q (cfs)
66.5	0
66.83	.5
67.16	1

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

>>>>> Structure No. 8 <<<<< (Input Data)

WEIR-VR

Weir - Vertical Rectangular

E1 elev.(ft)?	73.1
E2 elev.(ft)?	74.001
Weir coefficient?	3.0
Weir elev.(ft)?	73.1
Length (ft)?	100
Contracted/Suppressed	(C/S)? S

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

Outflow Rating Table for Structure #3 STAND PIPE Stand Pipe with weir or orifice flow

***** INLET CONTROL ASSUMED *****

Elevation (ft)	Q (cfs)	Computation Messages
66.50 67.00 67.18 67.50 68.00 68.50 69.00 69.50	0.0 0.0 0.0 0.0 0.0 0.0 0.0	E < Inv.El.= 70.6 E < E1=70.6 E < E1=70.6
70.50 71.00 71.50 72.00 72.50 73.00 73.50 74.00	0.0 10.5 35.4 68.7 83.4 93.7 103.0 111.6	E < E1=70.6 Weir:

Weir Cw = 3.3 Weir length = 12.56637 ft
Orifice Co = .6 Orifice area = 12.56637 sq.ft.
Q (cfs) = (Cw * L * H**1.5) or (Co * A * sqr(2*g*H))
No transition used, transition height = 0.0
Weir equation = Orifice equation @ elev.= 72.05908 ft

POND-2 Version: 5.20

Date Executed: Time Executed:

S/N:

Print Pack 86120-103 change riser structure

Outflow Rating Table for Structure #4
CULVERT-CR Circular Culvert (With Inlet Control)

***** INLET CONTROL ASSUMED *****

Elevation (ft)	Q (cfs)	Computation	Messages
Elevation (ft) 66.50 67.00 67.18 67.50 68.00 68.50 69.00 69.50 70.00 70.50 71.00 71.50 72.00 72.50 73.00	Q (cfs) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	E < E1=70.6 E < E1=70.6 Submerged:	Messages HW =7.38 HW =7.880 HW =8.38 HW =8.88 HW =9.38
73.50 74.00	47.1 48.4	Submerged: Submerged:	HW =9.88 HW =10.38

Used Unsubmerged Equ. Form (1) for elev. less than 65.87 ft Used Submerged Equation for elevations greater than 66.189 ft HW=Headwater (ft) dc=Critical depth (ft) Ac=Area (sq.ft) at dc

Transition flows interpolated from the following values: E1=65.87 ft; Q1=15.55 cfs; Dc=1.42 ft; E2=66.189 ft; Q2=17.77 cfs

POND-2 Version: 5.20 S/N:

Date Executed: Time Executed:

Print Pack 86120-103

change riser structure

Outflow Rating Table for Structure #2
ORIFICE-VC Orifice - Vertical Circular

Elevation (ft)	Q (cfs)	Computation Messages
66.50 67.00 67.18	0.0 0.0 1.0	E < E1=67.17 E < E1=67.17 H = .35
67.50 68.00 68.50	$1.4 \\ 1.8 \\ 2.2$	H = .67 H = 1.17 H = 1.67
69.00 69.50	2.5	H =2.17 H =2.67
70.00 70.50	3.0	H =3.17 H =3.67
71.00 71.50 72.00	3.5 3.7 3.9	H =4.17 H =4.67 H =5.17
72.50 72.50 73.00	4.0 4.2	H =5.67 H =6.17
73.50 74.00	4.4	H =6.670 H =7.170

C = .6 A = .3525653 sq.ft. H (ft) = Table elev. - Datum elev. (66.83 ft)

Q (cfs) = C * A * sqr(2g * H)

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

Outflow Rating Table for Structure #1
TABLE Input your own rating table.

Elevation (ft)	Q (cfs)	Computation Messages
66.50	0.0	
67.00	0.8	Interpolated from input table
67.18	0.0	E = or > E2 = 67.16
67.50	0.0	E = or > E2 = 67.16
68.00	0.0	E = or > E2 = 67.16
68.50	0.0	E = or > E2 = 67.16
69.00	0.0	E = or > E2 = 67.16
69.50	0.0	E = or > E2 = 67.16
70.00	0.0	E = or > E2 = 67.16
70.50	0.0	E = or > E2 = 67.16
71.00	0.0	E = or > E2 = 67.16
71.50	0.0	E = or > E2 = 67.16
72.00	0.0	E = or > E2 = 67.16
72.50	0.0	E = or > E2 = 67.16
73.00	0.0	E = or > E2 = 67.16
73.50	0.0	E = or > E2 = 67.16
74.00	0.0	E = or > E2=67.16

POND-2 Version: 5.20 S/N:

Date Executed: Time Executed:

Print Pack 86120-103

change riser structure

Outflow Rating Table for Structure #8
WEIR-VR Weir - Vertical Rectangular

***** INLET CONTROL ASSUMED *****

Q (cfs)	Computation Messages
Q (cfs) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	E < Inv.El.= 73.1 E < Inv.El.= 73.1
0.0 0.0 75.9 256.1	E < Inv.El.= 73.1 E < Inv.El.= 73.1 H = .4 H = .9
	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

C = 3 L (ft) = 100

H (ft) = Table elev. - Invert elev. (73.1 ft)
Q (cfs) = C * L * (H**1.5) -- Suppressed Weir

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

Print Pack 86120-103

change riser structure

Outflow Rating Table 5 Table 5 = 3 ? 4

Elevation (ft)	Q (cfs)	Contributing	Structures
66.50	0.0	-	
67.00	0.0		
67.18	0.0	-	
67.50	0.0	_	
68.00	0.0	<u>-</u>	
68.50	0.0	-	
69.00	0.0	- ,	
69.50	0.0	-	
70.00	0.0	_	
70.50	0.0	-	
71.00	10.5	3	
71.50	35.4	3	
72.00	42.8	4	
72.50	44.3	4	
73.00	45.7	4	
73.50	47.1	4	
74.00	48.4	4	

EXECUTED: 01-29-1998 12:52:12

* Print Pack *

* 86120-103 *

* existing pond *

*

Inflow Hydrograph: C:\86120-~1\SITE100 .HYD
Rating Table file: C:\86120-~1\EXIST .PND

----INITIAL CONDITIONS---Elevation = 66.50 ft
Outflow = 0.00 cfs
Storage = 0.00 ac-ft

GIVEN POND DATA

INTERMEDIATE ROUTING COMPUTATIONS

	- <i></i>			
ELEVATION		STORAGE	2S/t	2S/t + 0
(ft)	(cfs)	(ac-ft)	(cfs)	(cfs)
66.50	0.0	0.000	0.0	0.0
67.00	0.2	0.008	1.8	2.0
67.50	0.8	0.039	9.5	10.3
68.00	9.4	0.094	22.6	32.0
68.50	16.3	0.178	43.0	59.3
69.00	19.7	0.301	72.9	92.6
69.50	22.5	0.464	112.3	134.8
70.00	25.1	0.664	160.6	185.7
70.50	27.4	0.898	217.4	244.8
71.00	29.6	1.166	282.2	311.8
71.50	31.6	1.469	355.4	387.0
72.00	33.4	1.807	437.4	470.8
72.50	35.2	2.182	528.1	563.3
73.00	36.9	2.593	627.6	664.5
73.50	114.4	3.023	731.6	846.0
74.00	296.2	3.453	835.6	1131.8
				

Time increment (t) = 6.0 min.

POND-2 Version: 5.20 S/N:

EXECUTED: 01-29-1998 12:52:12

************* SUMMARY OF ROUTING COMPUTATIONS ***********

Pond File: C:\86120-~1\EXIST .PND Inflow Hydrograph: C:\86120-~1\SITE100 .HYD Outflow Hydrograph: C:\86120-~1\OUT .HYD

Starting Pond W.S. Elevation = 66.50 ft

***** Summary of Peak Outflow and Peak Elevation *****

Peak Inflow = 152.00 cfs Peak Outflow = 72.37 cfs Peak Elevation = 73.23 ft

***** Summary of Approximate Peak Storage *****

Warning: Inflow hydrograph truncated on left side.

POND-2 Version: 5.20 S/N: Page 7

Pond File: C:\86120-~1\EXIST .PND Inflow Hydrograph: C:\86120-~1\SITE100 .HYD Outflow Hydrograph: C:\86120-~1\OUT .HYD

EXECUTED: 01-29-1998

12:52:12

Peak Inflow = 152.00 cfs Peak Outflow = 72.37 cfs Peak Elevation = 73.23 ft EXECUTED: 01-29-1998 12:52:30

* Print Pack *

* 86120-103 *

* change riser structure *

* *

Inflow Hydrograph: C:\86120-~1\SITE100 .HYD
Rating Table file: C:\86120-~1\MODEXST3.PND

----INITIAL CONDITIONS---Elevation = 66.50 ft
Outflow = 0.00 cfs
Storage = 0.00 ac-ft

GIVEN POND DATA

INTERMEDIATE ROUTING COMPUTATIONS

ELEVATION	OUTFLOW	STORAGE	2S/t	2S/t + 0
(ft)	(cfs)	(ac-ft)	(cfs)	(cfs)
66.50	0.0	0.000	0.0	0.0
67.00	0.8	0.008	1.8	2.6
67.18	1.0	0.017	4.1	5.1
67.50	1.4	0.039	9.5	10.9
68.00	1.8	0.094	22.6	24.4
68.50	2.2	0.178	43.0	45.2
69.00	2.5	0.301	72.9	75.4
69.50	2.8	0.464	112.3	115.1
70.00	3.0	0.664	160.6	163.6
70.50	3.3	0.898	217.4	220.7
71.00	14.0	1.166	282.2	296.2
71.50	39.1	1.469	355.4	394.5
72.00	46.6	1.807	437.4	484.0
72.50	48.3	2.182	528.1	576.4
73.00	49.9	2.593	627.6	677.5
73.50	127.4	3.023	731.6	859.0
74.00	309.1	3.453	835.6	1144.7

Time increment (t) = 6.0 min.

POND-2 Version: 5.20 S/N:

EXECUTED: 01-29-1998 12:52:30

********** SUMMARY OF ROUTING COMPUTATIONS ************

Pond File: C:\86120-~1\MODEXST3.PND Inflow Hydrograph: C:\86120-~1\SITE100 .HYD Outflow Hydrograph: C:\86120-~1\OUT .HYD

Starting Pond W.S. Elevation = 66.50 ft

***** Summary of Peak Outflow and Peak Elevation *****

Peak Inflow = 152.00 cfs Peak Outflow = 111.46 cfs Peak Elevation = 73.40 ft

***** Summary of Approximate Peak Storage *****

Initial Storage = 0.00 ac-ft
Peak Storage From Storm = 2.93 ac-ft
Total Storage in Pond = 2.93 ac-ft

Warning: Inflow hydrograph truncated on left side.

POND-2 Version: 5.20 S/N: Page 7

Pond File: C:\86120-~1\MODEXST3.PND Inflow Hydrograph: C:\86120-~1\SITE100 .HYD Outflow Hydrograph: C:\86120-~1\OUT .HYD

EXECUTED: 01-29-1998

12:52:30

Peak Inflow = 152.00 cfs Peak Outflow = 111.46 cfs Peak Elevation = 73.40 ft

