

CERTIFICATE OF AUTHENTICITY

THIS IS TO CERTIFY THAT THE FOLLOWING ELECTRONIC RECORDS ARE TRUE AND ACCURATE REPRODUCTIONS OF THE ORIGINAL RECORDS OF JAMES CITY COUNTY GENERAL SERVICES DEPARTMENT- STORMWATER DIVISION; WERE SCANNED IN THE REGULAR COURSE OF BUSINESS PURSUANT TO GUIDELINES ESTABLISHED BY THE LIBRARY OF VIRGINIA AND ARCHIVES; AND HAVE BEEN VERIFIED IN THE CUSTODY OF THE INDIVIDUAL LISTED BELOW.

BMP NUMBER: CC-029

DATE VERIFIED: March 16, 2012

QUALITY ASSURANCE TECHNICIAN:

Leah Hardenbergh

Leah Hardenbergh

LOCATION: WILLIAMSBURG, VIRGINIA



Stormwater Division

MEMORANDUM

DATE:	March 11, 2010
TO:	Michael J. Gillis, Virginia Correctional Enterprises Document Management Services
FROM:	Jo Anna Ripley, Stormwater
PO:	270712
RE:	Files Approved for Scanning

General File ID or BMP ID: CC029

PIN: 3910100001

Subdivision,	Tract,	Business	or	Owner
N T				

Name (if known):				Dumont	, Pamela N	
Property Description	:			Godspee	d Animal Clini	с
Site Address:				102 Tew	ning Road	
(For internal use only)	Box	12		Drawer:	7	
Agreements: (in file as of scan date)	Y		Book or Doc#:		040029617	Page:
					010007854	

Comments

CONCERCION OF

CC029

Contents for Stormwater Management Facilities As-built Files

Each file is to contain:

- 1.) As-built plan
 - Completed construction certification
- 2 Completed construction c
 3 Construction Plan
 4 Design Calculations
 5 Watershed Map
 6 Maintenance Agreement
- 7. Correspondence with owners
- 8 **Inspection Records**
- **Enforcement Actions** 9.

040029617

COUNTY OF JAMES CITY, VIRGINIA

DECLARATION OF COVENANTS

INSPECTION/MAINTENANCE OF DRAINAGE SYSTEM

THIS DECLARATION, ma	dathis Ath	day of	May	.20 04.
		day of	TUOV	, 20,
between Pam Dum	ront_	·		, and
all successors in interest, ("COVEN				erty:
Street Address: <u>102</u> TE W Legal Description: <u>ROPER</u> Project Name: <u>Goodspeed</u>	NINCR	OAD		
Legal Description:	ANDT	TLLAG	E	
Project Name: Goodspeed	Animal C	are Expa	insion	
Document No. 01000 7854,	Deed Book		, Page 1	No;
Instrument No.	, and the <u>Co</u>	ounty of James	<u>City, Virginia</u> ("COUNTY.")

WITNESSETH:

We, the COVENANTOR(S), with full authority to execute deeds, mortgages, other covenants, and all rights, titles and interests in the property described above, do hereby covenant with the COUNTY as follows:

1. The COVENANTOR(S) shall provide maintenance for the drainage system including any runoff control facilities, conveyance systems and associated easements, hereinafter referred to as the "SYSTEM," located on and serving the above-described property to ensure that the SYSTEM is and remains in proper working condition in accordance with approved design standards, and with the law and applicable executive regulations. The SYSTEM shall not include any elements located within any Virginia Department of Transportation rights-of-way.

2. If necessary, the COVENANTOR(S) shall levy regular or special assessments against all present or subsequent owners of property served by the SYSTEM to ensure that the SYSTEM is properly maintained.

3. The COVENANTOR(S) shall provide and maintain perpetual access from public right-of-ways to the SYSTEM for the COUNTY, its agent and its contractor.

4. The COVENANTOR(S) shall grant the COUNTY, its agent and its contractor a right of entry to the SYSTEM for the purpose of inspecting, monitoring, operating, installing, constructing, reconstructing, maintaining or repairing the SYSTEM.

5. If, after reasonable notice by the COUNTY, the COVENANTOR(S) shall fail to maintain the SYSTEM in accordance with the approved design standards and with the law and applicable executive regulations, the COUNTY may perform all necessary repair or maintenance work, and the COUNTY may assess the COVENANTOR(S) and/or all property served by the SYSTEM for the cost of the work and any applicable penalties.

3

6. The COVENANTOR(S) shall indemnify and save the COUNTY harmless from any and all claims for damages to persons or property arising from the installation, construction, maintenance, repair, operation or use of the SYSTEM.

The COVENANTOR(s) shall promptly notify the COUNTY when the 7. COVENANTOR(S) legally transfers any of the COVENANTOR(S)' responsibilities for the SYSTEM. The COVENANTOR(S)' shall supply the COUNTY with a copy of any document of transfer, executed by both parties.

8. The covenants contained herein shall run with the land and shall bind the COVENANTOR(S) and the COVENANTOR(S)' heirs, executors, administrators, successors and assignees, and shall bind all present and subsequent owners of property served by the SYSTEM.

9. This COVENANT shall be recorded in the County Land Records.

IN WITNESS WHEREOF, the COVENANTOR(S) have executed this DECLARATION OF COVENANTS as of the date first above written.

COVENANTOR(S)

Print Name/Title Pam Dumont

ATTEST:

Kimberly Padgett

COVENANTOR(S)

ATTEST:

Print Name/Title

COMMONWEALTH OF_VIRGINIA CITY/COUNTY OF James City

I hereby certify that on this <u>Bin</u> day of <u>New mber</u>, 20<u>04</u>, before the subscribed, a Notary Public of the State of Virginia, and for the City/County of Kimes City, aforesaid personally appeared <u>famela Dumant</u> and did acknowledge the aforegoing instrument to be their Act.

IN WITNESS WHEREOF, I have hereunto set my hand and official seal this $\underline{\mathcal{B}^{H}}$ day of <u>November</u>, 20 <u>04</u>.

<u>n J. Mendcoli.</u> Iblic

My Commission expires: ______

Approved as to form:

Ass County Attorney

VIRGINIA: CITY OF WILLIAMSBURG & COUNTY OF JAMES CIT This document was admitted to record on 23 100 4 at AM/DH. The taxes imposed by Virginia Code Section 58.1-801, 58.1-802 & 58.1-814 have been paid. STATE TAX LOCAL TAX ADDITIONAL TAX	e
* TESTE: BETSY B. WOOLRIDGE, CLERK BY. Retry & Woolriche Clerk	

drainage.pre

This Declaration of Covenants prepared by:

Pamela N. Dumont

(Print Name)

President / Owner

(Title)

113 Forest Ln.

(Address)

Williamsburg VA 23183 (State) (City) (Zip)

3910/00001

James City County Environmental Division James City County Environmental Division Stormwater Management/BMP Record Drawing and Construction Certification Review Environmental Division Tracking Form

SP-70-04 County Plan No.: GODS PEED ANIMAL CARE Project Name: Stormwater Management Facility: ___ GOUNTY TYPE D-2 SURF SAND BMP Phase #: Ι Π 'III . Date/By: Avg 17 05 Information Package Received. Completeness Check: Date/By: <u>Arg 17 05</u> Date/By: <u>DE2 08 05</u> Record Drawing Construction Certification (Required for all BMPs after Feb 1st 2001Only) # / Date: #040029616 NOV 23 04 RD/CC Standard Forms ∎Insp/Maint Agreement Location: Sheet C-4 BMP Maintenance Plan □ Other:

 Standard E&SC Note on Approved Plan Requiring RD/CC or County comment in plan review file.

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 Standard E&SC N SITVATED IN PC DRAINS TO CITY Assign County BMP ID Code #: CC 029 Code: COLL. CREEK Preliminary Input/Log into Division's"As-Built Tracking Log" Add Location to GIS Database Map. Obtain basic site information (GPIN, Owner, Address, etc.) Preliminary Log into Access Database (BMP ID #, Plan No., GPIN, Project Name, etc.) Active Project File Review (correspondence, H&H, design computations, etc.). Anitial As-Built File setup (File label, folder, copy plan/details/design information, etc.). Conspector Check of RD/CC (forward to Inspector using transmittal for cursory review). Pre-Inspection Drawing Review of Approved Plan (Quick look prior to Field Inspection). Date: 10/07/05 Date: MAY 15 06 Final Inspection (FI) Performed Record Drawing (RD) Review Construction Certification (CC) Review Date: EMAIL ISSVED OFC 01 05 □ Actions: □ No comments. Date: Email issued CL, CR to Henderson Comments. Letter Forwarded. □ Record Drawing (RD) □ Construction Certification (CC) □ Construction-Related (CR) □ Site Issues (SI) □ Other : Second Submission: CONST CERT DELOBOS COOK Reinspection (if necessary): <u>*ORIVEST ON SEV OCLASSIONS (m/ Nob Gors there!!)*</u> Acceptable for SWM Purposes (RD/CC/CR/Other). Ok to proceed with bond release process. Complete"Surety Request Form'. Check/Clean active file of any remaining material and finish"As-Built'file. Add to County BMP Inventory/Inspection schedule (Phase I, II or III). Copy Final Inspection Report into County BMP Inspection Program file. Cobtain Digital Photographs of BMP and save into County BMP Inventory. Request mylar/reproducible from As-Built plan preparer. LAND TECH UNA PHONE 5.15.00 Complete"As-built Tracking Log'. REVENVED 5-26-06 -Aast check of BMP Access Database (County BMP Inventory). Add BMP to JCC Hydrology & Hydraulic database (optional). -Add BMP to PRIDE BMP ratings database. Final Sign-Off Date: ____5-15-06 Plan Reviewer: 1/A *** See separate checklist /if heeded.

Const Call



James City County, Virginia Environmental Division

REC	CEI	VED	
DEC	13	2005	
	RONME		

Stormwater Management / BMP Facilities Record Drawing and Construction Certification Forms

(Note: In accordance with the requirements of the Chesapeake Bay Preservation Ordinance, Chapter 23, Section 23-10(4), BMP's shall be designed and constructed in accordance with the manual entitled James City County Guidelines for Design and Construction of Stormwater Management BMP's. Erosion and sediment control policy and approved plans generally require that at the completion of the project and prior to release of surety, an "as-built" plan prepared by a registered Professional Engineer or Certified Land Surveyor must be provided for the drainage system for the project, including any Best Management Practice (BMP) facilities. In addition, for BMP facilities involving the construction of an impounding structure or dam embankment, certification is required by a Professional Engineer who has inspected the structure during its construction. Currently there are over 20 water quality type BMP's accepted by the County.)

Section 1 - Site Information:

Project Name: Structure/BMP Project Location BMP Location: County Plan No	Name: <u>Cou</u> n: <u>Drt</u> 102	evsection		c Sand Fil Rol + Tewnin	g Ro,	
Project Type:	 Residential Commercial Institutional Public Other 	Business O Office Industrial Roadway	Tax Map/Parcel No.: BMP ID Code (if know Zoning District:: Land Use: Site Area (sf or acres):	/n): 	ang Clints	,
Type	n of Stormwater N D-2 Sur Surhersy	face San		Crty Co Bated a penty	v nty	- - -
Nearest Visible	Landmark to SWN		sus Corner a and Tewning		conbound	Rð
D UCC	Ground Control (Geodetic Ground Number or Name:	if known): Control 🗇 USG	S 🗆 Temporary	□ Arbitrary	Other	
Control Control	Location from Su	bject Facility: C	67 Set in couc outrol location Red from the	n to approx		vance

Section 2 - Stormwater Management / BMP Facility Construction Information:

PreConstruction Meeting Held for Construction of SWM/BMP Facility: Approx. Construction Start Date for SWM/BMP Facility:		🗖 No	LUnknown
Facility Monitored by County Representative during Construction: Name of Site Work Contractor Who Constructed Facility:	🗂 Yes	□No neval	BUnknown Contractors
Name of Professional Firm Who Routinely Monitored Construction:k Date of Completion for SWM/BMP Facility:k	COWN		
Date of Record Drawing/Construction Certification Submittal:			

(Note: Record Drawing and Construction Certifications are required within thirty (30) days of the completion of Stormwater Management and/or BMP facility construction. Record Drawings and Construction Certifications must be reviewed and approved by the James City County Environmental Division prior to final inspection, acceptance and bond or surety release.)

Section 3 - Owner / Designer / Contractor Information:

Owner/Developer:

(Note: Site Owner or Applicant responsible for development of the project.)

Name: Dr. F	amela Dun	iont	·····
Mailing Address:	102 Tewnin	g Rd.	-
C	willrausbu	ig, Va. 2318	5
Business Phone:	253-0656	Fax: 25	3-1080
	Panela Dou	iont Title: Or	<u>}</u>

Design Professional:

(Note: Professional Engineer or Certified Land Surveyor responsible for the design and preparation of plans and specifications for the Stormwater Management / BMP facility.)

Firm Name: Vanasse Hangen Brustlin, Inc
Mailing Address: 115 South 15th Street, Surte 200
Richmond, Va. 23219
Business Phone: (804) 343-7100
Fax: (804) 343-1713
Responsible Plan Preparer: Steven O. Wigley P.E. #019307
Title: Professional Engineer
Plan Name: GOOSpeed Anrwel Cove
Firm's Project No. 31248.01
Plan Date: 1015 104
Sheet No.'s Applicable to SWM/BMP Facility: C-3/C-4 / C-5 / C-7 /

BMP Contractor:

(Note: Site Work Contractor directly responsible for construction of the Stormwater Management / BMP facility.)

Name: Henderson, General Contractors
Mailing Address: 5800 Hoovetown Ro.
Williamsburg, Va. 23188
Business Phone: 565-1090
Fax: 564-9120
Contact Person: Bruce Gillian
Site Foreman/Supervisor: Bruce Grilliam
Specialty Subcontractors & Purpose (for BMP Construction Only):

Section 4 - Professional Certifications:

Certifying Professionals: (Note: A Registered Professional Engineer or Certified Land Surveyor is responsible for preparation of a Record Drawing, sometimes referred to as an As-Built plan, for the drainage system for the project including any Stormwater Management/BMP Facilities. A Registered Professional Engineer is responsible for the inspection, monitoring and certification of Stormwater Management / BMP facilities during its construction.)

Record Drawing and Construction Certifications for Stormwater Management / BMP Facilities

Record Drawing Certification

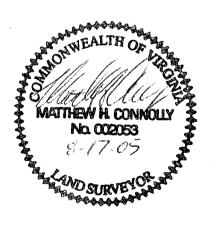
Firm Name: <u>LandTech</u> Resources, Du Mailing Address: <u>5810-F Moorctown</u> Ra Willram 360m, Ve. 23188	<u>،</u>
Business Phone: 565-1677	
Fax: 565-0782	
Name: <u>Matthew Connolly</u> Title: Prostdent	
Signature: Martin Cull	
Date: 8-17.2005	

I hereby certify to the best of my knowledge and belief that this record drawing represents the actual condition of the Stormwater Management / BMP facility. The facility appears to conform with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.

Construction Certification
Firm Name: VANAGE HANGEN BRUSTLIN, Inc
Mailing Address: 115 South 15th St.
Rickmoud VA Z3185
Business Phone: 804 - 323 - 7100
Fax:
Name: Richard S. H. Thips, Title: DENICO FONGLAISED
Signature:
Date: 72/8/05

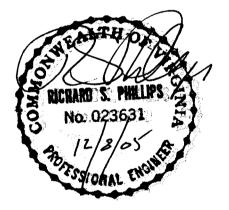
Construction Cortification

I hereby certify to the best of my knowledge and belief that this Stormwater Management/BMP facility was monitored and constructed in accordance with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.



(Seal)

Virginia Registered Professional Engineer or Certified Land Surveyor



(Seal)

Virginia Registered **Professional Engineer**

Section 5 - Record Drawing and Construction Certification Requirements and Instructions:

X

X

PreConstruction Meeting - Provides an opportunity to review SWM / BMP facility construction, maintenance and operation plans and address any questions regarding construction and/or monitoring of the structure. The design engineer, certifying professionals (if different), Owner/Applicant, Contractor and County representative(s) are encouraged to attend the preconstruction meeting. Advanced notice to the Environmental Division is requested. Usually, this requirement can be met simultaneously with Erosion and Sediment Control preconstruction meetings held for the project.

A fully completed STORMWATER MANAGEMENT / BMP FACILITIES, RECORD DRAWING and CONSTRUCTION CERTIFICATION FORM and RECORD DRAWING CHECKLIST. All applicable sections shall be completed in their entirety and certification statements signed and sealed by the registered professional responsible for individual record drawing and/or construction certification.

The Record Drawing shall be prepared by a Registered Professional Engineer or Certified Land Surveyor for the drainage system of the project including any Best Management Practices.

Construction Certification. Construction of Stormwater Management / BMP facilities which contain impoundments, embankments and related engineered appurtenances including subgrade preparation, compacted soils, structural fills, liners, geosynthetics, filters, seepage controls, cutoffs, toe drains, hydraulic flow control structures, etc. shall be visually observed and monitored by a Registered Professional Engineer or his/her authorized representative. The Engineer must certify that the structure, embankment and associated appurtenances were built in accordance with the approved design plan, specifications and stormwater management plan and standard accepted construction practice and shall submit a written certification and/or drawings to the Environmental Division as required. Soil and compaction test reports, concrete test reports, inspection reports, logs and other required construction material or installation documentation may be required by the Environmental Division to substantiate the certification, if specifically requested. The Engineer shall have the authority and responsibility to make minor changes to the approved plan, in coordination with the assigned County inspector, in order to compensate for unsafe or unusual conditions encountered during construction such as those related to bedrock, soils, groundwater, topography, etc. as long as changes do not adversely affect the integrity of the structure(s). Major changes to the approved design plan or structure must be reviewed and approved by the original design professional and the James City County Environmental Division.

Record Drawing and Construction Certifications are required within thirty (30) days of the completion of Stormwater Management / BMP facility construction. Submittals must be reviewed and accepted by James City County Environmental Division prior to final inspection, acceptance and bond/surety release.

Dual Purpose Facilities - Completion of construction also includes an interim stage for Stormwater Management / BMP facilities which serve dual purpose as temporary sediment basins during construction and as permanent stormwater management / BMP facilities following construction, once development and stabilization are substantially complete. For these dual purpose facilities, construction certification is required once the temporary sediment basin phase of construction is complete. Final record drawing and construction certification of additional permanent components is required once permanent facility construction is complete.

Interim Construction Certification is required for those dual purpose embankment-type facilities that are generally ten (10) feet or greater in dam height (*) and may not be converted, modified or begin function as a permanent SWM / BMP structure for a period generally ranging from six (6) to eighteen (18) months or more from issuance of a Land Disturbance permit for construction.

Interim or final record drawing and construction certifications are not required for temporary sediment basins which are designed and constructed in accordance with current minimum standards and specifications for temporary sediment basins per the Virginia Erosion and Sediment Control Handbook (VESCH); have a temporary service life of less than eighteen (18) months; and will be removed completely once associated disturbed areas are stabilized, <u>unless</u> a distinct hazard to the public's health, safety and welfare is determined by the Environmental Division due to the size or presence of the structure or due to evidence of improper construction.

(*Note: Dam Height as referenced above is generally defined as the vertical distance from the natural bed of the stream or waterway at the downstream toe of the embankment to the top of the embankment structure in accordance with 4VAC50-20-30, Virginia Impoundment Structure Regulations and the Virginia Dam Safety Program.)

X

X

Record Drawings shall provide, at a minimum, all information as shown within these requirements and the attached **RECORD DRAWING CHECKLIST** specific to the type of SWM/BMP facility being constructed. Other additional record data may be formally requested by the James City County Environmental Division. (*Note: Refer to the current edition of the James City County Guidelines for Design and Construction of Stormwater Management BMP's manual for a complete list of acceptable BMP's. Currently there are over 20 acceptable water quality type BMP's accepted by the County.)*

Record Drawings shall consist of blue/black line prints and a reproducible (mylar, sepia, diazo, etc.) set of the approved stormwater management plan including applicable plan views, profiles, sections, details, maintenance plans, etc. as related to the subject SWM / BMP facility. The set shall indicate "**RECORD DRAWING**" in large text in the lower right hand corner of each sheet with record elevations, dimensions and data drawn in a clearly annotated format and/or boxed beside design values. Approved design plan values, dimensions and data shall not be removed or erased. Drawing sheet revision blocks shall be modified as required to indicate record drawing status. Elevations to the nearest 0.1' are sufficiently accurate except where higher accuracy is needed to show positive drainage. Certification statements as shown in Section 4 of the Record Drawing and Construction Certification Form, *or similar forms thereof*, and professional signatures and seals, with dates matching that of the record drawing status in the revision or title block, are also required on all associated record drawing plans, prints or reproducibles.

Submission Requirements. Initial and subsequent submissions for review shall consist of a minimum of one (1) blue/black line set for record drawings and one copy of the construction certification documents with appropriate transmittal. Under certain circumstances, it is understood that the record drawing and construction certification submissions may be performed by different professional firms. Therefore, record drawing submission may be in advance of construction certification or vice versa. Upon approval and prior to release of bond/surety, final submission shall include one (1) reproducible set of the record drawings, one (1) blue/black line set of the record drawings and one (1) copy of the construction certification. Also for current and/or future incorporation into the County BMP database and GIS system, it is requested that the record drawings also be submitted to the Environmental Division on a diskette or CD-ROM in an acceptable electronic file format such as *.dxf, *.dwg, etc. or in a standard scanned and readable format. The electronic file requirement can be discussed and coordinated with Environmental Division staff at the time of final submission.

STORMWATER MANAGEMENT / BMP FACILITIES RECORD DRAWING CHECKLIST

(Key for Checklist is as follows: <u>XX</u> Acceptable <u>N/A</u> Not Applicable <u>Inc</u> Incomplete)

- I. <u>Methods and Presentation:</u> (Required for all Stormwater Management / BMP facilities.)
- 1. All constructed facilities meet approved design plans, unless otherwise shown. Record information or deviations from approved design plan shown in clearly annotated format and/or boxed beside design values.
- 2. Elevations to the nearest 0.1' unless higher accuracy is needed to show positive drainage.
- 3. All plan sheets labeled with "RECORD DRAWING" in large text in lower right hand corner (Approved County Plan Number and BMP ID Code can be included if known).
- 4. All plan sheet revision blocks modified to indicate date and record drawing status.
- 5. All plan sheets have certification statements and certifying professional's signature and seal.
- **II.** <u>Minimum Standards:</u> (Required for all Stormwater Management / BMP facilities, as applicable.)
- 1. All requirements of Section I (Methods and Presentation) apply to this section.
- 2. Plan Views: Show general location, arrangement and dimensions. Location and alignment shall generally match approved design plans.
- 3. Profile or elevations along top or berm of the facility. At a minimum, elevations are required at each end, at intervals not to exceed 50 feet and where low spots may be present. Top of embankment or berm elevations must be no less than design elevation plus any settlement allowances.
- \checkmark 4. Top widths, berm widths and embankment side slopes.
- 5. Show length, width and depth of facility or grading, contours or spot elevations as required to verify permanent pool and design storage volumes were met or were reasonably close to the approved design. Evaluation of as-built grading, contours, spot elevations, or cross-sections, may be necessary by the professional to ensure approved design configurations, depths and volumes were closely maintained. If grading or elevations are significantly different from the approved plan, the Environmental Division shall be contacted immediately to determine whether the variation is acceptable or whether further evidence will be required. Facilities which do not closely resemble approved plan grades, elevations or configurations may require regrading by the Contractor; check volumetric computations; and/or a check hydraulic routing to ensure approved design water surface elevations, discharges or freeboard were closely maintained.
- 6. Cross-section of the embankment through the principal spillway or outlet barrel. Must extend at least 100 ft. downstream of the pipe outlet or to recorded site property line, whichever is closer. Proper correlation is required between principal spillway (control structure) crest, emergency spillway crest, orifice and weirs and the top of the dam or facility. All elevations and dimensions must reasonably match the design plan or be sequentially relative to each other and the facility must reflect the required design storage volume(s) and/or design depth.
- **<u>PIP</u>** 7. Profile or elevations along the entire centerline of the emergency spillway. Emergency spillway may be steeper, but no flatter or narrower than design.
- 8. Elevation of the principal spillway crest or outlet crest of the structure.

44	9.	Primary control structure (riser) diameter or dimensions, height, type of material and base size. Indicate provisions for access that are present such as steps, ladders, etc.
YX	10.	Dimensions, locations and elevations of outlet orifices, weirs, slots and drains.
<u> </u>	11.	Type and size of anti-vortex and trash rack device. Height, diameter, dimensions, bar spacings (if applicable) and elevations relative to the principal spillway crest. Indicate if lockable hatch is present or not.
NA	12.	Type, location, size and number of anti-seep collars or documentation of other methods utilized for seepage control. May need to obtain this information during construction.
<u>414</u>	13.	Top of impervious core embankment, core trench limits and elevation of cut-off trench bottom. May need to obtain this information during construction.
	14.	Elevation of the principal spillway barrel (outlet pipe) inlet and outlet invert.
¥	15.	Outlet barrel diameter, length, slope, type and thickness class of material and type of flared end sections, headwall or endwall.
14	16.	Outfall protection dimension, type and depth of rock and if underlain filter fabric is present.
Inc.	17.	BMP interior and periphery landscaping zones conform with arrangements and requirements of the approved design plan.
	18.	Maintenance plan taken from approved design plan transposed onto record drawing set.
MA	19.	Fencing location and type, if applicable to facility.
XX	20.	BMP vicinity properly cleaned of stockpiles and construction debris.
	21.	No visual signs of erosion or channel degradation immediately downstream of facility.
XX-	22.	Any other information formally requested by the Environmental Division specific to the constructed SWM/BMP facility.

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STORMWATER MANAGEMENT / BMP FACILITIES RECORD DRAWING CHECKLIST

(Key for Checklist is as follows: <u>XX</u> Acceptable <u>N/A</u> Not Applicable <u>Inc</u> Incomplete)

- VI. <u>Group D Filtering Systems</u> (Includes D-1 Bioretention Cells; D-2 Surface Sand Filters; D-3 Underground Sand Filters; D-4 Perimeter Sand Filters; D-5 Organic Filters; and D-6 Pocket Sand Filters)
- XX D1. All requirements of Section II, Minimum Standards, apply to Group D facilities.
- **TVA** D2. Sediment pretreatment devices provided.
- D3. For D-1 BMPs (Bioretention Cells), pretreatment consisting of a grass filter strip below level spreader (deflector); a gravel diaphragm; and mulch and planting soil layers were provided.
- D4. For D-1 BMPs (Bioretention Cells), plantings consist of native plant species; vegetation provided was based on zones of hydric tolerances; trees and understory of shrubs and herbaceous materials were provided; woody vegetation is absent from inflow locations; and trees are located around facility perimeter.
- **XX** D5. Facility was not used for erosion and sediment control purposes and sediment was prevented from entering the facility to the greatest extent possible during construction.
- **The**. D6. No visible signs of accumulated silt/sediment were present in the facility following construction or alternately, accumulated silt/sediment was properly removed.
- \checkmark D7. Filtering system is off-line from storm drainage conveyance system.
- 44 D8. Overflow outlet has adequate erosion protection.
- **D**9. Deflector, diversion, flow splitter or regulator structure provided to divert the water quality volume to the filtering structure.
- D10. Minimum four (4) inch perforated underdrain provided in a clean aggregate envelope layer beneath the facility.
- D11. Minimum fifty (50) foot separation from any slope fifteen (15) percent or greater. Minimum one hundred (100) foot separation horizontally from any known water supply well. Minimum one hundred (100) foot separation upslope and twenty-five (25) foot separation downslope from any building.
- <u>744</u> D12. Stabilization and acceptable vegetative cover established over contributing drainage area prior to conveyance of stormwater to the facility.
- \checkmark D13. No visual signs of erosion or channel degradation immediately downstream of facility.
- D14. Adequate, direct access provided to the pretreatment area and/or filter bed for future maintenance.

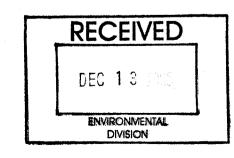


James City County, Virginia Environmental Division

Stormwater Management / BMP Facilities Record Drawing and Construction Certification

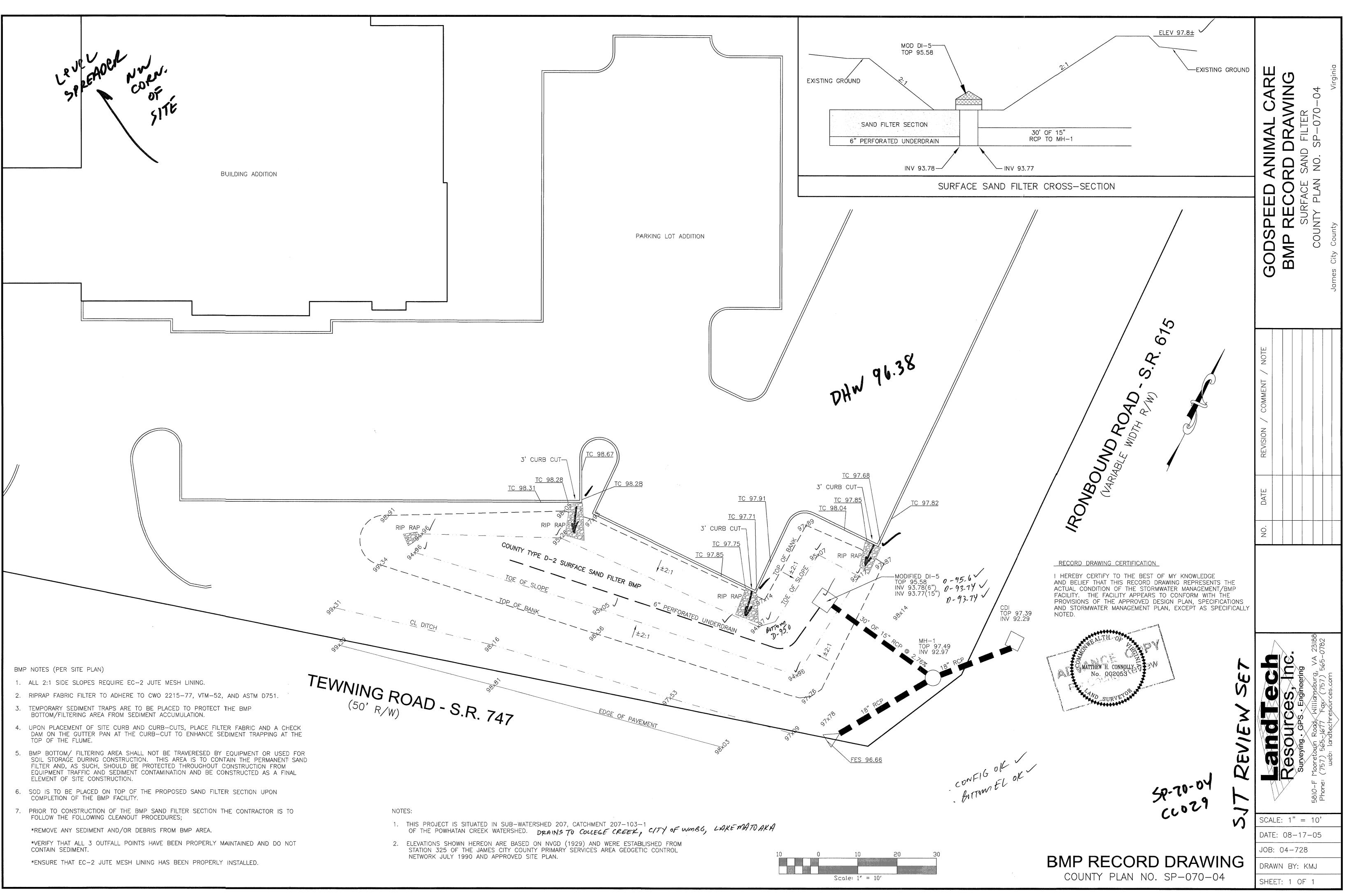
Standard Forms & Instructions

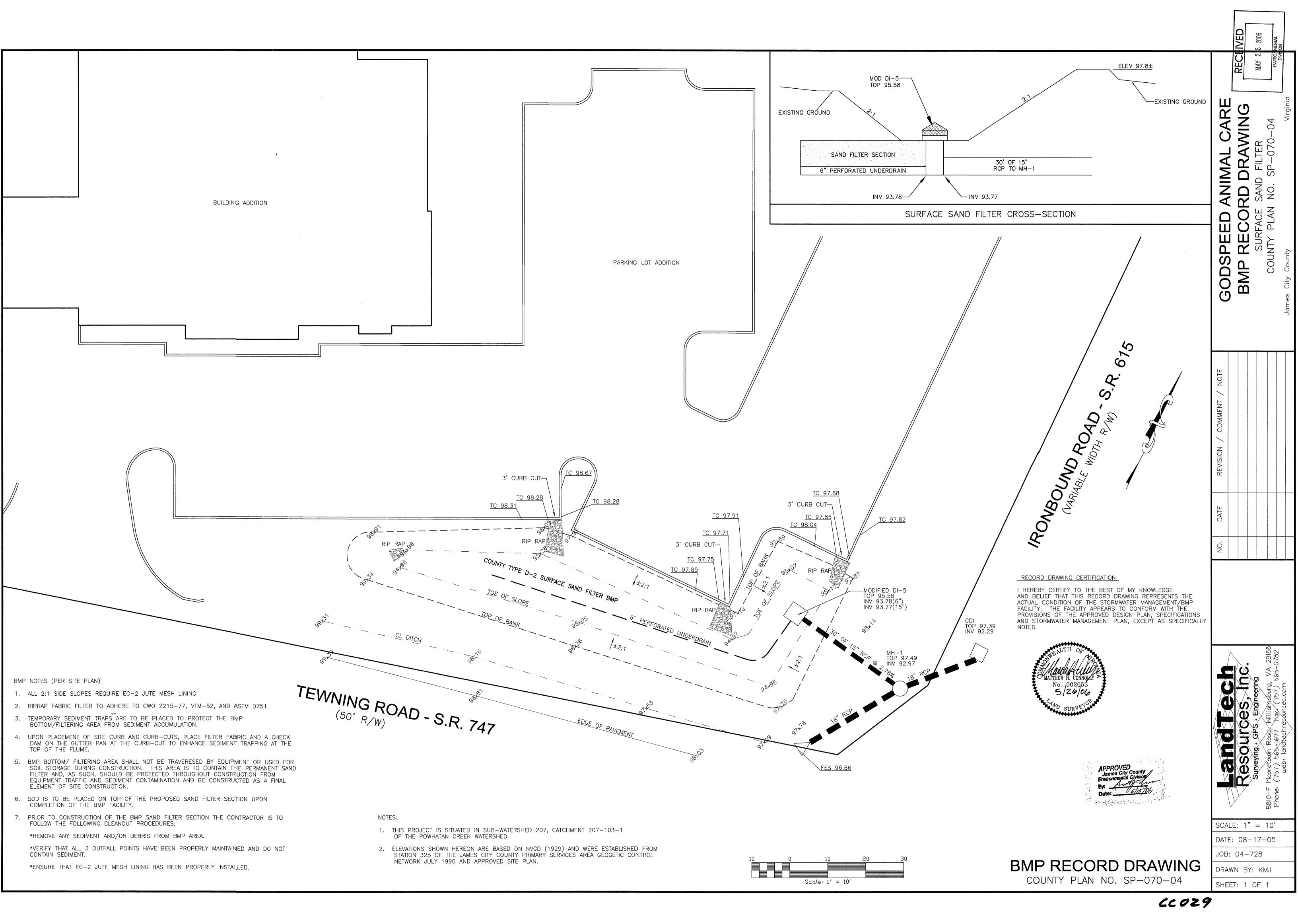
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6005PEED PC197-CC029 5P-70-04

Issue Date February 1, 2001





Transmittal

LandTech Resources, Inc.

Surveying - Mapping - GPS 5810-F Mooretown Road, Williamsburg, VA 23188 Tel: 757-565-1677 Fax: 757-565-0782

To: Scott Thomas, P.E. Company: James City County Environmental Division From: Kenneth Jenkins Date: 8/17/05 Job Name/Number: 05-001

The following have been sent:

as requested

 \boxtimes for review and comment

please sign and return

for temporary use, please return by _____

Quantity Drawing Description Date 8/17/05 Preliminary Record Drawings 1 BMP Record Drawing & Construction Certification Forms 1 8/17/05

Remarks:

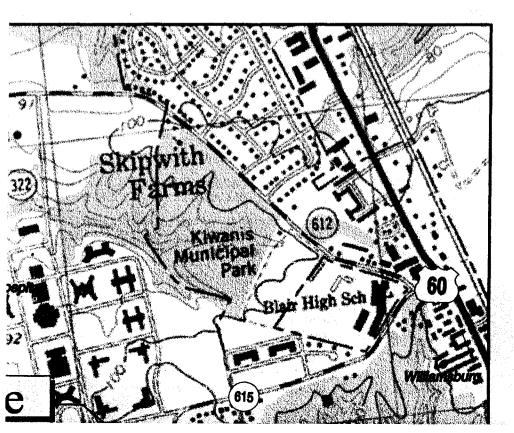
cc:Henderson, Inc.

Signature: Konneel M. Jenker

6005PEED 197 cc029 5P-70-04



odspeed Animal Care Tewning Road (State Route 747) les City County, Virginia



Property Inform: tion

Owner:

Dr. Pamela Dumont 102 Tewning Road Williamsburg, VA 23185

Applicant: Dr. Pamela Dumont

-070-04 SP 59-070-04 COUNTY OF JAMES CITY FINAL SITE PLAN JCC C APPROVALS DATE Fire Dept. NHLEC 6/23/04 NOT BWIEL 10/29/04 4/23/6 Environ DECLEC 11/22/04

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SP-70-04

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g Regulation rements	Required	Provided
E (LOT) SIZE	10,000 sf	63,600 sf
SETBACK NT THERN SIDE" JTHERN SIDE" R	50 FT. 75 FT. 20 FT. 20 FT.	50 FT.± • 20 FT.±••••• 20 FT.± 20 FT.±
JILDING HEIGHT	35'	2 STORY 28'-6
AP PARKING SIZE	9' X 18'	9'X 18'
; SPACE SIZE	9' X 18'	9'X 18'

Land Use Statistics

Total Site Area = 1.46 Acres

Decentration	Exis	ting	Prop	osed	Proposed Percentage	
Description	(S.F.)	(ĀC)	(S.F.)	(AC)	of Total Site	
BUILDING FOOTPRINT	3895	0.09	11,798	0.27	18%	
PAVEMENT	7840	0.18	17,116	0.39	27%	
CONCRETE	719	0.02	1700	0.04	3%	
OPEN SPACE	51144	1.17	32,984	0.76	52%	
TOTAL	63598	1.46	63,598	1.46	100%	

Total Area of Land Disturbance = 0.77 Acres

DISTRICT: M-1: LIMITED BUSINESS/ INDUSTRIAL DISTRICT

Parking S	ummary (Chart	
ption	Existing	Required	Provided
RD SPACES (9'x18')	N/A	40	40***
OF HANDICAPPED - STD.*	_	2	2
PACES	-	42	42
SPACES (10' X 50') **	_	-1	1

6

1

LIMITS OF WORK

14 PIN

SHED

HEADWALL

TOP=96.25 INV=93.78

CMF

REQUIREMENTS

COUNTY ZONING ORDINANCE

ROVED BY THE PLANNING DIRECTOR AT THE E OF CONCEPTUAL VIEW IN ACCORDANCE WITH TION 24-59(D) AND AFTER REVIEWING THE KING QUALIFICATION INFORMATION (SEE BELOW).

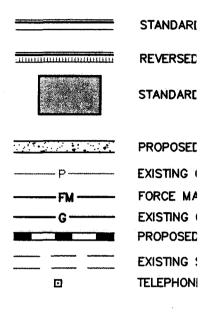
IANCE TO SECTION 24-416 (NOV. 1, 2001), D REGULATIONS, ESTABLISH THE SETBACK 20 FEET FROM NORTHERN MOST PROPERTY WITH THE CONDITION THAT ALL OUTDOOR KENNELS BE LOCATED AT LEAST 35 FEET M THE NORTHERN MOST PROPERTY LINE.

M.U.T.C.D. Number	Specif	Specification					
Number	Width	Height	Desc.				
R7-8	12"	18″	RESERVED PARKING				
R7-8A	12*	6″	VAN ACCESSIBLE				

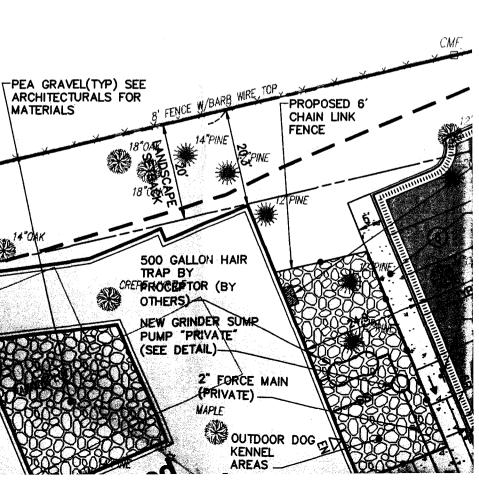
PROPOSED CHAIN LINK FENCE

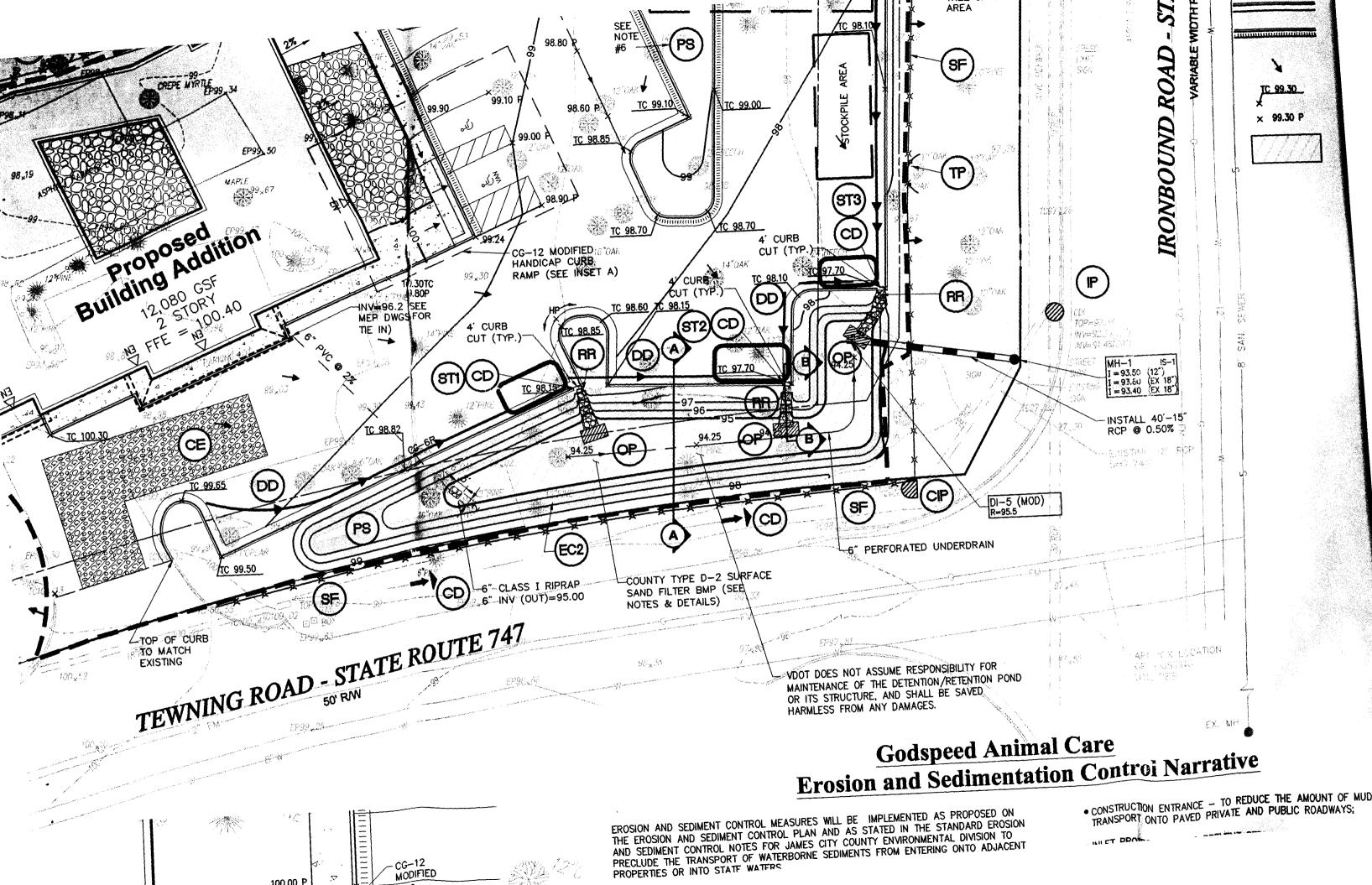
FENCED IN GRAVEL PET AREAS TO BE GRADED AT 2% SLOPE AWAY FROM BUILDING

Legen



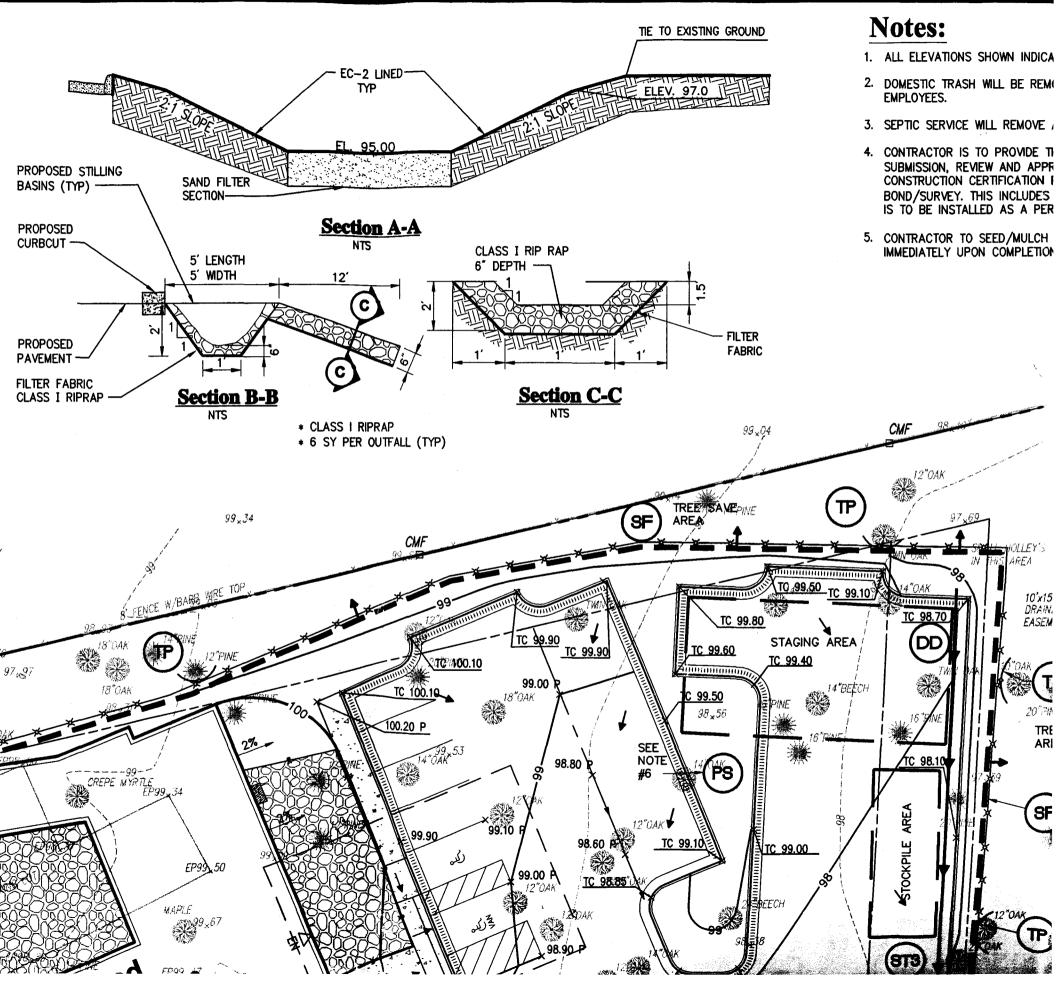
N/F COMMONWEALTH OF VIRGINIA EASTERN STATE HOSPITAL TAX MAP (39-1)(1-152) ZONED R2

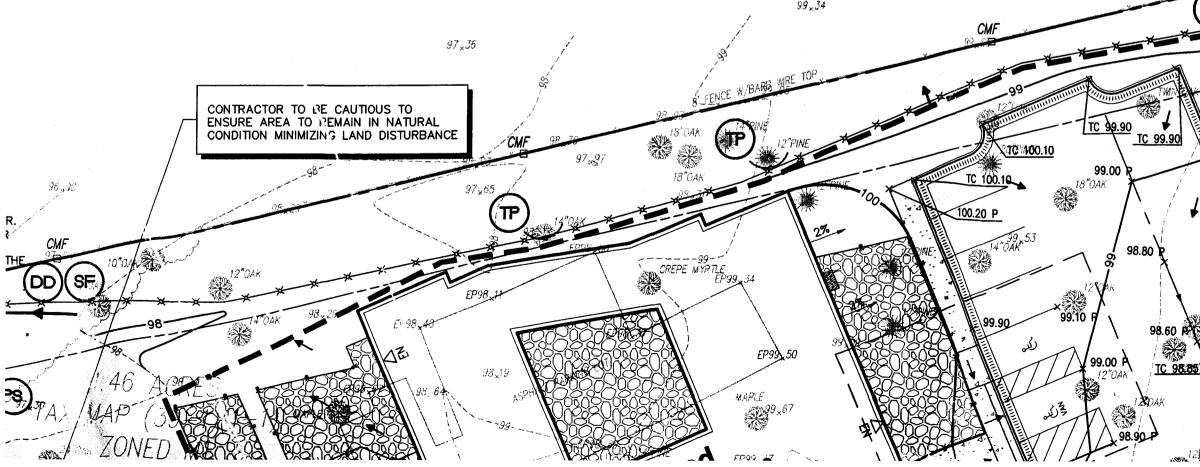


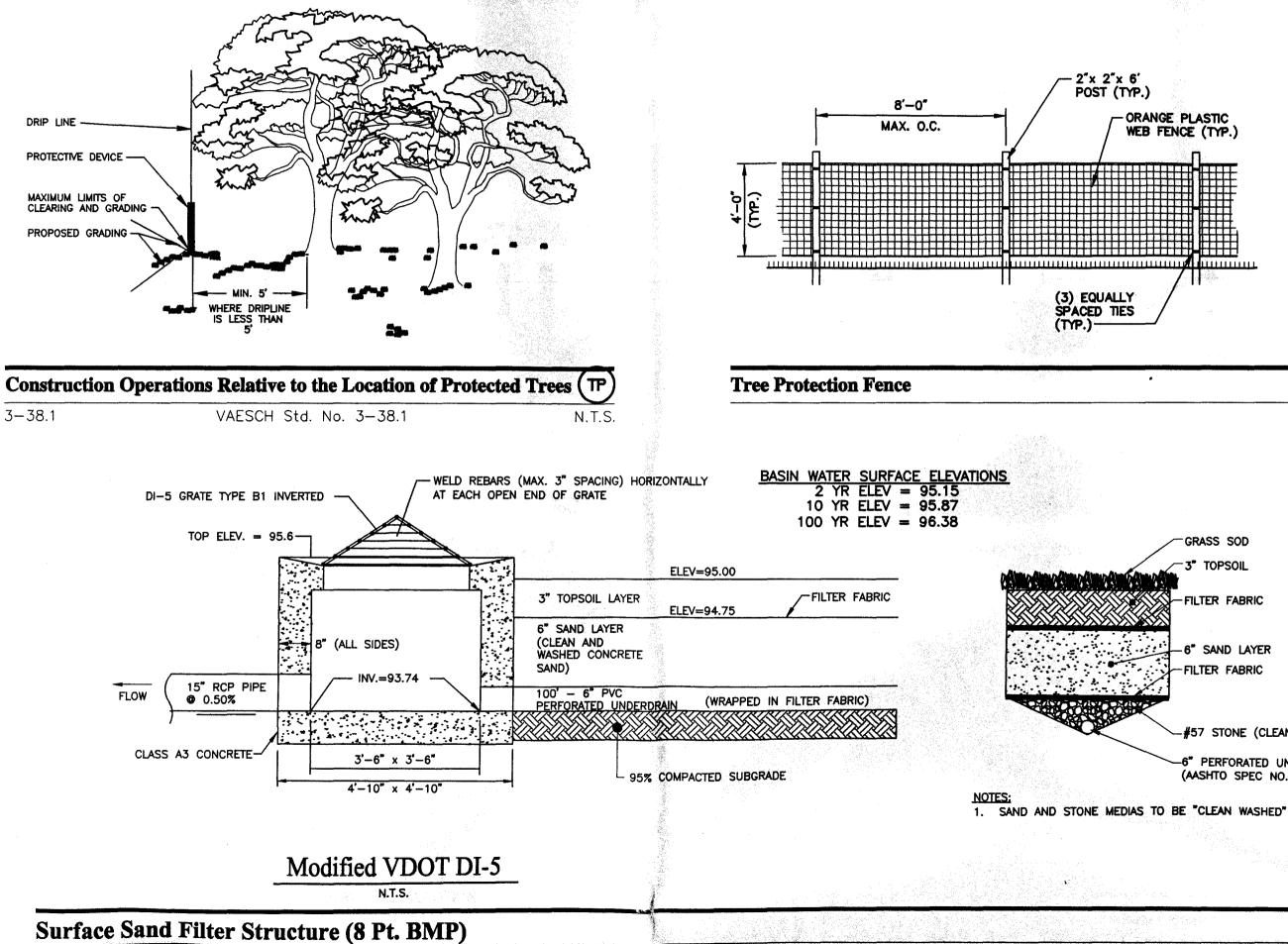


BMP Notes:

- 1. ALL 2:1 SIDE SLOPES REQUIRE EC-2 JUTE MESH LINING
- 2. RIPRAP FABRIC FILTER TO ADHERE TO CWO 2215-77, VTM-52, AND ASTM D751
- 3. TEMPORARY SEDIMENT TRAPS ARE TO BE PLACED TO PROTECT THE BMP BOTTOM/FILTERING AREA FROM SEDIMENT CONTAMINATION.
- 4. UPON PLACEMENT OF SITE CURB AND CURB-CUTS, PLACE FILTER FABRIC AND A CHECK DAM ON THE GUTTER PAN AT THE CURB-CUT TO ENHANCE SEDIMENT TRAPPING AT THE TOP OF THE FLUME.
- 5. BMP BOTTOM/FILTERING AREA SHALL NOT BE TRAVERSED BY EQUIPMENT OR USED FOR SOIL STORAGE DURING CONSTRUCTION. THIS AREA IS TO CONTAIN THE PERMANENT SAND FILTER AND, AS SUCH, SHOULD BE PROTECTED THROUGHOUT CONSTRUCTION FROM EQUIPMENT TRAFFIC AND SEDIMENT CONTAMINATION AND BE CONSTRUCTED AS A FINAL ELEMENT OF SITE CONSTRUCTION.
- 6. SOD IS TO BE PLACED ON TOP OF THE PROPOSED SAND FILTER SECTION UPON COMPLETION OF THE BMP FACILITY.
- 7. PRIOR TO CONSTRUCTION OF THE BMP SAND FILTER SECTION THE CONTRACTOR IS TO FOLLOW THE FOLLOWING CLEANOUT PROCEDURES;
- *REMOVE ANY SEDIMENT AND/OR DEBRIS FROM BMP AREA
- *VERIFY THAT ALL 3 OUTFALL POINTS HAVE BEEN PROPERLY MAINTAINED AND DO NOT CONTAIN SEDIMENT.
- *ENSURE THAT EC-2 JUTE MESH LINING HAS BEEN PROPERLY INSTALLED.







VDOT #3, #357, # #57 COARSE AGGF GALVANIZED WIRE

* FILTER CLOTH-SECURE WRE TO I WITH WRE STAPLE



+ MIN. P



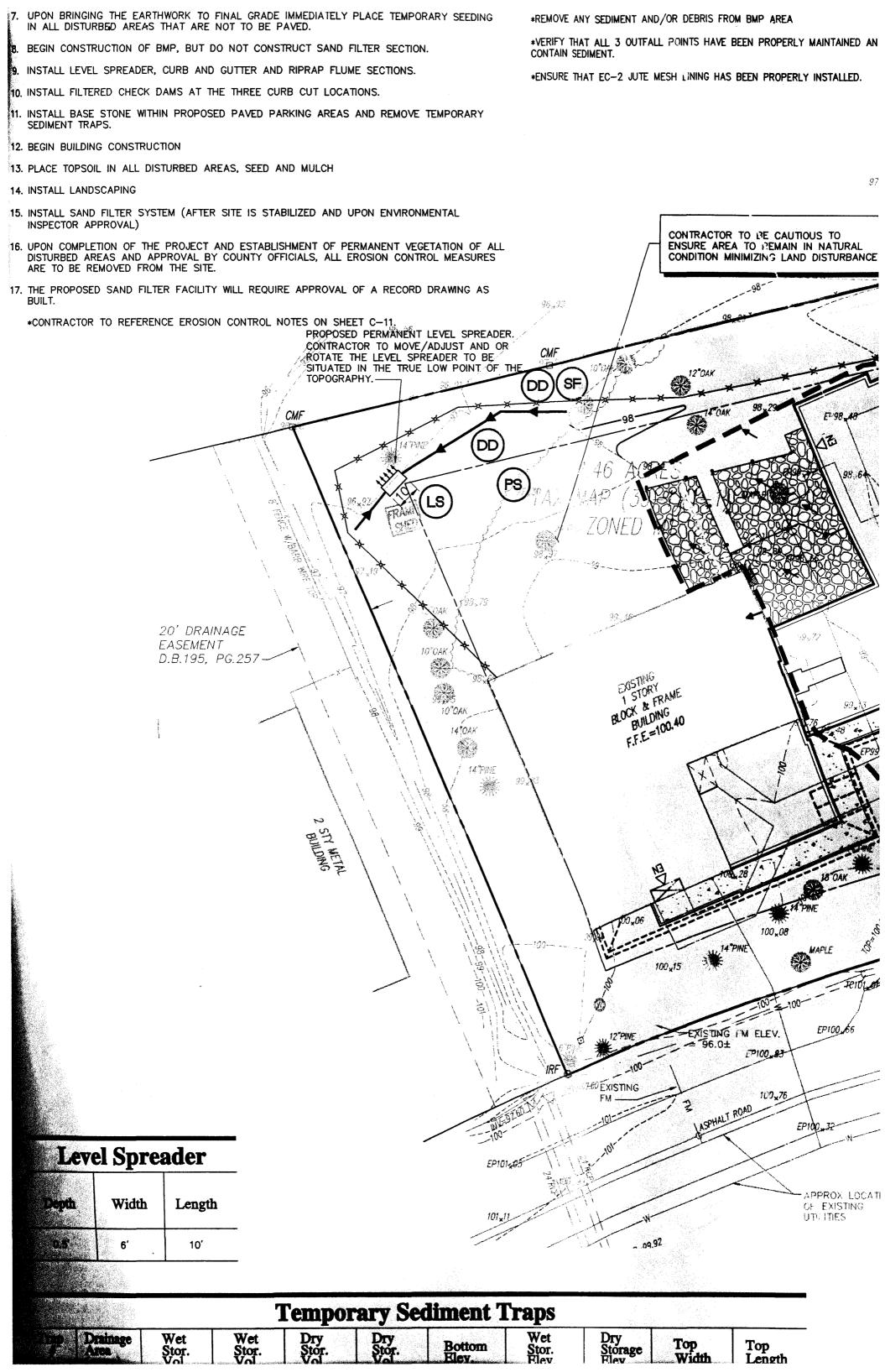
FILTER FABRIC 6" SAND LAYER FILTER FABRIC

#57 STONE (CLEANED AND WASHED)

(77)

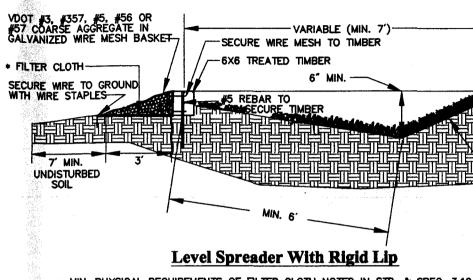
N.T.S.

-6" PERFORATED UNDERDRAIN (AASHTO SPEC NO. M 252M-96)



2"x 2"x 6' POST (TYP.) 8'-0" ORANGE PLASTIC MAX. O.C. WEB FENCE (TYP.) 1.1 こ шиш (3) EQUALLY SPACED TIES (TYP.)ee Protection Fence (\mathbf{TP}) N.T.S. BASIN WATER SURFACE ELEVATIONS 2 YR ELEV = 95.15 10 YR ELEV = 95.87 100 YR ELEV = 96.38GRASS SOD 3" TOPSOIL FILTER FABRIC -FILTER FABRIC -6" SAND LAYER -FILTER FABRIC D IN FILTER FABRIC) #57 STONE (CLEANED AND WASHED) -6" PERFORATED UNDERDRAIN (AASHTO SPEC NO. M 252M-96) GRADE

> NOTES: 1. SAND AND STONE MEDIAS TO BE "CLEAN WASHED"



+ MIN. PHYSICAL REQUIREMENTS OF FILTER CLOTH NOTED IN STD. & SPEC. 3.1

Level Spreader

N.T.S.

Source: Virginia Erosion And Sediment Control Handbook

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		4 . }	
2:1 OR FLATTER			
3.19, 'RIPRAP			
11/02			
Plate 3.21-2	· ·		

RIGHT-OF-WAYS. WHERE SEDIMENT IS TRANSPORTED ONTO A PUBLIC ROAD SURFACE, THE ROAD SHALL BE THOROUGHLY CLEANED AT THE END OF EACH DAY (STD & SPEC 3.02).

5. SEDIMENT BASINS AND TRAPS (STD & SPEC 3.13 AND 3.14), PERIMETER DIKES (STD 5. SEDIMENT BASINS AND TRAPS (STD & SPEC 3.13 AND 3.14), PERIMETER DIKES (STD & SPEC 3.09 AND 3.12), SEDIMENT FILTER BARRIERS (STD. & SPEC 3.05) AND OTHER MEASURES INTENDED TO TRAP SEDIMENT ON-SITE MUST BE CONSTRUCTED AS A FIRST STEP IN GRADING AND MUST BE MADE FUNCTIONAL PRIOR TO ANY UPSLOPE LAND DISTURBANCE TAKING PLACE. EARTHEN STRUCTURES SUCH AS DAMS, DIKES AND DIVERSIONS MUST BE SEEDED AND MULCHED IMMEDIATELY AFTER INSTALLATION. PERIODIC INSPECTIONS OF THE EROSION CONTROL MEASURES BY THE OWNER OR OWNERS REPRESENTATIVES SHALL BE MADE TO ASSESS THEIR CONDITION. ANY NECESSARY MAINTENANCE OF THE MEASURES SHALL BE ACCOMPLISHED IMMEDIATELY AND SHALL INCLUDE THE REPAIR OF MEASURES DAMAGED BY ANY SUBCONTRACTOR INCLUDING THOSE INCLUDE THE REPAIR OF MEASURES DAMAGED BY ANY SUBCONTRACTOR INCLUDING THOSE OF THE PUBLIC UTILITY COMPANIES.

6. SURFACE FLOWS OVER CUT AND FILL SLOPES SHALL BE CONTROLLED BY EITHER REDIRECTING FLOWS FROM TRANSVERSING THE SLOPES OR BY INSTALLING MECHANICAL DEVICES TO SAFELY LOWER WATER DOWNSLOPE WITHOUT CAUSING EROSION. A TEMPORARY FILL DIVERSION (STD. & SPEC. 3.10) AND SLOPE DRAIN (STD. & SPEC. 3.15) SHALL BE INSTALLED PRIOR TO THE END OF EACH WORKING DAY.

7. SEDIMENT CONTROL MEASURES MAY REQUIRE MINOR FIELD ADJUSTMENTS AT TIME OF CONSTRUCTION TO INSURE THEIR INTENDED PURPOSE IS ACCOMPLISHED. ENVIRONMENTAL DIVISION APPROVAL WILL BE REQUIRED FOR OTHER DEVIATIONS FROM THE APPROVED PLAN.

8. THE CONTRACTOR SHALL PLACE SOIL STOCKPILES AT THE LOCATIONS SHOWN ON THE PLAN. SOIL STOCKPILES SHALL BE STABILIZED OR PROTECTED WITH SEDIMENT TRAPPING MEASURES. OFF-SITE WASTE OR BORROW AREAS SHALL BE APPROVED BY THE ENVIRONMENTAL DIVISION PRIOR TO THE IMPORT OF ANY BORROW OR EXPORT OF ANY WASTE TO OR FROM THE PROJECT SITE.

9. THE CONTRACTOR SHALL COMPLETE DRAINAGE FACILITIES WITHIN 30 DAYS FOLLOWING COMPLETION OF ROUGH GRADING AT ANY POINT WITHIN THE PROJECT. THE INSTALLATION OF DRAINAGE FACILITIES SHALL TAKE PRECEDENCE OVER ALL UNDERGROUND UTILITIES. OUTFALL DITCHES FROM DRAINAGE STRUCTURES SHALL BE STABILIZED IMMEDIATELY AFTER CONSTRUCTION OF THE SAME (STD & SPEC 3.18). THIS INCLUDES INSTALLATION OF EROSION CONTROL STONE OR PAVED DITCHES WHERE REQUIRED. ANY DRAINAGE OUTFALLS REQUIRED FOR A STREET MUST BE COMPLETED BEFORE STREET GRADING OR UTILITY INSTALLATION BEGINS.

10. PERMANENT OR TEMPORARY SOLL STABILIZATION SHALL BE APPLIED TO DENUDED ARE TO BE LEFT DORMANT FOR MORE THAN ONE YEAR.

11. NO MORE THAN 300 FEET OF SANITARY SEWER, STORM DRAIN, WATER OR UNDERGROUND UTILITY LINES ARE TO BE OPEN AT ONE TIME. FOLLOWING INSTALLATION OF ANY PORTION OF THESE ITEMS, ALL DISTURBED AREAS ARE TO BE IMMEDIATELY STABILIZED (I.E., THE SAME DAY).

12. IF DISTURBED AREA STABILIZATION IS TO BE ACCOMPLISHED DURING THE MONTHS OF DECEMBER, JANUARY OR FEBRUARY, STABILIZATION SHALL CONSIST OF MULCHING (STD & SPEC 3.35). SEEDING WILL THEN TAKE PLACE AS SOON AS THE SEASON PERMITS.

13. THE TERM SEEDING, FINAL VEGETATIVE COVER OR STABILIZATION ON THIS PLAN SHALL MEAN THE SUCCESSFUL GERMINATION AND ESTABLISHMENT OF A STABLE GRASS COVER FROM A PROPERLY PREPARED SEEDBED CONTAINING THE SPECIFIED AMOUNTS OF SEED, LIME AND FERTILIZER (STD & SPEC 3.32). IRRIGATION SHALL BE REQUIRED AS NECESSARY TO ENSURE ESTABLISHMENT OF GRASS COVER.

14. ALL SLOPES STEEPER THAN 3H: 1V SHALL REQUIRE THE USE OF EROSION CONTROL BLANKETS AND MATTINGS TO AID IN THE ESTABLISHMENT OF A VEGETATIVE COVER. INSTALLATION SHALL BE IN ACCORDANCE WITH STD. & SPEC. 3.35, MULCHING, STD. & SPEC. 3.36, SOIL STABILIZATION BLANKETS AND MATTING AND MANUFACTURERS INSTRUCTIONS. NO SLOPES SHALL BE CREATED STEEPER THAN 2H: 1V.

15. INLET PROTECTION (STD & SPEC 3.07 AND 3.08) SHALL BE PROVIDED FOR ALL STORM DRAIN AND CULVERT INLETS FOLLOWING CONSTRUCTION OF THE SAME.

16. TEMPORARY LINERS, SUCH AS POLYETHYLENE SHEETS, SHALL BE PROVIDED FOR ALL PAVED DITCHES UNTIL THE PERMANENT CONCRETE LINER IS INSTALLED.

17. PAVED DITCHES SHALL BE REQUIRED WHEREVER ACCELERATED EROSION IS EVIDENT. PARTICULAR ATTENTION SHALL BE PAID TO THOSE AREAS WHERE GRADES EXCEED 3 PERCENT.

18. TEMPORARY EROSION CONTROL MEASURES SUCH AS SILT FENCE ARE NOT TO BE REMOVED UNTIL ALL DISTURBED AREAS ARE STABILIZED. TRAPPED SEDIMENT SHALL BE SPREAD, SEEDED AND MULCHED. AFTER THE PROJECT AND STABILIZATION IS COMPLETE, ALL EROSION AND SEDIMENT CONTROL MEASURES SHALL BE REMOVED WITHIN 30 DAYS.

19. NO SEDIMENT TRAP OR SEDIMENT BASIN SHALL BE REMOVED UNTIL A) AT LEAST 75 PERCENT OF THE LOTS WITHIN THE DRAINAGE AREA TO THE TRAP OR BASIN HAVE BEEN SOLD TO A THIRD PARTY (UNRELATED TO THE DEVELOPER) FOR THE CONSTRUCTION OF HOMES AND/OR B) 60 PERCENT OF THE SINGLE FAMILY LOTS WITHIN THE DRAINAGE AREA TO THE TRAP OR BASIN HAVE BEEN COMPLETED AND THE SOIL STABILIZED. BULK SALE OF THE LOTS TO ANOTHER BUILDER DOES NOT SATISFY THIS PROVISION. SEDIMENT TRAPS AND SEDIMENT BASINS SHALL NOT BE REMOVED WITHOUT THE EXPRESS AUTHORIZATION OF THE JAMES CITY COUNTY ENVIRONMENTAL DIVISION.

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Scole As Noted Project Title

Godspeed An **Proposed Site**

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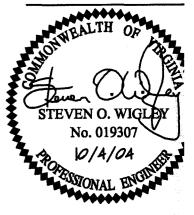
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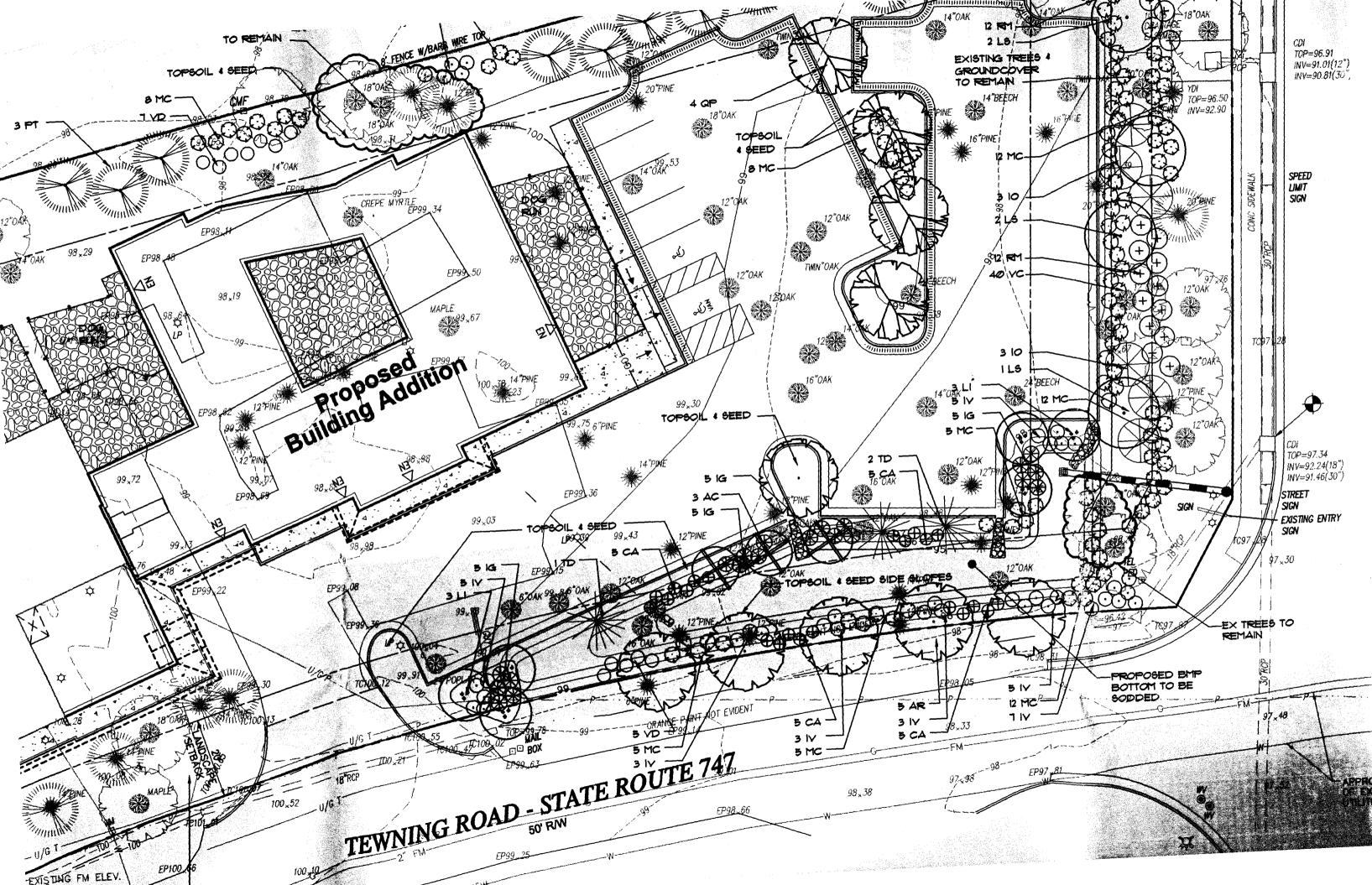
20. RECORD DRAWINGS (AS-BUILTS) AND CONSTRUCTION CERTIFICATIONS ARE BOTH REQUIRED FOR NEWLY CONSTRUCTED OR MODIFIED STORMWATER MANAGEMENT/BMP FACILITIES. CERTIFICATION ACTIVITIES SHALL BE ADEQUATELY COORDINATED AND PERFORMED BEFORE, DURING AND FOLLOWING CONSTRUCTION IN ACCORDANCE WITH THE CURRENT VERSION OF THE JAMES CITY COUNTY ENVIRONMENTAL DIVISION, STORMWATER MANAGEMENT/BMP FACILITIES, RECORD DRAWING AND CONSTRUCTION CERTIFICATION, STANDARD FORMS & INSTRUCTIONS.

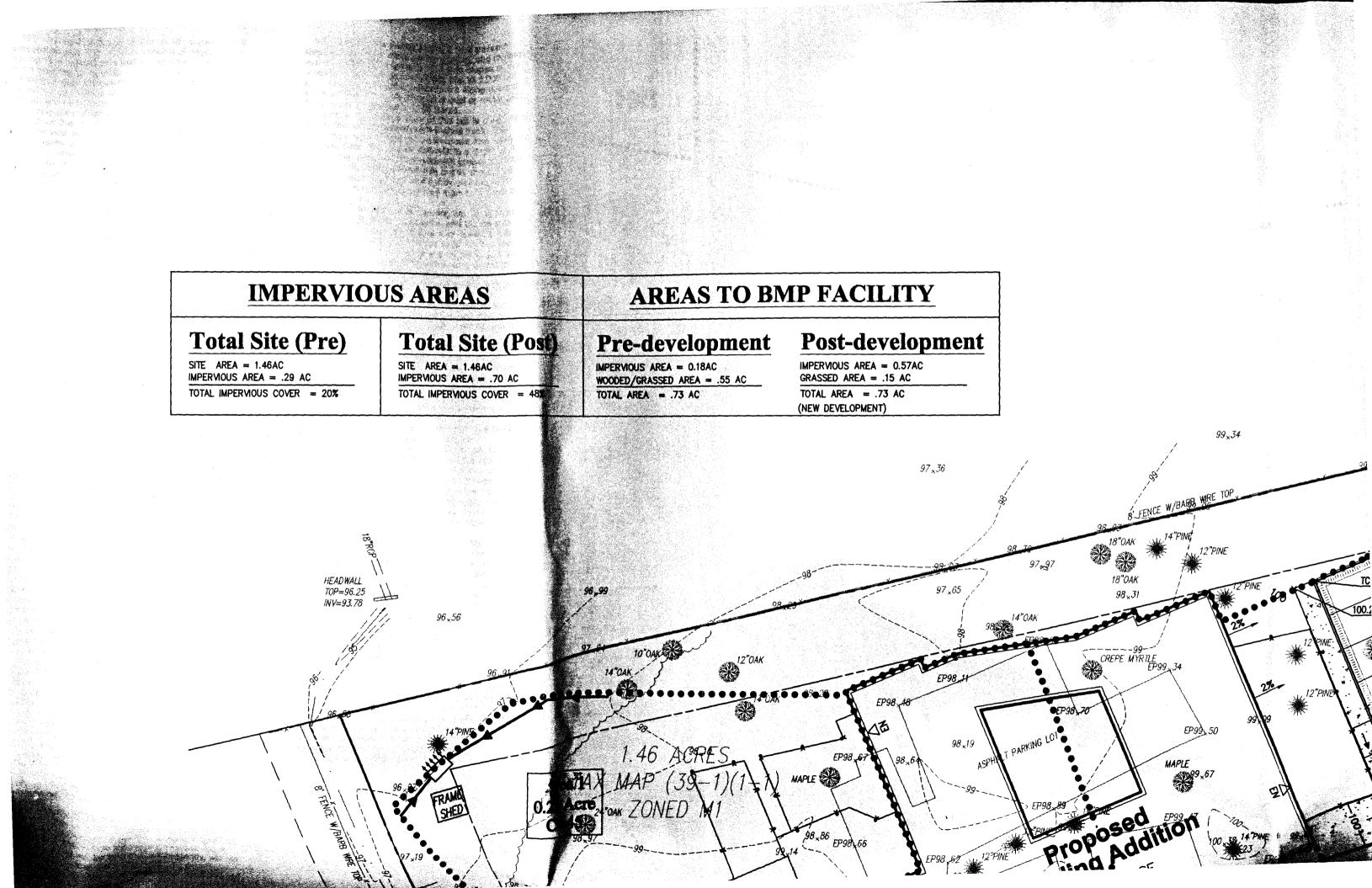
21. DESIGN AND CONSTRUCTION OF PRIVATE-TYPE SITE DRAINAGE SYSTEMS OUTSIDE VDOT RIGHTS-OF-WAY SHALL BE PERFORMED IN ACCORDANCE WITH THE CURRENT VERSION OF THE JAMES CITY COUNTY ENVIRONMENTAL DIVISION, STORMWATER DRAINAGE CONVEYANCE SYSTEMS (NON-BMP RELATED), GENERAL DESIGN AND CONSTRUCTION GUIDELINES.

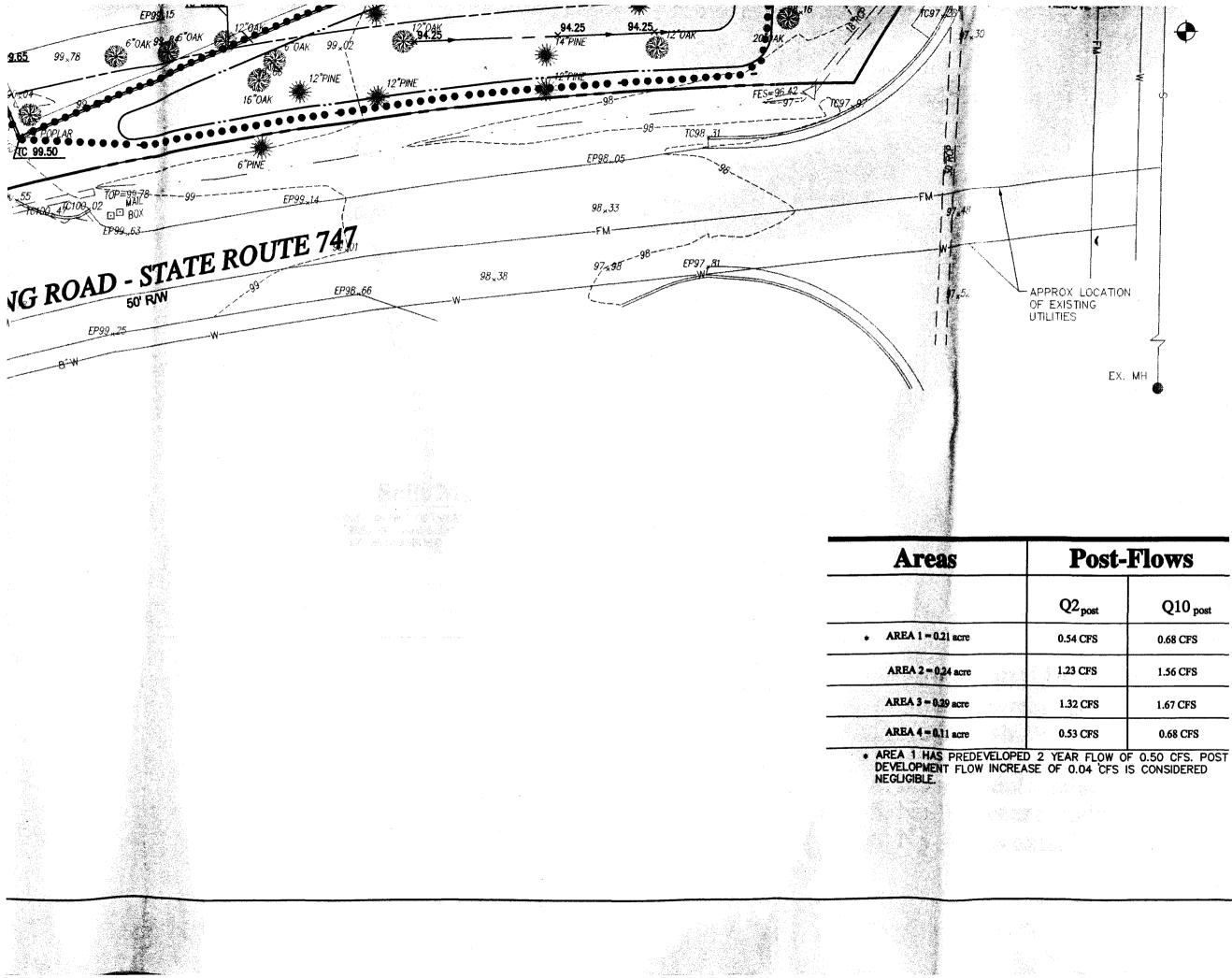
Erosion Cont and Details



N.T.S.







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Scale 1"=20'

Project Title

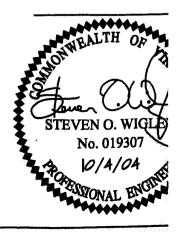
Godspeed 4 Proposed S

James City Cou

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Not Approved for Drawing Title

Drainage A and Calcula



• EX. MH

Post-Flows $Q10_{\text{ post}}$ 0.68 CFS 1.56 CFS 1.67 CFS 0.68 CFS

Godspeed Animal Care 102 Tewning Road

James City County, Virginia

Prepared for

Dr. Pamela Dumont Williamsburg, Virginia

Prepared by

/Vanasse Hangen Brustlin, Inc. Richmond, Virginia

(FINAL COMPS.)

Oct. 5, 2004

Godspeed Animal Care Building Expansion

Engineering Report

Table of Contents

- 1. Stormwater Management Design Narrative
- 2. Stormwater Management Calculations
- 3. Water Meter Sizing Calculations
- 4. Storm Water Calculations
- 5. Sewage Pump Station Design
- 6. BMP Geotechnical Report
- 7. Existing Site Photos

GODSPEED ANIMAL CARE BUILDING EXPANSION PROJECT

Stormwater Management Design Narrative

Project Description

The existing animal care facility is located at the corner of Tewning Road and Ironbound Road in James City County, Virginia. The project encompasses 1.46 acres of land and proposes an expansion of an existing building and associated parking. The project will generally include the addition of a two story building with a total gross square footage of 12,080, parking lots in the front and side of the site, and a comprehensive stormwater management system. The project site is identified as Tax Map Parcel #36-1 and is zoned M-1.

The proposed stormwater management plan for this project will include the use of a D-2 Surface Sand Filter System with 6" perforated underdrain piping to capture the filtered stormwater. The stormwater management system will attenuate the increased runoff anticipated from site development associated with the increased impervious cover.

The stormwater management system is designed to control up to the 100-year, twenty-four hour storm events, for post developed conditions. The volume created by the 10 year storm will have a 48 hour drawdown time before being released into the existing VDOT system along Ironbound Road. The proposed system is also designed to safely contain the 100-year storm event without the use of emergency spillways.

Description of Site

Under predevelopment conditions, the area to be developed is comprised of moderately wooded Hardwoods and Pines throughout. The general landform consists of elevations ranging from 100 to 97 and slopes gently away from the center outward to the east and west. Surface hydrology is directed by overland flow to two (2) ravines located along the rear of the property and also through an existing channel and culvert along Tewning Road. The site is located within the RPA but does not contain any wetlands or hydric soils.

General Description of Stormwater Management

The proposed onsite Sand Filter System will be the primary water quantity and quality control for this project. Surface waters drain to the proposed BMP by way of the pavement surface through curb cuts in the proposed curb and gutter. The water quality requirement is met by the use of the proposed sand filter and stilling basins located at each outfall curb cut from the proposed parking area. The depth of the

1

Surface Sand Filter BMP ranges from 3' to 4' below the proposed pavement elevations. The outlet control structure will consist of a VDOT DI-5 structure, modified with a 12" outfall pipe to accommodate the 48 hour detention storage drawdown.

Temporary Sediment Traps and silt fence will serve as temporary erosion and sediment control devices during initial land clearing, grading, and earthmoving operations. The addition of the sand filter system and a spreader box in the rear of the site will serve in controlling the quality of run-off from the site once the improvements are completed. Appropriate details to construct the facilities for temporary and permanent erosion and sediment control are shown on the site plan.

Hydrology and Hydraulics

Topographic data used for site hydrology and storm/pond hydraulics was obtained from field survey by Michaels Surveying and Mapping dated 12/17/01. The survey verified the site boundary and provided topography related to utilities, drainage structures, and other physical improvements.

Hydrology and hydraulic modeling was performed utilizing the Hydrocad stormwater modeling system as developed by Haestad Methods, Waterbury, Connecticut.

The SCS TR-20 Method is the basis for overall watershed modeling for this project. Precipitation data for the County was obtained by source data provided by the U. S. Weather Bureau as found in Technical Paper No. 76 Rainfall Frequency Atlas of the Untied States.

Storage-indication pond routing procedures were used to predict the drawdown storage response (outflow hydrograph and incremental stage) to the inflow hydrograph. This sequential routing method uses the elevation-storage and elevation-discharge relationships for repeatedly solving the continuity equation, each solution being a step in delineating the outflow hydrograph.

Pre-development Hydrology

Pre-development conditions were evaluated to determine the existing peak discharges at the eastern discharge point from the proposed sand filter system. Based on current conditions, peak discharges for the 1-year, 24-hour storm was determined to be 0.78 cfs. This discharge was computed based on a drainage area of 0.73 acres and an SCS Curve Number of 77. The Time of concentration (Tc) value (0.25 hours) was based on the "Overland Flow" Method, whereby the flow path was divided into segments according to the type of flows such as overland, shallow concentrated, and channel flow.

Post-development Hydrology

Post-development drainage patterns differ slightly from pre-development, in that all of the proposed improvements will be directed to the proposed BMP.

Post-development conditions are based on ultimate development of the site with current conditions of paved and non-paved areas, to determine overall peak discharges to the existing receiving channels as was performed for predevelopment conditions. Based on this criteria, peak discharges for the 1-year, 24 hour storm, was determined to be 0.0424 cfs for the BMP outfall point. These discharges were based on a total drainage area of 0.73 acres. As with pre-development methodology, runoff SCS values were based on land use and hydrologic soil group, and time of concentration values were based on the SCS velocity method.

Comparison of the predevelopment discharges with the post-development discharges results in an overall decrease in peak discharges to the existing storm system due to attenuation by the onsite sand filter facility.

<u>Hydraulics – Proposed Surface Sand Filter System</u>

The proposed stormwater management system consists of one (1) Surface Sand Filter system, to control the increased runoff from the site development.

Post-development inflow hydrographs were developed and routed through the storage volume and outlet structure for this system using level pool routing methods to determine post-development peak discharges. Simultaneously routing procedures allows the system to respond to dynamic changes such as variable tailwater created by downstream system components. The following is a performance summary for the system tabulating peak outflow and water surface elevation for the 1-year, 10-year, and 100-year storm events.

D-2 Sand Filter System

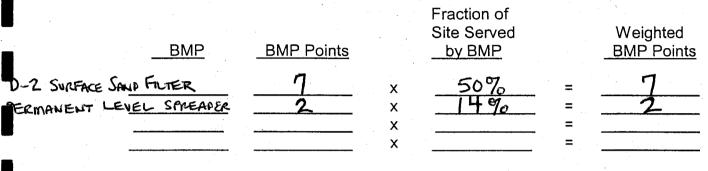
Storm Event	Outflow (cfs)	Elevation (ft.)	Release Time
1-Year	0.06	96.60	30 hrs. +
10-year	6.24	96.89	30 hrs. +
100-year	8.89	96.97	30 hrs. +

3

James City County BMP Guidelines

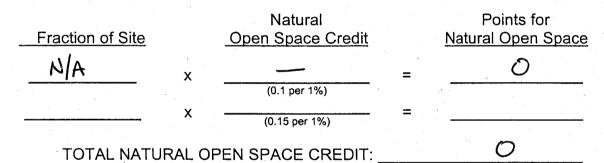
Table 2 Worksheet for BMP Point System

A. STRUCTURAL BMP POINT ALLOCATION



TOTAL WEIGHTED STRUCTURAL BMP POINTS:

B. <u>NATURAL OPEN SPACE CREDIT</u>



С.

TOTAL WEIGHTED POINTS

(9) 8.94 +		0		9
Structu	ral BMP Points	Natural	Open Space	Points	Total
SJTCHECK	< SITE = 0.70 AC	:.			
(DA = 0,73 AC.)	D-2 SAND FILTER	8 PT.	0.73 =	8.34	
DA = 0.21AL	LEVEL SPREADER IN ENST. UNCONTRIMIED AREA	2 PT.	0.21/ 0.70 =	0.60 8.94 ng	7
		Q	Ĩ	SEE WAIVER ETTER. CON	APAROVAL Y ATTACHED

9

September 14, 2004

Mr. Mitch Mitchell Vanasse Hangen Brustlin, Inc. 115 South 15th Street, Suite 200 Richmond, Va. 23219

SEE FOR OPY. FILE FOR OPY. SIGNED OPY.

Re: 10-point system and Sand Filter Variance Request Godspeed Animal Care Expansion County Plan No. SP-70-04

Dear Mr. Mitchell:

The Environmental Division is in receipt of your written variance request letter dated August 17th 2004 for the above referenced project. The variance request is dual-fold, as it requests variance from the County 10-point BMP water quality system and also requests a variance from a minimum depth of 18 inches to 6 inches for the filter sand layer associated with a County type D-2 BMP.

Based on our review of information as submitted, the variance as requested is hereby *approved* for this specific review case only. The variance was considered appropriate due to information as submitted in the letter request and the amended plan of development including:

- There is a distinct site constraint for the project. The restraint is the vertical elevation of an existing 18-inch storm drain pipe system along the west side of Ironbound Road. This storm drainage pipe system is the only reasonable receiving drainage facility to accept discharge from the development site.
- The site contains Soil Group 29B Slagle fine sandy loam, which exhibit seasonal high water tables and slow permeability of the subsoil. These characteristics limit the feasibility of certain types of onsite BMPs including bioretention and dry swales.
- The onsite BMP must be able to be landscaped in order to blend with aesthetics of the area and meet Zoning ordinance requirements.
- A wet pond pool at this location would generally be unsafe due to the location of the parking area and the presence of Ironbound Road and Tewning Road.

The following conditions apply to approval of this waiver request:

- 1. The owner should be made completely aware of waiver from the 10-point system and reduced depth of sand media. Reduced depth of sand media will result in more importance being placed on BMP maintenance as trash, debris, grass clippings and sediment can cause premature clogging of the sand layer.
- 2. The three stilling basins around the sand filter BMP as shown on Sheet C-4 of the plan set must be installed as permanent features and be adequately cleaned on a frequent basis.
- 3. The level spreader as situated in the northwest corner of the site must be installed as a permanent feature and be adequately cleaned and maintained on a routine basis.
- 4. Sod must be placed in the bottom of the sand filter BMP consistent with that shown on plan Sheet C-4 and Landscape plan Sheet C-7.
- 5. The variance approval shall become part of the approved site stormwater management plan.

Please note that approval of this variance, with the conditions stated, in no way implies final approval of a site or subdivision plan as required by the Chapter 24 Zoning or Chapter 19 Subdivisions of the County Code; nor, does it constitute final approval of an erosion and sediment control or stormwater management plan as required by Chapter 8 Erosion and Sediment Control and Chapter 23 Chesapeake Bay Preservation of the County Code. Approval of this variance is also contingent upon no major (substantial) changes in the development plan, the subject best management practice facility, or if site conditions change, become apparent or alter significantly following the date of this approval.

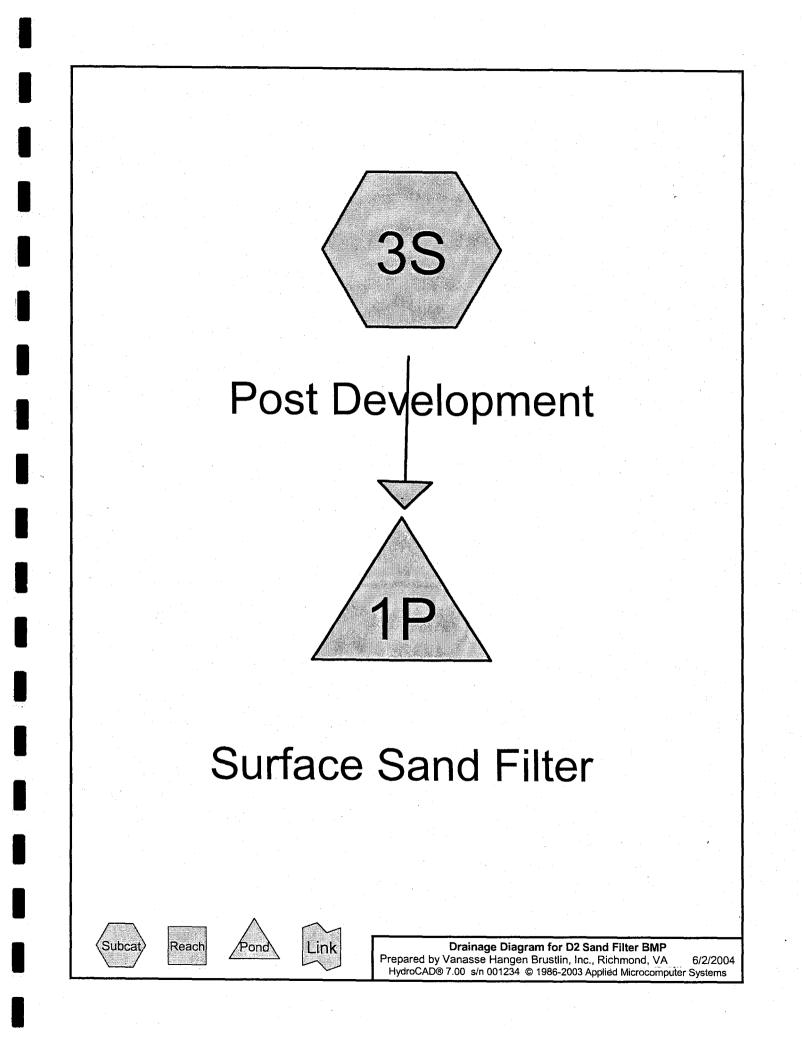
Sincerely,

Scott J. Thomas, P.E. Senior Engineer Environmental Division

SJT/sjt

cc: Ellen Cook, Planning

SWMProg/Variances/SPvar/Var091404.SP07004



	me : Godspeed An	CALCULAT	I <u>ON</u> James City (Sounty me	anou	Project # :	31248.01	
<u>r tojest nu</u>							01240.01	88000 (1886-1996) 1997 - Stateline (1996-1996)
One Yea	ar Precipitation :	P=	2.8 Inches	· · ·	TABLE F			
						ts for Rainfal		
PRE-DEVELOPM	ENT CONDITIONS				I _a /P	Co	C1	C ₂
Draina	age Area :	DA _{PRE} =	0.73 Acres		0.10	2.55323	-0.61512	-0.164
SCS C	Curve Number :	CN _{PRE} =	77 Unitless		0.30	2.46532	-0.62257	-0.116
Time of	Concentration :	Tc _{PRE} =	0.25 Hours		0.35	2.41896	-0.61594	-0.088
			minan multi senta dinge s		0.40	2.36409	-0.59857	-0.056
					0.45	2.29238	-0.57005	-0.022
					0.50	2.20282	-0.51599	-0.012
Initial	abstraction ;	I	_a =0.2x(1000/CN - 10) =	0.597	Inches			
			I _a /P =	0.21				
				•				
Accun	nulated direct runoff	: Q	$I_{U} = (P - I_{a})^{2} / (P + 4xI_{a}) =$	0.93	Inches			
							-	
Unit P	eak Discharge :		q _u =	731	cfs/sq.mile	e/in.		
	log(q _u)=C ₀ +C	log(T _c)+C ₂	[log(T _c)]^2					
	C ₀ ,C ₁ ,C ₂ ; Coe	efficients from	m TABLE F1 above					
Pre-de	evelopment peak di							
			_{ip} =q _u x DA x Q _U / 640 =	0.78	c.f.s.			
	MENT CONDITION	<u>s:</u>		0.78	c.f.s.			
Draina	age Area :	<u>S :</u> DA _{POST} =	0.73 Acres	0.78	c.f.s.			
Drain: SCS (age Area : Curve Number :	<u>S :</u> DA _{POST} = CN _{POST} =	0.73 Acres 92 Unitless	0.78	c.f.s.			
Drain: SCS (age Area :	<u>S :</u> DA _{POST} =	0.73 Acres	0.78	c.f.s.			
Draina SCS (Time	age Area : Curve Number : of Concentration	<u>S :</u> DA _{POST} = CN _{POST} =	0.73 Acres 92 Unitless 0.025 Hours					
Draina SCS (Time	age Area : Curve Number :	<u>S :</u> DA _{POST} = CN _{POST} =	0.73 Acres 92 Unitless 0.025 Hours 1 _a =	0.174	Inches			
Draina SCS (Time Initial	age Area : Curve Number : of Concentration abstraction ;	<u>S :</u> DA _{POST} = CN _{POST} = Tc _{POST} =	0.73 Acres 92 Unitless 0.025 Hours I _a = I _a /P =	0.174 0.10	Inches			
Draina SCS (Time Initial	age Area : Curve Number : of Concentration	<u>S :</u> DA _{POST} = CN _{POST} = Tc _{POST} =	0.73 Acres 92 Unitless 0.025 Hours I _a = I _a /P = Q _U =	0.174 0.10 1.97	Inches) Inches			
Draina SCS (Time Initial Accur	age Area : Curve Number : of Concentration abstraction ;	<u>S :</u> DA _{POST} = CN _{POST} = Tc _{POST} =	0.73 Acres 92 Unitless 0.025 Hours I _a = I _a /P =	0.174 0.10 1.97	Inches	e/in.		
Draina SCS (Time Initial Accur Unit F	age Area : Curve Number : of Concentration abstraction ; mulated direct runof	<u>S :</u> DA _{POST} = CN _{POST} = TC _{POST} =	0.73 Acres 92 Unitless 0.025 Hours I _a = I _a /P = Q _U = q _u =	0.174 0.10 1.97 1311	Inches) Inches	e/in.		
Draina SCS (Time Initial Accur Unit F Post o	age Area : Curve Number : of Concentration abstraction ; mulated direct runoff Peak Discharge : development peak d	<u>S :</u> DA _{POST} = CN _{POST} = TC _{POST} =	0.73 Acres 92 Unitless 0.025 Hours $I_a = I_a/P = Q_U = Q_U = q_u = q_u = q_i = q_p =$	0.174 0.10 1.97 1311 2.95	Inches) Inches cfs/sq.mil c.f.s.	e/in.		
Draina SCS (Time Initial Accur Unit F Post o	age Area : Curve Number : of Concentration abstraction ; mulated direct runoff Peak Discharge : development peak d n of outflow to inflow	S: DA _{POST} = CN _{POST} = Tc _{POST} = f: lischarge rat	0.73 Acres 92 Unitless 0.025 Hours $I_a = I_a/P = Q_U $	0.174 0.10 1.97 1311 2.95 0.0144	Inches) Inches cfs/sq.mil c.f.s.			
Draina SCS (Time Initial Accur Unit F Post o	age Area : Curve Number : of Concentration abstraction ; mulated direct runoff Peak Discharge : development peak d n of outflow to inflow	S: DA _{POST} = CN _{POST} = Tc _{POST} = f: lischarge rat	0.73 Acres 92 Unitless 0.025 Hours $I_a = I_a/P = Q_U = Q_U = q_u = q_u = q_i = q_p =$	0.174 0.10 1.97 1311 2.95 0.0144	Inches) Inches cfs/sq.mil c.f.s.		, MDE	
Draina SCS (Time Initial Accur Unit F Post (Ration	age Area : Curve Number : of Concentration abstraction ; mulated direct runoff Peak Discharge : development peak d n of outflow to inflow * Direct calcu	S: DA _{POST} = CN _{POST} = Tc _{POST} = f: lischarge rat	0.73 Acres 92 Unitless 0.025 Hours $I_a =$ $I_a/P =$ $Q_U =$ $q_u =$ te : $q_i = q_p =$ $/q_i = 11.98 \times q_u^{0.937} =$ equation for T=24hr. de	0.174 0.10 1.97 1311 2.95 0.0144 veloped by	Inches Inches cfs/sq.mil c.f.s.		, MDE	
Draina SCS (Time Initial Accur Unit F Post (Ration	age Area : Curve Number : of Concentration abstraction ; mulated direct runoff Peak Discharge : development peak d n of outflow to inflow	S: DA _{POST} = CN _{POST} = Tc _{POST} = f: lischarge rat	0.73 Acres 92 Unitless 0.025 Hours $I_a = I_a/P = Q_U $	0.174 0.10 1.97 1311 2.95 0.0144	Inches Inches cfs/sq.mil c.f.s.		, MDE	
Draina SCS (Time Initial Accur Unit F Post o Ration	age Area : Curve Number : of Concentration abstraction ; mulated direct runoff Peak Discharge : development peak d n of outflow to inflow * Direct calcu pw discharge :	S: DA _{POST} = CN _{POST} = TC _{POST} = f: lischarge rat	0.73 Acres 92 Unitless 0.025 Hours $I_a =$ $I_a/P =$ $Q_U =$ $q_u =$ $q_i = q_p =$ /q_i = 11.98 x q_u^0.937 = equation for T=24hr. de $q_o =$	0.174 0.10 1.97 1311 2.95 0.0144 veloped by	Inches Inches cfs/sq.mil c.f.s. Stewart Co c.f.s.		, MDE	
Draina SCS (Time Initial Accur Unit F Post o Ration	age Area : Curve Number : of Concentration abstraction ; mulated direct runoff Peak Discharge : development peak d n of outflow to inflow * Direct calcu ow discharge : of storage volume t	$\frac{S:}{DA_{POST}} = CN_{POST} = CN_{POST} = TC_{POST} = CONT$ f: discharge rate of the second seco	0.73 Acres 92 Unitless 0.025 Hours $I_a =$ $I_a/P =$ $Q_U =$ $q_u =$ $q_i = q_p =$ /q_i = 11.98 x q_u^0.937 = equation for T=24hr. de $q_o =$ Jume : $V_s/V_r =$	0.174 0.10 1.97 1311 2.95 0.0144 veloped by 0.0424	Inches Inches cfs/sq.mil c.f.s. Stewart Co c.f.s.		, MDE	
Draina SCS (Time Initial Accur Unit F Post o Ration	age Area : Curve Number : of Concentration abstraction ; mulated direct runoff Peak Discharge : development peak d n of outflow to inflow * Direct calcu ow discharge : of storage volume t	$\frac{S:}{DA_{POST}} = CN_{POST} = CN_{POST} = TC_{POST} = CONT$ f: discharge rate of the second seco	0.73 Acres 92 Unitless 0.025 Hours $I_a =$ $I_a/P =$ $Q_U =$ $q_u =$ $q_i = q_p =$ /q_i = 11.98 x q_u^0.937 = equation for T=24hr. de $q_o =$	0.174 0.10 1.97 1311 2.95 0.0144 veloped by 0.0424	Inches Inches cfs/sq.mil c.f.s. Stewart Co c.f.s.		, MDE	
Draina SCS (Time Initial Accur Unit F Post (Ration Ration	age Area : Curve Number : of Concentration abstraction ; mulated direct runoff Peak Discharge : development peak d n of outflow to inflow * Direct calcu ow discharge : of storage volume t	$\frac{S:}{DA_{POST}} = \frac{CN_{POST}}{CP_{OST}} = \frac{1}{TC_{POST}}$ f: discharge rate v: * q_ould a state of the	0.73 Acres 92 Unitless 0.025 Hours $I_a =$ $I_a/P =$ $Q_U =$ $q_u =$ $q_i = q_p =$ /q_i = 11.98 x q_u^0.937 = equation for T=24hr. de $q_o =$ Jume : $V_s/V_r =$	0.174 0.10 1.97 1311 2.95 0.0144 veloped by 0.0424	Inches Inches cfs/sq.mil c.f.s. Stewart Co c.f.s.		, MDE	

D2 Sand Filter BMP

Prepared by Vanasse Hangen Brustlin, Inc., Richmond, VA HydroCAD® 7.00 s/n 001234 © 1986-2003 Applied Microcomputer Systems

8/11/2004

Hydrograph for Pond 1P: Surface Sand Filter

	Time	Inflow	Storage	Elevation	Primary
	(hours)	(cfs)	(cubic-feet)	(feet)	(cfs)
	0.00	0.00	0	94.25	0.00
	1.00	0.00	0	94.25	0.00
	2.00	0.00	0	94.25	0.00
	3.00	0.00	0	94.25	0.00
	4.00	0.00	0	94.25	0.00
	5.00	0.00	0	94.25	0.00
	6.00	0.00	2	94.26	0.00
	7.00	0.01	6	94.27	0:01
	8.00	0.01	10	94.28	0.01
	9.00	0.02	36	94.35	0.01
	10.00	0.04	103	94.55	0.01
	11.00	0.09	272	95.01	0.01
	12.00	1.00	2,276	96.31	1.47
	13.00	0.12	2,042	96.22	0.13
	14.00	0.07	2,025	96.21	0.07
	15.00	0.06	2,019	96.21	0.06
	16.00	0.04	2,015	96.20	0.05
	17.00	0.04	2,013	96.20	.0.04
	18.00	0.03	2,011	96.20	0.04
	19.00	0.03	2,007	96.20	0.03
	20.00	0.03	1,998	96.20	0.03
	21.00	0.02	1,980	96.19	0.03
	22.00	0.02	1,958	96.18	0.03
	23.00	0.02	1,934	96.17	0.03
	24.00	0.02	1,907	96.16	0.03
	25.00	0.00	1,804	96.12	0.03
	26.00	0.00	1,701	96.08	0.03
	27.00	0.00	1,599	96.03	0.03
	28.00	0.00	1,499	95.99	0.03
	29.00	0.00	1,405	95.94	0.02
	30.00	0.00	1,320	95.89	0.02
	31.00	0.00	1,242	95.84	0.02
	32.00	0.00	1,170	95.80	0.02
	33.00	0.00	1,104	95.75	0.02
	34.00	0.00	1,039	95.69	0.02
	35.00	0.00	976	95.63	0.02
	36.00	0.00	914	95.58	0.02
	37.00	0.00	855	95.53	0.02
	38.00	0.00	797	95.48	0.02
	39.00	0.00	741	95.43	0.02
	40.00	0.00	686	95.38	0.02
	41.00	0.00	633	95.33	0.01
	42.00	0.00	582	95.29	0.01
-	43.00	0.00	532	95.24	0.01
	44.00	0.00	483	95.24 95.20	0.01
	45.00	0.00	436	95.16	0.01
	46.00	0.00	390	95.12	0.01
	47.00	0.00	345	95.08	0.01
	48.00	0.00	302	95.04	0.01
		0.00	502	55.04	0.01

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HydroCAD® 7.00 s/n 001234 © 1986-2003 Applied Microcomputer Systems		8/16/2004

Subcatchment 3S: Post Development

Runoff = 2.86 cfs @ 11.92 hrs, Volume=	0.120 af, Depth= 1.97"
--	------------------------

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type II 24-hr 1 year JCC Rainfall=2.80"

Area (ac) CN	Description			с.	and a second second Second second
0.570 98 0.160 70	0	loofs			
0.730 92	2 Weighted Av	erage			·····
Tc Length (min) (feet)	Slope Velocity (ft/ft) (ft/sec		Description		
1.5 100	0.0100 1.1		Sheet Flow, Paverr Smooth surfaces r	nent n= 0.011 P2= 3.50	н Н Н Полония С полония Н
		Pond 1P: Su	urface Sand Filt	er	
Peak Elev= 96.60' Plug-Flow detentic Center-of-Mass de	d method, Time S @ 14.94 hrs Storn time= 910.8 m et. time= 832.3 m	92 hrs, Volum 94 hrs, Volum 94 hrs, Volum 00 hrs, Volum Span= 0.00-48. Inf.Area= 2,553 In calculated fo in (1,627.7 - 75	e= 0.120 a e= 0.097 a e= 0.097 a e= 0.000 a 00 hrs, dt= 0.01 hrs sf Storage= 3,56 r 0.097 af (81% of 95.4)	f f, Atten= 98%, La f f s / 5 9 cf	g= 181.4 min
<u># Invert</u> 1 94.25'	Avail.Storage 4,542 cf	Storage Desc Custom Stag	pe Data (Irregular)	Listed below	
Elevation (feet)		rim. Voids eet) (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
94.25 94.90 95.00 96.00	863 22 1,422 2 2,087 3	17.0 40.0 20.0 40.0 76.0 100.0 19.0 100.0	0 223 113 1,744	0 223 336 2,080	850 1,026 3,237 5,294
97.00 # Routing		65.0 100.0 Devices	2,462	4,542	7,821
1 Primary 2 Device 1 3 Device 1 4 Secondary	93.74' 15.0'' Outlet 94.00' 0.000 96.60' 3.00' 97.00' 20.0'	x 40.0' long C Invert= 93.50' 800 fpm Sand x 3.00' Horiz. C ong x 15.0' br	S= 0.0060 '/' n= filter over Surface Drifice/Grate Limit	ut end projecting, K 0.013 Cc= 0.900 e area above invert ed to weir flow C= sted Rectangular V 0 1.20 1.40 1.60	= 0.600

Transportation Land Development Environmental Services

VHIB

Vanasse Hangen Brustlin, Inc.

101 Walnut Street Post Office Box 9151 Watertown Massachusetts 02471-9151 617.924.1770 FAX 617.924.2286

Phone	Person Contacted:	VHB Rep:
Notes	Title:	VHB Project No.:
	Company:	Project Name:
	Telephone No.:	Type of Call:

Date and Time:

BMP ODSPEED

FAX No.:

EVENT FIZEQ. W.S.E RELEXE TPEAK TIME 96.60 .OGds LYR 30 hrs. 96.65 ZYR ,49 cfs 30 hrs. 6.24 cts 96.89 30 hrs 104R 30 hrs. LOOYR 96.9 8.89

Type II 24-hr 1 year JCC Rainfall=2.80"

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Primary OutFlow Max=0.05 cfs @ 14.94 hrs HW=96.60' (Free Discharge) **1=Culvert** (Passes 0.05 cfs of 8.60 cfs potential flow) -2=Sand filter (Exfiltration Controls 0.03 cfs) -3=Orifice/Grate (Weir Controls 0.01 cfs @ 0.2 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=94.25' (Free Discharge) -4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Type II 24-hr 2 year JCC Rainfall=3.50"

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Page 5 8/16/2004

Primary OutFlow Max=0.48 cfs @ 12.04 hrs HW=96.65' (Free Discharge) 1=Culvert (Passes 0.48 cfs of 8.70 cfs potential flow) 2=Sand filter (Exfiltration Controls 0.03 cfs) -3=Orifice/Grate (Weir Controls 0.44 cfs @ 0.7 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=94.25' (Free Discharge)

Type II 24-hr 2 year JCC Rainfall=3.50"

Prepared by Vanasse Hangen Brustlin, Inc., Richmond, VAPage 4HydroCAD® 7.00 s/n 001234 © 1986-2003 Applied Microcomputer Systems8/16/2004

Subcatchment 3S: Post Development

Runoff = 3.74 cfs @ 11.92 hrs, Volume= 0.160 af, Depth= 2.64"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type II 24-hr 2 year JCC Rainfall=3.50"

Area (ac) C	N Description			•
	98 Paving and	Roofs		
	70 Lot area 92 Weighted A			
0.730	sz weighted A	verage		
Tc Length (min) (feet)	Slope Veloci (ft/ft) (ft/se		Description	
1.5 100	0.0100 1	.1	Sheet Flow, Pavement Smooth surfaces n= 0.011	P2= 3.50"
• •		Pond 1P:	Surface Sand Filter	
Inflow Area = Inflow =	0.730 ac, Infl 3.74 cfs @ 1	ow Depth = 2 1.92 hrs, Volu		
Outflow =	0.49 cfs @ 12	2.04 hrs, Volu	me= 0.136 af, Atten	= 87%, Lag= 7.6 min
Primary = Secondary =	Ý	2.04 hrs, Volu 0.00 hrs, Volu		· ·
Secondary -		5.00 m3, voic	me- 0.000 ai	
Peak Elev= 96.6	5' @ 12.04 hrs S	Surf.Area= 2,5	8.00 hrs, dt= 0.01 hrs / 5 38 sf Storage= 3,681 cf	
	det. time= 678.2 n		for 0.136 af (85% of inflow) 787.2)	
Center-of-Mass	det. time= 609.8 r	nin (1,397.0 -	787.2)	
		nin(1,397.0 - e Storage De	787.2)	elow
Center-of-Mass of the second s	det. time= 609.8 r <u>Avail.Storage</u> 4,542 c	nin (1,397.0 - <u>Storage De</u> f Custom S f	787.2) <u>scription</u> age Data (Irregular) Listed b	
Center-of-Mass of the second s	det. time= 609.8 r <u>Avail.Storage</u> 4,542 c Surf.Area P	nin (1,397.0 - <u>Storage De</u> f Custom S t erim. Voids	787.2) <u>scription</u> age Data (Irregular) Listed b Inc.Store Cum	.Store Wet.Area
Center-of-Mass of the second s	det. time= 609.8 r Avail.Storage 4,542 c Surf.Area P (sq-ft)	nin (1,397.0 - <u>Storage De</u> f Custom S f	787.2) <u>scription</u> age Data (Irregular) Listed b Inc.Store Cum	
Center-of-Mass of <u># Invert</u> 1 94.25' Elevation (feet) 94.25 94.90	det. time= 609.8 r <u>Avail.Storage</u> 4,542 c Surf.Area P (sq-ft) 850 2 863 2	nin (1,397.0 - <u>Storage De</u> f Custom S erim. Voids (feet) (%) 217.0 40.0 220.0 40.0	787.2) scription age Data (Irregular) Listed b Inc.Store Cum (cubic-feet) (cubic 0 223	.Store Wet.Area c-feet) (sq-ft) 0 850 223 1,026
Center-of-Mass of <u># Invert</u> 1 94.25' Elevation (feet) 94.25 94.90 95.00	det. time= 609.8 r <u>Avail.Storage</u> 4,542 c Surf.Area P (sq-ft) 850 863 1,422	nin (1,397.0 - <u>Storage De</u> f Custom St erim. Voids (feet) (%) 217.0 40.0 220.0 40.0 276.0 100.0	787.2) scription age Data (Irregular) Listed b Inc.Store Cum (cubic-feet) (cubic 0 223 113	.StoreWet.Areac-feet)(sq-ft)08502231,0263363,237
Center-of-Mass of <u># Invert</u> 1 94.25' Elevation (feet) 94.25 94.90	det. time= 609.8 r Avail.Storage 4,542 c Surf.Area P (sq-ft) 850 863 1,422 2,087	nin (1,397.0 - <u>Storage De</u> f Custom S erim. Voids (feet) (%) 217.0 40.0 220.0 40.0	787.2) scription age Data (Irregular) Listed b Inc.Store Cum (cubic-feet) (cubic 0 223	.Store Wet.Area c-feet) (sq-ft) 0 850 223 1,026
Center-of-Mass of <u># Invert</u> 1 94.25' Elevation (feet) 94.25 94.90 95.00 96.00 97.00	det. time= 609.8 r Avail.Storage 4,542 c Surf.Area P (sq-ft) 850 2,858 1,422 2,087 2,858	nin (1,397.0 - <u>Storage De</u> f Custom S erim. Voids (feet) (%) 217.0 40.0 220.0 40.0 220.0 40.0 276.0 100.0 319.0 100.0 365.0 100.0	787.2) scription age Data (Irregular) Listed b Inc.Store Cum (cubic-feet) (cubic 0 223 113 1,744	.StoreWet.Areac-feet)(sq-ft)08502231,0263363,2372,0805,294
Center-of-Mass of <u># Invert</u> 1 94.25' Elevation (feet) 94.25 94.90 95.00 95.00 96.00 97.00 <u># Routing</u>	det. time= 609.8 r <u>Avail.Storage</u> 4,542 c Surf.Area P (sq-ft) 850 863 1,422 2,087 2,858 Invert Outle	nin (1,397.0 - <u>Storage De</u> f Custom S erim. Voids (feet) (%) 217.0 40.0 220.0 40.0 276.0 100.0 319.0 100.0 365.0 100.0 et Devices	787.2) scription age Data (Irregular) Listed b Inc.Store Cum (cubic-feet) (cubic 0 223 113 1,744 2,462	.StoreWet.Areac-feet)(sq-ft)08502231,0263363,2372,0805,2944,5427,821
Center-of-Mass of <u># Invert</u> 1 94.25' Elevation (feet) 94.25 94.90 95.00 96.00 97.00	det. time= 609.8 r <u>Avail.Storage</u> 4,542 c Surf.Area P (sq-ft) 850 2,858 <u>Invert</u> Outle 93.74' 15.0 '	nin (1,397.0 - <u>Storage De</u> f Custom St erim. Voids (feet) (%) 217.0 40.0 220.0 40.0 220.0 40.0 276.0 100.0 319.0 100.0 365.0 100.0 <u>et Devices</u> x 40.0' long	787.2) scription age Data (Irregular) Listed b Inc.Store Cum (cubic-feet) (cubic 0 223 113 1,744	.Store Wet.Area c-feet) (sq-ft) 0 850 223 1,026 336 3,237 2,080 5,294 4,542 7,821
Center-of-Mass of <u># Invert</u> 1 94.25' Elevation (feet) 94.25 94.90 95.00 95.00 96.00 97.00 <u># Routing</u> 1 Primary 2 Device 1	det. time= 609.8 r <u>Avail.Storage</u> 4,542 c Surf.Area P (sq-ft) 850 2,858 <u>Invert Outle</u> 93.74' 15.0' Outle 94.00' 0.00	nin (1,397.0 - <u>Storage De</u> f Custom St erim. Voids (feet) (%) 217.0 40.0 220.0 40.0 220.0 40.0 276.0 100.0 319.0 100.0 365.0 100.0 at Devices ' x 40.0' long et Invert= 93.5 0800 fpm San	787.2) scription age Data (Irregular) Listed b Inc.Store Cum (cubic-feet) (cubid 0 223 113 1,744 2,462 Culvert RCP, sq.cut end pr 0' S= 0.0060 '/' n= 0.013 d filter over Surface area at	.Store Wet.Area c-feet) (sq-ft) 0 850 223 1,026 336 3,237 2,080 5,294 4,542 7,821 rojecting, Ke= 0.500 Cc= 0.900 Dove invert
Center-of-Mass of <u># Invert</u> 1 94.25' Elevation (feet) 94.25 94.90 95.00 95.00 96.00 97.00 <u># Routing</u> 1 Primary 2 Device 1 3 Device 1	det. time= 609.8 r <u>Avail.Storage</u> 4,542 c Surf.Area P (sq-ft) 850 2,087 2,858 <u>Invert Outle</u> 93.74' 15.0' Outle 94.00' 0.00 96.60' 3.00'	nin (1,397.0 - <u>Storage De</u> f Custom St erim. Voids (feet) (%) 217.0 40.0 220.0 40.0 220.0 40.0 276.0 100.0 319.0 100.0 365.0 100.0 et Devices ' x 40.0' long et Invert= 93.5 0800 fpm San ' x 3.00' Horiz	787.2) scription age Data (Irregular) Listed b Inc.Store Cum (cubic-feet) (cubic 0 223 113 1,744 2,462 Culvert RCP, sq.cut end pr 0' S= 0.0060 '/' n= 0.013 d filter over Surface area at Orifice/Grate Limited to we	.Store Wet.Area c-feet) (sq-ft) 0 850 223 1,026 336 3,237 2,080 5,294 4,542 7,821 rojecting, Ke= 0.500 Cc= 0.900 Dove invert bir flow C= 0.600
Center-of-Mass of <u># Invert</u> 1 94.25' Elevation (feet) 94.25 94.90 95.00 95.00 96.00 97.00 <u># Routing</u> 1 Primary 2 Device 1	det. time= 609.8 r <u>Avail.Storage</u> 4,542 c Surf.Area P (sq-ft) 850 863 1,422 2,087 2,858 <u>Invert Outle</u> 93.74' 15.0' Outle 94.00' 0.00 96.60' 3.00' 97.00' 20.0' Head	nin (1,397.0 - <u>Storage De</u> f Custom St erim. Voids (feet) (%) 217.0 40.0 220.0 40.0 220.0 40.0 276.0 100.0 319.0 100.0 365.0 100.0 <u>St Devices</u> x 40.0' long et Invert= 93.5 0800 fpm San x 3.00' Horiz ' long x 15.0' d (feet) 0.20	787.2) scription age Data (Irregular) Listed b Inc.Store Cum (cubic-feet) (cubid 0 223 113 1,744 2,462 Culvert RCP, sq.cut end pr 0' S= 0.0060 '/' n= 0.013 d filter over Surface area at	.Store Wet.Area c-feet) (sq-ft) 0 850 223 1,026 336 3,237 2,080 5,294 4,542 7,821 rojecting, Ke= 0.500 Cc= 0.900 cove invert eir flow C= 0.600 ctangular Weir .40 1.60

Type II 24-hr 10 year JCC Rainfall=5.80"

Prepared by Vanasse Hangen Brustlin, Inc., Richmond, VAPage 6HydroCAD® 7.00 s/n 001234 © 1986-2003 Applied Microcomputer Systems8/16/2004

Subcatchment 3S: Post Development

Runoff = 6.61 cfs @ 11.92 hrs, Volume= 0.296 af, Depth= 4.87"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type II 24-hr 10 year JCC Rainfall=5.80"

Area (ac) CN Description								
0.570 98 Paving and Roofs								
0.160 70 Lot area	·							
0.730 92 Weighted Average								
Tc Length Slope Velocity Capacity (min) (feet) (ft/ft) (ft/sec) (cfs)	Description							
1.5 100 0.0100 1.1	Sheet Flow, Pavement Smooth surfaces n= 0.011 P2= 3.50"							
Pond 1P:	Pond 1P: Surface Sand Filter							
Inflow Area = 0.730 ac, Inflow Depth = 4 Inflow = 6.61 cfs @ 11.92 hrs, Volu Outflow = - 6.24 cfs @ 11.93 hrs, Volu Primary = 6.24 cfs @ 11.93 hrs, Volu 0.00 cfs @ 0.00 hrs, Volu	Ime= 0.271 af, Atten= 6%, Lag= 0.9 min Ime= 0.271 af							

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5 Peak Elev= 96.89' @ 11.93 hrs Surf.Area= 2,775 sf Storage= 4,277 cf Plug-Flow detention time= 367.1 min calculated for 0.271 af (91% of inflow) Center-of-Mass det. time= 321.3 min (1,091.9 - 770.6)

#	Invert	Avail.St	orage	Sto	rage Des	cription			
1	94.25'	4,	542 cf	Cus	stom Sta	ge Data (Irregular)	Listed below		
	ation feet)	Surf.Area (sq-ft)		rim. eet)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
ç	4.25	850	21	7.0	40.0	0	0	850	
ę	4.90	863	22	0.0	40.0	223	223	1,026	
<u> </u>	95.00	1,422	27	6.0	100.0	113	336	3,237	
g	96.00	2,087	31	9.0	100.0	1,744	2,080	5,294	
Ş	97.00	2,858	36	5.0	100.0	2,462	4,542	7,821	
#	Routing	Invert	Outlet	Devi	ces				
1	Primary	93.74'				Culvert RCP, sq.cu ' S= 0.0060 '/' n=			
2	Device 1	94.00'	0.0008	00 fr	om Sand	filter over Surface	area above inver	t .	
- 3	Device 1	96.60'	3.00' >	: 3.00)' Horiz. (Orifice/Grate Limit	ed to weir flow C=	= 0.600	
4 Secondary 97.00' 20.0' long x 15.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63									

Type II 24-hr 10 year JCC Rainfall=5.80"

Prepared by Vanasse Hangen Brustlin, Inc., Richmond, VA HydroCAD® 7.00 s/n 001234 © 1986-2003 Applied Microcomputer Systems 8/16/2004

Primary OutFlow Max=6.22 cfs @ 11.93 hrs HW=96.89' (Free Discharge) 1=Culvert (Passes 6.22 cfs of 9.24 cfs potential flow) 2=Sand filter (Exfiltration Controls 0.04 cfs) 3=Orifice/Grate (Weir Controls 6.18 cfs @ 1.8 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=94.25' (Free Discharge) -4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Type II 24-hr 100year JCC Rainfall=8.00" D2 Sand Filter 81204 BMP الارابية ألا المتعادية Prepared by Vanasse Hangen Brustlin, Inc., Richmond, VA Page 8 HydroCAD® 7.00 s/n 001234 © 1986-2003 Applied Microcomputer Systems 8/16/2004 Subcatchment 1S: Pre development 4.93 cfs @ 12.07 hrs, Volume= Runoff 0.321 af, Depth= 5.27" Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type II 24-hr 100year JCC Rainfall=8.00" Description Area (ac) CN 0.180 .98 Roof & Paving 0.550 70 Wooded 0.730 77 Weighted Average Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs) 15.0 **Direct Entry**, Subcatchment 3S: Post Development 9.32 cfs @ 11.92 hrs, Volume= 0.428 af. Depth= 7.04" Runoff Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type II 24-hr 100year JCC Rainfall=8.00" Area (ac) CN Description 98 Paving and Roofs 0.570 0.160 70 Lot area 0.730 Weighted Average 92 Velocity Capacity Description Tc Length Slope (min) (feet) (ft/ft) (ft/sec) (cfs) 0.0100 **Sheet Flow, Pavement** 1.5 100 1.1 Smooth surfaces n= 0.011 P2= 3.50" Pond 1P: Surface Sand Filter Inflow Area = 0.730 ac, Inflow Depth = 7.04" for 100year JCC event Inflow 9.32 cfs @ 11.92 hrs, Volume= 0.428 af Ξ Outflow 8.89 cfs @ 11.93 hrs, Volume= 0.403 af, Atten= 5%, Lag= 0.8 min = 8.89 cfs @ 11.93 hrs, Volume= 0.403 af Primary = 0.00 hrs. Volume= 0.000 af 0.00 cfs @ Secondary =

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5 Peak Elev= 96.97' @ 11.93 hrs Surf.Area= 2,835 sf Storage= 4,470 cf Plug-Flow detention time= 263.4 min calculated for 0.403 af (94% of inflow) Center-of-Mass det. time= 228.7 min (990.0 - 761.3)

#	Invert	Avail.Storage	Storage Description	
1	94.25'	4,542 cf	Custom Stage Data (Irregular) Listed below	

Type II 24-hr 100year JCC Rainfall=8.00"

Page 9

8/16/2004

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Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)		
94.25	850	217.0	40.0	0	0	850		
94.90	863	220.0	40.0	223	223	1,026		
95.00	1,422	276.0	100.0	113	336	3,237		
96.00	2,087	319.0	100.0	1,744	2,080	5,294		
97.00	2,858	365.0	100.0	2,462	4,542	7,821		
# Routing	Invert	Outlet Dev	ices	······································				
1 Primary	93.74'				cut end projecting,			
					n= 0.013 Cc= 0.90			
2 Device 1	94.00'				ce area above inv			
3 Device 1	96.60'	3.00' x 3.0	3.00' x 3.00' Horiz. Orifice/Grate Limited to weir flow C= 0.600					
4 Secondary	/ 97.00'		20.0' long x 15.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60					

Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=8.89 cfs @ 11.93 hrs HW=96.97' (Free Discharge) 1=Culvert (Passes 8.89 cfs of 9.41 cfs potential flow) 2=Sand filter (Exfiltration Controls 0.04 cfs)

-3=Orifice/Grate (Weir Controls 8.85 cfs @ 2.0 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=94.25' (Free Discharge)

	Godspeed Animal Tewning Road County, VA	Care James C	102 ity			-		8/11/200
	SIZING WATE	R SERVIC	E LINES	AND	MET	ERS	<u> </u>	
	(PLL	MBING FL	TURE VAL	LUE)				æ
				xture alue		o. of xtures	1	otal Fixture Value
Bathtub				8	x	4	=	32
Bedpan washers				10	x		=	0
Combination sink	and tray	-		3	x		=	0
Dental unit				1	x	0	=	0
Dental lavatory				2	х	1	=	2
Drinking fountain	(cooler)			1	×	0	=	0
Drinking fountain	(public)			2	x	0	=	0
Kitchen sink:				3	x	1	=	3
	3/4" connection		· ·	7	x		=	0
Lavatory:	3/8" connection			2	x		Ξ.	0
	1/2" connection	, , , , , , , , , , , , , , , , , , ,		4	х	6	=	24
Laundry tray:	1/2" connection			3	х	1	Ξ	3
	3/4" connection			7	х			0
Shower head (sho				4	х	2	=	8
Service sink:	1/2" connection			3	x	2	=	6
	3/4" connection			7	x	0	- E	0
Urinal:	Pedestal flush valve			35	X		= '	0
	Wall or stall		- 25	12	x	A Destroy	=	0
	Trough (2' unit)			2	X		=	0
Wash sink (each s		la anna 147		4	X	19	= 4	76
Water closet:	Flush valve			35	x	-	=	0
5.1.1	Tank type			3	X	1		21
Dishwasher:	1/2" connection		20 A	4	X	1	=	4
Washing machine	3/4" connection	23		10 5	X	0 2	_	10
w asning machine				12	X		_	0
	3/4" connection				X			
	1" connection			25	X		=	0
Hose connections	(wash down): 1/2"			6	x	<u>с</u>	=	30
	3/4"			10	X	0	=	0
Hose (50' length-	wash down): 1/2"			6.2	X		=	0
	5/8"			9	X		. =	0
	3/4"			12	X	1	=	0
GRAND TOTAL	OF FIXTURE VALU	ES			10			219

SIZING WATER SERVICE LINES AND METERS

TABLE 4.3	
Plumbing Fixture	Value

Fixture Type	Fixture Value Based on 35 gsi at Meter Outlet
Bathtub	
Bedpan washers	
Combination sink and tray	
Dental unit	
Dental lavatory	
Drinking fountain (cooler)	1
Drinking fountain (public)	
Kitchen sink: 1/2-in. connection	
3/4-in. connection	7
Lavatory: 3/8-in. connection	
1/2-in. connection	4
Laundry tray: 1/2-in. connection	
3/4-in. connection	7
Shower head (shower only)	4
Service sink: 1/2-in. connection	
3/4-in. connection	7
Urinal: Pedestal flush valve	
Wall or stall	
Trough (2-ft unit)	2
Wash sink (each set of faucets)	4
Water closet: Flush valve	
Tank type	3
Dishwasher: 1/2-in. connection	4
3/4-in. connection	
Washing machine: 1/2-in. connection	
3/4-in connection	
l-in. connection	
Hose connections (wash down): 1/2-in.	6
3/4-in.	
Hose (50-ft length-wash down): 1/2-in.	
5/8 in	
3/4 in.	

value of a number of units by simply multiplying the single value times the number of fixtures in the customer's use to get a total value. The list of plumbing items in Table 4.3 represents those most commonly used; however, the estimator will eventually encounter special equipment that will need to be evaluated. Since the fixture flow requirements in gallons per minute and the fixture values are the same in Table 4.3, the engineer can list the demand in gallons per minute for the special equipment, along with the other fixtures, to obtain one total.

Demand

After the fixture values have been determined, the results can be applied to a graph to obtain the customer demand in gallons per minute at 35 psi at the meter outlet. The maximum water flow of any one fixture is above the average of any one of a number of fixtures when operated in a customer's service. This is because the probability of all SIZING WATER SERVICE LINES AND METERS

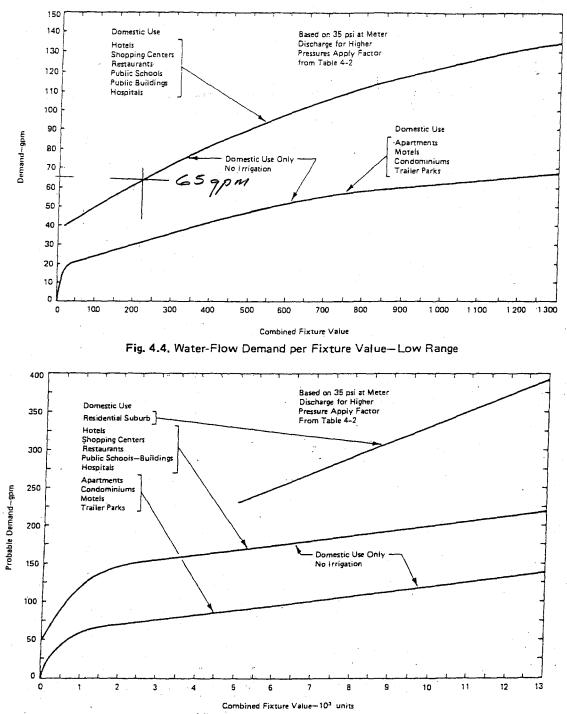


Fig. 4.5. Water-Flow Demand per Fixture Value-High Range

detailed lists of fixtures before estimates can be prepared. If the structure is in the planning stage, the mechanical engineer or architect is the best source of information, and, if construction is underway, the plumbing contractor or the building permits section of the city will have the information. Field trips by the estimator are often necessary to assist the customer as well as to properly assess the project when

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TABLE 5.6

Displacement-Type Meters Meeting AWWA Standards Flow-Pressure Loss Averages of 1990-Model Meters

Size	Maximum AWWA Flo	Capacity w Criteria	Recomment Criteria	U	Continu Criteria-	Brands Included		
in.			gpm	psi	gpm	psi	in Averages	
1/2	15	7.9	12	5.0	7.5	2.0	1	
5/8	20	9.7	16	6.2	10	2.4	5	
3/4	30	10.4	24	6.7	.15	2.6	5	
1 .	50	9.8	40	6.3	25	2.5	5	
$\rightarrow 1 \frac{1}{2}$	100	10.6	80	6.8	50	2.7	4	
2	160	11.3	130	7.1	80	2.8	4	

TABLE 5.7

Compound-Type Meters Meeting AWWA Standards Flow-Pressure Loss Averages of 1990-Model Meters

Size	1	n Capacity low Criteria	1	nded Design –80% Cap.	1	Continuous Flow Criteria—50% Cap.					
in.	gpm	psi	gpm	gpm psi		psi	in Averages				
2	160	8.0	130	5.1	80	2.0	5				
3	320	7.2	255	4.6	160	1.8	5				
4	500	6.2	400	4.1	250	1.6	5				
6	1000	8.4	800	5.4	500	2.1	5				
8	1600	14.5	1300	9.3	800	3.8	1				

TABLE 5.8

Class II Turbine-Type Meters Meeting AWWA Standards Flow-Pressure Loss Averages of 1990-Model Meters

Size	f	i Capacity ow Criteria	1	nded Design -80% Cap.	Continue Criteria—	Brands Included	
in.	gpm	psi	gpm	psi	gpm	psi	in Averages
2	160	4.0	130	2.5	100	1.0	5
3	350	4.0	280	2.6	240	.9	5
4	630	2.0	500	1.4	420	.7	5
6	1 400	2.0	1 100	1.2	920	.5	5
8	2 400	2.7	1 900	1.7	1 600	.7	5
10	3 800	2.6	3 000	1.4	2 500	.5	5
12	5 000	1.7	4 000	1.1	3 300	1	

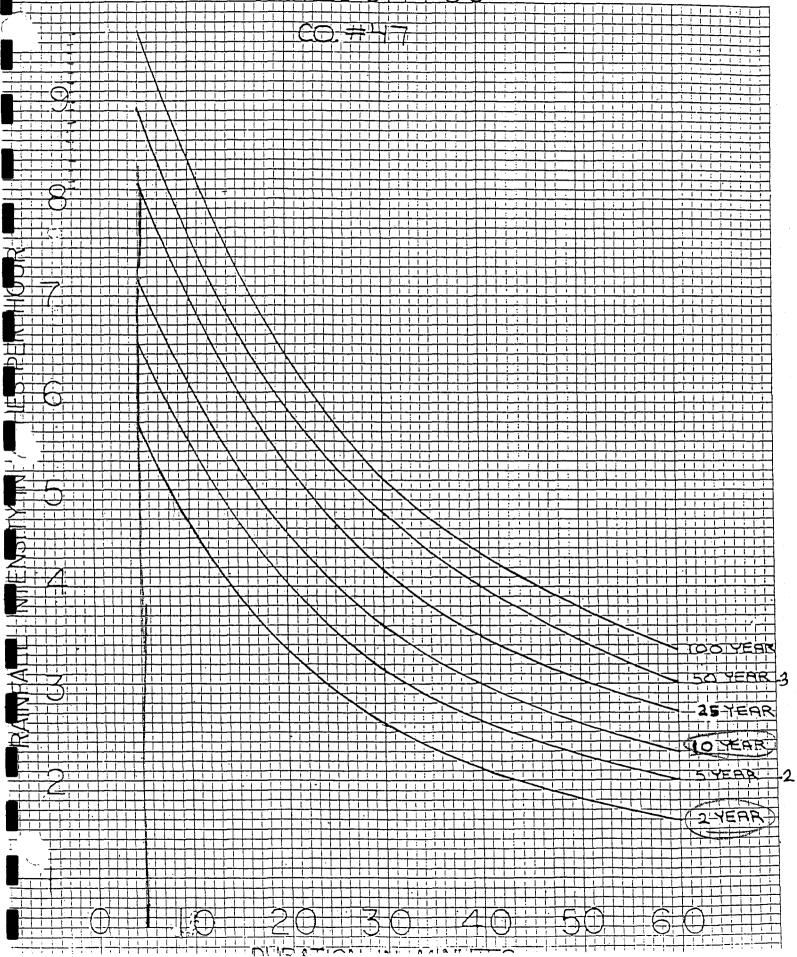
5.9 as the equivalent length of straight pipe that will give the friction loss that will occur as the water passes through the fitting. The values will be approximate in some cases because the pipe's inside diameter is based on the size of the fittings, and in some cases the inside diameter will be slightly larger or smaller; however, the effects of the error will be negligible and the values are considered sufficiently accurate for the purpose of this manual.

Pressure-reducing valves are used in mountainous and hilly areas to protect the

Computations VHB GODSPEED 31248.01 Project: Project # Location: Jcc l of l Sheet Calculated by: WEAR Date: Checked by: Date: Title "AREA | TO LEVEL SPREADER" PRE -ALEA = 0.21AC "C" = 0.42 Q2= CIA = 0.50 cfs $T_{c=5Min}$, I = 5.7Post -Area = 0.21AC "C" = 0.45 $Q_2 = CIA = 0.54 CFS$ Te= 5min I= 5.7

mkgr.forms.humanres.computations.pm65





:

Computations

VHB

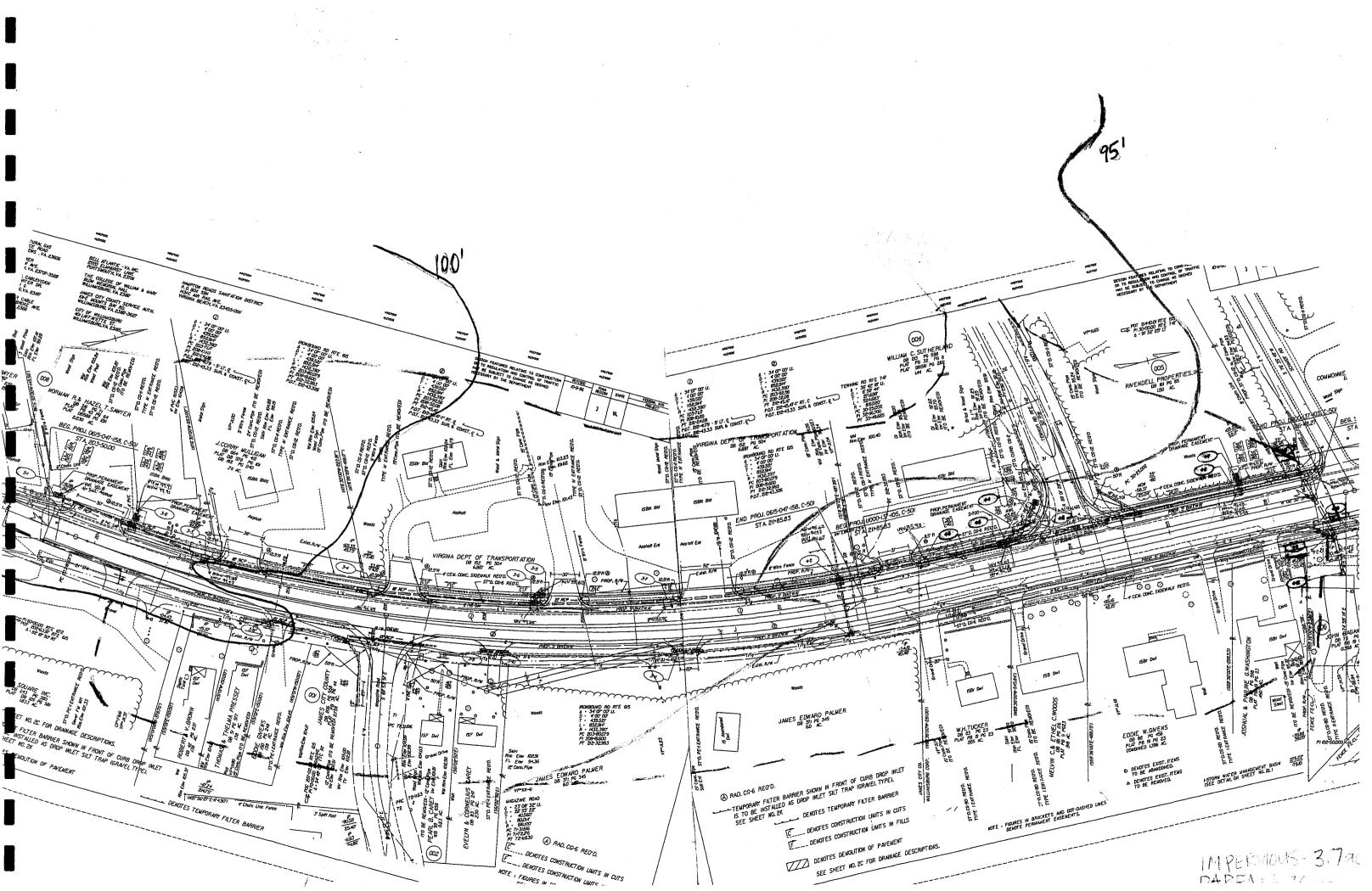
Project: GODSPEED	F
Location: JCC	
Calculated by: WEM KL	I
Checked by:	. 1
Title	

31248.01 Project # l of l Sheet Date: Date:

mkgr.forms.humanres.computations.pm65

EXISTING VOOT SYSTEM

- AS SHOWN IN THE "STORM DRAINAGE COMPUTATIONS", THE CAPACITY OF THE EXISTING 30" RCP (STR. 4-78) IS 37.37 CFS AND THE EXISTING QID = 17.47 CFS THE IMPROVEMENTS TO GOOSPEED (QID OUTFLOW = 6.24 CFS) IS ACCEPTABLE AND THE EXISTING SYSTEM CAN HANDLE THESE FLOWS.



VHB Vanasse Hangen Brustlin, Inc.

Storm Drainage Computations

115 South 15th Street	
Suite 200	Design Parameters

Suite 200	Design Parameters	Name	Godspeed	Proj. No.	31248.01
Richmond, VA 23219	10 Year Storm	Client		Date	8/12/2004
804-343-7100	15" Min. Pipe Size	Subject	PIPE SIZING	Computed by	KEL
	n=0.013			Checked by	

FROM	TO	AREA	RUNOFF	C	A	INLET	RAIN-	RUNOFF	INV	ERT	LENGTH	SLOPE	DIA.	CAPA-	VELO-	FLOW	MINIMUM
		DRAIN,	COEF.	INCRE-	ACCUM-	TIME	FALL	Q	ELEV	ATIONS				CITY	CITY	TIME	PIPE
POINT	POINT	ACRES	С	MENT	ULATED	MIN.	IN./HR.	C.F.S.	UPPER	LOWER	FT.	FT./FT.	INCHES	C.F.S.	F.P.S,	SEC.	DIA(in)
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
											1						
Ex. 18"	Ex. JB	0,430	0.460	0.198	0.198	5.00	7.17	- 1.42	97.270	93.090	65.0	0.06431	18	26.64	8.01	8.11	5.99
Ex. JB	No. 4-8	3.500	N/A	2.710	2.908	10.00	6.01	= 17.47	92.310	91.480	100.0	0.00830	30	•• 37.37	7.48	13.37	22.56
No. 4-8	No. 4-9	0.260	0.900	0.234	3.314	10.22	5.96	19.76	91.480	90.980	66.0	0.00758	30	35.70	7.61	8.67	24.03
No. 4-9	No. 4-11	0.050	0.900	0.045	3.359	10.37	5.94	19.94	88.500	87.990	66.0	0.00773	30	36.06	7.63	8.65	24.02
No. 4-11	No. 4-12	1.730	0.610	1.055	4.414	10.51	5.91	26.08	87.990	87.700	34.0	0.00853	30	37.88	8.50	4.00	26.08
18.1.18 1																	
No, 4-7	No. 4-8	0.430	0.400	0.172	0.172	5.00	7.17	1.23	94.020	93.980	10.0	0.00400	12	2.25	2.93	3.41	9.57
														1			
No. 4-6	No. 4-8	N/A	N/A	2.710	2.710	10.00	6.01	16.28	93.030	92.310	132.0	0.00545	30	30.29	6.08	21.71	23.77

. This shows that there is capacity in the system. by estimating existing conditions

VHB Vanasse Hangen Brustlin, Inc.

Hf= Ho+Hi+H 스

HYDRAULIC GRADE LINE

25° K = 0.22

115 South 15th Street							 . ÷ .
Suite 200			Project :	Godspe	ed		
Richmond, VA 23219			Calculated by:	KEL			
804-343-7100		•	· Date:	8/12/200	4		 1
			n = 0.013			· · · ·	

				10 A		1						JUNG	CTION LO	SS									
INLET STATION	OUTLET WATER SURFACE ELEV.	D _o (IN)	Q _o (CFS)		S _{F0} %	(+1)	Vo (FPS)	Ho (FT)	Qi (CFS)	Vi (FPS)	QixVi	¥,² 2g	(FT)	Angle	(#1)			0.5 H		Inlet Water Surface Elev.		Flow Through Drop Inlet (CFS)	Inlet Shaping Y/N
#	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)		(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)	(23)
No. 4-11	89.70	30	26.08	34.00	0.4074	0,14	8.50	0.28	19.94	7.63	152.14	0.90	0.32	0	0.00	0.60	N.A.	N.A.	0.74	90.44	96.33	0.00	N
No. 4-9	90.44	30	19.94	66.00	0.2381	0.16	7.63	0.23	19.76	7.61	150.37	0,90	0.31	90	0.63	1.17	N.A.	N.A.	1.33	91.76	97.70	0.00	N
No. 4-8	92.98	30	19.76	66.00	0.2339	0.15	7.61	0.22	17.47	7.48	130.68	0.87	0.30	0	0.00	0.53	N.A.	N.A,	0.68	93.66	- 97.73	0.00	N
Ex. JB	93.66	30	17.47	100.00	0.1828	0,18	7.48	0.22	16.28	6.08	98.98	0.57	0.20	0	0.00	0.42	N.A.	N.A.	0.60	94.26	98.19	0.00	N
			T																				
			1																	1.			
																	1						
			1			1.00															· ·		
			1																	1917 - Carlos Maria			
Equations: Outlet Wa	ter Elevation	≈ 80% d	lameter	Ho = 0.2	25 V _o ²/2g			P.		<u>.</u>		90° K :				0.47		20° K =		1	L	· ·	L
Sf = [nQ _o /(1	.486AR ^{2/3})] ²				•							80° K :				0.38		15° K =	0.10				
				H ∆ =K V	°2/2g	,						70° K :	= 0.61		30° K =	0.28							

 $60^{\circ} \text{K} = 0.55$

H_i = 0.35 V_i²/2g

FINAL $H = H_f + H_i$

This approximates the existing Hydraulic Grade Line.

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SEWAGE PUMP STATION DESIGN:

James City Service Authority Water and Sanitary Sewer Design criteria, Table 2.1, indicate that the average daily flow for a Veterinary Clinic should be 0.18 Gallons Per Day Per Gross Square Foot of Building Area. For the proposed addition this would translate as Sewage pump <u>design</u>. <u>Flow of 7.05</u> gallons per minute.

Actual Water use records for the last quarter billed indicate a daily water demand of 0.25 Gallons Per day Per Gross Square Foot, which gives a Sewage pump <u>design flow of 9.75</u> gallons per minute.

Fixture plans for the addition indicate that the peak water demand would be 57 to 63 gallons per minute and the resulting sewage flow could be <u>30 to 36</u> gallons per minute.

In their review comments the James City Service Authority indicated that we would be able to connect to the existing force main in Tewning Road only if we identify the model of each of the other pumps on the system to assure that our pump will not over ride and cause problems with the others.

We have determined by directly contacting the owners that all of the pumps on the system are the E-one semi-positive displacement pumps. There are a total of 13 pump stations on the system. The addition would increase this to fourteen. We have also determined that the JCSA force main does not connect to the HRSD force main as we were originally informed, but ties into the gravity sewer parallel to the HRSD main.

The duplex E-one system as we proposed in our June 14, 2004 Memorandum to Danny Poe of the Service Authority would be a solution that would be fully compatible with the system. However, the maximum flow rate obtainable with the E-one is less than 16 g.p.m., which is above the flow rate required by JCSA standards, but less than the IPC Code estimate of 30 g.p.m.

With this information we have re-evaluated the pump design and are proposing to use a submersible grinder pump system as manufactured by Crane Pumps & System, Barnes Professional Plumbing.

For a system of 10 to 18 pumps the probable maximum number of pumps operating simultaneously is four. Calculations indicate that the selected pump will operate above the JCSA Standard design rate of 10 g.p.m. with up to eight other pumps operating. At the maximum probable flow condition it will provide 36 g.p.m. and with no other pumps operating it will discharge at 44 g.p.m.

VHB

	EED ANIMAL CARE EXPAN COAD, JAMES CITY COUMT						
TIMATED DESIGN FLOW :				_			
S.A.TABLE 2.1; VETERINARY J.C.S.A. WATER METER		0.18 GPD/GSF 0.25 GPD/GSF	11270 S. 11270 S.			GPD @ DF = 12 GPD @ DF = 12	
J.G.J.A. WATER METER	USE HIGHER VA		112/0 3.	.г.	2017.3		
	ool hould the			Qavq. =	3.91	g.p.m.	~ °¥
				Qmin. ≖	1.96	g.p.m.	
SE	WAGE PUMP FLOW AT	PEAK FACTOR:	2.50	Q _{DESIGN} =	9.78	g.p.m.	
U	sing 2000 IPC as Basis :						
	TOTAL FIXUTRE UNIT	VALUE FOR ADDITION :	119 SI		TABLE E1		
	ESTIN	ATED PEAK DEMAND :	48 g.		TABLE E1	02	
		PEAKING FACTOR:	Qpeak = 4.0	48.00 Qavg. =	g.p.m. 12.00	a a m	
		FEAKING FACTOR.	4.0	Qavy. – Qmin. =	6.00	g.p.m. g.p.m.	
	SEWAGE PUM	P DESIGN FLOW AT	2.5	Q _{PEAK} =		* ·	
					10.00		
ET WELL DIMENSIONS & C		PU	MP DESIGN F	LOW RATE:	10.00	g.p.m.	
	ONTROL POINTS .						
				UMP /ETWELL		W=0 IF ROUND	
	LOCKABLE		**	DorL		W *	
	SAFETY	·	INTERIOR :	4.00	FEET	0.00	
	GRATE		THICKNESS :	4.00	INCHES		
			EXTENSION : THICKNESS :	8.00 8.00	INCHES		
TOP/	8.		THICKNESS :	0.00	INCHES	Neglect top weight	
			TOP :	100.50	FEET		
·	A .	. w	GROUND : ATER TABLE :	100.00 96.50	FEET		
		SIBLE	IPE OUT INV. :	97.00	FEET		
	RAIL MO	UNTED SE	WER IN INV. :	96.00	FEET		
l í fi	SYSTEM	HIGH WA	ATER ALARM :	95.83	FEET		
			AG PUMP ON : AD PUMP ON :	95.33 95.00	FEET		
			PUMPS OFF :	94.33	FEET		
		WETV	VELL FLOOR :	93.50	FEET		
			UNIT DISPLACE	MENT: Vdisp =	17.10	CF/VF	
				ORAGE ; Vint =	12.57	CF/VF	
ALARM	DISCHARGE		BA	SE AREA; Ab =	28.27	SQ.FT.	
				TOP AREA; A _T =	12.57		
LEAD ON			CONCRETE :	150 (/ C.F	
			GHT WATER :		POUNDS		
воттом			EIGHT SOIL :		POUNDS		
				VOLUMES ;			
A THE MERINA STREET			TOTAL :	71	C.CF.>GA		
<u> Anna an Anna an Aona</u>	\overline{A}		LAG :	4	C.CF.>GA		
	n an an fair fair an fa		OPERATING :	8	C.CF.>GA		
		ΔΕ	BOVE ALARM :	52	C.CF.>GA	NL 392	
		~					

- FILL TIME @ MINIMUM FLOW ; 31 MINUTES
- PUMP RUN TIME@ MINIMUM FLOW ; MINUTES 8
 - CYCLE TIME ; 39 MINUTES

 - OVERFLOW TIME ; 39
- DISPLACEMENT BELOW GROUND WATER ; 70 CU.FT.
- BOUYANT FORCE (UPWARD); 4378 POUNDS WEIGHT OF STRUCTURE ; 7592 POUNDS WEIGHT OF SOIL ; 6510 POUNDS TOTAL RESISTING FORCE ; 14102 POUNDS

RESISTANCE TO FLOTATION: CHECK F.S.~= 1.5

3.2

FILL / RUN TIME CALCULATIONS :

BOUYANCY CALCULATION :

Page 1

MINUTES

Vanasse Hangen Brustlin, Inc.

SEWAGE PUMP STATION CALCULATIONS

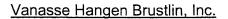
FILE NO.: 31248.01

GODSPEED ANIMAL CARE EXPANSION TEWNING ROAD, JAMES CITY COUMTY, VA

PIPE SIZE	Well/Pit		EQUIN	/ALENT
	FITTING TYPE	QUANTITY OF FITTINGS	LENGTH IN DIAMETERS	LENGTH IN FEET
1.50	GATE VALVE			
	FULL OPEN	1	13	1.6
-	GLOBE VALVE OPEN	0	340	0.0
	SWING CHECK VALVE	1	80	10.0
	ELBOWS			
	90° STANDARD	2	31	7.8
	90° LONG RADIUS	0	20	0.0
	45° STANDARD	0	16	0.0
	TEE (BRANCH)	1	75	9.4
	TEE (LINE)	0	20	0.0
		TOTAL EQUIVAL	ENT LENGTH ;	29

		EQUIN	/ALENT
Q	UANTITY OF FITTINGS	LENGTH IN DIAMETERS	LENGTH IN FEET
LL OPEN	2	13	3.3
/E OPEN	0	340	0.0
VALVE	0	80	0.0
ANDARD	1	31	3.9
RADIUS		20	0.0
ANDARD	0	16	0.0
)	1	75	9.4
	1	20	2.5
тс	DTAL EQUIVA	LENT LENGTH ;	19
	LL OPEN /E OPEN VALVE ANDARD RADIUS ANDARD	LL OPEN 2 /E OPEN 0 VALVE 0 ANDARD 1 & RADIUS ANDARD 0) 1 1	QUANTITY OF FITTINGSLENGTH IN DIAMETERSLL OPEN213/E OPEN0340VALVE080ANDARD131S RADIUS20ANDARD016)175

PIPE				
SIZE	Force Main		EQUIV	ALENT
	FITTING TYPE	QUANTITY OF FITTINGS	LENGTH IN DIAMETERS	LENGTH IN FEET
2.00	GATE VALVE			
	FULL OPEN	- 1	13	2.2
	GLOBE VALVE OPEN	0	340	0.0
	SWING CHECK VALVE	0	80	0.0
	ELBOWS			
	90° STANDARD	0	31	0.0
	90° LONG RADIUS	;	20	0.0
	45° STANDARD	0	16	0.0
	TEE (BRANCH)	1	75	12.5
	TEE (LINE)		20	0.0
		TOTAL EQUIVAL	ENT LENGTH ;	15



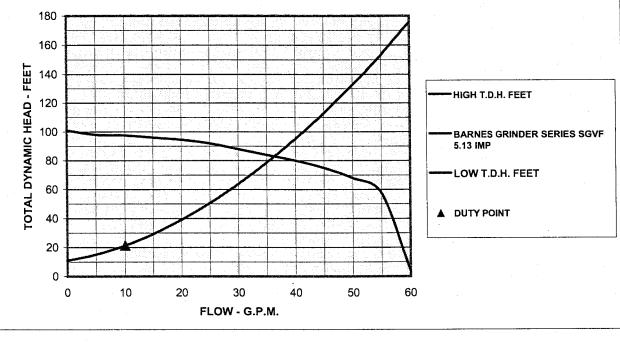
SEWAGE PUMP STATION CALCULATIONS

VHB

FILE NO.:

31248.01

Goo	ispeed A	nimal Care						
Williamsburg /	James (City County	,					5
	MAXI	MUM PROB	ABLE FLO	N CONDI	TION			
· *	THRE	E OTHER F	UMPS OPE	RATING		1	BARNES GRINDE	R
							SERIES SGVF	
			n.	_ \	FLOW	HIGH T.D.H.	5.13 IMP	
PUMP TOTAL DYNAMIC HEAD O	CALCULA	ATION:			G.P.M.	FEET		
	Other F	low to Shared	Forcemain :	33	0	10.99	101	
PUMP ON LIQUID ELEV .:	95.00	FEET	7		5	15.12	98	
PUMP OFF LIQUID ELEV .:	94.33	FEET			10	21.32	97.5	
HIGH POINT ELEV. :	97.00	FEET			15	29.38	96	
ELEVATION AT CONNECTION :	95.00	FEET			20	39.21	94.5	
NORMAL LOW HEAD AT CONNECTION .:	0.00	FEET			25	50.74	92	
MAXIMUM HEAD AT CONNECTION .:	0.00	FEET		0	30	63.92	88	
STATIC HEAD :	0.67	FEET			35	78.70	84	
	Well/Pit	Onsite	Force Main		40	95.07	80	
LENGTH OF PIPE :	10	245	350	FEET	45	112.98	75	
EQUIVALENT LENGTH OF FITTINGS :	29	19	15	FEET	50	132.42	68	
PIPE DIAMETER :	1.50	1.50	2	INCHES	55	153.36	57.5	
HAZEN-WILLIAMS CONSTANT	130	130	130		60	175.78	4	
DESIGN FLOW RATE :	10	10	43	G.P.M.				
DESIGN FLOW VELOCITY =	1.82	1.82	4.39	F.P.S.				
DESIGN FLOW FRICTION HEAD =	0.49	3.33	16.84	FEET				
TOTAL DYNAMIC =	21.32	2 FEET						



HIGH RANGE OPERATING FLOW : HIGH RANGE OPERATING HEAD : WATER HORSEPOWER : MAIN VELOCITY : 36.30 G.P.M. 82.81 FEET 0.76 H.P. 6.59 F.P.S.

F.P.S.

F.P.S.

MEETS DESIGN RATE

69.3 G.P.M. TOTAL F.M. FLOW

COMBINED FLOW

6.59

7.08

Well/Pit

Onsite

Force Main

Land Development Environmental Services

Vanasse Hangen Brustlin, Inc.

VHB

SEWAGE PUMP STATION CALCULATIONS

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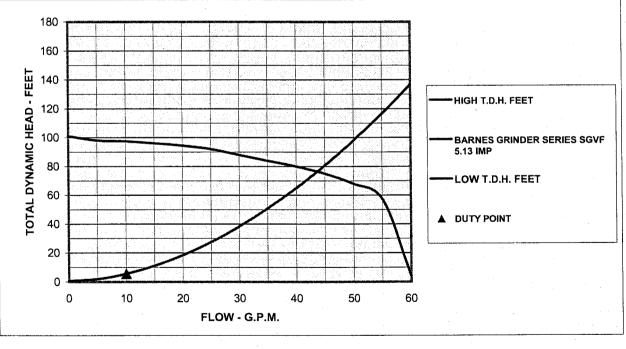
31248.01

Transportation Land Development

5

Godspeed Animal Care Williamsburg / James City County

		O OTHER					BARNES GRINDER	
	C	OPERATIN	G				SERIES SGVF	
	L	· · · · · · · · · · · · · · · · · · ·			FLOW	HIGH T.D.H.	5.13 IMP	ľ
PUMP TOTAL DYNAMIC HEAD (CALCUL	ATION:		\searrow	G.P.M.	FEET		ŀ
•	Other F	low to Share	d Forcemain :	Ō	0	0.67	101	
PUMP ON LIQUID ELEV .:	95.00	FEET			5	2.04	98	
PUMP OFF LIQUID ELEV .:	94.33	FEET			10	5.62	97.5	
HIGH POINT ELEV. :	97.00	FEET			15	11.15	96	
ELEVATION AT CONNECTION :	95.00	FEET			20	18.51	94.5	
NORMAL LOW HEAD AT CONNECTION .:	0.00	FEET			25	27.62	92	
MAXIMUM HEAD AT CONNECTION .:	0.00	FEET		0	30	38.44	88	
STATIC HEAD :	0.67	FEET			35	50.90	84	
	Well/Pit	Onsite	Force Main		40	64.97	80	
LENGTH OF PIPE :	10	245	350	FEET .	45	80.63	75	
EQUIVALENT LENGTH OF FITTINGS :	29	19	15	FEET	50	97.84	68	
PIPE DIAMETER :	1.50	1.50	2	INCHES	55	116.57	57.5	
HAZEN-WILLIAMS CONSTANT :	130	130	130		60	136.81	4 .	
DESIGN FLOW RATE :	10	10	10	G.P.M.				
DESIGN FLOW VELOCITY =	1.82	1.82	1.02	F.P.S.				
DESIGN FLOW FRICTION HEAD =	0.49	3.33	1.13	FEET				
TOTAL DYNAMIC =	5.6	2 FEET						
						•		



HIGH RANGE OPERATING FLOW : HIGH RANGE OPERATING HEAD : WATER HORSEPOWER : 43.64 G.P.M. 76.21 FEET 0.84 H.P. MEETS DESIGN RATE

MAIN VELOCITY :		
Well/Pit	7.92	F.P.S.
Onsite	7.92	F.P.S.
Force Main	4.46	F.P.S.

Godspeed Barnes GrinderPump.XLW

5

SEWAGE PUMP STATION CALCULATIONS

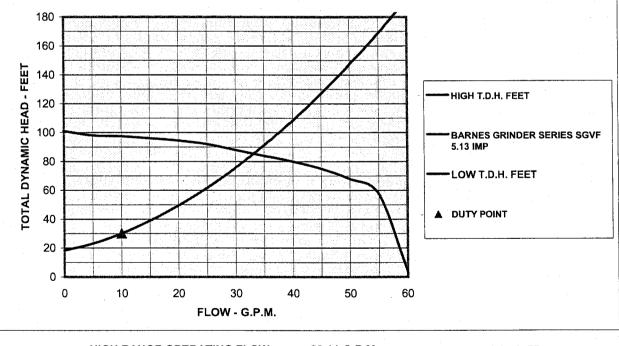
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FILE NO .:

31248.01

Godspeed Animal Care
Williamsburg / James City County

	41 IN 4 A 1 1		FODOF MAI	N 1	·····		
			FORCE MAI				BARNES GRINDER
		NDITION 4	OTHER PU	MPS	1		SERIES SGVF
OPER	ATING				low	HIGH T.D.H.	5.13 IMP
PUMP TOTAL DYNAMIC HEAD C	ALCUL	ATION:			G.P.M.	FEET	
	Other F	low to Share	d Forcemain :	44	0	18.24	101
PUMP ON LIQUID ELEV .:	95.00	FEET			5	23.17	98
PUMP OFF LIQUID ELEV .:	94.33	FEET			10	30.15	97.5
HIGH POINT ELEV. :	97.00	FEET			15	38.98	96
ELEVATION AT CONNECTION :	95.00	FEET			20	49.56	94.5
NORMAL LOW HEAD AT CONNECTION .:	0.00	FEET			25	61.84	92
MAXIMUM HEAD AT CONNECTION .:	0.00	FEET		0	30	75.75	88
STATIC HEAD :	0.67	FEET			35	91.27	84
	Well/Pit	Onsite	Force Main		40	108.36	80
LENGTH OF PIPE :	10	245	350	FEET	45	126.99	75
EQUIVALENT LENGTH OF FITTINGS :	29	19	15	FEET	50	147.14	68
PIPE DIAMETER :	1.50	1.50	2	INCHES	55	168.78	57.5
HAZEN-WILLIAMS CONSTANT :	130	130	130		60	191.90	4
DESIGN FLOW RATE :	10	10	54	G.P.M.			
DESIGN FLOW VELOCITY =	1.82	1.82	5.52	F.P.S.			
DESIGN FLOW FRICTION HEAD =	0.49	3.33	25.66	FEET			
TOTAL DYNAMIC =	30.1	5 FEET					



HIGH RANGE OPERATING FLOW : HIGH RANGE OPERATING HEAD : WATER HORSEPOWER : MAIN VELOCITY : 33.14 G.P.M. 85.30 FEET 0.71 H.P. F.P.S.

F.P.S.

F.P.S.

MEETS DESIGN RATE

77.1 G.P.M. TOTAL F.M. FLOW

COMBINED FLOW

6.02

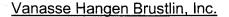
6.02

7.88

Well/Pit

Onsite

Force Main



5

SEWAGE PUMP STATION CALCULATIONS

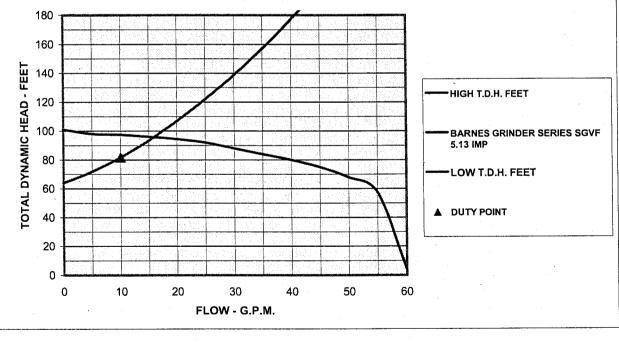
VHB

FILE NO .:

31248.01

Godspeed Animal Care Williamsburg / James City County

		IGHT OTHE					BARNES GRINDER SERIES SGVF	
			~ ~	<u> </u>	FLOW	HIGH T.D.H.	5.13 IMP	
PUMP TOTAL DYNAMIC HEAD (ALCUL	ATION:		\searrow	G.P.M.	FEET		
	Other F	low to Shared	i Forcemain :	88	0	64.01	101	
PUMP ON LIQUID ELEV .:	95.00	FEET			5	71.88	98	
PUMP OFF LIQUID ELEV .:	94.33	FEET			10	81.78	97.5	l
HIGH POINT ELEV. :	97.00	FEET			15	93.49	96	
ELEVATION AT CONNECTION :	95.00	FEET			20	106.93	94.5	ĺ
NORMAL LOW HEAD AT CONNECTION .:	0.00	FEET			25	122.04	92	ĺ
MAXIMUM HEAD AT CONNECTION .:	0.00	FEET		0	30	138.76	88	ŀ
STATIC HEAD :	0.67	FEET			35	157.07	84	
	Well/Pit	Onsite	Force Main		40	176.92	80	
LENGTH OF PIPE :	10	245	350	FEET	45	198.30	75	
EQUIVALENT LENGTH OF FITTINGS :	29	19	15	FEET	50	221.17	68	
PIPE DIAMETER :	1.50	1.50	2	INCHES	55	245.52	57.5	
HAZEN-WILLIAMS CONSTANT :	130	130	130		60	271.34	4	1
DESIGN FLOW RATE :	10	10	98	G.P.M.				ļ
DESIGN FLOW VELOCITY =	1.82	1.82	10.01	F.P.S.	•			
DESIGN FLOW FRICTION HEAD =	0.49	3.33	77.29	FEET				
TOTAL DYNAMIC =	81.7	8 FEET						



HIGH RANGE OPERATING FLOW : HIGH RANGE OPERATING HEAD : WATER HORSEPOWER : MAIN VELOCITY : 15.84 G.P.M. 95.63 FEET 0.38 H.P. 2.88 F.P.S.

F.P.S.

F.P.S.

MEETS DESIGN RATE

103.8 G.P.M. TOTAL F.M. FLOW

COMBINED FLOW

2.88

10.61

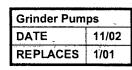
Well/Pit Onsite

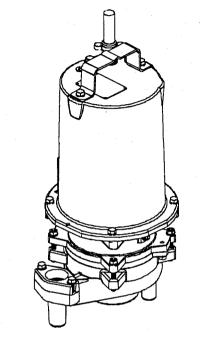
Force Main



SGVF & SGVH

SUBMERSIBLE GRINDER PUMPS Recessed Vortex





Series: SGVF & SGVH 2 HP, 3450 RPM, 60Hz High-Flow and High Head





CSA 108 - File No. LR16567 UL 778 Models SGVF2002L and SGVH2002L are NOT UL or CSA listed.

Description:

NRTL\C

THE GRINDER PUMP IS DESIGNED TO REDUCE DOMESTIC, COMMERCIAL, INSTITUTIONAL AND LIGHT INDUSTRIAL SEWAGE TO A FINELY GROUND SLURRY. DISCHARGE: LIQUID TEMPERATURE: VOLUTE: MOTOR HOUSING: SEAL PLATE: IMPELLER: Design:

Specifications:

Material:

SHREDDING RING:

CUTTER:

SHAFT: SQUARE RINGS: HARDWARE: PAINT: SEAL: Design: Material:

CABLE ENTRY:

CABLE: UPPER BEARING: Load: INTERMEDIATE BEARING: Load: LOWER BEARING: Design: Lubrication: Load: MOTOR: Design: 1-1/4" NPT, Vertical 160°F (71°C) Intermittent Cast Iron ASTM A-48, Class 30. Cast Iron ASTM A-48, Class 30. Cast Iron ASTM A-48, Class 30. 12 Vane, Vortex, With Pump Out Vanes On Back Side. Dynamically Balanced, ISO G6.3. 85-5-5-5 Bronze (Std). ASTM A-48 Cast Iron (Optional) Hardened 440C Stainless Steel Rockwell® C-55 Hardened 440CStainless Steel, Rockwell® C-55. 416 Stainless Steel Buna-N 300 Series Stainless Steel Air Dry Enamel. Tandem Mechanical, Oil Filled Reservoir. Rotating Faces - Carbon Stationary Faces - Ceramic Elastomer - Buna-N Hardware -300 Series Stainless 15 ft. (4.6M) Std. Cord. Custom Molded Quick Connect, for Sealing and Strain Relief. Other Lengths Available Include 8ft (2.4M), 20ft (6M), 30ft (9M), 50ft (15M), 75ft (22.8M) & 100ft (30.5M). CSA/UL Approved 12/4 Type SOW.

Single Row, Ball, Oil Lubricated Radial

Single Row, Ball, Oil Lubricated Radial & Thrust

Sleeve Oil Radial NEMA L

NEMA L-Single Phase, (SGVF2022L or SGVH2022L includes overload protection in the motor). NEMA B-Three Phase Torque Curve. Oil-Filled, Squirrel Cage Induction. Class B.

Insulation:

SINGLE PHASE: Capacitor Start/Capacitor Run. Requires Overload Protection to be Included In control panel, except SGVF2022L or SGVH2022L. Requires Barnes® Starter or Control Panel which Includes Capacitors, or Capacitor pack. THREE PHASE: Dual Voltage 240/480; Requires Overload Protection to

be Included in control panel. **OPTIONAL EQUIPMENT:** Seal Material, Impeller Trims, Cable Length. Moisture Sensors, Leg Kit P/N: 108339.



PUMPS & SYSTEMS

A Crane Co. Company Mansfield, Ohio 4490 Db: (027) 778 9047

Mansfield, Ohio 44907-2674 Ph: (937) 778-8947 Fax: (419) 774-1530 www.Barnes-PS.com 420 Third Street Piqua, Ohio 45356-0603 Ph: (937) 778-8947 Fax: (937)773-2238 www.cranepumps.com



PS-001

MODEL PART HP VOLT PH RPM NEMA FULL LOCKED CORD CORD 10.05 2.72 (69) 1 4450 Logs OPTIONAL CORD CORD CORD TYPE O NO. NO. 10.051 2.72 (69) 1 NEMA FULL LOCKED CORD CORD TYPE O HIGH-FLOW SGVF20021* 110614 2 200 1 3450 F 17.0 53.0 12/4 SOW SGVF20021* 110611 2 200 3 3450 H 15.0 53.8 12/4 SOW SGVF2032L 110611 2 240 3 3450 H 9.0 36.0 12/4 SOW SGVF2032L 110611 2 240 3 3450 H 4.0 18.0 12/4 SOW SGVF2032L 110611 2 600 3 3450 H 4.0 18.0 12/4 SOW SGVF2052L 110613 10013 2	YSTEMS
NO. NO. (NOM) START CODE LOAD AMPS ROTOR AMPS SIZE TYPE O. HIGH-FLOW	
SGVF2002L* 110614 2 200 1 3450 F 17.0 53.0 12/4 SOW SGVF2022L 110609 2 240 1 3450 H 15.0 53.8 12/4 SOW SGVF2022L 110610 2 200 3 3450 J 11.0 42.0 12/4 SOW SGVF2032L 110611 2 240 3 3450 H 9.0 36.0 12/4 SOW SGVF2032L 110611 2 240 3 3450 H 9.0 36.0 12/4 SOW SGVF2042L 110612 2 480 3 3450 H 4.0 18.0 12/4 SOW SGVF2052L 110613 2 600 3 3450 H 3.2 14.4 12/4 SOW HIGH-HEAD No No <th>CORD D. ± .02 (.5) in (mm)</th>	CORD D. ± .02 (.5) in (mm)
SGVF2022L 110609 2 240 1 3450 H 15.0 53.8 12/4 SOW SGVF2022L 110610 2 200 3 3450 J 11.0 42.0 12/4 SOW SGVF2032L 110611 2 240 3 3450 H 9.0 36.0 12/4 SOW SGVF2032L 110612 2 480 3 3450 H 9.0 36.0 12/4 SOW SGVF2042L 110612 2 480 3 3450 H 4.0 18.0 12/4 SOW SGVF2052L 110613 2 600 3 3450 H 3.2 14.4 12/4 SOW HIGH-HEAD	0.07 (17)
SGVF2062L 110610 2 200 3 3450 J 11.0 42.0 12/4 SOW SGVF2032L 110611 2 240 3 3450 H 9.0 36.0 12/4 SOW SGVF2042L 110612 2 480 3 3450 H 4.0 18.0 12/4 SOW SGVF2052L 110613 2 600 3 3450 H 3.2 14.4 12/4 SOW HIGH-HEAD SGVH2002L* 110620 2 200 1 3450 F 17.0 53.0 12/4 SOW	0.67 (17)
SGVF2032L 110611 2 240 3 3450 H 9.0 36.0 12/4 SOW SGVF2042L 110612 2 480 3 3450 H 4.0 18.0 12/4 SOW SGVF2052L 110613 2 600 3 3450 H 3.2 14.4 12/4 SOW HIGH-HEAD SGVH2002L* 110620 2 200 1 3450 F 17.0 53.0 12/4 SOW	0.67 (17)
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	0.07.((7)
	0.67 (17)
SGVH2022L 110615 2 240 1 3450 H 15.0 53.8 12/4 SOW	0.67 (17)
SGVH2062L 110616 2 200 3 3450 J 11.0 42.0 12/4 SOW	0.67 (17)
SGVH2032L 110617 2 240 3 3450 H 9.0 36.0 12/4 SOW	0.67 (17)
SGVH2042L 110618 2 480 3 3450 H 4.0 18.0 12/4 SOW	0.67 (17)
SGVH2052L 110619 2 600 3 3450 H 3.2 14.4 12/4 SOW	0.67 (17)

Standard Units:

Temperature Sensor cable is 14/3 SOW, 0.530 OD. (13.5mm) (Not used on SGVF2022L or SGVH2022L).

Optional - Moisture/Temperature sensor cable for all models is 18/5 SOW, 0.470 OD. (12mm), replaces Temp sensor cable.

* This pump is NOT UL or CSA listed.

- IMPORTANT ! 1.) PUMP MAY BE OPERATED "DRY" FOR EXTENDED PERIODS WITHOUT DAMAGE TO MOTOR AND/OR SEALS.
- 2.)

THIS PUMP IS APPROPRIATE FOR THOSE APPLICATIONS SPECIFIED AS CLASS I DIVISION II HAZARDOUS LOCATIONS. THIS PUMP IS NOT APPROPRIATE FOR THOSE APPLICATIONS SPECIFIED AS CLASS I DIVISION II HAZARDOUS LOCATIONS. INSTALLATIONS SUCH AS DECORATIVE FOUNTAINS OR WATER FEATURES PROVIDED FOR VISUAL ENJOYMENT MUST BE INSTALLED IN ACCORDANCE WITH THE NATIONAL ELECTRIC CODE ANSI/NFPA 70 AND/OR THE AUTHORITY HAVING JURISDICTION. THIS PUMP IS NOT INTENDED FOR USE IN SWIMMING POOLS, RECREATIONAL WATER PARKS, OR INSTALLATIONS IN WHICH HUMAN CONTACT WITH PUMPED 3.)́ 4.) MEDIA IS A COMMON OCCURRENCE.

CRANE

PUMPS & SYSTEMS

A Crane Co. Company

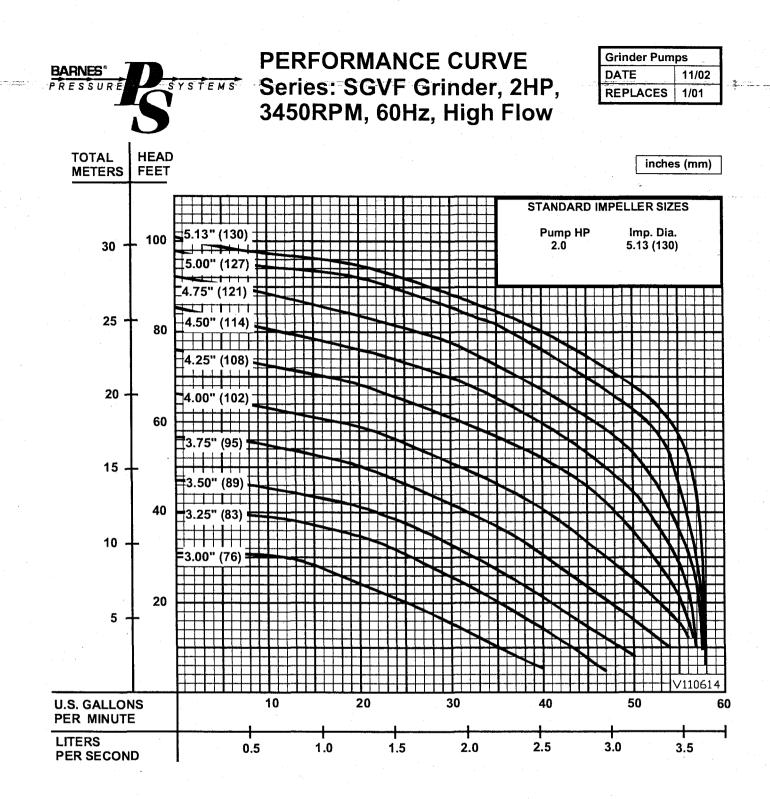
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420 Third Street Piqua, Ohio 45356-0603 Ph: (937) 778-8947 Fax: (937)773-2238 www.cranepumps.com



PS-002



Testing is performed with water, specific gravity of 1.0 @ 68° F (20°C), other fluids may vary performance.

and the second second



PUMPS & SYSTEMS

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PS-003

and the second states

Twening Road Pressurized Sewer System

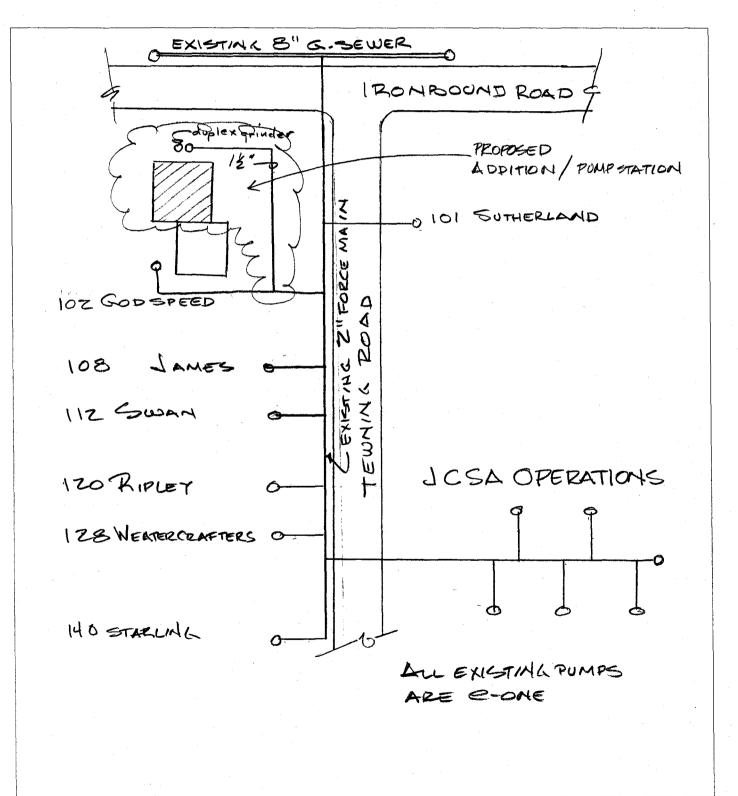
In response to comments from the James City Service Authority relative to the sewage pump for the Godspeed Animal Care Facility, VHB has completed a study to determine the state of the pressurized sewer system serving the property and its ability to accept additional sewage from the proposed improvements. The following are the findings:

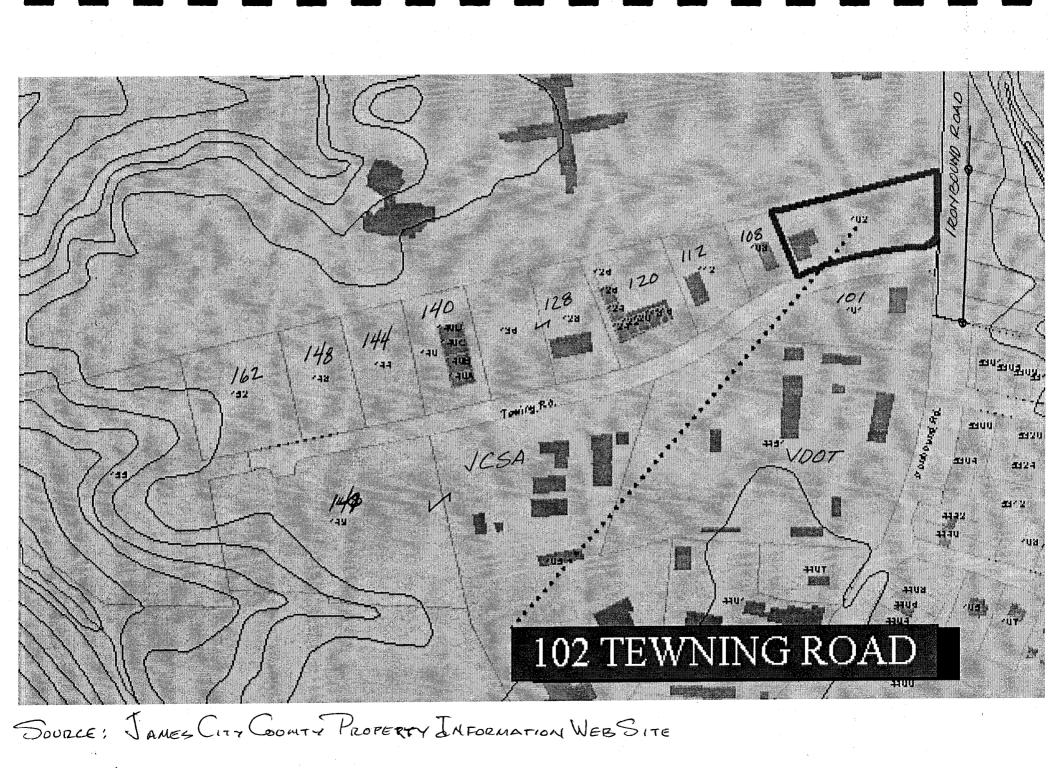
- 1. The existing sewer does not tie into the Hampton Roads Sanitary District force main in Ironbound Road. Rather it ties into the gravity sewer on the north side of Ironbound Road.
- 2. By contacting all of the property owners directly, it has been determined that all use the E-one semi-positive displacement type pump. There are presently 13 pumps connected. Six pumps are on the JCSA operations site and the is one pump one each of the seven developed lots which includes the existing Godspeed Animal Care facility. There are four undeveloped lots on Tewning Road.
- 3. We have obtained actual water usage data for the properties and determined that the water consumption for the existing Godspeed facility is 0.25 gallons per day per square foot of building area.
- 4. The capacity of the existing force main limited by a maximum permissible velocity of 5 feet per second is 78.3 g.p.m.
- 5. The probable maximum flow condition for a system of 10 to 18 pumps is four (4) pumps operating simuletaneously.

The conclusion is that the pressure sewer system can accept as much as 45 g.p.m. from a single pump station with three other pumps operating without exceeding the permissible velocity standard.



GODSPEED ANIMA		4. 4.
Project: CAIZE	Project #	31248.01
Location:	Sheet	of
Calculated by:	Date:	
Checked by:	Date:	,
Title		e.





Telephone contacts August 3 thru 11, 2004

1.101 Tewning E-one 2010-74

Sutherland Optometry 1-757-229-6302 Dr. Sutherland Replaced by Just Plumbing, Newport News 1-757-877-8540, within last year.

2. 102 Tewning Godspeed Animal Care E-One Replaced by Just Plumbing 2001

3. 108 Tewning James Pest Control 1-757-229-3370 Environment ONE Observed by R S Phillips 8/11/04

4. 112 Tewning E-One Receiver observed by R S Phillips 8/11/04 Swan Cleaners Etta & Richard Eggelston 1-757-566-3266, cell 1-757-870-8221

- 5. 120 Tewning E-one, Ripley Construction 1-757-253-0233 Robert Ripley new pump 2004
- 6. 128 Tewning E-one Tewning Commercial Park, Weathercrafters Heating and Air Conditioning Jim Smith 1-757-244-4357

7. 140 Tewning E-one Starling Guttering, Glen Starling 1-757-465-7662 1-800-390-3839 Recently replaced: Steve Ziegler Plumber 1-757-877-2054

From: Tim Fortune [tfortune@james-city.va.us] Sent: Monday, July 26, 2004 2:34 PM To: Phillips, Richard Subject: FW: Godspeed Animal Clinic Dick, As promised, our billing department provided the following peak water usage data over the last quarter: 1) Dr Sutherland (101) - 12,150 Gallons 2) Godspeed Animal Clinic (102 Tewning Road) - 70,800 Gallons 3) James Peat Control (108 Tewning Road) - 70,800 Gallons 3) James Peat Control (108 Tewning Road) - 21,950 Gallons 6) Tewning Commercial Park (120 Tewning Road) - 21,950 Gallons 5) Tewning Commercial Park (120 Tewning Road) - 21,950 Gallons 7) Tewning Industrial Park (120 Tewning Road) - 49,900 Gallons 5) Tewning Commercial Park (120 Tewning Road) - 49,900 Gallons 8) JCSA Operations/JCC Maint Facility: a) 103 Maint Facility: a) 103 Maint Facility: a) 103 Maint Facility: a) 103 Maint Facility: a) 000 Gallons c) 107 Ops Bidg - 31,650 Gallons d) 107 Shop - 11,750 Gallons g) 111 Old Maint - 8,4000 Gallons h) 113 Grounds & Maint - 9,500 Gallons h) 113 Grounds & Maint - 9,500 Gallons l) 115 Mosquito Control - 8,300 Gallons h) 113 Grounds & Maint - 9,500 Gallons l) 115 Mosquee- foo Gallons l) 11	Filinp	s, Richard			
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Thanks, Tim Original Message From: Tim Fortune Sent: Friday, July 23, 2004 11:10 AM To: 'rphillips@vhb.com' Cc: Danny Poe Subject: Godspeed Animal Clinic Dick,	1)1	15 Mosquito Control - 8,300 Gallons			
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Tim Original Message From: Tim Fortune Sent: Friday, July 23, 2004 11:10 AM To: 'rphillips@vhb.com' Cc: Danny Poe Subject: Godspeed Animal Clinic Dick,	-	have questions.			
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Cc: Danny Poe Subject: Godspeed Animal Clinic Dick,					
Dick,	Cc: Dann	y Poe			and the second
	Subject:	Godspeed Animal Clinic			
	- Dr. Suth	erlands Optometry (101 Tewning Road) 565-2699			

- Godspeed Animal Clinic (102 Tewning Road)
- James Pest Control (108 Tewning Road) 229-3370
- Swan Cleaners (112 Tewning Road) 220-3874
- Tewning Commercial Park (120 Tewning Road) 565-2436
- Tewning Commercial Park (128 Tewning Road) 566-0237
- Tewning Industrial Park (140 Tewning Road) 253-0233
- JCSA Operations/JCC Maint Facility (107 Tewning Road) 259-4096

7/26/2004

de.

You may want to verify the phone numbers above as our records date back to 1985 on some of these properties.

Concerning JCSA Operations/Maintenance yard, there are 6 grinder pumps serving the various functions there (all are E-one grinders w/1 HP motors). Billing is compiling water usage data for the various parcels noted above. I will forward this data to you once completed. Nice meeting you today and should you have questions, please do not hesitate to call.

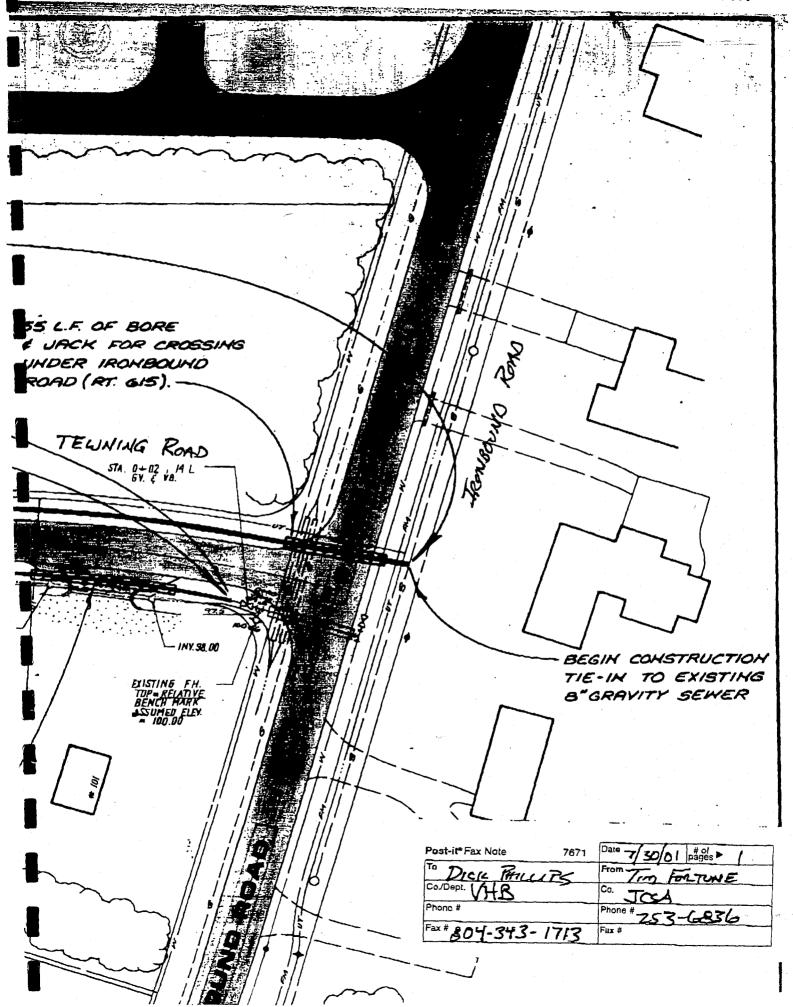
Thanks,

Timothy O. Fortune, P.E.

James City Service Authority Phone (757) 253-6836 Fax (757) 253-6850 JUL. -30' 04 (FRI) 09:36 JCC/JCSA

TEL:757-253-6850

P. 001



_Computations

Project: COUSPEED A.C. 31248.01 Project # Location: TEWNING ROAD of Sheet Calculated by: RCP Date: Checked by: Date: Title

mkgr.forms.humanres.computations.pm65

ESTIMATED SEWAGE FLOW: TESA TABLE 2.1 UNITFLOW 0.18 GPD BILLING RECORDS 15T GTR 2004 TO800 GALLONS BASED ON 78 BUSINESS DAYS PER OTR. \$ EXISTA BUILDING 3612 G.S.F. UNIT = 0.25 CPO PROBATED FLOW FOR NEW FALILITY: AVERAGE DAILY FLOW (ADF) ADF EXISTING PUMP: 4422 GSFX, 25 GPD = 1106 GPD ADF NEW DUMP: 11270 GSF ×.25 GPD = 2818 GPD 3924 500 SEWAGE PUMA DESIGN FLOW; DURATION OF FLOW 12 HR/DAY EXISTING PUMP: 1106 = 92 GPH = 15 GPM NEW PUMP: 2818 = 235 GPH = 3.91 GPM DESIGN FLOW : 2.5×3.9 = 9.75 GPM

Earthworks Consulting Engineers, Inc.

Mr. Scott Van Voorhees Guernsey Tingle Architects 3200 Ironbound Road Williamsburg, Virginia 23188

Earthworks Project No. 1316

May 28, 2004

Reference: Godspeed Animal Clinic Infiltration Investigation

EARTHWORKS

Dear Mr. Van Voorhees:

Pursuant to your request, an engineer from Earthworks visited the above referenced site to perform a subsurface investigation to determine the suitability of the soils for support of a proposed stormwater infiltration facility. This investigation was completed by performing two (2) handauger borings at locations within the proposed infiltration facility, as determined by the project Civil Engineer. The borings were extended to depths of 82 inches below existing surface elevations. In addition, two 15-foot deep soil test borings performed adjacent to the infiltration facility as part of our subsurface investigation for the proposed building addition were used in this investigation. A boring location diagram and logs of the two handauger borings and two soil test borings are attached to this report.

In general, the soil test and handauger borings encountered Silty Sand with Clay, Clayey Sand, and Sandy Clay to depths of about 5 feet. These soils contained seasonal water indicators below a depth of about 40 inches and appeared to be moderately to poorly drained. Soils below about 5 or 6 feet consisted of moderately well drained Silty Sands. These soils too contained seasonal water indicators, but to a lesser degree. The groundwater table was encountered at a depth of about 10 feet.

Based on the results of our field classifications of the soils encountered, it is estimated that soils above a depth of about 5 feet possess an infiltration rate less than about 0.5 inches per hour. Water movement through these soils appears to be restricted, based on soil color, and water appears to be present in these soils during wet seasonal conditions. Soils below a depth of about 5 feet also appear to be seasonally wet. However, these soils are moderately well drained. We estimate that these soils possess an infiltration rate of 0.6 inches per hour or better.

It is expected that construction of pavements and other impervious surfaces will substantially reduce the presence of seasonal water in the soils surrounding the proposed infiltration facility. If an infiltration facility is considered feasible based on seasonal water conditions, we recommend the infiltration level be placed about 5 to 6 feet below existing grades and that side-wall infiltration rates be considered minimal.

Should the client or Civil Engineer require more extensive investigation, Earthworks can provide infield infiltration testing to confirm our estimated infiltration rates upon request. Godspeed Animal Clinic Infiltration Investigation Earthworks Project No. 1316 Page 2

We appreciate this opportunity to be of service to you. Should you have questions concerning this investigation or wish to discuss our findings in more detail, please contact our office.

ROBERT C. MOSS, III No. 019982

SIONA

Respectfully,

EARTHWORKS CONSULTING ENGINEERS, INC.

COMA

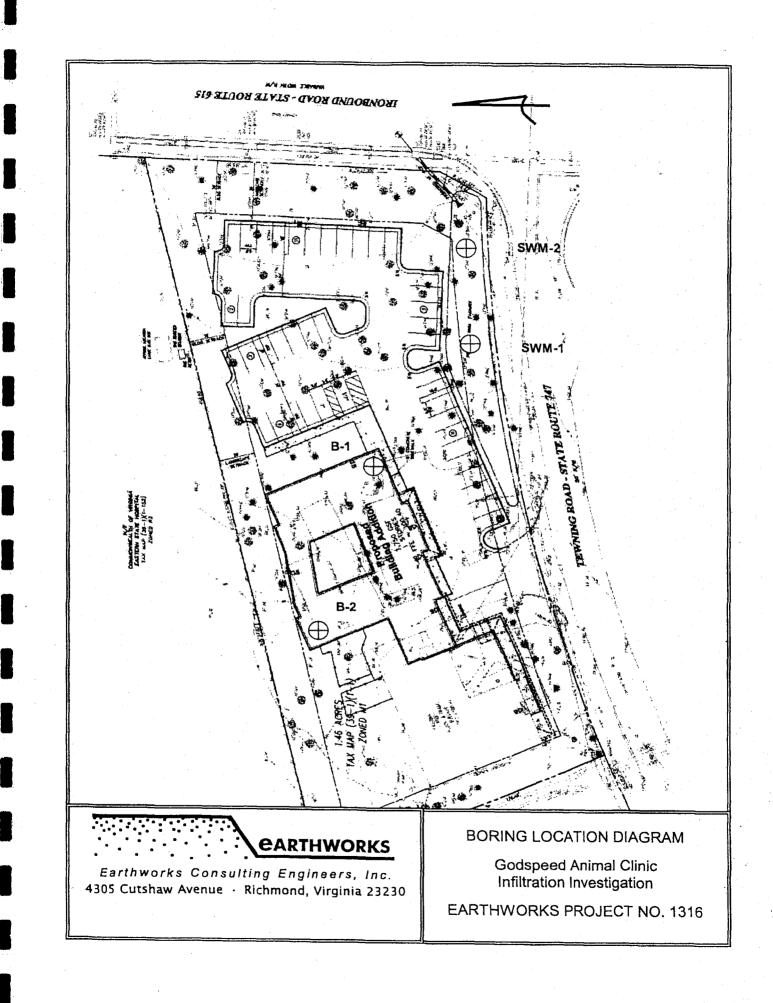
Moss. III. P.E.

President / Principal Engineer

Enclosures: Boring Location Diagram Soil Test and Handauger Boring Logs Summary of Laboratory Test Data

Copies: (1) Client (1) VHB – Mitchell Warren

geotech/letters/1316.doc



EARTHWORKS CONSULTING ENGINEERS, INC. HANDAUGER BORING LOGS

Godspeed Animal Clinic Infiltration Investigation

DEPTH	BORING NUMBER SWM-1
(IN)	DESCRIPTION OF SOILS
0-4	Topsoil
4-20	Light tan, Silty, fine SAND (SM) with roots
20-27	Brownish tan, Silty to Clayey, fine SAND (SM-SC)
27-40	Brownish orange, fine Sandy CLAY (CL)
40-52	Brownish orange with gray mottles, Clayey to Silty, fine SAND (SC-SM)
52-82	Light gray with orange brown, Silty, fine SAND (SM) trace Clay lenses Moisture Content – 17.2% Silt/Clay Content – 34.7%
	Seasonal Water Indicators below 40 inches. No free groundwater.
	END OF BORING AT 82 INCHES

DEPTH	BORING NUMBER SWM-2
(IN)	DESCRIPTION OF SOILS
0-3	Topsoil
3-21	Light tan, Silty, fine SAND (SM) with roots
21-46	Brownish tan, Silty to Clayey, fine SAND (SM-SC)
46-67	Brownish orange with gray mottles, Silty, fine SAND (SM) trace Clay
67-82	Light gray with orangish brown, Silty, fine SAND (SM)
	Seasonal Water Indicators below 46 inches. No free groundwater.
	END OF BORING AT 82 INCHES

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Godspeed Animal Clinic				1316 ARCHITECT-EN		.1	1	OF	1)	earthy	VORKS									
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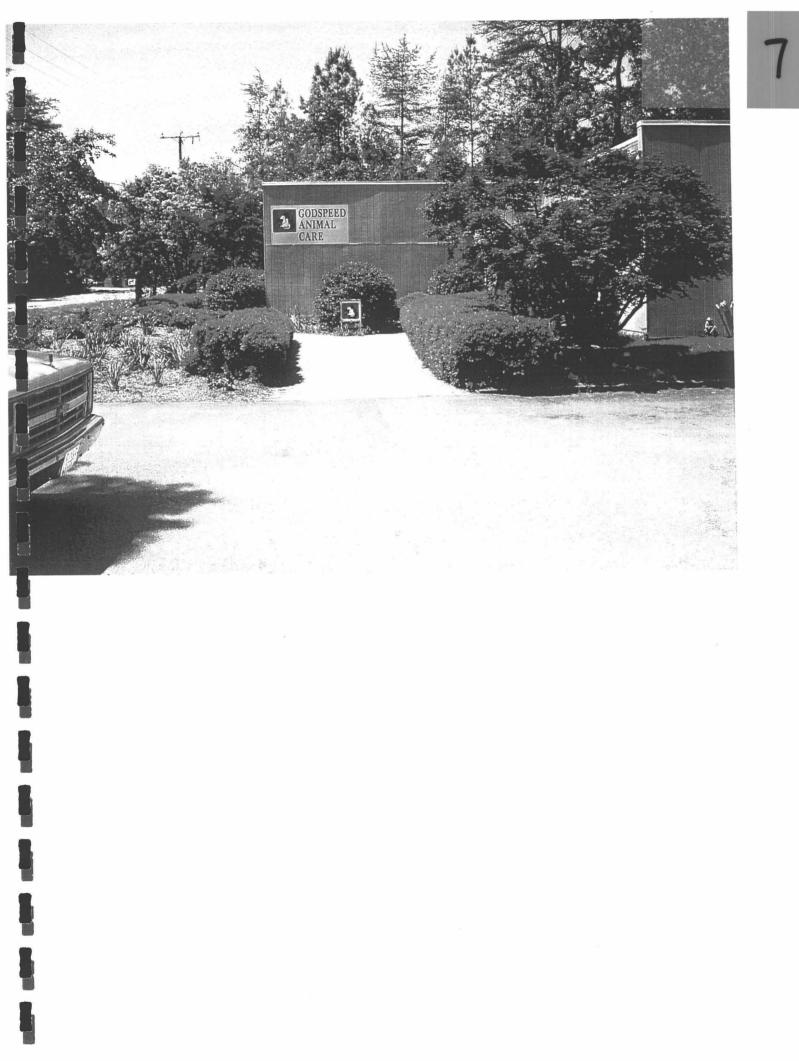
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·	4	SS	24	19	Light gray and tan, mois fine SAND (SM) trace C		ise, Silty,	-			21	⊢ ⊗	· · · ·	 	
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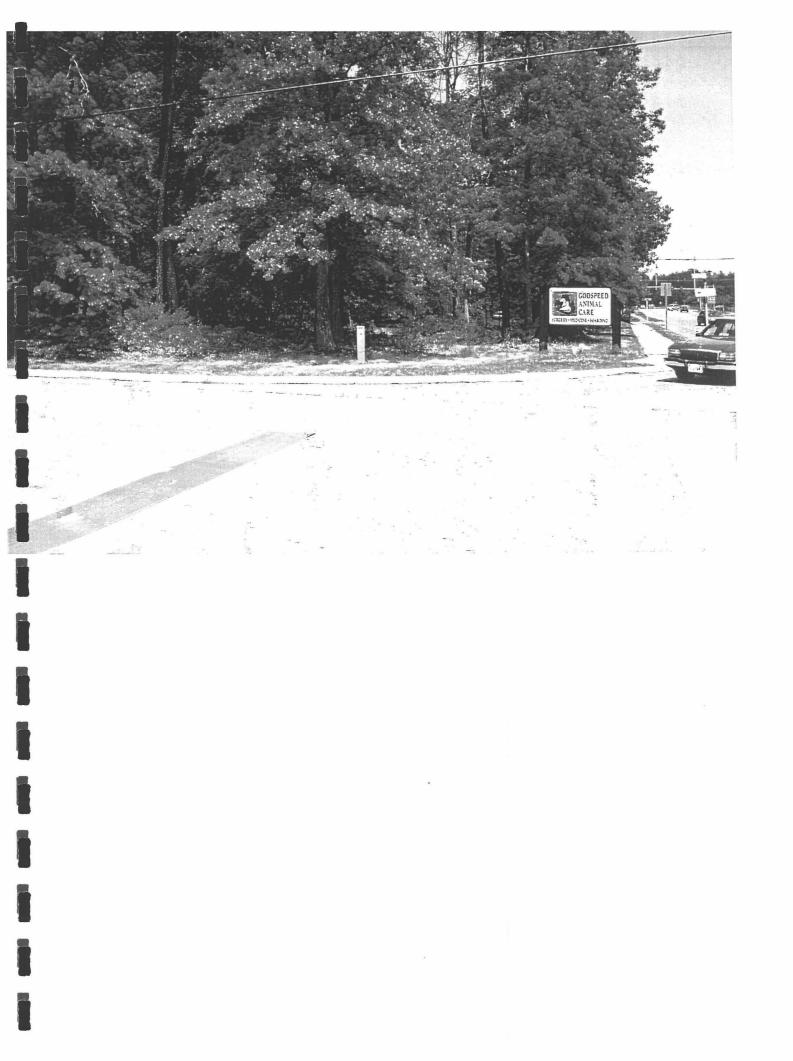
SUMMARY OF LABORATORY TEST DATA

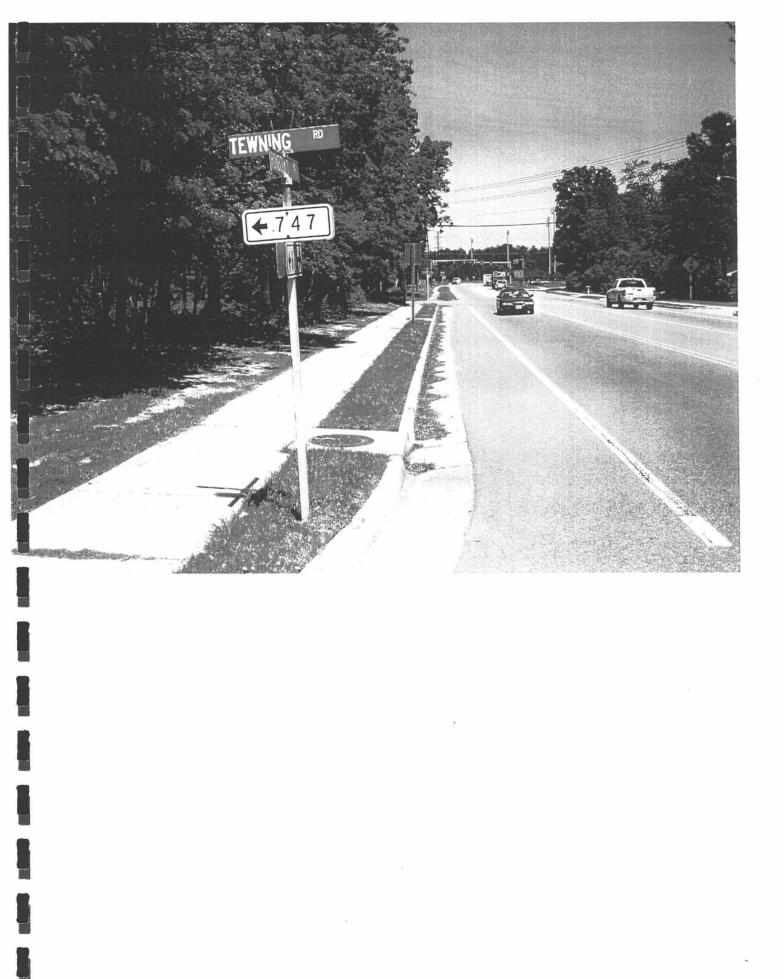
GODSPEED ANIMAL CLINIC INFILTRATION INVESTIGATION

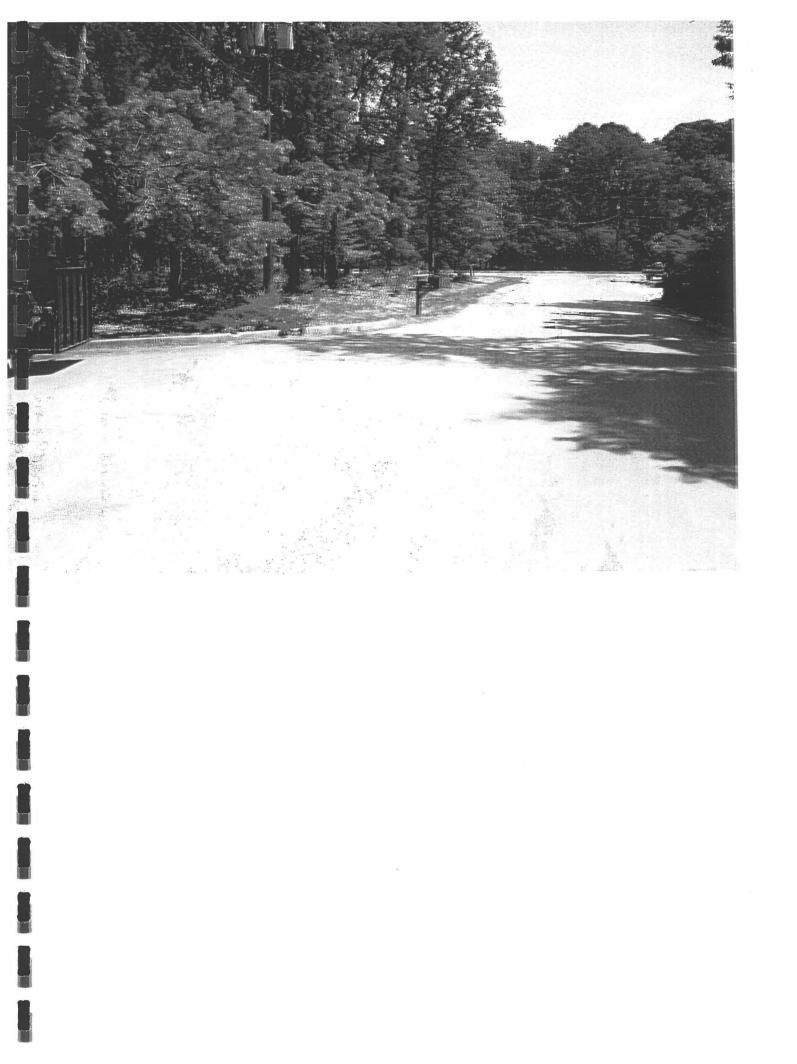
EARTHWORKS PROJECT NO. 1316

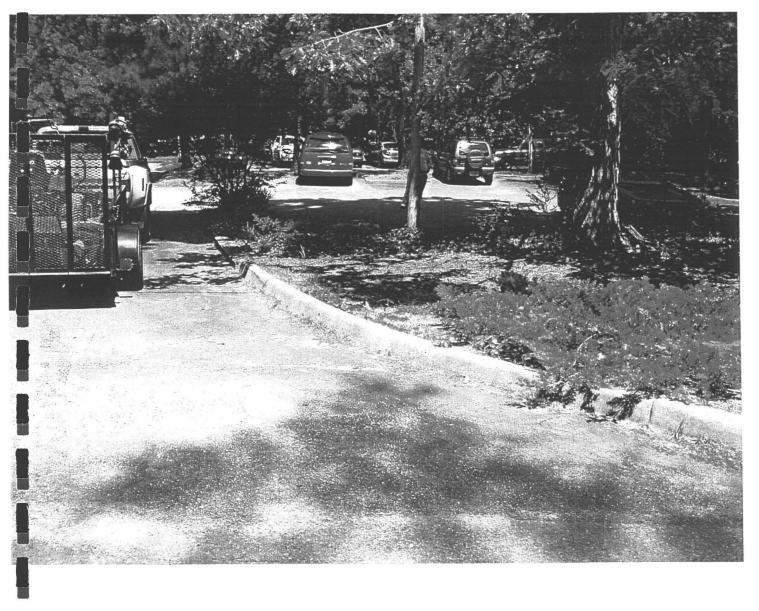
Boring No.	Sample No.	Sample Depth (in)	Natural Moisture Content (%)	Silt and/or Clay Fraction (%)	Unified Soil Classification
SWM-1	1	66-70	17.2	34.7	SM
B-1	S-1	0-24	11.8	49.5	SM-ML
B-1	S-2	24-48	17.7	51.8	CL-SC
B-2	S-3	48-72	15.5	43.2	SC



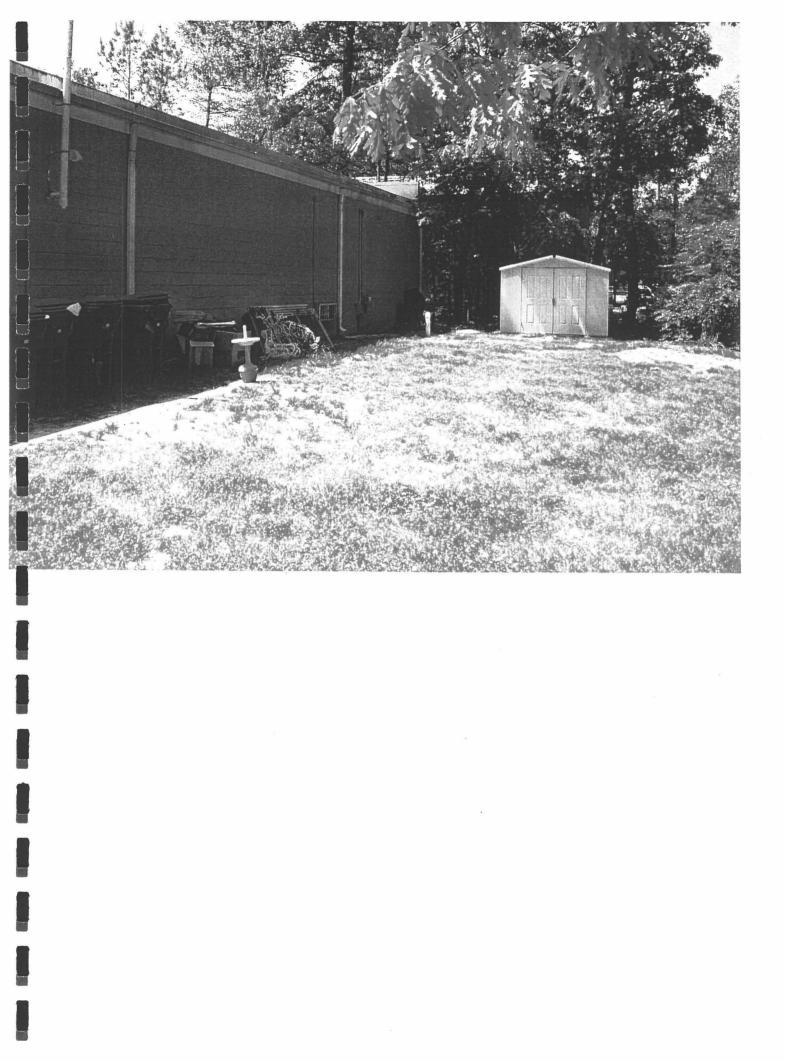


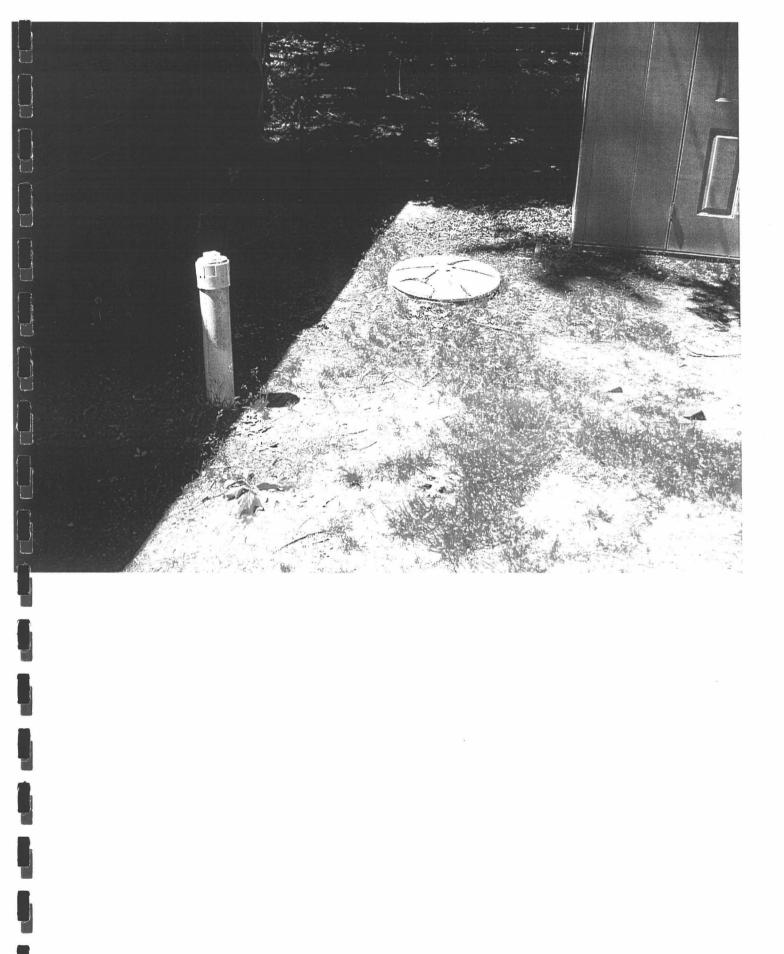


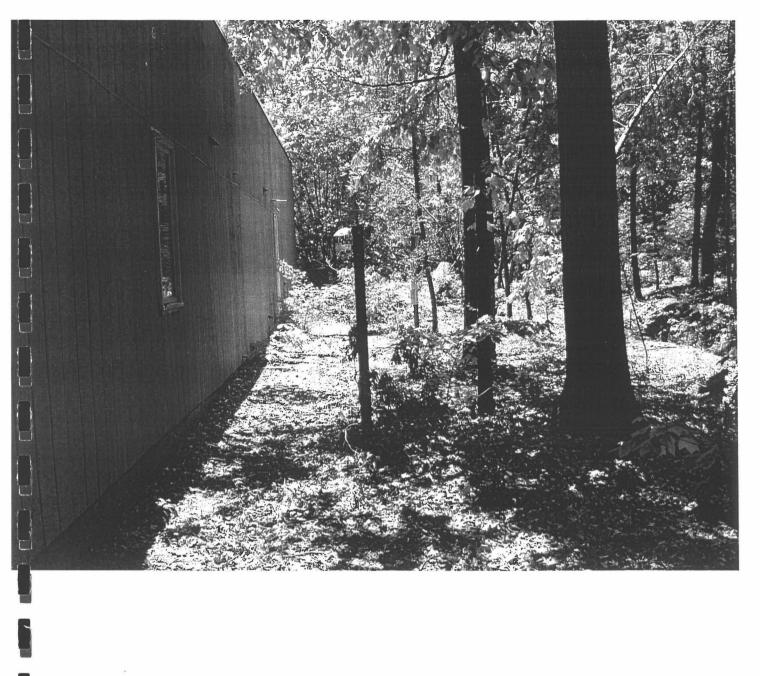




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Godspeed Animal Care 102 Tewning Road

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James City County, Virginia

Prepared for

Dr. Pamela Dumont Williamsburg, Virginia

Prepared by

/Vanasse Hangen Brustlin, Inc. Richmond, Virginia

2mp 50B 2p-70-04

Aug. 17, 2004

Godspeed Animal Care Building Expansion

Engineering Report

Table of Contents

- 1. Stormwater Management Design Narrative
- 2. Stormwater Management Calculations
- 3. Water Meter Sizing Calculations
- 4. Storm Water Calculations
- 5. BMP Geotechnical Report
- 6. Existing Site Photos

Vanasse Hangen Brustlin, Inc.

GODSPEED ANIMAL CARE BUILDING EXPANSION PROJECT

Stormwater Management Design Narrative

Project Description

DIST ALEA DIST D. TAC

The existing animal care facility is located at the corner of Tewning Road and Ironbound Road in James City County, Virginia. The project encompasses 1.46 acres of land and proposes an expansion of an existing building and associated parking. The project will generally include the addition of a two story building with a total gross square footage of 12,080, parking lots in the front and side of the site, and a comprehensive stormwater management system. The project site is identified as Tax Map Parcel #36-1 and is zoned M-1.

The proposed stormwater management plan for this project will include the use of a D-2 Surface Sand Filter System with 6" perforated underdrain piping to capture the filtered stormwater. The stormwater management system will attenuate the increased runoff anticipated from site development associated with the increased impervious cover.

The stormwater management system is designed to control up to the 100-year, twenty-four hour storm events, for post developed conditions. The volume created by the 10 year storm will have a 48 hour drawdown time before being released into the existing VDOT system along Ironbound Road. The proposed system is also designed to safely contain the 100-year storm event without the use of emergency spillways.

Description of Site

Under predevelopment conditions, the area to be developed is comprised of moderately wooded Hardwoods and Pines throughout. The general landform consists of elevations ranging from 100 to 97 and slopes gently away from the center outward to the east and west. Surface hydrology is directed by overland flow to two (2) ravines located along the rear of the property and also through an existing channel and culvert along Tewning Road. The site is located within the RPA but does not contain any wetlands or hydric soils.

General Description of Stormwater Management

The proposed onsite Sand Filter System will be the primary water quantity and quality control for this project. Surface waters drain to the proposed BMP by way of the pavement surface through curb cuts in the proposed curb and gutter. The water quality requirement is met by the use of the proposed sand filter and stilling basins located at each outfall curb cut from the proposed parking area. The depth of the Surface Sand Filter BMP ranges from 3' to 4' below the proposed pavement elevations. The outlet control structure will consist of a VDOT DI-5 structure, modified with a 12" outfall pipe to accommodate the 48 hour detention storage drawdown.

Temporary Sediment Traps and silt fence will serve as temporary erosion and sediment control devices during initial land clearing, grading, and earthmoving operations. The addition of the sand filter system and a spreader box in the rear of the site will serve in controlling the quality of run-off from the site once the improvements are completed. Appropriate details to construct the facilities for temporary and permanent erosion and sediment control are shown on the site plan.

Hydrology and Hydraulics

Topographic data used for site hydrology and storm/pond hydraulics was obtained from field survey by Michaels Surveying and Mapping dated 12/17/01. The survey verified the site boundary and provided topography related to utilities, drainage structures, and other physical improvements.

Hydrology and hydraulic modeling was performed utilizing the Hydrocad stormwater modeling system as developed by Haestad Methods, Waterbury, Connecticut.

The SCS TR-20 Method is the basis for overall watershed modeling for this project. Precipitation data for the County was obtained by source data provided by the U. S. Weather Bureau as found in Technical Paper No. 76 Rainfall Frequency Atlas of the Untied States.

Storage-indication pond routing procedures were used to predict the drawdown storage response (outflow hydrograph and incremental stage) to the inflow hydrograph. This sequential routing method uses the elevation-storage and elevation-discharge relationships for repeatedly solving the continuity equation, each solution being a step in delineating the outflow hydrograph.

Pre-development Hydrology

Pre-development conditions were evaluated to determine the existing peak discharges at the eastern discharge point from the proposed sand filter system. Based on current conditions, peak discharges for the 1-year, 24-hour storm was determined to be 0.78 cfs. This discharge was computed based on a drainage area of 0.73 acres and an SCS Curve Number of 77. The Time of concentration (Tc) value (0.25 hours) was based on the "Overland Flow" Method, whereby the flow path was divided into segments according to the type of flows such as overland, shallow concentrated, and channel flow.

Post-development Hydrology

Post-development drainage patterns differ slightly from pre-development, in that all of the proposed improvements will be directed to the proposed BMP.

Post-development conditions are based on ultimate development of the site with current conditions of paved and non-paved areas, to determine overall peak discharges to the existing receiving channels as was performed for predevelopment conditions. Based on this criteria, peak discharges for the 1-year, 24 hour storm, was determined to be 0.0424 cfs for the BMP outfall point. These discharges were based on a total drainage area of 0.73 acres. As with pre-development methodology, runoff SCS values were based on land use and hydrologic soil group, and time of concentration values were based on the SCS velocity method.

Comparison of the predevelopment discharges with the post-development discharges results in an overall decrease in peak discharges to the existing storm system due to attenuation by the onsite sand filter facility. NOT OVE CRITERIA

Hydraulics - Proposed Surface Sand Filter System

The proposed stormwater management system consists of one (1) Surface Sand Filter system to control the increased runoff from the site development.

Post-development inflow hydrographs were developed and routed through the storage volume and outlet structure for the system using evel pool routing methods to determine post-development peak discharges. Simultaneously routing procedures allows the system to respond to dynamic changes such as variable tailwater created by downstream system components. The following is a performance summary for the system tabulating peak outflow and water surface elevation for the 1-year, 10year, and 100-year storm events.

D-	2 Sand Filter System	m	OVITENON.	14 IT FOR
	Storm Event	Outflow (efs)	Elecation (ft.)	Release Time
	1-Year	0.06	96.60	30 hrs. +
	10-year	6.24	96.89	30 hrs. +
	100-year	8.89	96.97	30 hrs. +

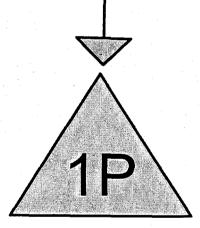
UNLESS THING TO most maintain

Prp -)

. jimiev Rey James City County BMP Guidelines I'mepth 2 AL. Table 2 0.13 AC. Worksheet for BMP Point System STRUCTURAL BMP POINT ALLOCATION Α. Fraction of 10070 Site Served Weighted BMP **BMP** Points **BMP** Points by BMP 6.87 8 D-Z SUFFACE SAND FUTER x 0.85 100 LEVIL SPREADER × 0.21 = x 0.85 Ξ х 8 TOTAL WEIGHTED STRUCTURAL BMP POINTS: 7.36 Β. NATURA OPEN SPACE CREDIT vatural Points for Fra en Space Credit Natural Open Space (0.15 per 1%) TOTAL NATURAL OPEN SPACE CREDIT: TOTAL WEIGHTED POINTS C. en Space Points ADDED TO THE DESIGN THLEE รกแม BOUCE PEDUCE FLOWS TO THE PLOPOSED FACILITY AND DDITIONAL SEDWEN TON CONTROL 400 WAIVER + LETTER) 0.6577 2 0.50 0.73 1.46 9 0.37 1.11 18.92% 0.94-



Post Development



Surface Sand Filter







Drainage Diagram for D2 Sand Filter BMP Prepared by Vanasse Hangen Brustlin, Inc., Richmond, VA 6/2/2004 HydroCAD® 7.00 s/n 001234 © 1986-2003 Applied Microcomputer Systems Transportation Land Development Environmental Services



Vanasse Hangen Brustlin, Inc.

101 Walnut Street Post Office Box 9151 Watertown Massachusetts 02471-9151 617.924.1770 FAX 617.924.2286

Phone	
Notes	

Person Contacted:
Title:
Company:
Telephone No.:
FAX No.:

VHB Rep:	
VHB Project No.:	
Project Name:	
Type of Call:	
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BMP ODSPEED

W.S.E EVENT FIZEQ. RELEASE PPEAK TIME 96.60 . OGds LYR 30 hrs. ZYR ,49cfs 96.65 30 hrs. hrs 96.89 (04R 6.24 cts 30 hrs. 96.97 LOOYR 6

CHANNE	L PROTECTION VOLUME	CALCULATION	James City C	ounty Me	thod			
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· • · • · · · · ·	One Year Precipitation :	.≞ P= 2	8 Inches	i iyu i	TABLE F1	/ TR-55		
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RE-DEV	ELOPMENT CONDITIONS	<u>8 :</u>			I _a /P	C ₀	C₁	C ₂
	Drainage Area :	DA _{PRE} = 0.	73 Acres		0.10	2.55323	-0.61512	-0.16403
	SCS Curve Number :		77 Unitless		0.30	2.46532	-0.62257	-0.11657
	Time of Concentration :	그는 그는 이상 위험을 받는	25 Hours		0.35	2.41896	-0.61594	-0.08820
					0.40	2.36409	-0.59857	-0.05621
	• •				0.45	2.29238	-0.57005	-0.02281
					0.50	2.20282	-0.51599	-0.01259
	Initial abstraction ;	$1 = 0.2 \times (1)$	000/CN - 10) =	0.597	Inches			
		18-0.2×(1	_/P =		Inches			
	•		18/1	0.21				
	Accumulated direct runo	ff : Qu = (P-la)^2 / (P+4xi _a) =	0.93	Inches			
			, (· · · · · · · · · · · · · · · · ·	0.00				
-	Unit Peak Discharge :		q _u =	731	cfs/sq.mile	e/in.		
	$\log(q_u) = C_0 + q_u$	C ₁ log(T _c)+C ₂ [log(T _c)]^	2					
	C ₀ ,C ₁ ,C ₂ , Co	pefficients from TABLI	E F1 above					
	Pre-development peak of		· .					
			0A x Q _U / 640 =	0.78	c.f.s.			
UST DE	EVELOPMENT CONDITION		72	1				
	Drainage Area :	- 11 11	73 Acres	<i>.</i>				
	SCS Curve Number :		92 Unitless 🖌					
	Time of Concentration	Tc _{POST} = 0.0	25 Hours				x N	1 al
	Initial abstraction ;		l _a =	0.174	Inches		S How COMP WIT	1012
an a	million about action ,		I _a /P =	0.10			COM	"LUN
	Accumulated direct runc		Q _U =	1.97			1.1	10
	Unit Peak Discharge :		q _u =		cfs/sq.mil	e/in	WIL	17.
		diacharra rata i			c.f.s.	C/111.	<u>ja 1</u>	ALF.
	Post development peak	discharge rate .	q _i = q _p =	2.95	C.I.S.			
	Ration of outflow to inflo	$w: * q_a/q_i = 11.$	98 x q _u ^0.937 =	0.0144				
		ulation using equation				mstock,P.E.,	MDE	
						x		
	Outflow discharge :		q _o =	0.0424	c.f.s. 🗸		· · ·	
	Datia of stars and the	4	V/ A/ -	0.00				
	Ratio of storage volume		$V_s/V_r =$	0.66				
	∨ _s /∨ _r = 0.683-1.	43(q _o /q _i)+1.64(q _o /q _i)^2	:-0.04(q _o /q _i)^3 =					
	Required Storage Volur	ne:						
	. loquilou oloitugo volui		A/12 x 43560 =	3465	cubic fee	F 1 - 1		

D2 Sand Filter BMP

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8/11/2004

Hydrograph for Pond 1P: Surface Sand Filter

North Contraction

	Time (hours)	Inflow (cfs)		torage ic-feet)	Elevation (feet)	Primary (cfs)
	0.00	0.00	1-2-2-	0	94.25	0.00
	1.00	0.00		0		
	2.00	0.00			94.25	0.00
				0	94.25	0.00
	3.00	0.00		0	94.25	0.00
	4.00	0.00		0	94.25	0.00
	5.00	0.00		0	94.25	0.00
	6.00	0.00		2	94.26	0.00
	7.00	0.01		6	94.27	0.01
	8.00	0.01		10	94.28	0.01
	9.00	0.02		36	94.35	0.01
	10.00	0.04		103	94.55	0.01
	11.00	0.09		272	95.01	0.01
	12.00	1.00		2,276	96.31	1.47
	13.00	0.12	÷	2,042	96.22	0.13
	14.00	0.07		2,025	96.21	0.07
	15.00	0.06		2,019	96.21	0.06
	16.00	0.04		2,015	96.20	0.05
	17.00	0.04		2,013	96.20	
	18.00	0.03				0.04
	19.00	0.03		2,011	96.20	0.04
	20.00			2,007	96.20	0.03
		0.03		1,998	96.20	0.03
	21.00	0.02		1,980	96.19	0.03
	22.00	0.02		1,958	96.18	0.03
·	23.00	0.02		1,934	96.17	0.03
	24.00	$L \ge 4 0.02 $	036	1,907	96.16	0.03
	25.00	0.00	DET	1,804	96.12	(0.03
	26.00	0.00		1,701	96.08	0.03
	27.00	0.00		1,599	96.03	0.03 /
	28.00	0.00		1,499	95.99	0.03
:	29.00	0.00		1,405	95.94	0.02
	30.00	0.00		1,320	95.89	0.02
	31.00	0.00		1,242	95.84	0.02
	32.00	0.00		1,170	95.80	0.02
	33.00	0.00		1,104	95.75	0.02
	34.00	0.00		1,039	95.69	0.02
	35.00	0.00		976	95.63	0.02
	36.00	0.00		914	95.58	0.02
	37.00	0.00		855	95.53	0.02
	38.00	0.00		797	95.48	0.02
	39.00	0.00		741	95.43	0.02
	40.00	0.00		686	95.38	0.01
	41.00	0.00		633	95.33	0.01
	42.00	0.00		582	95.29	0.01
	43.00	0.00		532	95.24	0.01
	44.00	0.00		483	95.24 95.20	0.01
	45.00	0.00		436	95.20	0.01
	46.00	0.00		390	95.10	
	47.00	0.00		345		0.01
	48.00	0.00			95.08	0.01
	-0.00	0.00		302	95.04	0.01

D2 Sand Filter 81204 BMP

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Type II 24-hr 1 year JCC Rainfall=2.80"

Section States

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Subcatchment 3S: Post Development

Runoff = 2.86 cfs @ 11.92 hrs, Volume=

0.120 af, Depth= 1.97"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type II 24-hr 1 year JCC Rainfall=2.80"

Area (ac) CN	Description				
0.570 98	Paving and Roofs				
0.160 70	Lot area				
0.730 92	Weighted Average				
Tc Length ((min) (feet)	Slope Velocity Capacity (ft/ft) (ft/sec) (cfs)	Description			
1.5 100 0.0100 1.1 Sheet Flow, Pavement Smooth surfaces n= 0.011 P2= 3.50"					
	Pond 1P:	Surface Sand Filter			
	0.730 ac, Inflow Depth =				
	2.86 cfs @ 11.92 hrs, Vol 0.06 cfs @ 14.94 hrs, Vol				
	0.06 cfs @ 14.94 hrs, Vol				
-	0.00 cfs @ 0.00 hrs, Vol				
Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5 Peak Elev= 96.60' @ 14.94 hrs Surf.Area= 2,553 sf Storage= 3,569 cf Plug-Flow detention time= 910.8 min calculated for 0.097 af (81% of inflow) Center-of-Mass det. time= 832.3 min (1,627.7 - 795.4)					
# invert	Avail.Storage Storage D	escription			
1 94.25'		tage Data (Irregular) Listed below			
Elevation S	urf.Area Perim. Voids	Inc.Store Cum.Store Wet.Area			
(feet)	(sq-ft) (feet) (%)				
94.25	850 217.0 40.0	0 0 850			
94.90	863 220.0 40.0	223 223 1,026			
95.00	1,422 276.0 100.0				
96.00	2,087 319.0 100.0				
97.00	2,858 365.0 100.0	2,462 4,542 7,821			
# Routing	Invert Outlet Devices				
1 Primary		g Culvert RCP, sq.cut end projecting, Ke= 0.500			
Outlet Invert= 93.50' S= 0.0060 '/' n= 0.013 Cc= 0.900 2 Device 1 94.00' 0.000800 fpm Sand filter over Surface area above invert 2 Device 1 94.00' 0.000800 fpm Sand filter over Surface area above invert					
			3 Device 1 96.60' 3.00' x 3.00' Horiz. Orifice/Grate Limited to weir flow C= 0.600		
4 Secondary 97.00' 20.0' long x 15.0' breadth Broad-Crested Rectangular Weir					
	Head (feet) 0.20				
•		0.40 0.60 0.80 1.00 1.20 1.40 1.60 .68 2.70 2.70 2.64 2.63 2.64 2.64 2.63			

D2 Sand Filter 81204 BMP

Type II 24-hr 1 year JCC Rainfall=2.80"

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Primary OutFlow Max=0.05 cfs @ 14.94 hrs HW=96.60' (Free Discharge) 1=Culvert (Passes 0.05 cfs of 8.60 cfs potential flow) -2=Sand filter (Exfiltration Controls 0.03 cfs) -3=Orifice/Grate (Weir Controls 0.01 cfs @ 0.2 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=94.25' (Free Discharge)

D2 Sand Filter 81204 BMP

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Type II 24-hr 2 year JCC Rainfall=3.50"

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HydroCAD® 7.00 s/n 001234 © 1986-2003 Applied Microcomputer Systems		8/16/2004
Subcatchment 3S: Post Developme	nt	

Runoff 3.74 cfs @ 11.92 hrs, Volume= 0.160 af, Depth= 2.64"

Туре	ll 24-hr 2 yea	r JCC Rai	nfall=3.50"	Time Sp	oan= 0.00-48.00	hrs, dt= 0.01 hrs	A= 0.73AC CN= 92	
	ea (ac) CN 0.570 98		and Roofs	· · · · · · · · · · · · · · · · · · ·			NE	·
	0.160 70						CH.	
<u></u>	0.730 92		ed Average	••••				-
			.ou / monage			e e e e e e e e e e e e e e e e e e e		
<u>(mi</u>	Гс Length n) (feet)		/elocity Ca (ft/sec)	apacity (cfs)	Description		· · · · · · · · · · · · · · · · · · ·	
1	.5 100	0.0100	1.1		Sheet Flow, Pav			
					Smooth surfaces	s n= 0.011 P2=	3.50"	
			Pon	d 1P: S	urface Sand F	Filter		
Inflow	/ Area =	0.730 ac	, Inflow Dep	oth = 2.6	64" for 2 year	JCC event		
Inflow	/ = .		2) 11.92 hr					
Outflo			D 12.04 hr			6 af, Atten= 87%	, Lag= 7.6 min	
Prima			@ 12.04 hr					
Seco	ndary =	0.00 cfs (@ 0.00 hr	s, volun	ne= 0.00	u ar		
Peak Plug-	Elev= 96.65'	@ 12.04 h on time= 67 et. time= 60	nrs Surf.Ar '8.2 min cal	ea= 2,58 culated fo ,397.0 - 7		,681 cf		
1	94.25'	4,	542 cf Cu	stom Sta	ge Data (Irregul	ar) Listed below		
Elev	ation	Surf.Area	Perim.	Voids	Inc.Store	Cum.Store	Wet.Area	
	feet)	(sq-ft)	(feet)	(%)	(cubic-feet)	(cubic-feet)	(sq-ft)	
	4.25	850	217.0	40.0	0	0	850	
	94.90	863	220.0	40.0	223	223	1,026	
	95.00	1,422	276.0	100.0	113	336	3,237	
	96.00 97.00	2,087 2,858	319.0	100.0 100.0	1,744 2,462	2,080 4,542	5,294 7,821	
	77.00	2,000	505.0	100.0	2,402	-+, J+2	7,021	
#_	Routing	Invert	Outlet Dev	ces				<u></u>
1	Primary	93.74'				q.cut end projectin n= 0.013 Cc= 0.		
2	Device 1	94.00'				ace area above ir		
3	Device 1	96.60'				imited to weir flow		
4	Secondary	97.00'	Head (feet)	0.20 0.	.40 0.60 0.80 1	r ested Rectangu 1.00 1.20 1.40 1. 64 2.63 2.64 2.64	60	•
			、 · J	,				

Type II 24-hr 2 year JCC Rainfall=3.50"

D2 Sand Filter 81204 BMP

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Primary OutFlow Max=0.48 cfs @ 12.04 hrs HW=96.65' (Free Discharge) -2=Sand filter (Exfiltration Controls 0.03 cfs) -3=Orifice/Grate (Weir Controls 0.44 cfs @ 0.7 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=94.25' (Free Discharge) -4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

D2 Sand Filter 81204 BMP

Type II 24-hr 10 year JCC Rainfall=5.80"

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Subcatchment 3S: Post Development

Runoff	=	6.61	cfs @	11.92 hrs,	Volume=	0

0.296 af, Depth= 4.87"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type II 24-hr 10 year JCC Rainfall=5.80"

Area (ac) CN Description	
0.570 98 Paving and Roo	ofs
0.160 70 Lot area	· · · · · · · · · · · · · · · · · · ·
0.730 92 Weighted Aver	age
Tc Length Slope Velocity (min) (feet) (ft/ft) (ft/sec)	Capacity Description (cfs)
1.5 100 0.0100 1.1	Sheet Flow, Pavement Smooth surfaces n= 0.011 P2= 3.50"
P	ond 1P: Surface Sand Filter
Routing by Stor-Ind method, Time Sp Peak Elev= 96.89' @ 11.93 hrs Surf Plug-Flow detention time= 367.1 min Center-of-Mass det. time= 321.3 min	2 hrs, Volume= 0.296 af 3 hrs, Volume= 0.271 af, Atten= 6%, Lag= 0.9 min 3 hrs, Volume= 0.271 af 0 hrs, Volume= 0.200 af an= 0.00-48.00 hrs, dt= 0.01 hrs / 5 Area= 2,775 sf Storage= 4,277 cf calculated for 0.271 af (91% of inflow)
	Custom Stage Data (Irregular) Listed below
Elevation Surf.Area Perir (feet) (sq-ft) (feet)	
94.2585021794.9086322095.001,42227696.002,08731997.002,858365	0.040.02232231,0260.0100.01133363,2370.0100.01,7442,0805,294
# Routing Invert Outlet D	Devices
Outlet In 2 Device 1 94.00' 0.00080 3 Device 1 96.60' 3.00' x 4 Secondary 97.00' 20.0' lo Head (f	40.0' long Culvert RCP, sq.cut end projecting, Ke= 0.500 nvert= 93.50' S= 0.0060 '/' n= 0.013 Cc= 0.900 00 fpm Sand filter over Surface area above invert 3.00' Horiz. Orifice/Grate Limited to weir flow C= 0.600 ng x 15.0' breadth Broad-Crested Rectangular Weir eet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Type II 24-hr 10 year JCC Rainfall=5.80"

D2 Sand Filter 81204 BMP

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Primary OutFlow Max=6.22 cfs @ 11.93 hrs HW=96.89' (Free Discharge) **1=Culvert** (Passes 6.22 cfs of 9.24 cfs potential flow) -2=Sand filter (Exfiltration Controls 0.04 cfs) -3=Orifice/Grate (Weir Controls 6.18 cfs @ 1.8 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=94.25' (Free Discharge) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

D2 Sand Filter 81204 BMP Type II 24-hr 100vear JCC Rainfall=8.00" Prepared by Vanasse Hangen Brustlin, Inc., Richmond, VA -----Page 8 HydroCAD® 7.00 s/n 001234 © 1986-2003 Applied Microcomputer Systems 8/16/2004 Subcatchment 1S: Pre development Runoff 4.93 cfs @ 12.07 hrs, Volume= 0.321 af, Depth= 5.27" Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type II 24-hr 100year JCC Rainfall=8.00" Area (ac) CN Description 0.180 98 Roof & Paving 0.550 70 Wooded 0.730 Weighted Average 77 Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs) 15.0 Direct Entry, Subcatchment 3S: Post Development Runoff 9.32 cfs @ 11.92 hrs. Volume= 0.428 af, Depth= 7.04" Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type II 24-hr 100year JCC Rainfall=8.00" CN Area (ac) Description 0.570 98 Paving and Roofs 0.160 70 Lot area 0.730 92 Weighted Average Tc Lenath Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs) 1.5 100 0.0100 Sheet Flow, Pavement 1.1 Smooth surfaces n= 0.011 P2= 3.50" Pond 1P: Surface Sand Filter Inflow Area = 0.730 ac, Inflow Depth = 7.04" for 100year JCC event Inflow 9.32 cfs @ 11.92 hrs, Volume= = 0.428 af **Outflow** 8.89 cfs @ 11.93 hrs, Volume= 0.403 af, Atten= 5%, Lag= 0.8 min = 8.89 cfs @ 11.93 hrs, Volume= Primary = 0.403 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5 Peak Elev= 96.97' @ 11.93 hrs Surf.Area= 2,835 sf Storage= 4,470 cf Plug-Flow detention time= 263.4 min calculated for 0.403 af (94% of inflow)

Center-of-Mass det. time= 228.7 min (990.0 - 761.3)

	Invert	Avail.Storage	Storage Description	· · · · · · · · · · · · · · · · · · ·
1	94.25'	4,542 cf	Custom Stage Data (Irregular) Listed below	

D2 Sand Filter 81204 BMP

Type II 24-hr 100year JCC Rainfall=8.00"

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	Elevation Surf.Area		Perim.	Voids	Inc.Store	Cum.Store	Wet.Area	
_	(feet) (sq-ft)		(feet)	(feet) (%) (cubic-feet) (cubic-feet)		(cubic-feet)	(sq-ft)	
	S	4.25	850	217.0	40.0	0	0	850
	9	4.90	863	220.0	40.0	223	223	1,026
	9	95.00	1,422	276.0	100.0	113	336	3,237
	S	96.00	2,087	319.0	100.0	1,744	2,080	5,294
	g	97.00	2,858	365.0	100.0	2,462	4,542	7,821
				•				
_	#	Routing	Invert	Outlet Devi	ces			
	1	Primary	93.74'	15.0" x 40	.0' long	Culvert RCP, sq.o	cut end projecting,	Ke= 0.500
				Outlet Inve	rt= 93.50)' S= 0.0060 '/' n	= 0.013 Cc= 0.900)
	2	Device 1	94.00'	0.000800 f	pm Sand	d filter over Surfac	e area above inver	t
	3	Device 1	96.60'	3.00' x 3.0	0' Horiz.	Orifice/Grate Lim	nited to weir flow C	= 0.600
	4	Secondary	97.00'	20.0' long	x 15.0' b	oreadth Broad-Cre	ested Rectangular \	Weir
		-		Head (feet)) 0.20 0	.40 0.60 0.80 1.0	0 1.20 1.40 1.60	
				Coef. (Eng	lish) 2.6	8 2.70 2.70 2.64	2.63 2.64 2.64 2.	.63

Primary OutFlow Max=8.89 cfs @ 11.93 hrs HW=96.97' (Free Discharge) -1=Culvert (Passes 8.89 cfs of 9.41 cfs potential flow) 2=Sand filter (Exfiltration Controls 0.04 cfs) -3=Orifice/Grate (Weir Controls 8.85 cfs @ 2.0 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=94.25' (Free Discharge) -4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Godspeed Animal Care 102 Tewning Road James City	2	₩		
County, VA				8/11/2004
SIZING WATER SERVICE L	INES AND	METERS		
(PLUMBING FIXTU	RE VALUE)			
	Fixture	No. of	J	otal Fixture
	Value	Fixture	i	Value
Bathtub	8	x 4	=	32
Bedpan washers	10	x	=	0
Combination sink and tray	- 3	X	=	0
Dental unit	1	x 0	=	0
Dental lavatory	2	x 1	=	2
Drinking fountain (cooler)	1	x 0	=	0
Drinking fountain (public)	2	x 0.	=	0
Kitchen sink: 1/2" connection	3	x 1	=	3
3/4" connection	7	X	=	0
Lavatory: 3/8" connection	2	X	Ξ	0
1/2" connection	4	x 6	=	24
Laundry tray: 1/2" connection 3/4" connection	3	x 1	=	3
Shower head (shower only)	7	X x 7	-	0
Service sink: 1/2" connection	3	$\frac{x}{x}$ 2	=	6
3/4" connection	7	x 0	1 = L	0
Urinal: Pedestal flush valve	35	x	=	0
Wall or stall	12	Х	=	0
Trough (2' unit)	2	x	=	0
Wash sink (each set of faucets)	4	x 19	=	76
Water closet: Flush valve	35	X	=	0
Tank type		x 7		21
Dishwasher: 1/2" connection 3/4" connection	4	\mathbf{x} 1 \mathbf{x} 0		4
Washing machine: 1/2" connection	5	x 2	=	10
3/4" connection	12	x	=	0.
1" connection	25	X	=	0
Hose connections (wash down): 1/2"	6	x 5	· =	30
3/4"	10	x 0	=	0 .
Hose (50' length-wash down): 1/2"	6.	x	· = ·	0
5/8"	9	X	=	0
3/4"	12		= *	0 ····
			a section.	
GRAND TOTAL OF FIXTURE VALUES		11. S. A.		219

1 4 10

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October 12, 1998

SIZING WATER SERVICE LINES AND METERS

TABLE 4.3 Plumbing Fixture Value

	Fixture Value
Fixture Type	Based on 35 psi at Meter Outlet
Bathtub	8
Bedpan washers	
Combination sink and tray	3
Dental unit	
Dental lavatory	
Drinking fountain (cooler)	
Drinking fountain (public)	
Kitchen sink: 1/2-in. connection	
3/4-in. connection	
Lavatory: 3/8-in. connection	
1/2-in connection	
Laundry tray: 1/2-in. connection	
3/4-in. connection	
Shower head (shower only)	
Service sink: 1/2-in. connection	3
3/4-in. connection	
Urinal: Pedestal flush valve	
Wall or stall	
Trough (2-ft unit)	
Wash sink (each set of faucets)	
Water closet: Flush valve	
Tank type	
Dishwasher: 1/2-in. connection	
3/4-in. connection	
Vashing machine: 1/2-in. connection	
3/4-in connection	
1-in. connection	
lose connections (wash down): 1/2-in.	
3/4-in.	
Iose (50-ft length-wash down): 1/2-in.	
5/8 in.	
3/4 in	<u></u>

value of a number of units by simply multiplying the single value times the number of fixtures in the customer's use to get a total value. The list of plumbing items in Table 4.3 represents those most commonly used; however, the estimator will eventually encounter special equipment that will need to be evaluated. Since the fixture flow requirements in gallons per minute and the fixture values are the same in Table 4.3, the engineer can list the demand in gallons per minute for the special equipment, along with the other fixtures, to obtain one total.

Demand

After the fixture values have been determined, the results can be applied to a graph to obtain the customer demand in gallons per minute at 35 psi at the meter outlet. The maximum water flow of any one fixture is above the average of any one of a number of fixtures when operated in a customer's service. This is because the probability of all

SIZING WATER SERVICE LINES AND METERS

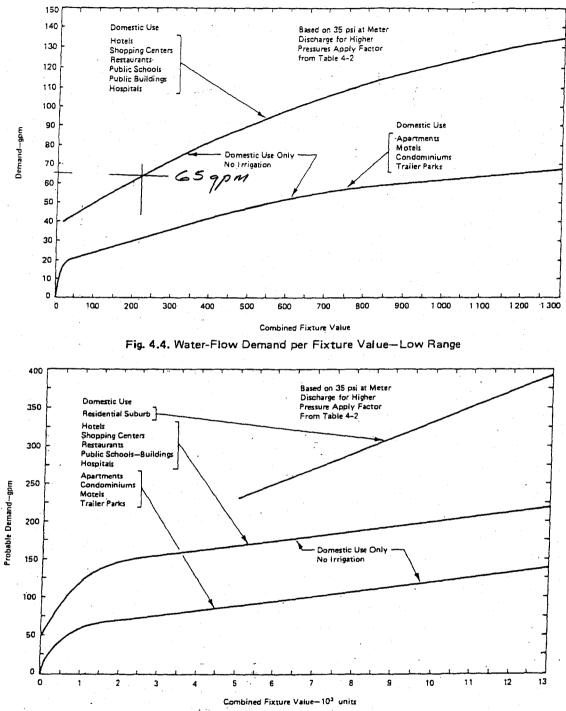


Fig. 4.5. Water-Flow Demand per Fixture Value-High Range

detailed lists of fixtures before estimates can be prepared. If the structure is in the planning stage, the mechanical engineer or architect is the best source of information, and, if construction is underway, the plumbing contractor or the building permits section of the city will have the information. Field trips by the estimator are often necessary to assist the customer as well as to properly assess the project when

TABLE 5.6

Displacement-Type Meters Meeting AWWA Standards Flow-Pressure Loss Averages of 1990-Model Meters

	Size		i Capacity ow Criteria	Recommen Criteria—	ded Design 80% Cap.	Continu Criteria-	Brands Included	
	in.	gpm	psi	gpm	psi	gpm	psi	in Averages
	1/2	15	7.9	12	5.0	7.5	2.0	1
	5/8	20	9.7	16	6.2	10	2.4	5
	3/4	30	10.4	24	6.7	15	2.6	5
	1	50	9.8	40	6.3	25	2.5	5
	>1 1/2	100	10.6	80	6.8	50	2.7	4
	2	160	11.3	130	7.1	80	2.8	4

TABLE 5.7

Compound-Type Meters Meeting AWWA Standards Flow-Pressure Loss Averages of 1990-Model Meters

Size	1	n Capacity low Criteria	1	nded Design 80% Cap.	Continu Criteria	Brands Included		
in.	gpm	psi	gpm	psi	gpm	psi	in Averages	
2	160	8.0	130	5.1	80	2.0	5	
3	320	7.2	255	4.6	160	1.8	5	
4	500	6.2	400	4.1	250	1.6	5	
6	1000	8.4	800	5.4	500	2.1	5	
8	1600	14.5	1300	9.3	800	3.8	. 1	

TABLE 5.8

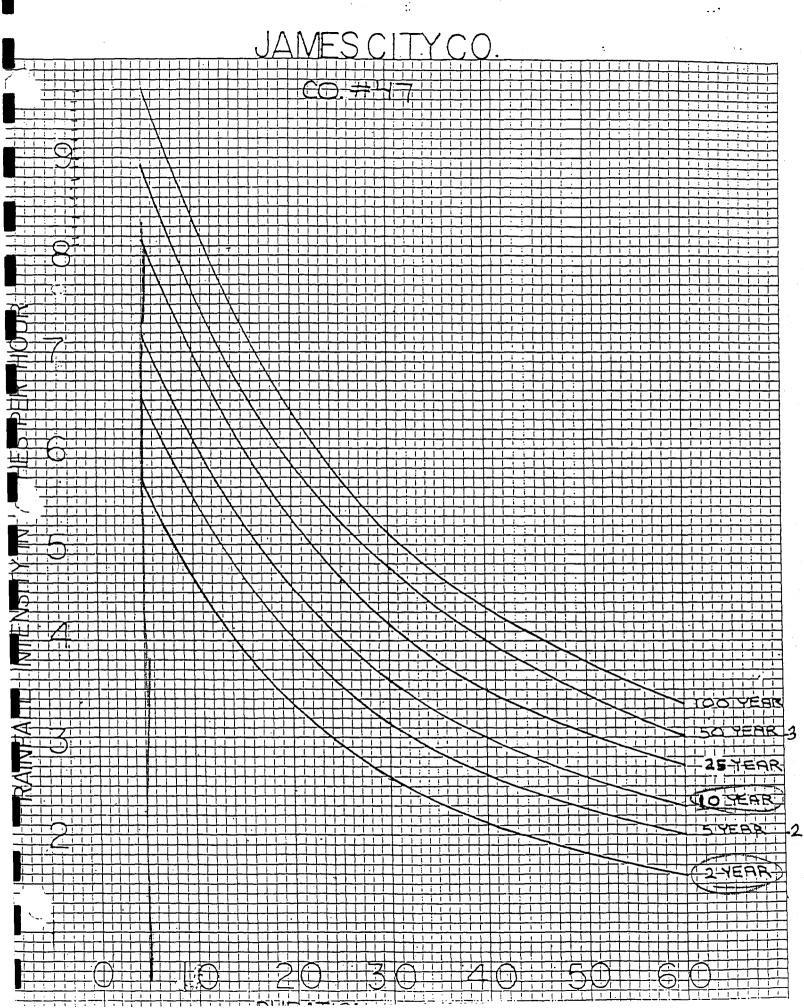
Class II Turbine-Type Meters Meeting AWWA Standards Flow-Pressure Loss Averages of 1990-Model Meters

Size in.	Maximum AWWA Flo	Capacity w Criteria		nded Design 80% Cap.	Continue Criteria—	Brands Included	
	gpm	psi	gpm	psi	gpm	psi	in Averages
2	160	4.0	130	2.5	100	1.0	5
3	350	4.0	280	2.6	240	.9	-5
4	630	2.0	500	1.4	420	.7	5
6	1 400	2.0	1 100	1.2	920	.5	5
8	2 400	2.7	1 900	1.7	1 600	.7	5
10	3 800	2.6	3 000	1.4	2 500	.5	5
12	5 000	1.7	4 000	1.1	3 300	.4	1

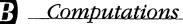
5.9 as the equivalent length of straight pipe that will give the friction loss that will occur as the water passes through the fitting. The values will be approximate in some cases because the pipe's inside diameter is based on the size of the fittings, and in some cases the inside diameter will be slightly larger or smaller; however, the effects of the error will be negligible and the values are considered sufficiently accurate for the purpose of this manual.

Pressure-reducing valves are used in mountainous and hilly areas to protect the

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- a) -



Project: GO Location: J	OSPEED CC	Project # Sheet
	WEM/KL	Date:
Checked by:		Date:
Title		. .

EKISTING VOOT SYSTEM

- AS SHOWN IN THE "STORM DRAINAGE COMPUTATIONS", THE CAPACITY OF THE EXISTING 30"RCP (STR. 4-78) IS 37.37 CES AND THE EXISTING QIO = 17.47 CFS THE IMPROVE MENTS TO GOOSPEED (QIO OUTFLOW) = 6.24 CFS IS ACCEPTABLE AND THE EXISTING SYSTEM CAN HANDLE THESE FLOWS.

don vi From b.24 cFS Qui 6.24 cFS

31248.01

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VHB Vanasse Hangen Brustlin, Inc.

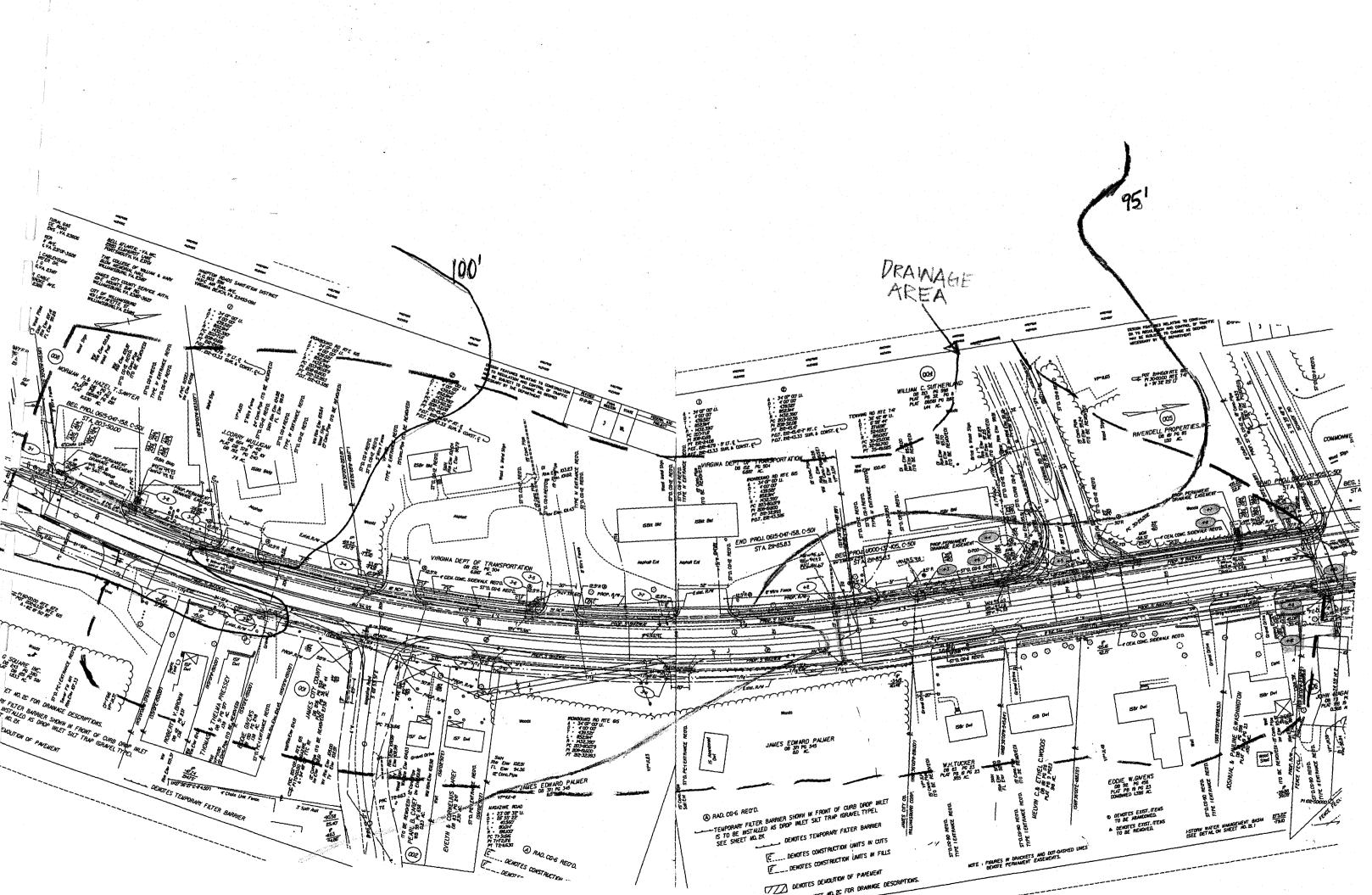
115 South 15th Street

Storm Drainage Computations

Suite 200	Design Parameters	Name	Godspeed	Proj. No.	31248.01
Richmond, VA 23219	10 Year Storm	Client		Date	8/12/2004
804-343-7100	15" Min. Pipe Size	Subject	PIPE SIZING	Computed by	KEL
	n=0.013			Checked by	•

FROM	то	AREA	RUNOFF	С	A	INLET	RAIN-	RUNOFF	INV	ERT	LENGTH	SLOPE	DIA.	CAPA-	VELO-	FLOW	MINIMUM
		DRAIN.	COEF.	INCRE-	ACCUM-	TIME	FALL	Q	ELEV	ATIONS	•			CITY	CITY	TIME	PIPE
POINT	POINT	ACRES	С	MENT	ULATED	MIN.	IN./HR.	C.F.S.	UPPER	LOWER	FT.	FT./FT.	INCHES	C.F.S.	F.P.S.	SEC.	DIA(in)
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
Ex. 18"	Ex. JB	0.430	0.460	0.198	0.198	5.00	7.17	= 1.42	97.270	93.090	65.0	0.06431	18	26.64	8.01	8.11	5,99
Ex. JB	No. 4-8	3.500 -	N/A	2.710	2.908	10.00	6.01	= 17.47	92.310	91.480	100.0	0.00830	30 .	- 37.37	7.48	13.37	22.56
No. 4-8	No. 4-9	0.260	0.900	0.234	3.314	10.22	5.96	19.76	91.480	90.980	66.0	0.00758	30	35.70	7.61	8.67	24.03
No. 4-9	No. 4-11	0.050	0.900	0.045	3.359	10.37	5.94	19.94	88.500	87.990	66.0	0.00773	30	36.06	7.63	8.65	24.02
No. 4-11	No. 4-12	1,730	0.610	1.055	4.414	10.51	5.91	26.08	87.990	87.700	34.0	0.00853	30	37.88	8.50	4.00	26.08
						-											
No. 4-7	No. 4-8	0.430	0.400	0.172	0.172	5.00	7.17	1.23	94.020	93.980	. 10.0	0.00400	- 12	2.25	2.93	3.41	9.57
							1	1						× .	and the second		
No. 4-6	No. 4-8	N/A	N/A	2.710	2.710	10.00	6.01	16.28	93.030	92.310	132.0	0.00545	30	30.29	6,08	21.71	23.77

. This shows that there is capacity in the system. by estimating existing conditions





May 28, 2004

Mr. Scott Van Voorhees Guernsey Tingle Architects 3200 Ironbound Road Williamsburg, Virginia 23188

Earthworks Project No. 1316

Reference: Godspeed Animal Clinic Infiltration Investigation

Dear Mr. Van Voorhees:

Pursuant to your request, an engineer from Earthworks visited the above referenced site to perform a subsurface investigation to determine the suitability of the soils for support of a proposed stormwater infiltration facility. This investigation was completed by performing two (2) handauger borings at locations within the proposed infiltration facility, as determined by the project Civil Engineer. The borings were extended to depths of 82 inches below existing surface elevations. In addition, two 15-foot deep soil test borings performed adjacent to the infiltration facility as part of our subsurface investigation. A boring location diagram and logs of the two handauger borings and two soil test borings are attached to this report.

In general, the soil test and handauger borings encountered Silty Sand with Clay, Clayey Sand, and Sandy Clay to depths of about 5 feet. These soils contained seasonal water indicators below a depth of about 40 inches and appeared to be moderately to poorly drained. Soils below about 5 or 6 feet consisted of moderately well drained Silty Sands. These soils too contained seasonal water indicators, but to a lesser degree. The groundwater table was encountered at a depth of about 10 feet.

Based on the results of our field classifications of the soils encountered, it is estimated that soils above a depth of about 5 feet possess an infiltration rate less than about 0.5 inches per hour. Water movement through these soils appears to be restricted, based on soil color, and water appears to be present in these soils during wet seasonal conditions. Soils below a depth of about 5 feet also appear to be seasonally wet. However, these soils are moderately well drained. We estimate that these soils possess an infiltration rate of 0.6 inches per hour or better.

It is expected that construction of pavements and other impervious surfaces will substantially reduce the presence of seasonal water in the soils surrounding the proposed infiltration facility. If an infiltration facility is considered feasible based on seasonal water conditions, we recommend the infiltration level be placed about 5 to 6 feet below existing grades and that side-wall infiltration rates be considered minimal.

Should the client or Civil Engineer require more extensive investigation, Earthworks can provide infield infiltration testing to confirm our estimated infiltration rates upon request. Godspeed Animal Clinic Infiltration Investigation Earthworks Project No. 1316 Page 2

We appreciate this opportunity to be of service to you. Should you have questions concerning this investigation or wish to discuss our findings in more detail, please contact our office.

Respectfully,

EARTHWORKS CONSULTING ENGINEERS, INC.

s: Boring Location Diagram Soil Test and Handauger Boring Logs Summary of Laboratory Test Data

(1) Client(1) VHB – Mitchell Warren

geotech/letters/1316.doc

Copies:

VHR Vanasse Hangen Brustlin, Inc.

Hf= Ho+Hi+H

HYDRAULIC GRADE LINE

115 South 15th Street
Suite 200
Richmond, VA 23219
804-343-7100

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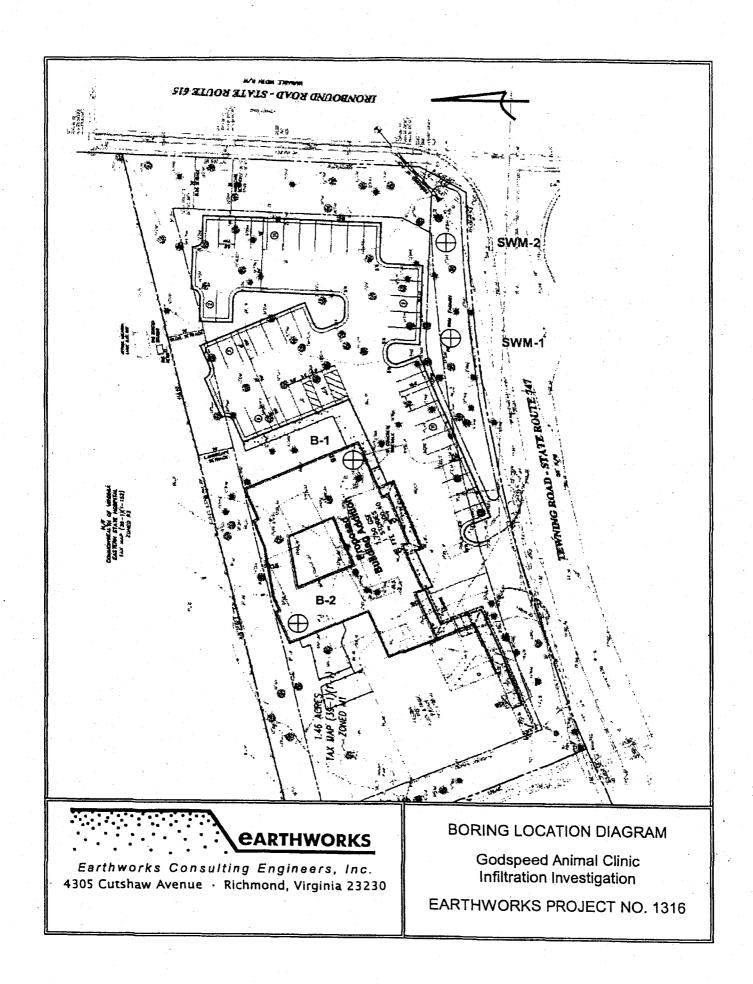
Godspeed KËL 8/12/2004

JUNCTION LOSS OUTLET Flow Inlet INLET WATER Qi 2g ¥↓? D_o Qo Hſ Vo Ho Vi H 1,3 Final H Inlet Water Rim Elev./ Through H۵ L。(FT) Qi x Vi 8r. Angle (FT) Shaping STATION SURFACE (CFS) (FPS) (CFS) (FPS) (IN) (FT) (FT) Surface Elev. Gutter Elev. **Drop Inlet** (FT) (FT) (FT) Y/N ELEV. (CFS) # (3) (5) (10) (11) (12) (14)(15) (18)(19) (20) (21) (22) (23)(2) (4) (6) (7) (8) . (9) (13)(16) (17) No. 4-11 89.70 30 26.08 34.00 0.4074 0.14 8.50 0.28 19.94 7.63 152.14 0.00 N.A. N.A. × 0.74 90.44 96.33 0.90 0.32 0 0.60 0.00 Ν No. 4-9 90.44 30 0.2361 0.16 0.23 19.76 7.61 150.37 0.90 0.31 90 19.94 66.00 7.63 0.63 1.17 N.A. N.A. 1.33 91.76 97.70 .0.00 Ν No. 4-8 92.98 30 19.76 66.00 0.2339 0.15 7.61 0.22 17.47 7.48 130.68 0.87 0.30 0.00 0.53 N.A. N.A. | 0.68 93.66 · 97.73 0 0.00 Ν Ex. JB 93.66 30 17.47 100.00 0.1828 0.18 7.48 0.22 16.28 6.08 98.98 0.57 0.20 0 0.00 0.42 N.A. N.A. 0.60 94.26 98.19 0.00 'N 200 300-90 1 d_{10} 6. C. C. and the 2000 Equations: Outlet Water Elevation = 80% diameter $H_0 = 0.25 V_o^2/2g$ 90° K = 0.70 50° K = 20°K = 0.16 0.47 $Sf = [nQ_0/(1.486AR^{2/3})]^2$ $80^{\circ} \text{K} = 0.66$ $15^{\circ} K = 0.10$ 0.38 Ho=K V²/2g 70° K = 0.61 30° K = 0.28 60° K = 0.55 25° K = 0.22

 $H_i = 0.35 V_i^2/2g$

FINAL $H = H_1 + H_1$

This approximates the existing Hydrardic Grade Line.



EARTHWORKS CONSULTING ENGINEERS, INC. HANDAUGER BORING LOGS

Godspeed Animal Clinic Infiltration Investigation

DEPTH	BORING NUMBER SWM-1
(IN)	DESCRIPTION OF SOILS
0-4	Topsoil
4-20	Light tan, Silty, fine SAND (SM) with roots
20-27	Brownish tan, Silty to Clayey, fine SAND (SM-SC)
27-40	Brownish orange, fine Sandy CLAY (CL)
40-52	Brownish orange with gray mottles, Clayey to Silty, fine SAND (SC-SM)
52-82	Light gray with orange brown, Silty, fine SAND (SM) trace Clay lenses Moisture Content – 17.2% Silt/Clay Content – 34.7%
	Seasonal Water Indicators below 40 inches. No free groundwater.
	END OF BORING AT 82 INCHES

DEPTH	BORING NUMBER SWM-2
(IN)	DESCRIPTION OF SOILS
0-3	Topsoil
3-21	Light tan, Silty, fine SAND (SM) with roots
21-46	Brownish tan, Silty to Clayey, fine SAND (SM-SC)
46-67	Brownish orange with gray mottles, Silty, fine SAND (SM) trace Clay
67-82	Light gray with orangish brown, Silty, fine SAND (SM)
	Seasonal Water Indicators below 46 inches. No free groundwater.
	END OF BORING AT 82 INCHES

OWNE	R						JOB #	BORING	#		SHEET								
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PROJE	CTN	NAM	E	cou		ARCHITECT-ENGINEER							Consulting Geotechnical Engineers						
	١ddi	tion	to (God	speed Animal Clir	nic	Guer	nsey Tin	gle A	rchite	ects		Consulting	Geotech	nical Engi	neers			
SITE L									1			CALIBI	RATED PE		METER				
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	2	SS	24	19	Light gray and t fine Sandy CLA	orown, ve Y (CL)	ery moist, med	ium stiff,		95	98			. 	
5	3	ss	24	18	Light gray and I fine SAND (SC	orown, ve)	ery moist, loos	e, Clayey,			-9&			 	
-	4	ss	24	19	Light gray and t fine SAND (SM			ise, Silty,	-			21 🛞	<mark>┼</mark> ╎ │ │ │	 	
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SUMMARY OF LABORATORY TEST DATA

GODSPEED ANIMAL CLINIC INFILTRATION INVESTIGATION

EARTHWORKS PROJECT NO. 1316

Boring No.	Sample No.	Sample Depth (in)	Natural Moisture Content (%)	Silt and/or Clay Fraction (%)	Unified Soil Classification
SWM-1	1	66-70	17.2	34.7	SM
B-1	S-1	0-24	11.8	49.5	SM-ML
B-1	S-2	24-48	17.7	51.8	CL-SC
B-2	S-3	48-72	15.5	43.2	SC

Earthworks Consulting Engineers, Inc.

Mr. Scott Van Voorhees **Guernsey Tingle Architects** 3200 Ironbound Road Williamsburg, Virginia 23188

May 28, 2004

99.5

61.

Earthworks Project No. 1316

1 OK.

Reference: Godspeed Animal Clinic Infiltration Investigation

EARTHWORKS

Dear Mr. Van Voorhees:

Pursuant to your request, an engineer from Earthworks visited the above referenced site to perform a subsurface investigation to determine the suitability of the soils for support of a proposed stormwater infiltration facility. This investigation was completed by performing two (2) handauger borings at locations within the proposed infiltration facility, as determined by the project Civil Engineer. The borings were extended to depths of 82 inches below existing surface elevations. In addition, two 15foot deep soil test borings performed adjacent to the infiltration facility as part of our subsurface investigation for the proposed building addition were used in this investigation. A boring location diagram and logs of the two handauger borings and two soil test borings are attached to this report.

WSEL 87.10 (7.65' be ON BMP IN. In general, the soil test and handauger borings encountered Silty Sand with Clay, Clayey Sand, and Sandy Clay to depths of about 5 feet. These soils contained seasonal water indicators below a depth of about 40 inches and appeared to be moderately to poorly drained. Soils below about 5 or 6 feet consisted of moderately well drained Silty Sands. These soils too contained seasonal water indicators, but to a lesser degree. The groundwater table was encountered at a depth of about 10 feet.

94.5 +0 93.5

Based on the results of our field classifications of the soils encountered, it is estimated that soils above a depth of about 5 feet possess an infiltration rate less than about 0.5 inches per hour. Water movement through these soils appears to be restricted, based on soil color, and water appears to be present in these soils during wet seasonal conditions. Soils below a depth of about 5 feet also appear to be seasonally wet. However, these soils are moderately well drained. We estimate that these soils INV : UNDERTRAIN 93.15 MIN. possess an infiltration rate of 0.6 inches per hour or better. 94.5-43.5

(below 5' delp It is expected that construction of pavements and other impervious surfaces will substantially reduce the presence of seasonal water in the soils surrounding the proposed infiltration facility. If an infiltration facility is considered feasible based on seasonal water conditions, we recommend the infiltration level be placed about 5 to 6 feet below existing grades and that side-wall infiltration rates be considered minimal.

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Godspeed Animal Clinic Infiltration Investigation Earthworks Project No. 1316 Page 2

We appreciate this opportunity to be of service to you. Should you have questions concerning this investigation or wish to discuss our findings in more detail, please contact our office.

ROBERT C. MOSS, III No. 019982

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Respectfully,

EARTHWORKS CONSULTING ENGINEERS, INC.

COMM,

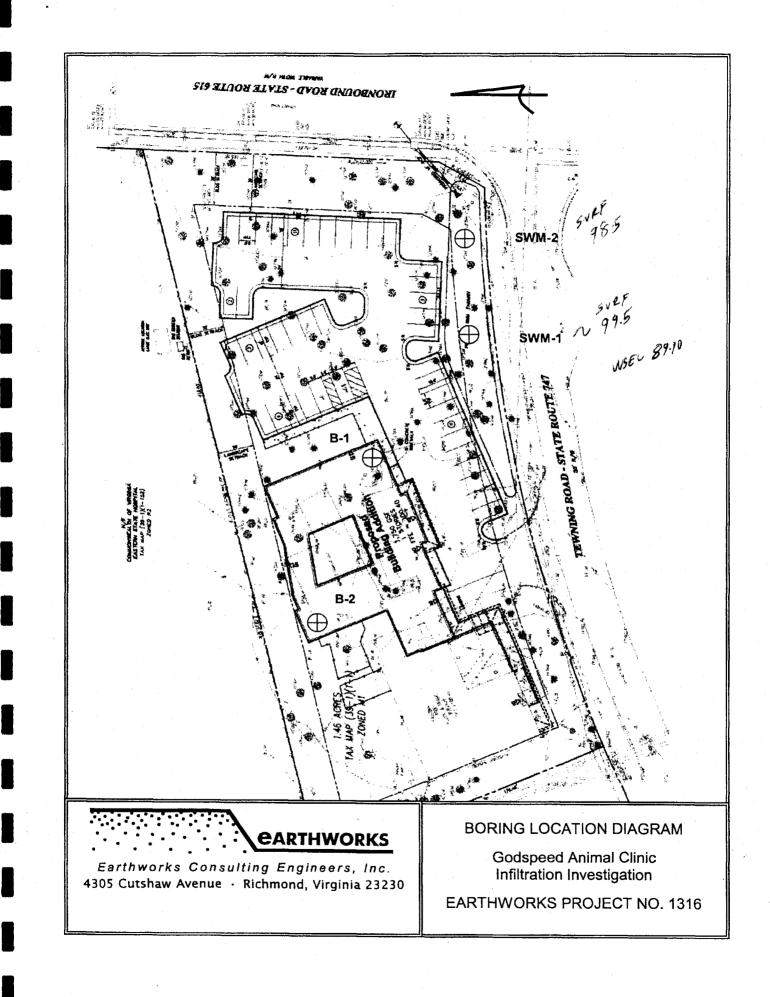
Moss, III, P.E.

President / Principal Engineer

Enclosures: Boring Location Diagram Soil Test and Handauger Boring Logs Summary of Laboratory Test Data

Copies: (1) Client (1) VHB – Mitchell Warren

geotech/letters/1316.doc



EARTHWORKS CONSULTING ENGINEERS, INC. HANDAUGER BORING LOGS

Godspeed Animal Clinic Infiltration Investigation

99.5 DEPTH **BORING NUMBER SWM-1 DESCRIPTION OF SOILS** (IN) 0-4 Topsoil Light tan, Silty, fine SAND (SM) with roots 4-20 Brownish tan, Silty to Clayey, fine SAND (SM-SC) 20-27 Brownish orange, fine Sandy CLAY (CL) 27-40 Brownish orange with gray mottles, Clayey to Silty, fine SAND (SC-SM) 40-52 52-82 Light gray with orange brown, Silty, fine SAND (SM) trace Clay lenses Moisture Content – 17.2% Silt/Clay Content – 34.7% Seasonal Water Indicators below 40 inches. No free groundwater. **END OF BORING AT 82 INCHES**

DEPTH	BORING NUMBER SWM-2
(IN)	DESCRIPTION OF SOILS
0-3	Topsoil
3-21	Light tan, Silty, fine SAND (SM) with roots
21-46	Brownish tan, Silty to Clayey, fine SAND (SM-SC)
46-67	Brownish orange with gray mottles, Silty, fine SAND (SM) trace Clay
67-82	Light gray with orangish brown, Silty, fine SAND (SM)
	Seasonal Water Indicators below 46 inches. No free groundwater.
	END OF BORING AT 82 INCHES

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OWNEF	2						JOB #	BORIN	G #		SHEET		<u>ye</u> rere	Taganan]
ROJE		Go IAMF	dsp	eed	Animal Clinic		ARCHITECT-ENGINEER				<u>1 OF 1</u>				eart	HWORKS	
				Gode	speed Animal Cl	inic		iernsey Ti		rchite	cts		Consult	ng Geoti	echnical		
SITE LC													BRATED		ROMETI	ER	1
T					James City (County, V	Α) [2	NS/FT2 3	4	5+	1
			(F						(FEET)	PLAST		CON	TER TENT %		LIQUID LIMIT %	
Ē	ġ	SAMPLE TYPE	CE (IN	SAMPLE RECOVERY (IN)	DES	SCRIPTION	OF MATER	IAL		ON (F	1	-	20	30	40	50+	
DEPTH (FT)	SAMPLE NO.	MPLE	MPLE	MPLE						ELEVATION	8		IDARD F	· PENETR /S/FT.	ATION	·	
	SA	SA	SA	SA		· · · · ·			666733335	- 100	1				40	50+	4
-	1	ss	24	16	Grayish brown, (SM-ML) with re		ise, Slity, fin	e SAND		-	×	•					
1	2	ss	24	16	Light brown, m	oist, mediı	um stiff, fine	Sandy			10 \$		<u> </u>	<u> </u> 	<u> </u>		1
4	2		24	10	CLAY (CL-SC)		• • •				100		′¦ .∔	 	 		1
5	3	ss	24	22	Light gray and I Clayey, fine SA	prown, mo ND (SC)	hist, medium	i dense,		- 95		?	<u> </u>	<u> </u> 	1	1	-
. <u>†</u>			24	10	Light gray and f	lan, very n	noist, mediu	m dense,				->	 	†			1
1	4	SS	24	18	Silty, fine SAND	0 (SM) trac	ce Clay			- -		58	ļ	ļ	1		
-	5	SS	24	20						-		18 &	N N	 	1	1	
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4					Light brown, we SAND (SM) tra			ty, fine		_				1	1		
4	6	ss	24	23		ce olay le	1303		-	-	12	\bigotimes	1	1	1.		
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							RING COMPLETED 19 April 2004				CAVE-IN DEPTH AT 13 FT DRILLING METHOD Hollow Stem Auger						1

OWNE	R					JOB #	BORING	#	1	SHEET	T					
PROJE	CTN		dsp	eed	Animal Clinic	1316 ARCHITECT-E		-2	1	OF	1)	earth	VORKS	
				2od	speed Animal Clinic		ernsey Tir		rchito	ote		Consulti	ng Geotec	hnical Ei	gineers	
ITE L				<u>30u</u>	speed Allina Chine	<u></u>	ernsey in		d crinte			BRATED PENETROMETER				
					James City County, V	/A)	TONS/FT2 2 3 4 5+				
IJ	Ō,	YPE	(IN)	SAMPLE RECOVERY (IN)	DESCRIPTIO	N OF MATERIA	AL		ELEVATION (FEET)	PLAST LIMIT 9	° ⊢		TER TENT %	U	QUID MIT %	
DЕРТН (FT)	SAMPLE NO.	SAMPLE TYPE	PLE	PLE DVER		·			ATIO		STAN	DARD P	ENETRA	·	÷	
	SAM	SAM	SAM DIST	SAM REC	SURFACE ELEVATION: 98	FT			ELEV	8		BLOW	/S/FT. 30 4	05	0+	
0	1	SS	24	11	Dark gray, moist, loose, ML) with roots [FILL]	Silty, fine SA	ND (SM-		-	8		1			1	
-	2	SS	24	19	Light gray and brown, ve fine Sandy CLAY (CL)	ry moist, meo	dium stiff,		95	98) .	 			 	
5	3	SS	24	18	Light gray and brown, ve fine SAND (SC)	ry moist, loos	se, Clayey,			-98	•	 	1	 	 	
-	4	55	24	19	Light gray and tan, moist fine SAND (SM) trace Cl		nse, Silty,		-		21	+ ⊗	 	 	 	
	5	SS	24	19			-		90 		21	\bigotimes				
10 -												/ 	1i	<u>}</u> 	 	
					Light brown, wet, medium dense, Silty, fine							• - 	╂ <u>─</u> _──┤ . :	₩	╂_─── 	
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THE	STR	ATIFIC	CATIC	N LIN	IES REPRESENT THE APPROXIMA			_		S: IN-SITU	THE TR	RANSITI	ON MAY	BE GRA	DUAL	
WATE	ER D	EPTI	H IN	BOR	EHOLE BORING S	TARTED 19	April 2004		Т	OPSOIL	DEPTH	H: 3 IN	1			
AFTE	ROF	RILLI	NG	9.	5 FT. BORING C	COMPLETED 1	19 April 20	04	c	AVE-IN [DEPTH	AT 1	0.8 FT			
AFTE	R		H	RS:	FT. DRILLER	Scott Drillin	a		D	RILLING	METH		ollow	Stem	Aua	

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SUMMARY OF LABORATORY TEST DATA

GODSPEED ANIMAL CLINIC INFILTRATION INVESTIGATION

EARTHWORKS PROJECT NO. 1316

Boring No.	Sample No.	Sample Depth (in)	Natural Moisture Content (%)	Silt and/or Clay Fraction (%)	Unified Soil Classification
SWM-1	1	66-70	17.2	34.7	SM
B-1	S-1	0-24	11.8	49.5	SM-ML
B-1	S-2	24-48	17.7	51.8	CL-SC
B-2	S-3	48-72	15.5	43.2	SC

GUNGHOUD FINAL DESIGN ANIMAL CUMU SP-70-04 James City County BMP Guidelines D-2 D-2 Figure 10 Example of a Surface Sand Filter UNDERDRAIN COLLECTION SYSTEM FLOW DIVERSION BYPASS 13 HC mpervac STRUCTURE FILTER BED OUTFLOW PRETREATMENT SEDIMENTATION \square \square CHAMBER l OVERFLOW SPILLWAY PLAN VIEW FLOW DIVERSION STRUCTURE PERFORATED STANDPIPE DETENTION STRUCTURE INFLOW OVERFLOW SPILLWAY -FILTER BED 118¹¹-111-110-1 PRETREATMENT Ш OUTFLOW IIII m Ш -UNDERDRAIN COLLECTION SYSTEM 3" TOPSOIL FILTER FABRIC il 18" CLEAN WASHED "CONCRETE" SAND FILTER FABRIC 6" PERFORATED PIPE / GRAVEL UNDERDRAIN SYSTEM TYPICAL SECTION PROFILE Surface sand filters can serve the largest drainage area of all the filtering systems.

Transportation Land Development Environmental Services



imagination innovation energy Creating results for our clients and benefits for our communities

Aug. 17, 2004

Ref: 31248.01

Scott J. Thomas, P.E. Senior Engineer **Environmental Division** 101 Mounts Bay Road, P.O. Box 8784 Williamsburg, Virginia 23187

Re: Godspeed Animal Care Case No. C-45-04

Dear Mr. Thomas:

Alve upoints instead of 10 Alggypoints them and blean washed so and blean washed so broken blean washed so broken blean washed so broken blean washed so broken blean washed so broken blean blow washed of the blow blean blow washed blow blean blow washed blow blean blow washed blow blean blow washed blow blean blow washed blow blean blow washed blow blean blow washed blow blean blow washed blow blean blow washed blow b Vanasse Hangen Brustlin, Inc. (VHB) on behalf of Dr. Pamela Dumont (property owner) hereby and in accordance with the James City County Zoning Ordinance respectfully request a waiver/modification of the 10 point BMP requirement for the proposed Surface Sand Filter System. As it states in the James City County BMP guidelines, this type of system only provides 8 of the required 10 points per site. Our waiver request is two-fold and involves the following:

fra D

- First, we are proposing to install pretreatment stone "Stilling Basins" at each of the three • curb cut locations prior to entering the proposed Sand Filter Facility. We feel that due to the limited amounts of surface drainage area contributing to these locations, that this should be an adequate filtering measure and should make up for the lack of BMP Points.
- Second, we are requesting that the sand filter layer be reduced from the 18-inch minimum requirement to the proposed 6 inches shown. The reason for this request is due to our elevation limitations we have tieing into the existing VDOT storm system on Ironbound Road. The calculations for the system show that we meet the county quantity requirements for the BMP, however we could not achieve the depth requirements for the filtering materials due to the elevation constraints. As requested in your comment letter, the installation of SOD was added to the surface of the BMP and we feel that this improvement will help protect the sand filter layer and also assist in slowing the permeability rate thus providing an adequate filtering system as intended.

We appreciate your consideration of this waiver/modification and hope these efforts will be an acceptable alternative. Therefore, VHB respectfully requests approval of this waiver request to satisfy the quality requirements.

Should you have any questions please give me a call.

Very truly yours,

VANASSE HANGEN BRUSTLIN, INC.

Mitch Mitche

Sr. Project Engineer

115 South 15th Street, Suite 200 Richmond, Virginia 23219-4209 804.343.7100 . FAX 804.343.1713 email: info@vhb.com www.vhb.com

Vanasse Hangen Brustlin, Inc.

PRETREATMENT

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monval



DEVELOPMENT MANAGEMENT

 101-E MOUNTS BAY ROAD, P.O. BOX 8784, WILLIAMSBURG, VIRGINIA 23187-8784

 (757) 253-6671
 Fax: (757) 253-6850
 E-MAIL: devtman@james-city.va.us

CODE COMPLIANCE (757) 253-6626 codecomp@james-city.va.us Environmental Division (757) 253-6670 environ@james-city.va.us PLANNING (757) 253-6685 planning@james-city.va.us County Engineer (757) 253-6678 Integrated Pest Management (757) 253-2620

September 14, 2004

Mr. Mitch Mitchell Vanasse Hangen Brustlin, Inc. 115 South 15th Street, Suite 200 Richmond, Va. 23219

Re: 10-point system and Sand Filter Variance Request Godspeed Animal Care Expansion County Plan No. SP-70-04

Dear Mr. Mitchell:

The Environmental Division is in receipt of your written variance request letter dated August 17th 2004 for the above referenced project. The variance request is dual-fold, as it requests variance from the County 10-point BMP water quality system and also requests a variance from a minimum depth of 18 inches to 6 inches for the filter sand layer associated with a County type D-2 BMP.

Based on our review of information as submitted, the variance as requested is hereby *approved* for this specific review case only. The variance was considered appropriate due to information as submitted in the letter request and the amended plan of development including:

- There is a distinct site constraint for the project. The restraint is the vertical elevation of an existing 18-inch storm drain pipe system along the west side of Ironbound Road. This storm drainage pipe system is the only reasonable receiving drainage facility to accept discharge from the development site.
- The site contains Soil Group 29B Slagle fine sandy loam, which exhibit seasonal high water tables and slow permeability of the subsoil. These characteristics limit the feasibility of certain types of onsite BMPs including bioretention and dry swales.
- The onsite BMP must be able to be landscaped in order to blend with aesthetics of the area and meet Zoning ordinance requirements.
- A wet pond pool at this location would generally be unsafe due to the location of the parking area and the presence of Ironbound Road and Tewning Road.

The following conditions apply to approval of this waiver request:

- 1. The owner should be made completely aware of waiver from the 10-point system and reduced depth of sand media. Reduced depth of sand media will result in more importance being placed on BMP maintenance as trash, debris, grass clippings and sediment can cause premature clogging of the sand layer.
- 2. The three stilling basins around the sand filter BMP as shown on Sheet C-4 of the plan set must be installed as permanent features and be adequately cleaned on a frequent basis.
- 3. The level spreader as situated in the northwest corner of the site must be installed as a permanent feature and be adequately cleaned and maintained on a routine basis.
- 4. Sod must be placed in the bottom of the sand filter BMP consistent with that shown on plan Sheet C-4 and Landscape plan Sheet C-7.
- 5. The variance approval shall become part of the approved site stormwater management plan.

Please note that approval of this variance, with the conditions stated, in no way implies final approval of a site or subdivision plan as required by the Chapter 24 Zoning or Chapter 19 Subdivisions of the County Code; nor, does it constitute final approval of an erosion and sediment control or stormwater management plan as required by Chapter 8 Erosion and Sediment Control and Chapter 23 Chesapeake Bay Preservation of the County Code. Approval of this variance is also contingent upon no major (substantial) changes in the development plan, the subject best management practice facility, or if site conditions change, become apparent or alter significantly following the date of this approval.

Sincepely,

Scott J. Phorhas, P.E. Senior Engineer Environmental Division

SJT/sjt

cc: Ellen Cook, Planning

SWMProg/Variances/SPvar/Var091404.SP07004

Transportation Land Development Environmental Services



imagination innovation energy Creating results for our clients and benefits for our communities

Aug. 17, 2004

Ref: 31248.01

Vanasse Hangen Brustlin, Inc.

Scott J. Thomas, P.E. Senior Engineer Environmental Division 101 Mounts Bay Road, P.O. Box 8784 Williamsburg, Virginia 23187

Re: Godspeed Animal Care Case No. C-45-04

Dear Mr. Thomas;

Vanasse Hangen Brustlin, Inc. (VHB) on behalf of Dr. Pamela Dumont (property owner) hereby and in accordance with the James City County Zoning Ordinance respectfully request a <u>waiver/modification of the 10 point BMP requirement for the proposed Surface Sand Filter</u> <u>System</u>. As it states in the James City County BMP guidelines, this type of system only provides 8 of the required 10 points per site. Our waiver request is two-fold and involves the following:

- First, we are proposing to install pretreatment stone "Stilling Basins" at each of the three curb cut locations prior to entering the proposed Sand Filter Facility. We feel that due to the limited amounts of surface drainage area contributing to these locations, that this should be an adequate filtering measure and should make up for the lack of BMP Points.
- Second, we are requesting that the sand filter layer be reduced from the 18-inch minimum requirement to the proposed 6 inches shown. The reason for this request is due to our elevation limitations we have tieing into the existing VDOT storm system on Ironbound Road. The calculations for the system show that we meet the county quantity requirements for the BMP, however we could not achieve the depth requirements for the filtering materials due to the elevation constraints. As requested in your comment letter, the installation of SOD was added to the surface of the BMP and we feel that this improvement will help protect the sand filter layer and also assist in slowing the permeability rate thus providing an adequate filtering system as intended.

We appreciate your consideration of this waiver/modification and hope these efforts will be an acceptable alternative. Therefore, VHB respectfully requests approval of this waiver request to satisfy the quality requirements.

Should you have any questions please give me a call.

Very truly yours,

VANASSE HANGEN BRUSTLIN, INC.

Mitch Mitch

Sr. Project Engineer

115 South 15th Street, Suite 200 Richmond, Virginia 23219-4209 804.343.7100 ► FAX 804.343.1713 email: info@vhb.com www.vhb.com

Scott Thomas

From: Scott Thomas

Sent: Thursday, December 01, 2005 5:07 PM

To: 'Jordan Anglin'

Cc: Darryl Cook; Pat Menichino

Subject: RE: God Speed animal clinic release

Jordan,

After I sent this email I looked through the submittal package from LandTech Resources dated August 17, 2005. The transmittal states that the asbuilts and certifications are provided; however, looking through the certification forms only the record drawing part is stamped and sealed. In summary, a construction certification was not provided and normally I do not do a final inspection on the BMP until this is provided except for unusual circumstances like a bond renewal is upcoming and things could be worked through quickly. If you cannot get me the construction certification quickly, I don't believe that this could be done in 15 days as I would still have to review the material, perform a final inspection and the contractor would need to complete any field-related punch list items. I have stopped to see the BMP during one rain spell and one of field related items would be to clean-up sediment within the BMP and also I thought the sand filter bottom was to have a sod lining (I believe the plans stipulated this, but I could be wrong).

If you previously provided me the construction certification, then I am in error, but I don't believe it was forwarded.

Scott J. Thomas, P.E. James City County Environmental Division

Visit: http://www.james-city.va.us/resources/devmgmt/div_devmgmt_environ.html and www.protectedwithpride.org -----Original Message-----From: Scott Thomas Sent: Thursday, December 01, 2005 4:47 PM To: 'Jordan Anglin' Subject: RE: God Speed animal clinic release

I will do my best to meet your request.

Scott J. Thomas, P.E. James City County Environmental Division

Visit: http://www.james-city.va.us/resources/devmgmt/div_devmgmt_environ.html and www.protectedwithpride.org -----Original Message-----

From: Jordan Anglin [mailto:jordan@hendersoninc.com] Sent: Wednesday, November 30, 2005 4:12 PM To: Scott Thomas; pmenichini@james-city.va.us Cc: Julie Russell; Bill Strack; bruce gilliam Subject: RE: God Speed animal clinic release Hi Scott,

• *

I am writing in regards to the final BMP inspection for God Speed Animal Clinic. You should have all the info you need as far as "as builts" and construction certification. The bond is up for renewal in 15 days and we would really like to close this one out. Please let me know where we stand.

Hope all is well at JCC

Thanks for your time,

Jordan Anglin Henderson Inc. (757) 565-1090 Jordan@hendersoninc.com

Scott Thomas

From:Jordan Anglin [jordan@hendersoninc.com]Sent:Thursday, April 13, 2006 9:07 AMTo:Jason Beck

Cc: Bill Strack; bruce gilliam; Peter Henderson; Scott Thomas; Joe Buchite; Julie Russell

Subject: RE: E&S Bond Reductions for God Speed Animal Clinic & The Magoon Building @ Newtown

Hello Jason,

I would like to request an E&S bond reduction/release for the following projects:

1) God Speed Animal Clinic 102 Tewning Rd.

The site has been stabilized, all E&S measures have been removed, and the BMP is in good working order. The rip-rap flumes leading to the BMP will be cleaned of debris today as per Scott Thomas' request. The current bond amount is **\$21,000**

2) The "Magoon Building" New Town-Block 2- Parcel F JCC-SP- 21-04

This building is complete and stabilized. The current bond amount is \$3,500

Thanks for your help!

Jordan Anglin Henderson Inc. phone 757-565 1090 cell 757 812 2394 Jordan@hendersoninc.com

Scott Thomas

- From: Jordan Anglin [jordan@hendersoninc.com]
- Sent: Friday, May 05, 2006 7:51 AM
- To: Scott Thomas
- Cc: Joe Conner; Bill Strack; Darryl Cook

Subject: RE: Prudential Mcardle BMP & God Speed Animal Clinic

Scott,

I was curious if you had a chance to look at both the **Courthouse BMP** as well as the **Godspeed Animal Clinic BMP**. All the requested work has been completed and seemed to hold up well after that huge storm we had a few weeks back. We would really like to close these projects out and they appear to be ready. Please let me know what you think.

Hope all is well at JCC

Thanks for your help,

Jordan Anglin Henderson Inc. phone 757-565 1090 cell 757 812 2394 Jordan@hendersoninc.com

City Cou	James City County Environmental Division Stormwater Management / BMP Inspection Report Detention and Retention Pond Facilities
Jamestowa 1607	SP-70-04
County BMP ID Co	ode (if known): <u>CC029</u>
Name of Facility:	GODSDEED ANIMAL CUMIC BMP No.: 1 of 1 Date: 10/07/05
T	102 Taxan Kaza
Name of Owner:	DR. PAMELA Dumont
Name of Inspector:	SJThomas
Type of Facility:	0-2 SNAFACE SAND Filter (6" deep)
Weather Condition	s: <u>Sunny</u> , <u>WARM</u> Type: Final Inspection County BMP Inspection Program Owner Inspection

If an inspection item is not applicable, mark NA, otherwise mark the appropriate column.

O.K. - The item checked is in adequate condition and the maintenance program is currently satisfactory. No action required. Routine - The item checked requires attention, but does not present an immediate threat to the function/integrity of the BMP. Urgent - The item checked requires immediate attention to keep the BMP operational and to prevent damage to the facility.

Provide an explanation and details in the comment column, if routine or urgent are marked.

Facility Item	0.K.	Routine	Urgent	Comments
Embankments and Side	Slopes:	EXCAN. AREA	7 ZH:IV	55 3-4' DEEP
Grass Height	~			
Vegetation Condition	~			
Tree Growth				None, except allowed Conoscape
Erosion	>			
Trash & Debris	 			
Seepage	\checkmark			None
Fencing or Benches		1		
Interior Landscaping/P	lanted Areas	s: None 🗆 Constru	cted Wetland/Shallo	ow Marsh D Naturally Established Vegetation
Vegetated Conditions	~			Sodded, perm. sond w
Trash & Debris	レ			Sodded, perm. sand w/ underdrain /afer.
Floating Material	~			
Erosion	~			
Sediment	レ			
Dead Plant	V			
Aesthetics	~			
Other				
Notes:	o Au	os + Park	lst Ares	15

Facility Item	О.К.	Routine	Urgent	Comments
water Pools: DP	ermanent Pool	(Retention Basin)	Shallow Marsh (Dete	ntion Basin) None, Dry (Detention Basin)
Shoreline Erosion	~			Filter demoters
Algae	~			
Trash & Debris				
Sediment	~			
Aesthetics				
Other				
Inflows (Describe Type	es/Locations):	3 PAVE	o Firme,	North and of Brippin
Condition of Structure				North side of Buspin
Erosion				parking lat.
Trash and Debris		~		
Sediment		~		
Outlet Protection			·	OK. STABLE
Other				
Principal Flow Contro	l Structure - F	Riser, Intake, etc. (Desc	cribe Type):	Nop. 01-5
Condition of Structure				Nov. PI-5 NZ'deep
Corrosion				Moo. 01-5 RZ' deep 15" RCP out, 6" pert.
Trash and Debris	V			CPP underdroin, while
Sediment				dewaters cand aver
Vegetation				a contraction of the second se
Other				
Principal Outlet Struc	ture - Barrel,	Conduit, etc. : 🛛 🖊	5 RLP	TO IRONBOUND RO
Condition of Structure				
Settlement	\sim		-	
Trash & Debris				
Erosion/Sediment				
Outlet Protection				
0.1			-	
Other		None.	OHW 14 1	antained.
Emergency Spillway (Overnow):	1		
Emergency Spillway (· ·	
Emergency Spillway (Vegetation			· · · · · · · · · · · · · · · · · · ·	
Emergency Spillway (Vegetation Lining				
Emergency Spillway (Vegetation Lining Erosion				

1	II		- <u></u>	
Facility Item	0.K.	Routine	Urgent	Comments
Nuisance Type Condition	ons:			
Mosquito Breeding				
Animal Burrows	~			
Graffiti				
Other		<u></u>		
Surrounding Perimeter	Conditions:	North-Pa	rking ; So	tht East, Voit Romo
Land Uses				
Vegetation	~	·····		
Trash & Debris	レ			
Aesthetics				LIO-BMP
Access /Maintenance Roads or Paths				CARV access from site PartiNG LUT
Other		<u> </u>		
۶۷۷ ایج Overall Environmental	b"T=	stand stand e "unt physical stand e "unt		iv ash from riprop firmes. trash from bottom voining during insp. Note: LS of! Also, visit Level spreader in NW Corner of site avound bldg. Not "africal "BMP, but inspect as part of conchy BMP Inventory.
Signature: <u> </u>	ior Ci	1/ Engine	er er	Date:

SWMProg\BMP\CoInspProg\InspForms\DetRet.wpd

ATERSHED	CC	MAINTENANCE PLAN	Yes	CTRL STRUC DESC	DI-5 Conc
MP ID NO	029	SITE AREA acre	1.46	CTRL STRUC SIZE inches	
LAN NO	SP-70-04	LAND USE	M1 Limited Busines	OTLT BARRL DESC	RCP Barrel
AX PARCEL	(39-01)(01-01)	old BMP TYP		OTLT BARRL SIZE inch	15
IN NO	3910100001	JCC BMP CODE	D2 Surface Sand Filter		
ONSTRUCTION DATE	7/1/2005	POINT VALUE	8	EMERG SPILLWAY	No
PROJECT NAME	Godspeed Animal Care (Tewning	Road)		DESIGN HW ELEV	96.38
ACILITY LOCATION	102 Tewning Road			PERM POOL ELE	na
ITY-STATE	Williamsburg, VA 23188	SVC DRAIN AREA acres	0.73	2-YR OUTFLOW cfs	0.49
	Dr. Pamela Dumont			10-YR OUTFLOW cfs	6.24
	102 Tewning Road			REC DRAWING	Yes
WNER ADDRESS 2		SERVICE AREA DESCRI	Building & Parking Lo	¢	
ITY-STATE-ZIP CODE	Williamsburg, VA 23188	IMPERV AREA acres	0.57	CONSTR CERTI	Yes
WNER PHONE	757-253-0656	RECV STREAM	UT of College Creek		
AINT AGREEMENT	Yes	EXT DET-WQ-CTRL	No	LAST INSP DATE	10/7/2005
MERG ACTION PLAN	No	WTR QUAL VOL acre-ft	0.05	INTERNAL RATING	3
		CHAN PROT CTRL CHAN PROT VOL acre-ft	Yes 0.08	MISC/COMMENTS	
Get Last BMP No		SW/FLOOD CONTROL	Yes	6" sand filter w/ 6" underdra level spreader in NW corn.	
	Return to Menu	GEOTECH REPORT	Yes		